Constructing robust gigantic drum-like hydrophobic [Co₂₄U₆] nanocage in metal-organic framework for high-performance SO₂ removal at humidity condition

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X-ray Crystallography. X-ray diffraction data of Cage-U-Co-MOF were collected at room temperature on a Bruker Appex II CCD diffractometer using graphite monochromated MoK α radiation (λ =0.71073 Å). The data reduction included a correction for Lorentz and polarization effects, with an applied multi-scan absorption correction (SADABS). The crystal structure was solved and refined using the SHELXTL program suite. Direct methods yielded all non-hydrogen atoms, which were refined with anisotropic thermal parameters. All hydrogen atom positions were calculated geometrically and were riding on their respective atoms. The SQUEEZE subroutine of the PLATON software¹⁵ suite was used to remove the scattering from the highly disordered guest molecules. CCDC 2032794 contains the supplementary crystallographic data of Cage-U-Co-MOF. These data can be obtained free of charge from the Cambridge Crystallographic Data Centre via www.ccdc.cam.ac.uk/data_request/cif.

Fitting of experimental data on pure component isotherms

The isotherm data for SO_2 and CO_2 in Cage-U-Co-MOF at 298 K were fitted with the dual-site Langmuir model, where we distinguish two distinct adsorption sites A and B:

$$q = \frac{q_{sat,A}b_Ap}{1+b_Ap} + \frac{q_{sat,B}b_Bp}{1+b_Bp}$$

The unary isotherm fit parameters are provided in Table S2.

The isotherm data for N₂ in Cage-U-Co-MOF at 298 K was fitted with the 1-site Langmuir model

$$q = q_{sat} \frac{bp}{1+bp}$$

The 1-site Langmuir fit parameters are provided in Table S3.

Isosteric heat of adsorption

The binding energy is reflected in the isosteric heat of adsorption, Q_{st} , is calculated from the Clausius-Clapeyron equation

$$Q_{st} = -RT^2 \left(\frac{\partial \ln p}{\partial T}\right)_q$$

For the 1-site Langmuir-Freundlich model the differentiation of the Clausius-Clapeyron equation can be carried out analytically.

IAST calculations of adsorption selectivities and uptake capacities

We consider the separation of binary mixtures at 298 K. The adsorption selectivity for SO_2/CO_2 , SO_2/N_2 separation is defined by

$$S_{ads} = \frac{q_1/q_2}{p_1/p_2}$$

Transient breakthrough simulations

The performance of industrial fixed bed adsorbers is dictated by a combination of adsorption selectivity and uptake capacity. Transient breakthrough simulations were carried out using the methodology described in earlier publications (*Microporous Mesoporous Mater.* **2014**, *185*, 30-50; *Sep. Purif. Technol.* **2018**, *194*, 281-300; *ACS Omega* **2020**, *5*, 16987–17004). The following two mixtures were investigated.

1/99 SO₂/CO₂ mixtures at 298 K,

1/99 SO₂/N₂ mixtures at 298 K,

For the breakthrough simulations, the following parameter values were used: length of packed bed, L = 0.3 m; voidage of packed bed, $\varepsilon = 0.4$; superficial gas velocity at inlet, u = 0.04 m/s.

The *y*-axis is the dimensionless concentrations of each component at the exit of the fixed bed, c_i/c_{i0} normalized with respect to the inlet feed concentrations. The *x*-axis is the *dimensionless* time,

 $\tau = \frac{tu}{L\varepsilon}$, defined by dividing the actual time, *t*, by the characteristic time, $\frac{L\varepsilon}{u}$.



Fig. S1 The TG plot of Cage-U-Co-MOF and the CH₃OH-exchanged samples.



Fig. S2 A comparison of Ar adsorption at 77 K for the activated samples and the samples after immersing in water and pH=3 and 12 solution. The corresponding BET surface area is 208 m²/g, $212m^2/g$, $201 m^2/g$, and $199 m^2/g$, respectively.



Fig. S3 The SO_2 and CO_2 adsorption at 273 K.



Fig. S4 The Qst value of SO_2 and CO_2 for Cage-U-Co-MOF.



Fig. S5 The transient breakthrough simulations for a 1:99 v/v SO₂/CO₂ mixture based on **Cage-U-Co-MOF** bed.



Fig. S6 The transient breakthrough simulations for a 1:99 v/v SO_2/N_2 mixture based on Cage-U-Co-MOF bed.



Fig. S7 Repeating SO₂ adsorption test for Cage-U-Co-MOF.



Fig. S8 A comparison of PXRD patterns of the as-synthesized samples and the samples after all breakthrough experiments.

MOF tpyes	SO ₂ adsorption capacity	SO ₂ /CO ₂	References
	(1 bar, 298 K), mmol/g	selectivity	
SIFSIX-2-Cu-i	11.0	87.1	1
Ni(bdc)(ted) _{0.5}	9.97	-	2
MFM-300(In)	8.28	50	3
MFM-202a	10.2	-	4
NOTT-300 (Al)	7.1	-	5
MFM-170	17.5	28	6
MOF-5	Less than 0.016	-	7
IRMOF-3	0.094	-	7
MOF-74	3.03	-	7
MOF-199	0.5	-	7
P(TMGA-co-MBA)	4.0	-	8
Activated Carbon	3.3	-	9
Cage-U-Co-MOF	3.62	80.7	Our work

Table S1. A comparison of reported MOFs for SO₂ removal.

"-" denotes the data can not be obtaind from corresponding reference.

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	Site A		Site B	
	q _{A,sat} mol kg ⁻¹	$b_{\rm A}$ ${\rm Pa}^{-1}$	q _{B,sat} mol kg ⁻¹	$b_{\rm B}$ Pa ⁻¹
SO ₂	11	2.875E-06	1.1	8.548E-04

Table S2. Dual-site Langmuir parameter fits for SO₂ and CO₂ in Cage-U-Co-MOF at 298 K.

CO ₂	0.2	5.562E-06	2	5.441E-06

Table S3. 1-site L	angmuir parameter	fits for N_2 in (Cage-U-Co-MOF	at 298 K.
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	$q_{ m sat}$	b
	mol kg ⁻¹	Pa ⁻¹
N ₂	0.15	3.21095E-06