

# A computational study of the $\text{HO}_2 + \text{SO}_3 \rightarrow \text{HOSO}_2 + {}^3\text{O}_2$ reaction catalyzed by water monomer, water dimer and small clusters of sulfuric acid: kinetics and atmospheric implications

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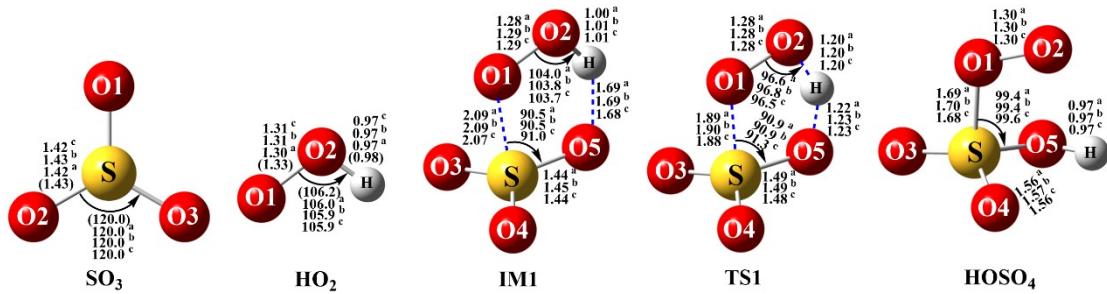
S. NO	Caption
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	$\text{HO}_2\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ , $t\text{-SO}_3\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ , $(\text{H}_2\text{SO}_4)_2$ , $\text{HO}_2\cdots(\text{H}_2\text{SO}_4)_2$ and $\text{SO}_3\cdots(\text{H}_2\text{SO}_4)_2$ within the temperature range of 280-320 K
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S14	<b>Table S4</b> The rate constants ( $k_{R1}$ ) for the $\text{HO}_2 + \text{SO}_3$ reaction without and with HIR treatments within the temperature range of 280-320 K (at 760 Torr)
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S16	<b>Part B Bimolecular rate constants (<math>\text{cm}^3\cdot\text{molecules}^{-1}\cdot\text{s}^{-1}</math>) for the <math>\text{SO}_3 + \text{HO}_2\cdots X</math> (<math>X = \text{H}_2\text{O}</math>, <math>(\text{H}_2\text{O})_2</math>, <math>\text{H}_2\text{SO}_4</math>, <math>\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}</math> and <math>(\text{H}_2\text{SO}_4)_2</math>) and <math>\text{HO}_2 + \text{SO}_3\cdots X</math> reaction</b>
S17	<b>Table S6</b> Bimolecular rate constants ( $\text{cm}^3\cdot\text{molecules}^{-1}\cdot\text{s}^{-1}$ ) for the $\text{HO}_2 + \text{SO}_3\cdots X$ ( $X = \text{H}_2\text{O}$ , $(\text{H}_2\text{O})_2$ , $\text{H}_2\text{SO}_4$ , $\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ and $(\text{H}_2\text{SO}_4)_2$ ) reaction calculated by master equation within the temperature range of 280-320 K (at 760 Torr)
S18	<b>Table S7</b> The calculated rate constants ( $\text{cm}^3\cdot\text{molecules}^{-1}\cdot\text{s}^{-1}$ ) for the $\text{HO}_2 + \text{SO}_3$ reaction without and with $\text{H}_2\text{O}$ , $(\text{H}_2\text{O})_2$ and $\text{H}_2\text{SO}_4$ within the temperature range of 280-320 K and the pressure range of 10-760 Torr
S19	<b>Table S8</b> Effective rate constants ( $k'$ ) for the $\text{HO}_2 + \text{SO}_3$ reaction with $X$ ( $X = \text{H}_2\text{O}$ , $(\text{H}_2\text{O})_2$ , $\text{H}_2\text{SO}_4$ , $\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ and $(\text{H}_2\text{SO}_4)_2$ ) within the temperature range of 280-320 K (at 0 km altitude)
S20	<b>Table S9</b> Equilibrium constants ( $K_{eq}$ , $\text{cm}^3\cdot\text{molecules}^{-1}$ ) for the formation of $\text{HO}_2\cdots\text{H}_2\text{O}$ , $\text{HO}_2\cdots(\text{H}_2\text{O})_2$ , $c\text{-HO}_2\cdots\text{H}_2\text{SO}_4$ and $c\text{-HO}_2\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ complexes, concentrations (molecules·cm <sup>-3</sup> ) of $\text{H}_2\text{O}$ , $(\text{H}_2\text{O})_2$ , $\text{H}_2\text{SO}_4$ and $\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ , and rate constants ( $\text{cm}^3\cdot\text{molecules}^{-1}\cdot\text{s}^{-1}$ ) of the $\text{HO}_2 + \text{SO}_3$ reaction with $\text{H}_2\text{O}$ , $(\text{H}_2\text{O})_2$ , $\text{H}_2\text{SO}_4$ and $\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ at different altitudes in troposphere
S21-S25	<b>Table S10</b> Coordinates stationary points for the $\text{HO}_2 + \text{SO}_3$ reaction without and with $X$ ( $X = \text{H}_2\text{O}$ , $(\text{H}_2\text{O})_2$ , $\text{H}_2\text{SO}_4$ , $\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ and $(\text{H}_2\text{SO}_4)_2$ ) at the M06-2X/6-311+G(2df,2pd) level of theory



**Fig. S1** The optimized geometries for the species involved in the  $\text{HO}_2 + \text{SO}_3$  reaction at several different levels of theory

a, b, c and d respectively represent the values obtained at the M06-2X/6-311+G(2df,2pd), M06-2X/aug-cc-pVTZ, M06-2X/aug-cc-pV(T+d)Z and M06-2X/6-311++G(2df,2pd) level of theory. (The values in parentheses were the experimental values; bond length is in angstrom and angle is in degree.)

In order to check whether the geometric parameters of the reactants, pre-reactive complexes, transition states and products for the  $\text{HO}_2 + \text{SO}_3$  reaction can give good and reliable results at the M06-2X/6-311+G(2df,2pd) level, we have re-optimized all equilibrium structures at the M06-2X/aug-cc-pVTZ and M06-2X/aug-cc-pV(T+d)Z levels. As shown in Fig. S1, for the calculated geometrical parameters of the above species, the mean absolute deviation of calculated bond distances and bond angles between the M06-2X/6-311+G(2df,2pd) level and the M06-2X/aug-cc-pVTZ level were 0.005 Å and 0.1°, respectively. Meanwhile, when comparing the M06-2X/6-311+G(2df,2pd) and M06-2X/aug-cc-pV(T+d)Z levels, it was found that the calculated the mean absolute deviation of calculated bond distances and bond angles were found to be 0.006 Å and 0.23°. Therefore, the bond lengths and angles for the reactants, pre-reactive complexes, transition states and products at the M06-2X/6-311+G(2df,2pd) level are close to those from the M06-2X/aug-cc-pVTZ and M06-2X/aug-cc-pV(T+d)Z method. In addition, the calculated bond distances and bond angles for the M06-2X/6-311+G(2df,2pd) level agree well with the corresponding experimental values (From the NIST chemistry webbook, <http://webbook.nist.gov/chemistry/>). Therefore, due to its efficiency, the M06-2X/6-311+G(2df,2pd) was adopted to optimize the geometries of all stationary points for the  $\text{HO}_2 + \text{SO}_3$  reactions.

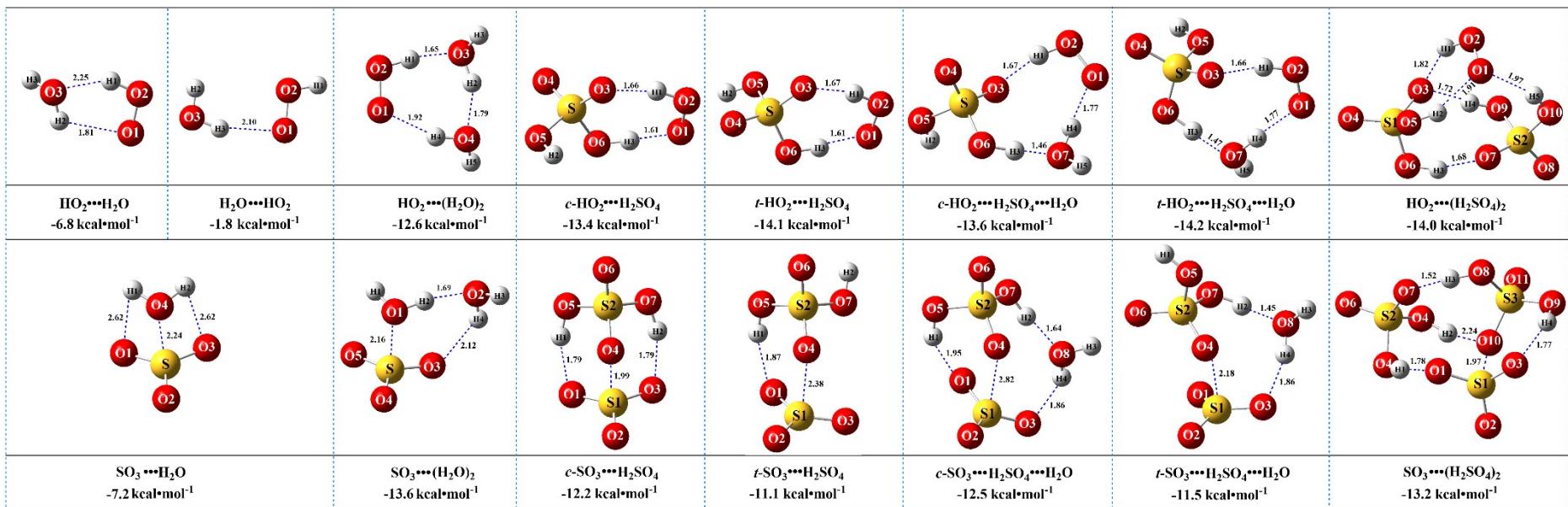
**Table S1** The energy barriers ( $\Delta E$ ) and unsigned error (UE) (kcal·mol<sup>-1</sup>) for the HO<sub>2</sub> + SO<sub>3</sub> → HOSO<sub>2</sub> + <sup>3</sup>O<sub>2</sub> reaction at different theoretical methods with zero-point energy (ZPE) correction

Methods	$\Delta E^a$	$\Delta E^b$	$\Delta E^c$	UE
W3X-L//M06-2X/6-311+G(2df,2pd)	-10.6	-9.7	-14.4	0.00
W2X//M06-2X/6-311+G(2df,2pd)	-10.7	-10.0	-14.8	0.38
CCSD(T)/aug-cc-pVTZ//M06-2X/6-311+G(2df,2pd)	-10.5(-10.48) <sup>d</sup>	-9.8(-9.68) <sup>d</sup>	-14.2(-13.81) <sup>d</sup>	0.13
CCSD(T)/aug-cc-pVTZ//M06-2X/6-311++G(2df,2pd)	-10.5(-10.48) <sup>d</sup>	-9.8(-9.68) <sup>d</sup>	-14.2(-13.81) <sup>d</sup>	0.13
CCSD(T)/aug-cc-pVTZ//M06-2X//aug-cc-pVTZ	-10.4	-9.8	-14.1	0.20
CCSD(T)/aug-cc-pV(T+d)Z//M06-2X//aug-cc-pV(T+d)Z	10.8	10.1	14.8	0.33
DLPNO-CCSD(T)-F12/cc-pVDZ-F12//M06-2X/6-311+G(2df,2pd)	-10.6	-9.9	-14.8	0.20
CCSD(T)-F12a/cc-pVDZ-F12//M06-2X/6-311+G(2df,2pd)	-11.7	-11.0	-15.8	1.27
CCSD(T)/cc-pVTZ//M06-2X/6-311+G(2df,2pd)	-9.4(-9.44) <sup>d</sup>	-8.9(-8.67) <sup>d</sup>	-12.4(-12.64) <sup>d</sup>	1.33
CCSD(T)/aug-cc-pVDZ//M06-2X/6-311+G(2df,2pd)	-9.1	-7.3	-11.7	2.17
CCSD(T)/cc-pVDZ//M06-2X/6-311+G(2df,2pd)	-7.5	-5.4	-7.1	4.9

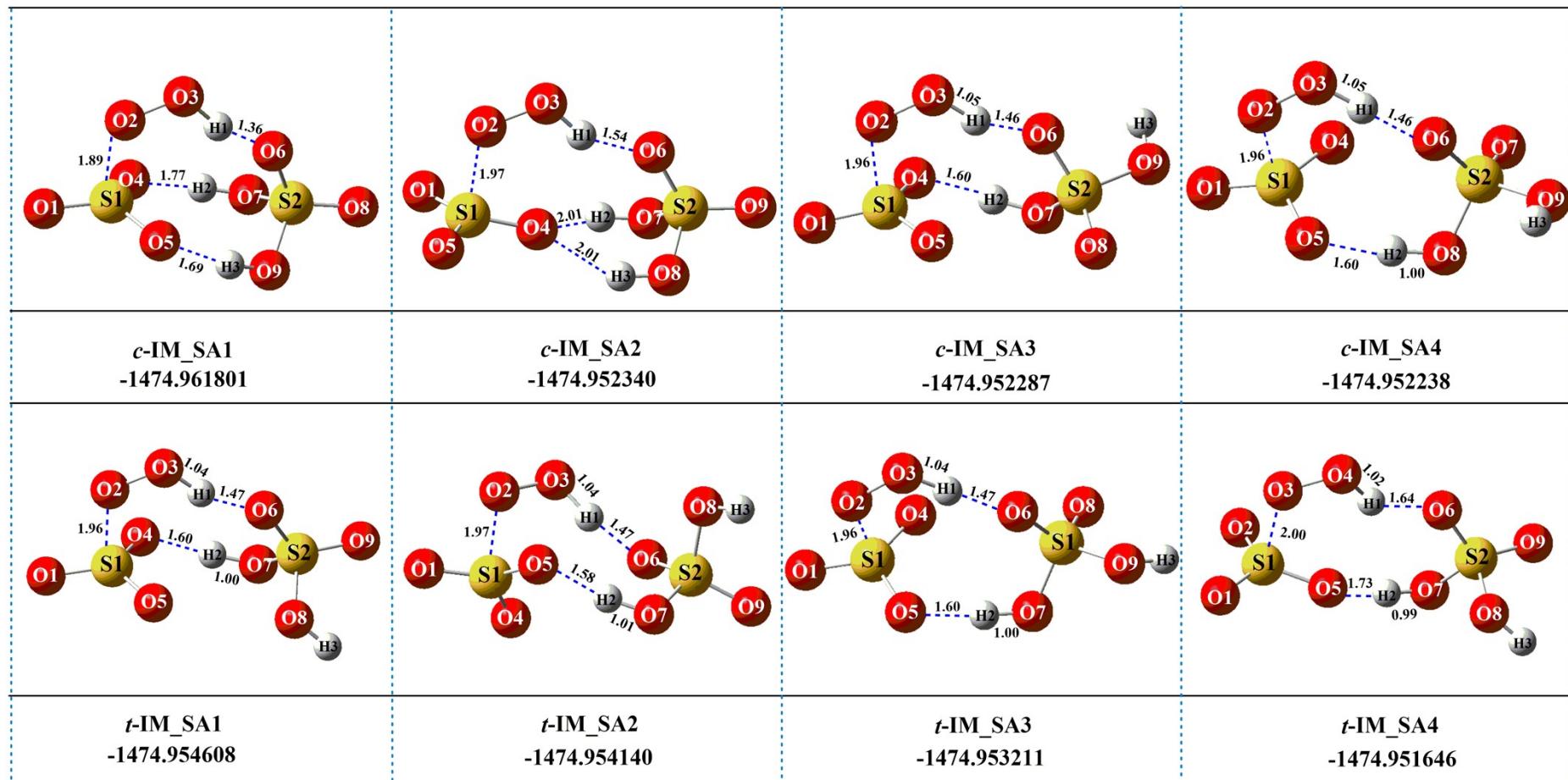
a, b and c respectively denote the species of pre-reactive complexes, transition states and post-reactive complexes involved in HO<sub>2</sub> + SO<sub>3</sub> reaction.

<sup>d</sup>The value taken from reference 1.

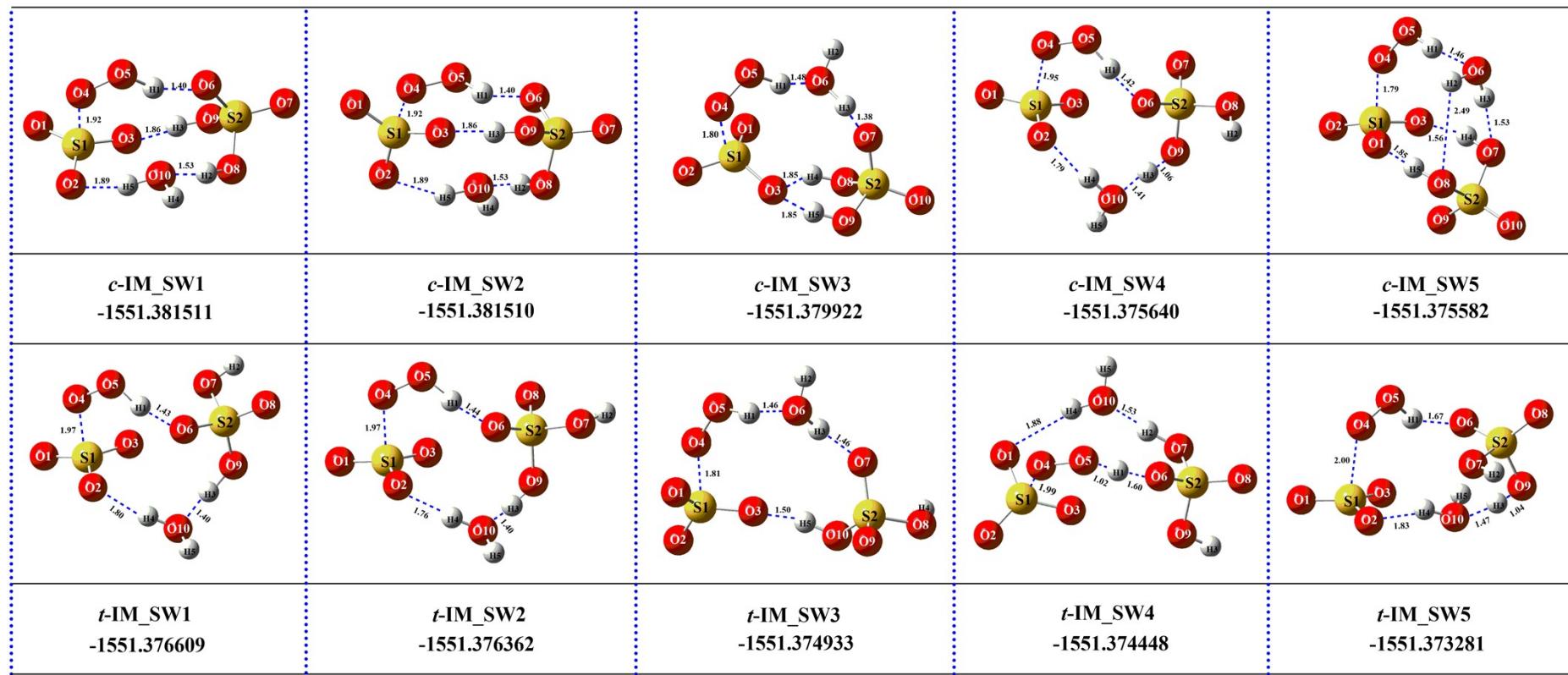
To further confirm the reliability of the M06-2X/6-311+G(2df,2pd) method, the CCSD(T)/aug-cc-pVTZ single point energies based on the M06-2X/6-311+G(2df,2pd) optimized geometries were redefined. As presented in Table S1, the relative energy of pre-reactive complexes, transition states and products to the reactants at the CCSD(T)/aug-cc-pVTZ//M06-2X/6-311+G(2df,2pd) level was respectively -10.5 kcal·mol<sup>-1</sup>, -9.8 kcal·mol<sup>-1</sup> and -14.2 kcal·mol<sup>-1</sup>, which were consistent with the corresponding predicted values at the CCSD(T)/aug-cc-pVTZ//M06-2X//aug-cc-pVTZ level. Similarly, the energies difference at the CCSD(T)/aug-cc-pVTZ//M06-2X//aug-cc-pVTZ, CCSD(T)/aug-cc-pVTZ//M06-2X/6-311+G(2df,2pd) and CCSD(T)/aug-cc-pV(T+d)Z//M06-2X//aug-cc-pV(T+d)Z levels compared to the relative energies calculated at the W3X-L//M06-2X/6-311+G(2df,2pd) level, were less than 0.33 kcal·mol<sup>-1</sup>. This suggests that the relative energies obtained at the CCSD(T)/aug-cc-pVTZ//M06-2X/6-311+G(2df,2pd) level are also reasonable. Considering the computational accuracy and cost, the CCSD(T)/aug-cc-pVTZ//M06-2X/6-311+G(2df,2pd) method was chosen to calculate the single point energies of all species for the HO<sub>2</sub> + SO<sub>3</sub> reactions.



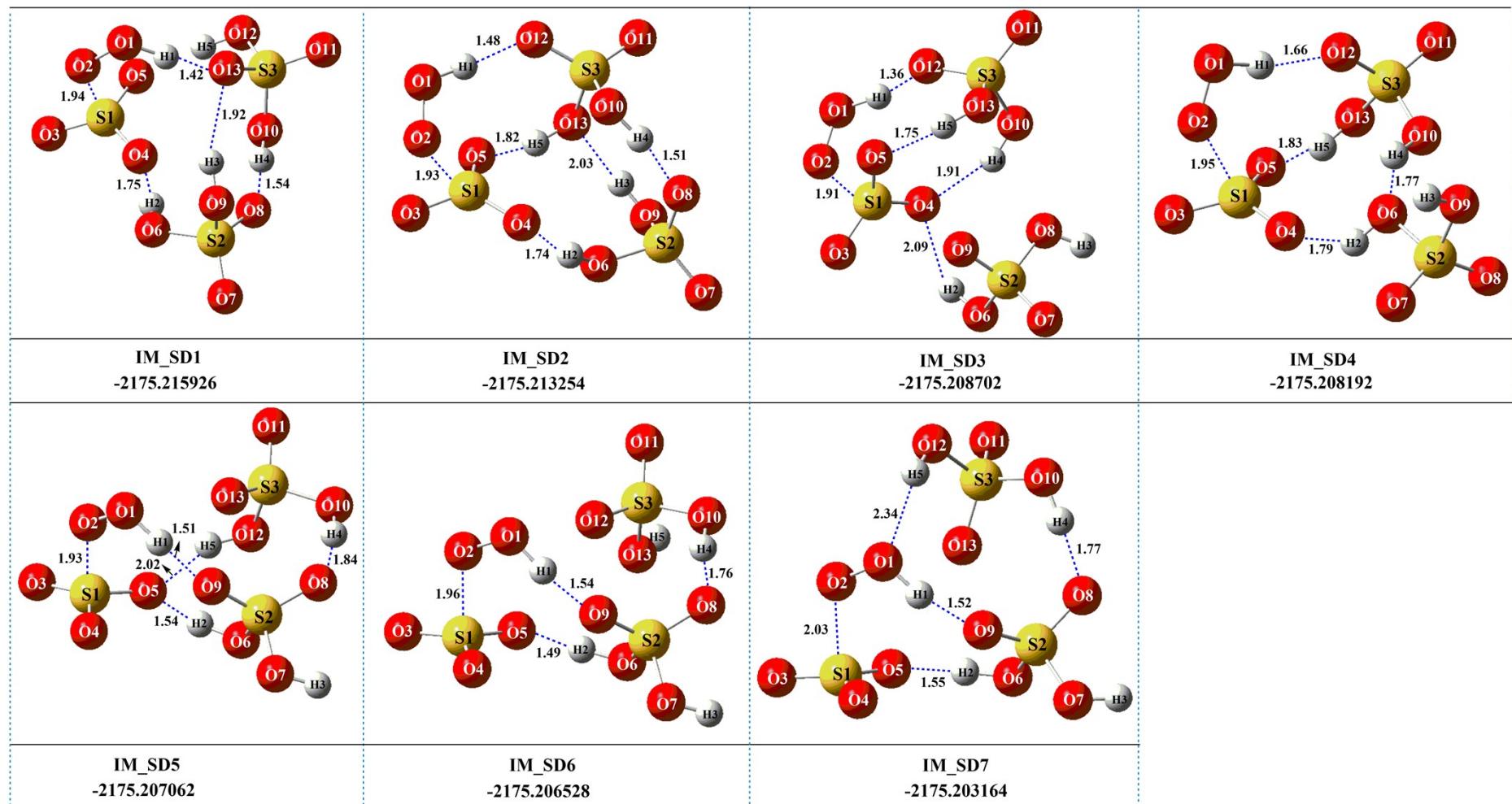
**Fig. S2** Optimized geometries and binding energies of the reactant complexes  $\text{HO}_2\cdots X$  ( $X = \text{H}_2\text{O}, (\text{H}_2\text{O})_2, \text{H}_2\text{SO}_4, \text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$  and  $(\text{H}_2\text{SO}_4)_2$ ) and  $\text{SO}_3\cdots X$  at the CCSD(T)/aug-cc-pVTZ//M06-2X/6-311+G(2df,2pd) level of theory (bond distance in Angstroms and angles in degrees)



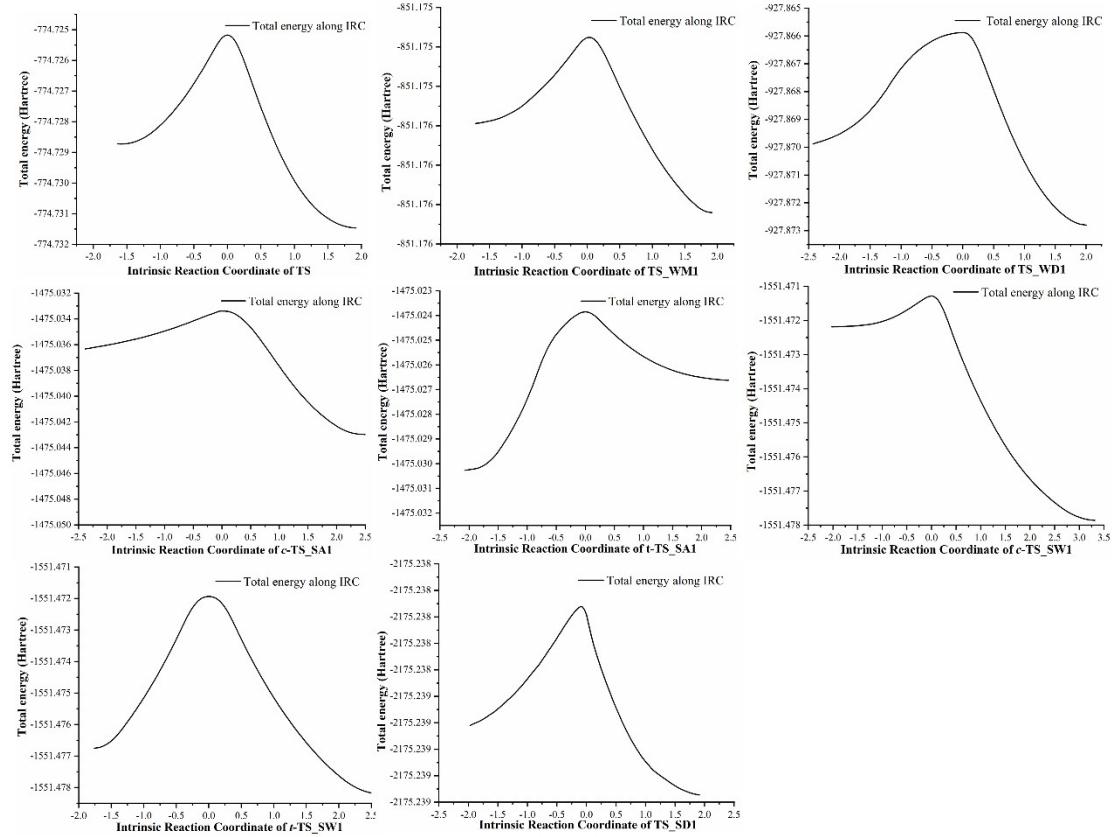
**Fig. S3** The optimized geometries and electric energies (in Hartree-Fock) of  $\text{HO}_2\cdots\text{SO}_3\cdots\text{H}_2\text{SO}_4$  at the M06-2X/6-311+G(2df,2pd) level of theory (Bond distances in Angstroms and angles in degrees)



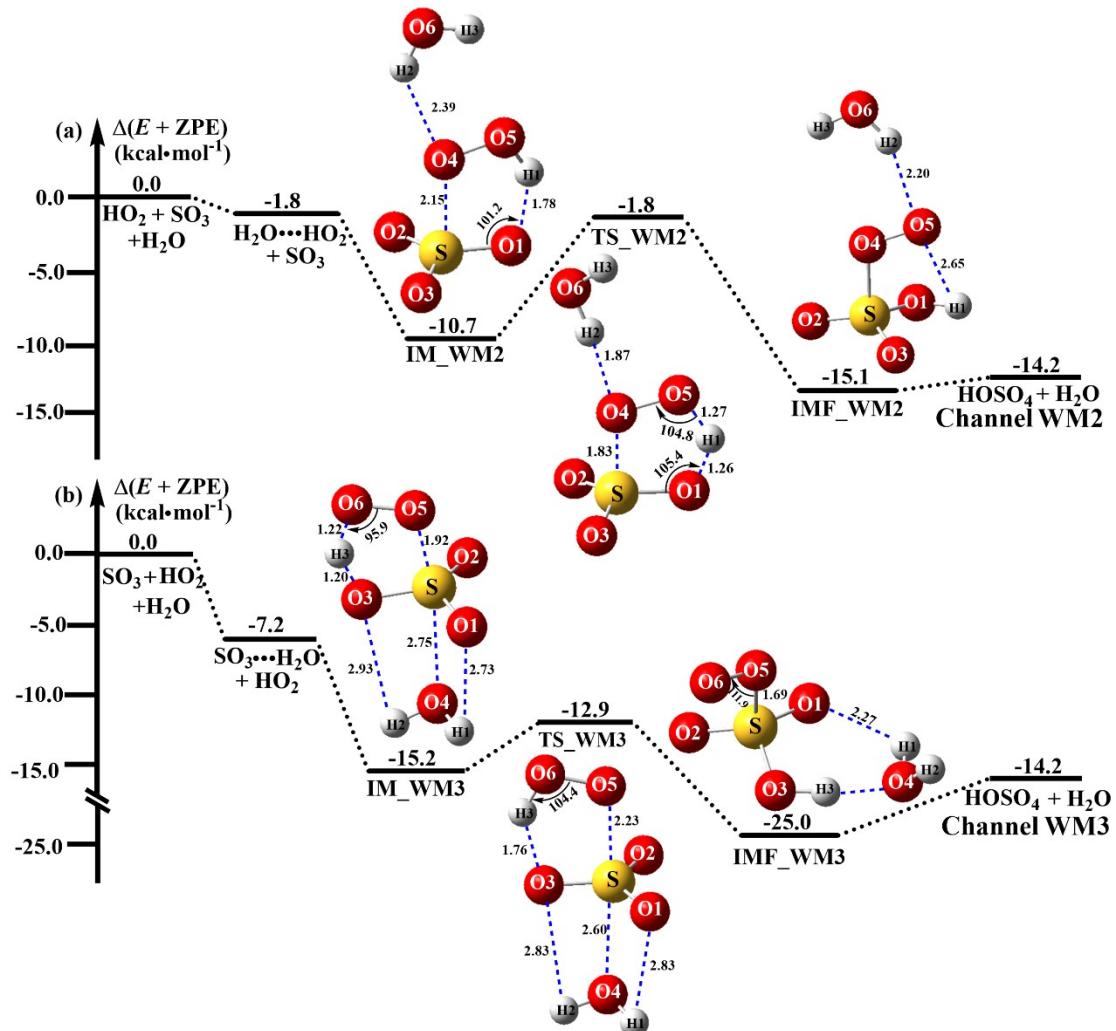
**Fig. S4** The optimized geometries and electric energies (in Hartree-Fock) of HO<sub>2</sub>···SO<sub>3</sub>···H<sub>2</sub>SO<sub>4</sub>···H<sub>2</sub>O at the M06-2X/6-311+G(2df,2pd) level of theory (Bond distances in Angstroms and angles in degrees)



**Fig. S5** The optimized geometries and electric energies (in Hartree-Fock) of  $\text{HO}_2\cdots\text{SO}_3\cdots(\text{H}_2\text{SO}_4)_2$  at the M06-2X/6-311+G(2df,2pd) level of theory (Bond distances in Angstroms and angles in degrees)



**Fig. S6** The results of IRC calculations for all the transition states involved in the  $\text{HO}_2 + \text{SO}_3$  reactions without and with catalyst  $X$  ( $X = \text{H}_2\text{O}$ ,  $(\text{H}_2\text{O})_2$ ,  $\text{H}_2\text{SO}_4$ ,  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  and  $(\text{H}_2\text{SO}_4)_2$ )



**Fig. S7** Potential energy surface for the unfavorable routes in the  $\text{HO}_2 + \text{SO}_3$  reaction with  $\text{H}_2\text{O}$  at the CCSD(T)/aug-cc-pVTZ//M06-2X/6-311+G(2df,2pd) level of theory

**Table S2** The equilibrium constant ( $K_{eq}$ , in  $\text{cm}^3 \cdot \text{molecules}^{-1}$ )<sup>a</sup>, and concentrations (molecules $\cdot\text{cm}^{-3}$ ) of complexes  $\text{HO}_2\cdots\text{H}_2\text{O}$ ,  $\text{SO}_3\cdots\text{H}_2\text{O}$ ,  $\text{H}_2\text{O}\cdots\text{HO}_2$ ,  $\text{HO}_2\cdots(\text{H}_2\text{O})_2$ ,  $\text{SO}_3\cdots(\text{H}_2\text{O})_2$ ,  $c\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4$ ,  $c\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4$ ,  $t\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4$ ,  $t\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4$ ,  $c\text{-}\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ ,  $c\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ ,  $c\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ ,  $t\text{-}\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ ,  $t\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ ,  $t\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$ ,  $(\text{H}_2\text{SO}_4)_2$ ,  $\text{HO}_2\cdots(\text{H}_2\text{SO}_4)_2$  and  $\text{SO}_3\cdots(\text{H}_2\text{SO}_4)_2$  within the temperature range of 280–320 K

T/K	$K_{eq1A}$	$[\text{HO}_2\cdots\text{H}_2\text{O}]$	$K_{eq1B}$	$[\text{SO}_3\cdots\text{H}_2\text{O}]$	$K_{eq1C}$	$[\text{H}_2\text{O}\cdots\text{HO}_2]$
280	$1.53 \times 10^{-20}$	$1.18 \times 10^6$	$1.73 \times 10^{-20}$	4.46	$1.88 \times 10^{-23}$	$1.45 \times 10^3$
290	$9.42 \times 10^{-21}$	$1.35 \times 10^6$	$1.07 \times 10^{-20}$	5.12	$1.68 \times 10^{-23}$	$2.41 \times 10^3$
298	$6.55 \times 10^{-21}$	$1.52 \times 10^6$	$7.50 \times 10^{-21}$	5.80	$1.54 \times 10^{-23}$	$3.58 \times 10^3$
300	$6.00 \times 10^{-21}$	$1.55 \times 10^6$	$6.88 \times 10^{-21}$	5.90	$1.51 \times 10^{-23}$	$3.90 \times 10^3$
310	$3.94 \times 10^{-21}$	$1.73 \times 10^6$	$4.55 \times 10^{-21}$	6.65	$1.38 \times 10^{-23}$	$6.03 \times 10^3$
320	$2.66 \times 10^{-21}$	$1.87 \times 10^6$	$3.10 \times 10^{-21}$	7.28	$1.26 \times 10^{-23}$	$8.89 \times 10^3$
T/K	$K_{eq2A}$	$[\text{HO}_2\cdots(\text{H}_2\text{O})_2]$	$K_{eq2B}$	$[\text{SO}_3\cdots(\text{H}_2\text{O})_2]$	$K_{eq3A}$	$[c\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4]$
280	$3.45 \times 10^{-18}$	$2.11 \times 10^5$	$1.10 \times 10^{-17}$	2.25	$8.24 \times 10^{-18}$	$9.64 \times 10^{-1}$
290	$1.47 \times 10^{-18}$	$2.60 \times 10^5$	$4.80 \times 10^{-18}$	2.83	$3.90 \times 10^{-18}$	$4.45 \times 10^{-1}$
298	$7.72 \times 10^{-19}$	$3.15 \times 10^5$	$2.57 \times 10^{-18}$	3.49	$2.23 \times 10^{-18}$	$2.47 \times 10^{-1}$
300	$6.61 \times 10^{-19}$	$3.21 \times 10^5$	$2.21 \times 10^{-18}$	3.58	$1.95 \times 10^{-18}$	$2.10 \times 10^{-1}$
310	$3.14 \times 10^{-19}$	$3.82 \times 10^5$	$1.07 \times 10^{-18}$	4.35	$1.02 \times 10^{-18}$	$1.07 \times 10^{-1}$
320	$1.56 \times 10^{-19}$	$4.32 \times 10^5$	$5.44 \times 10^{-19}$	5.03	$4.55 \times 10^{-19}$	$4.64 \times 10^{-2}$
T/K	$K_{eq3B}$	$[c\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4]$	$K_{eq4A}$	$[t\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4]$	$K_{eq4B}$	$[t\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4]$
280	$1.09 \times 10^{-18}$	$4.25 \times 10^{-7}$	$2.85 \times 10^{-16}$	$3.33 \times 10^1$	$3.09 \times 10^{-19}$	$1.21 \times 10^{-7}$
290	$5.13 \times 10^{-19}$	$1.95 \times 10^{-7}$	$1.19 \times 10^{-16}$	$1.36 \times 10^1$	$1.62 \times 10^{-19}$	$6.17 \times 10^{-8}$
298	$2.91 \times 10^{-19}$	$1.08 \times 10^{-7}$	$6.20 \times 10^{-17}$	6.89	$1.00 \times 10^{-19}$	$3.71 \times 10^{-8}$
300	$2.54 \times 10^{-19}$	$9.15 \times 10^{-8}$	$5.30 \times 10^{-17}$	5.72	$8.92 \times 10^{-20}$	$3.21 \times 10^{-8}$
310	$1.32 \times 10^{-19}$	$4.62 \times 10^{-8}$	$2.49 \times 10^{-17}$	2.61	$5.11 \times 10^{-20}$	$1.79 \times 10^{-8}$
320	$7.16 \times 10^{-20}$	$2.43 \times 10^{-8}$	$1.22 \times 10^{-17}$	1.25	$3.04 \times 10^{-20}$	$1.03 \times 10^{-8}$
T/K	$K_{eq(c\text{-SW})}$	$[c\text{-}\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}]$	$K_{eq5A}$	$[c\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}]$	$K_{eq5B}$	$[c\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}]$
280	$2.03 \times 10^{-19}$	$2.04 \times 10^7$	$3.02 \times 10^{-16}$	1.85	$5.30 \times 10^{-19}$	$1.08 \times 10^{-8}$
290	$1.20 \times 10^{-19}$	$2.18 \times 10^7$	$1.30 \times 10^{-16}$	$8.53 \times 10^{-1}$	$2.44 \times 10^{-19}$	$5.33 \times 10^{-9}$
298	$8.10 \times 10^{-20}$	$2.31 \times 10^7$ $(2.40 \times 10^7)^b$	$6.94 \times 10^{-17}$	$4.80 \times 10^{-1}$	$1.37 \times 10^{-19}$	$3.16 \times 10^{-9}$
300	$7.36 \times 10^{-20}$	$2.27 \times 10^7$	$5.96 \times 10^{-17}$	$4.07 \times 10^{-1}$	$1.19 \times 10^{-19}$	$2.71 \times 10^{-9}$
310	$4.67 \times 10^{-20}$	$2.39 \times 10^7$	$2.87 \times 10^{-17}$	$2.05 \times 10^{-1}$	$6.08 \times 10^{-20}$	$1.45 \times 10^{-9}$
320	$3.05 \times 10^{-20}$	$2.44 \times 10^7$	$1.45 \times 10^{-17}$	$1.06 \times 10^{-1}$	$3.24 \times 10^{-20}$	$7.91 \times 10^{-10}$
T/K	$K_{eq(t\text{-SW})}$	$[t\text{-}\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}]$	$K_{eq6A}$	$[t\text{-}\text{HO}_2\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}]$	$K_{eq6B}$	$[t\text{-}\text{SO}_3\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}]$
280	$4.05 \times 10^{-19}$	$4.08 \times 10^7$	$2.20 \times 10^{-15}$	$2.69 \times 10^1$	$1.68 \times 10^{-18}$	$3.43 \times 10^{-8}$
290	$2.24 \times 10^{-19}$	$4.07 \times 10^7$	$9.24 \times 10^{-16}$	$1.13 \times 10^1$	$8.58 \times 10^{-19}$	$1.87 \times 10^{-8}$
298	$1.44 \times 10^{-19}$	$4.09 \times 10^7$	$4.82 \times 10^{-16}$	5.92	$5.18 \times 10^{-19}$	$1.20 \times 10^{-8}$
300	$1.29 \times 10^{-19}$	$3.99 \times 10^7$	$4.12 \times 10^{-16}$	4.93	$4.59 \times 10^{-19}$	$1.04 \times 10^{-8}$
310	$7.71 \times 10^{-20}$	$3.94 \times 10^7$	$1.94 \times 10^{-16}$	2.29	$2.56 \times 10^{-19}$	$6.11 \times 10^{-9}$
320	$4.77 \times 10^{-20}$	$3.81 \times 10^7$	$9.58 \times 10^{-17}$	1.10	$1.49 \times 10^{-19}$	$3.63 \times 10^{-9}$

T/K	$K_{eq(SD)}$	$[(H_2SO_4)_2]$	$K_{eq7A}$	$[HO_2\cdots(H_2SO_4)_2]$	$K_{eq7B}$	$[SO_3\cdots(H_2SO_4)_2]$
280	$4.88 \times 10^{-17}$	7.42	$1.03 \times 10^{-16}$	$2.29 \times 10^{-7}$	$1.55 \times 10^{-17}$	$1.15 \times 10^{-13}$
290	$1.84 \times 10^{-17}$	2.65	$4.36 \times 10^{-17}$	$3.46 \times 10^{-8}$	$6.96 \times 10^{-18}$	$1.84 \times 10^{-14}$
298	$8.82 \times 10^{-18}$	1.21	$2.29 \times 10^{-17}$	$8.31 \times 10^{-9}$	$3.83 \times 10^{-18}$	$4.63 \times 10^{-15}$
300	$7.38 \times 10^{-18}$	1.01	$1.96 \times 10^{-17}$	$5.94 \times 10^{-9}$	$3.31 \times 10^{-18}$	$3.35 \times 10^{-15}$
310	$3.15 \times 10^{-18}$	$4.09 \times 10^{-1}$	$9.30 \times 10^{-18}$	$1.14 \times 10^{-9}$	$1.66 \times 10^{-18}$	$6.78 \times 10^{-16}$
320	$1.42 \times 10^{-18}$	$1.64 \times 10^{-1}$	$4.63 \times 10^{-18}$	$2.28 \times 10^{-10}$	$8.69 \times 10^{-19}$	$1.42 \times 10^{-16}$

<sup>a</sup>  $K_{eq1A}$ ,  $K_{eq1B}$  and  $K_{eq1C}$  represented the equilibrium constant of  $HO_2\cdots H_2O$ ,  $SO_3\cdots H_2O$  and  $H_2O\cdots HO_2$ ;  $K_{eq2A}$  and  $K_{eq2B}$  denoted the equilibrium constant of  $HO_2\cdots (H_2O)_2$  and  $SO_3\cdots (H_2O)_2$ ;  $K_{eq3A}$  and  $K_{eq3B}$  represented the equilibrium constant of  $c-HO_2\cdots H_2SO_4$  and  $c-SO_3\cdots H_2SO_4$ ;  $K_{eq4A}$  and  $K_{eq4B}$  denoted the equilibrium constant of  $t-HO_2\cdots H_2SO_4$  and  $t-SO_3\cdots H_2SO_4$ ;  $K_{eq(c-SW)}$ ,  $K_{eq5A}$  and  $K_{eq5B}$  denoted the equilibrium constant of  $c-H_2SO_4\cdots H_2O$ ,  $c-HO_2\cdots H_2SO_4\cdots H_2O$  and  $c-SO_3\cdots H_2SO_4\cdots H_2O$ ;  $K_{eq(t-SW)}$ ,  $K_{eq6A}$  and  $K_{eq6B}$  represented the equilibrium constant of  $t-H_2SO_4\cdots H_2O$ ,  $t-HO_2\cdots H_2SO_4\cdots H_2O$  and  $t-SO_3\cdots H_2SO_4\cdots H_2O$ ;  $K_{eq(SD)}$ ,  $K_{eq7A}$  and  $K_{eq7B}$  denoted the equilibrium constant of  $(H_2SO_4)_2$ ,  $HO_2\cdots (H_2SO_4)_2$  and  $SO_3\cdots (H_2SO_4)_2$ .

<sup>b</sup> The concentrations of  $HO_2\cdots H_2O$ ,  $SO_3\cdots H_2O$  and  $H_2O\cdots HO_2$  were respectively expressed as  $[HO_2\cdots H_2O] = K_{eq1A} \times [H_2O] \times [HO_2]$ ,  $[SO_3\cdots H_2O] = K_{eq1B} \times [H_2O] \times [SO_3]$  and  $[H_2O\cdots HO_2] = K_{eq1C} \times [H_2O] \times [HO_2]$ ; the concentrations of  $HO_2\cdots (H_2O)_2$  and  $SO_3\cdots (H_2O)_2$  were respectively expressed as  $[HO_2\cdots (H_2O)_2] = K_{eq2A} \times [(H_2O)_2] \times [HO_2]$  and  $[SO_3\cdots (H_2O)_2] = K_{eq2B} \times [(H_2O)_2] \times [SO_3]$ ; the concentrations of  $c-HO_2\cdots H_2SO_4$  and  $c-SO_3\cdots H_2SO_4$  were respectively expressed as  $[c-HO_2\cdots H_2SO_4] = K_{eq3A} \times [H_2SO_4] \times [HO_2]$  and  $[c-SO_3\cdots H_2SO_4] = K_{eq3B} \times [H_2SO_4] \times [SO_3]$ ; the concentrations of  $t-HO_2\cdots H_2SO_4$  and  $t-SO_3\cdots H_2SO_4$  were respectively expressed as  $[t-HO_2\cdots H_2SO_4] = K_{eq4A} \times [H_2SO_4] \times [HO_2]$  and  $[t-SO_3\cdots H_2SO_4] = K_{eq4B} \times [H_2SO_4] \times [SO_3]$ ; the concentrations of  $c-H_2SO_4\cdots H_2O$ ,  $c-HO_2\cdots H_2SO_4\cdots H_2O$  and  $c-SO_3\cdots H_2SO_4\cdots H_2O$  were respectively expressed as  $[c-H_2SO_4\cdots H_2O] = K_{eq(c-SW)} \times [H_2SO_4] \times [H_2O]$ ,  $[c-HO_2\cdots H_2SO_4\cdots H_2O] = K_{eq5A} \times [H_2SO_4\cdots H_2O] \times [HO_2]$  and  $[c-SO_3\cdots H_2SO_4\cdots H_2O] = K_{eq5B} \times [H_2SO_4\cdots H_2O] \times [SO_3]$ ; the concentrations of  $t-H_2SO_4\cdots H_2O$ ,  $t-HO_2\cdots H_2SO_4\cdots H_2O$  and  $t-SO_3\cdots H_2SO_4\cdots H_2O$  were respectively expressed as  $[t-H_2SO_4\cdots H_2O] = K_{eq(t-SW)} \times [H_2SO_4] \times [H_2O]$ ,  $[t-HO_2\cdots H_2SO_4\cdots H_2O] = K_{eq6A} \times [H_2SO_4\cdots H_2O] \times [HO_2]$  and  $[t-SO_3\cdots H_2SO_4\cdots H_2O] = K_{eq6B} \times [H_2SO_4\cdots H_2O] \times [SO_3]$ ; the concentrations of  $(H_2SO_4)_2$ ,  $HO_2\cdots (H_2SO_4)_2$  and  $SO_3\cdots (H_2SO_4)_2$  were respectively expressed as  $[(H_2SO_4)_2] = K_{eq(SD)} \times [H_2SO_4]^2$ ,  $[HO_2\cdots (H_2SO_4)_2] = K_{eq7A} \times [(H_2SO_4)_2] \times [HO_2]$  and  $[SO_3\cdots (H_2SO_4)_2] = K_{eq7B} \times [(H_2SO_4)_2] \times [SO_3]$ .

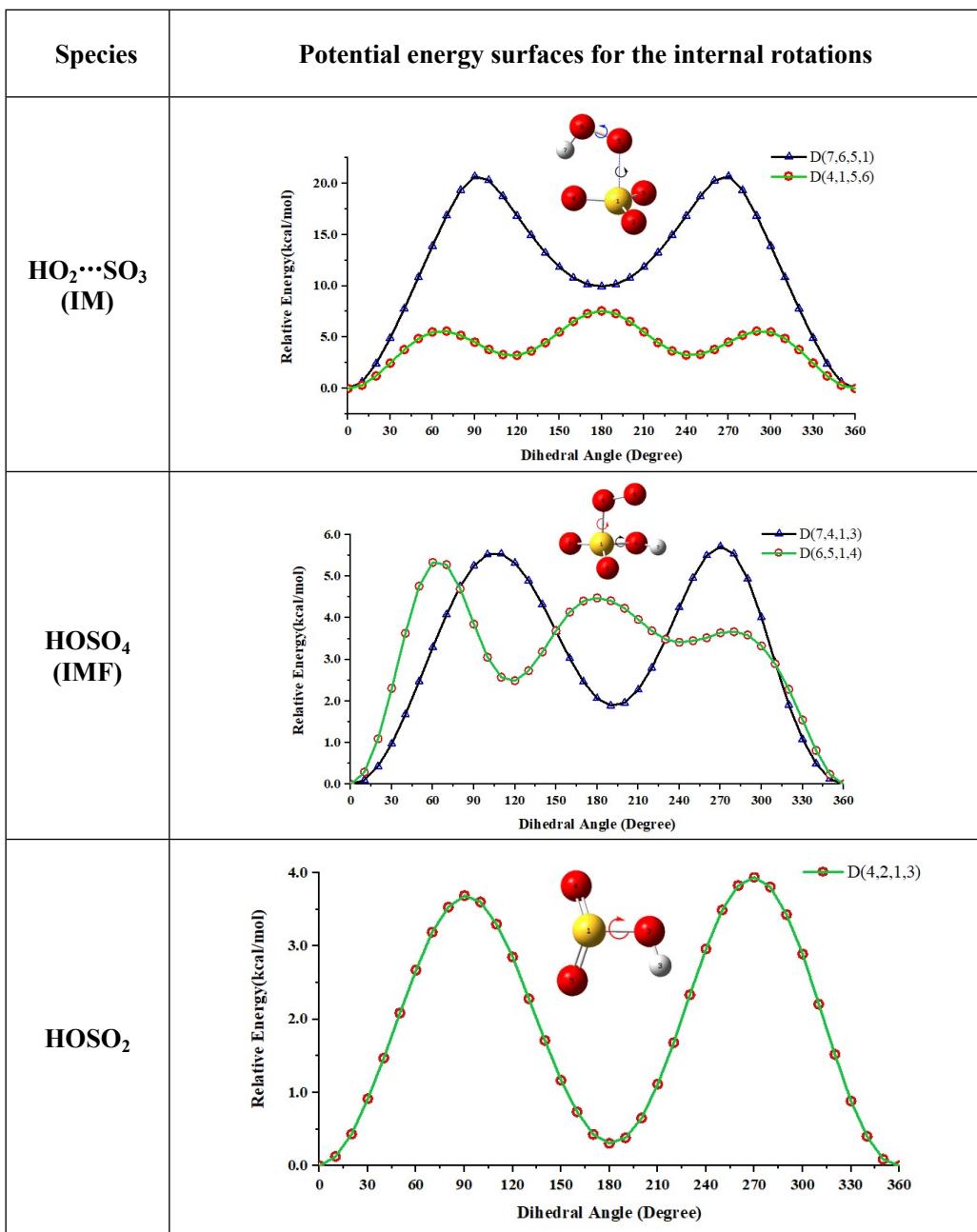
<sup>c</sup> The typical tropospheric concentrations<sup>2,3</sup> of  $2.60 \times 10^{17}$  -  $2.30 \times 10^{18}$  molecules $\cdot cm^{-3}$  for  $H_2O$ ,  $2.04 \times 10^{14}$  -  $9.24 \times 10^{15}$  molecules $\cdot cm^{-3}$  for  $(H_2O)_2$  and  $5.0 \times 10^7$  molecules $\cdot cm^{-3}$  of  $H_2SO_4$  were respectively taken from reference. Besides, the concentrations of  $H_2SO_4\cdots H_2O$  and  $(H_2SO_4)_2$  were respectively calculated to be  $2.04 \times 10^7$  -  $2.44 \times 10^7$  molecules $\cdot cm^{-3}$  and  $7.42 \times 10^0$  -  $1.64 \times 10^{-1}$  molecules $\cdot cm^{-3}$ .

As for  $HO_2\cdots X$  ( $X = H_2O$ ,  $(H_2O)_2$ ,  $H_2SO_4$ ,  $H_2SO_4\cdots H_2O$  and  $(H_2SO_4)_2$ ) and  $SO_3\cdots X$  complexes, their corresponding equilibrium constants and concentrations within the temperature range of 280-320 K have been listed in Table S2. However, due to the concentration<sup>1,4</sup> of  $SO_3$  ( $1.0 \times 10^3$  molecules $\cdot cm^{-3}$ ) is much lower than that of  $HO_2$  ( $3.0 \times 10^8$  molecules $\cdot cm^{-3}$ ), the concentrations of  $HO_2\cdots X$  complexes shown in Table S2 are larger than those of  $SO_3\cdots X$  complexes. Thus, we predict that the  $HO_2 + SO_3$  reaction in the presence of  $X$  mainly occurs through the  $HO_2\cdots X + SO_3$  reaction.

**Table S3** Zero point energy (ZPE/(kcal·mol<sup>-1</sup>)), entropies (S/(cal·mol<sup>-1</sup>·K<sup>-1</sup>)), relative energies ( $\Delta E$  and  $\Delta(E + \text{ZPE})$ /(kcal·mol<sup>-1</sup>)), enthalpies ( $\Delta H(298)$ /(kcal·mol<sup>-1</sup>)) and free energies ( $\Delta G(298)$ /(kcal·mol<sup>-1</sup>)) for the HO<sub>2</sub> + SO<sub>3</sub> reaction without and with catalyst X ( $X = \text{H}_2\text{O}$ , (H<sub>2</sub>O)<sub>2</sub>, H<sub>2</sub>SO<sub>4</sub>, H<sub>2</sub>SO<sub>4</sub>···H<sub>2</sub>O and (H<sub>2</sub>SO<sub>4</sub>)<sub>2</sub>)

Species	ZPE	$\Delta E$	S	$\Delta G$	$\Delta(E + \text{ZPE})$	$\Delta H$	$T_1$
HO <sub>2</sub> + SO <sub>3</sub>	16.3	0.0	115.8	0.0	0.0	0.0	0.0256; 0.0177
IM	18.6	-12.9	79.6	-9.8	-10.5	-11.2	0.0231
TS	16.5	-10.0	75.8	-8.6	-9.8	-11.1	0.0197
HOSO <sub>4</sub>	18.6	-16.5	78.1	-13.1	-14.2	-15.0	0.0227
HOSO <sub>2</sub> + <sup>3</sup> O <sub>2</sub>	15.9	-2.6	48.9	12.8	-3.0	-2.9	0.0204, 0.0168
HO <sub>2</sub> + H <sub>2</sub> O + SO <sub>3</sub>	29.2	0.0	160.8	0.0	0.0	0.0	0.0256, 0.0106, 0.0177
HO <sub>2</sub> ···H <sub>2</sub> O + SO <sub>3</sub>	31.6	-9.2	132.3	1.0	-6.8	-7.5	0.0239, 0.0177
SO <sub>3</sub> ···H <sub>2</sub> O + HO <sub>2</sub>	31.5	-9.4	132.5	1.9	-7.2	-7.6	0.0163, 0.0256
IM_WM1	33.6	-23.9	90.2	0.2	-19.5	-20.9	0.0226
TS_WM1	32.6	-22.0	84.6	1.9	-18.5	-20.8	0.0245
IMF_WM1	33.7	-30.8	90.2	-6.7	-26.3	-27.8	0.0224
HOSO <sub>4</sub> + H <sub>2</sub> O	31.5	-16.5	123.1	-3.7	-14.2	-15.0	0.0227, 0.0106
HO <sub>2</sub> + H <sub>2</sub> O + SO <sub>3</sub>	29.2	0.0	160.8	0.0	0.0	0.0	0.0256, 0.0106, 0.0177
H <sub>2</sub> O···HO <sub>2</sub> + SO <sub>3</sub>	30.7	-3.3	142.6	4.3	-1.8	-1.8	0.0235, 0.0177
IM_WM2	32.3	-13.9	104.3	5.9	-10.7	-11.0	0.0222
TS_WM2	30.8	-3.4	92.4	16.7	-1.8	-3.7	0.0242
IMF_WM2	32.8	-18.7	101.3	2.1	-15.1	-15.7	0.0222
HOSO <sub>4</sub> + H <sub>2</sub> O	31.5	-16.5	123.2	-3.8	-14.2	-15.0	0.0227, 0.0106
HO <sub>2</sub> + H <sub>2</sub> O + SO <sub>3</sub>	29.2	0.0	160.8	0.0	0.0	29.2	0.0256, 0.0106, 0.0177
SO <sub>3</sub> ···H <sub>2</sub> O + HO <sub>2</sub>	31.5	-9.4	132.5	0.9	-7.0	31.5	0.0163, 0.0177
IM_WM3	32.8	-18.9	98.1	2.9	-15.2	32.8	0.0222
TS_WM3	30.7	-14.5	93.4	5.9	-12.9	30.7	0.0186
IMF_WM3	33.6	-29.4	91.9	-5.8	-25.0	33.6	0.0215
HOSO <sub>4</sub> + H <sub>2</sub> O	31.5	-16.5	123.2	-3.8	-14.2	31.5	0.0227, 0.0106
HO <sub>2</sub> + (H <sub>2</sub> O) <sub>2</sub> + SO <sub>3</sub>	45.5	0.0	187.7	0.0	0.0	0.0	0.0256, 0.0123, 0.0177
HO <sub>2</sub> ···(H <sub>2</sub> O) <sub>2</sub> + SO <sub>3</sub>	48.8	-15.9	147.1	-1.9	-12.6	-14.0	0.0240, 0.0256
SO <sub>3</sub> ···(H <sub>2</sub> O) <sub>2</sub> + HO <sub>2</sub>	48.4	-16.5	146.6	-2.3	-13.6	-14.6	0.0233, 0.0177
IM_WD1	49.4	-28.6	108.0	-2.5	-24.6	-26.2	0.0224
TS_WD1	48.3	-27.9	91.5	-1.9	-25.2	-27.5	0.0240
IMF_WD1	50.3	-35.0	106.9	-7.5	-30.2	-32.2	0.0212
HOSO <sub>4</sub> + (H <sub>2</sub> O) <sub>2</sub>	31.5	-16.5	123.2	-3.8	-14.2	31.5	0.0227, 0.0123
HO <sub>2</sub> + c-H <sub>2</sub> SO <sub>4</sub> + SO <sub>3</sub>	40.0	0.0	188.2	0.0	0.0	0.0	0.0256, 0.0161, 0.0177
c-HO <sub>2</sub> ···H <sub>2</sub> SO <sub>4</sub> + SO <sub>3</sub>	41.8	-15.1	152.1	-3.1	-13.4	-13.9	0.0225, 0.0177

<i>c</i> - SO <sub>3</sub> …H <sub>2</sub> SO <sub>4</sub> + HO <sub>2</sub>	41.5	-13.6	148.5	-0.8	-12.2	-12.6	0.0169, 0.0256
<i>c</i> -IM_SA1	42.6	-26.4	109.0	-1.2	-23.8	-24.8	0.0175
<i>c</i> -TS_SA1	41.5	-24.9	105.2	-0.4	-23.5	-25.1	0.0205
<i>c</i> -IMF_SA1	43.3	-32.8	108.1	-6.7	-29.5	-30.6	0.0219
HOSO <sub>4</sub> + <i>c</i> -H <sub>2</sub> SO <sub>4</sub>	42.4	-16.5	150.6	-3.8	-14.2	-15.0	0.0227, 0.0161
HO <sub>2</sub> + <i>t</i> -H <sub>2</sub> SO <sub>4</sub> + SO <sub>3</sub>	40.3	0.0	189.5	0.0	0.0	0.0	0.0256, 0.0162, 0.0177
<i>t</i> -HO <sub>2</sub> …H <sub>2</sub> SO <sub>4</sub> + SO <sub>3</sub>	41.7	-15.5	153.9	-3.9	-14.1	-14.5	0.0225, 0.0177
<i>t</i> -SO <sub>3</sub> …H <sub>2</sub> SO <sub>4</sub> + HO <sub>2</sub>	41.3	-12.1	154.6	-0.4	-11.1	-10.8	0.0169, 0.0256
<i>t</i> -IM_SA1	42.8	-23.8	111.1	1.5	-21.3	-21.9	0.0198
<i>t</i> -TS_SA1	40.2	-18.3	106.6	4.9	-18.4	-19.8	0.0207
<i>t</i> -IMF_SA1	42.8	-27.1	111.8	-7.1	-24.6	-30.3	0.0222
HOSO <sub>4</sub> + <i>t</i> -H <sub>2</sub> SO <sub>4</sub>	42.4	-16.5	149.7	-3.8	-14.2	-15.0	0.0227, 0.0162
HO <sub>2</sub> + <i>c</i> -H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O + SO <sub>3</sub>	55.2	0.0	202.5	0.0	0.0	0.0	0.0256, 0.0148, 0.0177
<i>c</i> -HO <sub>2</sub> …H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O + SO <sub>3</sub>	56.5	-15.0	166.6	-3.3	-13.6	-14.1	0.0213, 0.0177
<i>c</i> -SO <sub>3</sub> …H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O + HO <sub>2</sub>	59.6	-17.0	156.8	-2.3	-12.5	-13.3	0.0162, 0.0256
<i>c</i> -IM_SW1	57.6	-28.0	119.8	-2.0	-25.6	-26.6	0.0192
<i>c</i> -TS_SW1	56.3	-26.5	117.6	-1.5	-25.3	-26.8	0.0174
<i>c</i> -IMF_SW1	57.8	-33.4	122.3	-7.9	-30.8	-31.8	0.0209
HOSO <sub>4</sub> + <i>c</i> - H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O	57.5	-16.5	164.9	-3.8	-14.2	-15.0	0.0227, 0.0148
HO <sub>2</sub> + <i>t</i> -H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O + SO <sub>3</sub>	55.4	0.0	200.6	0.0	0.0	0.0	0.0256, 0.0153, 0.0177
<i>t</i> -HO <sub>2</sub> …H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O + SO <sub>3</sub>	56.5	-15.3	167.2	-4.5	-14.2	-14.4	0.0213; 0.0177
<i>t</i> -SO <sub>3</sub> …H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O + HO <sub>2</sub>	55.8	-11.9	166.5	-1.1	-11.5	-11.3	0.0162, 0.0256
<i>t</i> -IM_SW1	57.3	-24.8	125.8	-1.2	-22.9	-23.5	0.0192
<i>t</i> -TS_SW1	54.9	-21.4	118.6	1.2	-21.8	-23.3	0.0174
<i>t</i> -IMF_SW1	57.4	-32.6	124.3	-8.7	-30.6	-31.4	0.0209
HOSO <sub>4</sub> + <i>t</i> - H <sub>2</sub> SO <sub>4</sub> …H <sub>2</sub> O	57.7	-16.5	162.9	-3.8	-14.2	-15.0	0.0227, 0.0153
HO <sub>2</sub> + (H <sub>2</sub> SO <sub>4</sub> ) <sub>2</sub> + SO <sub>3</sub>	65.1	0.0	224.0	0.0	0.0	0.0	0.0256, 0.0181, 0.0177
HO <sub>2</sub> …(H <sub>2</sub> SO <sub>4</sub> ) <sub>2</sub> + SO <sub>3</sub>	66.7	-15.7	184.0	-2.5	-14.0	-14.4	0.0218, 0.0177
SO <sub>3</sub> …(H <sub>2</sub> SO <sub>4</sub> ) <sub>2</sub> + HO <sub>2</sub>	57.2	-14.1	126.8	-0.8	-13.2	-13.4	0.0157, 0.0256
IM_SD1	67.7	-31.8	140.0	-5.0	-26.0	-30.0	0.0183
TS_SD1	65.8	-32.0	136.2	-6.4	-27.0	-32.7	0.0205
IMF_SD1	67.5	-36.3	139.5	-9.6	-31.3	-34.7	0.0215
HOSO <sub>4</sub> + (H <sub>2</sub> SO <sub>4</sub> ) <sub>2</sub>	67.4	-16.5	184.1	-3.8	-14.2	-15.0	0.0227, 0.0181



**Fig. S8** Hindrance potentials for  $\text{HO}_2\cdots\text{SO}_3$ ,  $\text{HOSO}_4$  and  $\text{HOSO}_2$  calculated at the M06-2X/6-311+G(2df,2pd) level of theory

For hindered internal rotation (HIR) treatment, the hindrance potentials,  $V(\theta)$ , as a function of torsional angle,  $\theta$ , along with the single bonds (i.e., S1-O4 and O4-O5, Fig. S8) were explicitly obtained at the M06-2X/6-311+G(2df,2pd) level via relaxed surface scans with the step size of  $10^\circ$  for the dihedral angles corresponding to the rotations. As seen in Fig. S8, the single bond of O4-O5 and S1-O4 in  $\text{HO}_2\cdots\text{SO}_3$ , the single bond of S1-O4 in  $\text{HOSO}_4$  and the single bond of S1-O4 in  $\text{HOSO}_2$  need to be treated by hindered internal rotators. The parameters of the HIR are automatically determined using the Graphical User Interface (GUI) in Mesmer software, and the procedural details of the hindered internal rotation (HIR) correction can be found in the works of Le et al.<sup>5,6</sup> and Mai et al.<sup>7-14</sup>

**Part A Hindered internal rotation analysis for the HO<sub>2</sub> + SO<sub>3</sub> reaction without and with X (X = H<sub>2</sub>O, (H<sub>2</sub>O)<sub>2</sub>, H<sub>2</sub>SO<sub>4</sub>, H<sub>2</sub>SO<sub>4</sub>···H<sub>2</sub>O and (H<sub>2</sub>SO<sub>4</sub>)<sub>2</sub>)**

Within the temperature range of 280-320 K, the rate constants ( $k_{R1}$ ) for the HO<sub>2</sub> + SO<sub>3</sub> reaction without and with HIR treatments at 760 Torr has been listed in Table S4. It should be noted that, at 760 Torr, the HIR correction just plays a minor role in the HO<sub>2</sub> + SO<sub>3</sub> reaction, e.g., HIR treatment listed in Table S4 enhanced the rate constants by a factor of 1.14 to 1.15 within the temperature range of 280-320 K. Besides, the hindered internal rotation analysis for the pre- and post-reactive complexes and transition states involved in the HO<sub>2</sub> + SO<sub>3</sub> reaction with  $X$  have been calculated in the Gaussian 09 program with the keywords of “freq = hindrot” and “integral = ultrafine”. The calculations reveal that no frequencies need to be corrected. So, we predict that the HIR correction just plays a minor role in the HO<sub>2</sub> + SO<sub>3</sub> reaction with  $X$ . This can be explained by two reasons as follows. On the one hand, the pre- and post-reactive complexes and transition states involved in the HO<sub>2</sub> + SO<sub>3</sub> reaction with  $X$  were shown the quasi-planar ring structures and cage-like ring structures. As compared with the naked reaction (Fig. 3(a)), these ring structures reduce the ring tension obviously and increase the stability of the pre- and post-reactive complex and transition state greatly. On the other hand, the numbers of hydrogen bonds in  $X$ -assisted pre- and post-reactive complexes and transition states were increased, which hinder the rotation bonds of S-O4 and O4-O5 (Fig. 3-6) in  $X$ -assisted pre- and post-reactive complex and transition state. The detail information for the rate constants ( $k_{R1}$ ) for the HO<sub>2</sub> + SO<sub>3</sub> reaction without and with HIR treatments has been displayed in Table S4.

**Table S4** The rate constants ( $k_{R1}$ ) for the HO<sub>2</sub> + SO<sub>3</sub> reaction without and with HIR treatments within the temperature range of 280-320 K (at 760 Torr)

with HIR treatments	without HIR treatments	Factor
$2.11 \times 10^{-11}$	$1.85 \times 10^{-11}$	1.14
$1.95 \times 10^{-11}$	$1.71 \times 10^{-11}$	1.14
$1.83 \times 10^{-11}$	$1.60 \times 10^{-11}$	1.14
$1.80 \times 10^{-11}$	$1.57 \times 10^{-11}$	1.14
$1.66 \times 10^{-11}$	$1.45 \times 10^{-11}$	1.15
$1.53 \times 10^{-11}$	$1.33 \times 10^{-11}$	1.15

**Table S5** The calculated branching ratio ( $\beta$ )<sup>a</sup> for the three pathways ( $\text{HO}_2\cdots\text{SO}_3\cdots X \rightarrow \text{HOSO}_2 + \text{O}_2 + X$ , path 1,  $\text{HO}_2\cdots\text{SO}_3\cdots X \rightarrow \text{HO}_2 + \text{SO}_3\cdots X$ , path 2, and  $\text{HO}_2\cdots\text{SO}_3\cdots X \rightarrow \text{HO}_2\cdots X + \text{SO}_3$ , path 3) yielding from  $\text{HO}_2\cdots\text{SO}_3\cdots X$  adduct within the pressure range of 10-300 Torr (at 298 K)

P (Torr)	Branching Ratio (%) for $\text{HO}_2\cdots\text{SO}_3\cdots X$ complex											
	$\text{HO}_2\cdots\text{SO}_3$		$\text{HO}_2\cdots\text{SO}_3\cdots\text{H}_2\text{O}$		$\text{HO}_2\cdots\text{SO}_3\cdots(\text{H}_2\text{O})_2$		$\text{HO}_2\cdots\text{SO}_3\cdots\text{H}_2\text{SO}_4$		$\text{HO}_2\cdots\text{SO}_3\cdots\text{H}_2\text{SO}_4\cdots\text{H}_2\text{O}$		$\text{HO}_2\cdots\text{SO}_3\cdots(\text{H}_2\text{SO}_4)_2$	
	$\beta_1$	$\beta_2 + \beta_3$	$\beta_1$	$\beta_2 + \beta_3$	$\beta_1$	$\beta_2 + \beta_3$	$\beta_1$	$\beta_2 + \beta_3$	$\beta_1$	$\beta_2 + \beta_3$	$\beta_1$	$\beta_2 + \beta_3$
300	99.89%	0.11%	99.85%	0.15%	99.97%	0.03%	99.93%	0.07%	99.93%	0.07%	99.88%	0.12%
100	99.84%	0.16%	99.86%	0.14%	99.98%	0.02%	99.95%	0.05%	99.95%	0.05%	99.95%	0.05%
50	99.80%	0.20%	99.87%	0.13%	99.98%	0.02%	99.96%	0.04%	99.96%	0.04%	99.96%	0.04%
10	99.76%	0.24%	99.87%	0.13%	99.99%	0.01%	99.97%	0.03%	99.97%	0.03%	99.98%	0.02%

<sup>a</sup>  $\beta_1$ ,  $\beta_2$  and  $\beta_3$  were the branching ratio for the path 1, path 2 and path 3. The calculated  $\beta_1$ ,  $\beta_2$  and  $\beta_3$  can be respectively expressed as  $\beta_1 = k_{\text{path } 1}/(k_{\text{path } 1} + k_{\text{path } 2} + k_{\text{path } 3})$ ,  $\beta_2 = k_{\text{path } 2}/(k_{\text{path } 1} + k_{\text{path } 2} + k_{\text{path } 3})$  and  $\beta_3 = k_{\text{path } 3}/(k_{\text{path } 1} + k_{\text{path } 2} + k_{\text{path } 3})$ .

The pressure dependent rate constant for the three pathways ( $\text{HO}_2\cdots\text{SO}_3\cdots X \rightarrow \text{HOSO}_2 + \text{O}_2 + X$ , path 1,  $\text{HO}_2\cdots\text{SO}_3\cdots X \rightarrow \text{HO}_2 + \text{SO}_3\cdots X$ , path 2, and  $\text{HO}_2\cdots\text{SO}_3\cdots X \rightarrow \text{HO}_2\cdots X + \text{SO}_3$ , path 3) yielding from  $\text{HO}_2\cdots\text{SO}_3\cdots X$  adduct as given below,

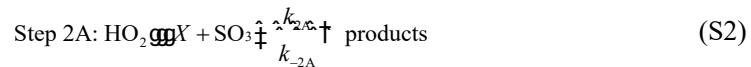
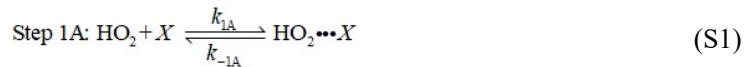


The pressure dependent rate constant at 298 K for the above-mentioned pathways were calculated within the pressure range of 10-300 Torr. Their corresponding branching ratios were given in Table S5. As can be seen from Table S5, one can easily conclude that path 1 was the major pathway, whereas paths 2 and 3 were the minor channels within the pressure range of 10-300 Torr. Since the branching ratios of path 1 were more than 99%, the paths 2 and 3 can be conveniently avoided for further discussion. The result and discussion will be based on the kinetics of path 1 only unless otherwise stated.

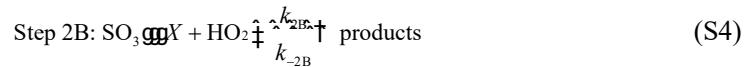
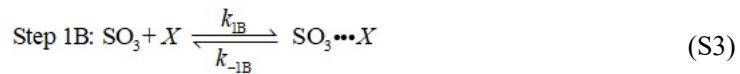
**Part B Bimolecular rate constants ( $\text{cm}^3 \cdot \text{molecules}^{-1} \cdot \text{s}^{-1}$ ) for the  $\text{SO}_3 + \text{HO}_2 \cdots X$  ( $X = \text{H}_2\text{O}$ ,  $(\text{H}_2\text{O})_2$ ,  $\text{H}_2\text{SO}_4$ ,  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  and  $(\text{H}_2\text{SO}_4)_2$ ) and  $\text{HO}_2 + \text{SO}_3 \cdots X$  reactions**

As for the  $\text{HO}_2 + \text{SO}_3 + X$  ( $X = \text{H}_2\text{O}$ ,  $(\text{H}_2\text{O})_2$ ,  $\text{H}_2\text{SO}_4$ ,  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  and  $(\text{H}_2\text{SO}_4)_2$ ) reaction, two entry channels  $\text{HO}_2 \cdots X + \text{SO}_3$  (Channel A) and  $\text{SO}_3 \cdots X + \text{HO}_2$  (Channel B) have been considered for the rate constants calculations as follows.

**Channel A**



**Channel B**



As for the  $\text{HO}_2 + \text{SO}_3 + X$  reaction, two entry channels  $\text{HO}_2 \cdots X + \text{SO}_3$  (Channel A) and  $\text{SO}_3 \cdots X + \text{HO}_2$  (Channel B) have been respectively considered for the rate constants calculations involved in Table S6 and Table S7. Due to the fact that both of the  $\text{HO}_2 \cdots X + \text{SO}_3$  and  $\text{SO}_3 \cdots X + \text{HO}_2$  reactions proceed through the same pre-reactive trimolecular complex  $\text{HO}_2 \cdots \text{SO}_3 \cdots X$ , so the product of  $K_{\text{eq1A}} \times k_{2A}$  is equal to the product of  $K_{\text{eq1B}} \times k_{2B}$ . Based on two facts above, the effective rate constant for the  $\text{HO}_2 \cdots X + \text{SO}_3$  reaction was equal to the  $\text{SO}_3 \cdots X + \text{HO}_2$  reaction. These results have been reported in our previous work<sup>15,16</sup>. The detail information of bimolecular rate constants ( $\text{cm}^3 \cdot \text{molecules}^{-1} \cdot \text{s}^{-1}$ ) for the  $\text{SO}_3 + \text{HO}_2 \cdots X$  ( $X = \text{H}_2\text{O}$ ,  $(\text{H}_2\text{O})_2$ ,  $\text{H}_2\text{SO}_4$ ,  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  and  $(\text{H}_2\text{SO}_4)_2$ ) and  $\text{HO}_2 + \text{SO}_3 \cdots X$  reaction have been respectively listed in Table 1 and Table S6.

**Table S6** Bimolecular rate constants ( $\text{cm}^3 \cdot \text{molecules}^{-1} \cdot \text{s}^{-1}$ ) for the  $\text{HO}_2 + \text{SO}_3 \cdots X$  ( $X = \text{H}_2\text{O}, (\text{H}_2\text{O})_2, \text{H}_2\text{SO}_4, \text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  and  $(\text{H}_2\text{SO}_4)_2$ ) reaction calculated by master equation within the temperature range of 280–320 K (at 760 Torr) <sup>a</sup>

Reaction	$T$ (K)	280	290	298	300	310	320
Channel WM1	$k_{\text{WM1\_b}}$	$1.61 \times 10^{-11}$	$1.34 \times 10^{-11}$	$1.16 \times 10^{-11}$	$1.12 \times 10^{-11}$	$9.25 \times 10^{-12}$	$7.65 \times 10^{-12}$
Channel WD1	$k_{\text{WD1\_b}}$	$1.15 \times 10^{-11}$	$8.75 \times 10^{-12}$	$7.01 \times 10^{-12}$	$6.63 \times 10^{-12}$	$5.01 \times 10^{-12}$	$3.77 \times 10^{-12}$
Channel <i>c</i> -SA	$k_{\text{c-SA\_b}}$	$2.05 \times 10^{-11}$	$1.57 \times 10^{-11}$	$1.26 \times 10^{-11}$	$1.20 \times 10^{-11}$	$9.06 \times 10^{-11}$	$6.84 \times 10^{-11}$
Channel <i>t</i> -SA	$k_{\text{t-SA\_b}}$	$1.77 \times 10^{-13}$	$1.25 \times 10^{-13}$	$9.41 \times 10^{-14}$	$8.77 \times 10^{-14}$	$6.18 \times 10^{-14}$	$4.37 \times 10^{-14}$
Channel <i>c</i> -SW	$k_{\text{c-SW\_b}}$	$6.06 \times 10^{-11}$	$5.09 \times 10^{-11}$	$4.38 \times 10^{-11}$	$4.21 \times 10^{-11}$	$3.45 \times 10^{-11}$	$2.79 \times 10^{-11}$
Channel <i>t</i> -SW	$k_{\text{t-SW\_b}}$	$7.18 \times 10^{-12}$	$5.61 \times 10^{-12}$	$4.60 \times 10^{-12}$	$4.37 \times 10^{-12}$	$3.39 \times 10^{-12}$	$2.62 \times 10^{-12}$
Channel SD	$k_{\text{SD\_b}}$	$6.59 \times 10^{-11}$	$5.40 \times 10^{-11}$	$4.55 \times 10^{-11}$	$4.35 \times 10^{-11}$	$3.44 \times 10^{-11}$	$2.68 \times 10^{-11}$

$k_{\text{WM1\_b}}, k_{\text{WD1\_b}}, k_{\text{c-SA\_b}}, k_{\text{t-SA\_b}}, k_{\text{c-SW\_b}}, k_{\text{t-SW\_b}}$  and  $k_{\text{SD\_b}}$  was respectively denoted the rate constants for the  $\text{HO}_2 + \text{SO}_3 \cdots \text{H}_2\text{O}$ ,  $\text{HO}_2 + \text{SO}_3 \cdots (\text{H}_2\text{O})_2$ ,  $\text{HO}_2 + c\text{-SO}_3 \cdots \text{H}_2\text{SO}_4$ ,  $\text{HO}_2 + t\text{-SO}_3 \cdots \text{H}_2\text{SO}_4$ ,  $\text{HO}_2 + c\text{-SO}_3 \cdots \text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$ ,  $\text{HO}_2 + t\text{-SO}_3 \cdots \text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  and  $\text{HO}_2 + c\text{-SO}_3 \cdots (\text{H}_2\text{SO}_4)_2$  reactions.

**Table S7** The calculated rate constants ( $\text{cm}^3 \cdot \text{molecules}^{-1} \cdot \text{s}^{-1}$ ) for the  $\text{HO}_2 + \text{SO}_3$  reaction without and with  $\text{H}_2\text{O}$ ,  $(\text{H}_2\text{O})_2$  and  $\text{H}_2\text{SO}_4$  within the temperature range of 280-320 K and the pressure range of 10-760 Torr

	T(K)	10 Torr	50 Torr	100 Torr	300 Torr	760 Torr
$k_{\text{RI}}$	280	$2.11 \times 10^{-11}$				
	290	$1.95 \times 10^{-11}$				
	298	$1.8 \times 10^{-11}$	$1.83 \times 10^{-11}$	$1.83 \times 10^{-11}$	$1.83 \times 10^{-11}$	$1.83 \times 10^{-11}$
	300	$1.80 \times 10^{-11}$				
	310	$1.66 \times 10^{-11}$				
	320	$1.53 \times 10^{-11}$				
$k_{\text{WM1}}$	280	$1.63 \times 10^{-11}$	$1.64 \times 10^{-11}$	$1.64 \times 10^{-11}$	$1.64 \times 10^{-11}$	$1.65 \times 10^{-11}$
	290	$1.39 \times 10^{-11}$	$1.40 \times 10^{-11}$	$1.40 \times 10^{-11}$	$1.40 \times 10^{-11}$	$1.40 \times 10^{-11}$
	298	$1.21 \times 10^{-11}$	$1.22 \times 10^{-11}$	$1.22 \times 10^{-11}$	$1.22 \times 10^{-11}$	$1.22 \times 10^{-11}$
	300	$1.17 \times 10^{-11}$	$1.18 \times 10^{-11}$	$1.18 \times 10^{-11}$	$1.18 \times 10^{-11}$	$1.18 \times 10^{-11}$
	310	$9.82 \times 10^{-12}$	$9.95 \times 10^{-12}$	$9.97 \times 10^{-12}$	$9.98 \times 10^{-12}$	$9.99 \times 10^{-12}$
	320	$8.22 \times 10^{-12}$	$8.38 \times 10^{-12}$	$8.40 \times 10^{-12}$	$8.41 \times 10^{-12}$	$8.42 \times 10^{-12}$
$k_{\text{WD}}$	280	$4.77 \times 10^{-11}$	$4.81 \times 10^{-11}$	$4.81 \times 10^{-11}$	$4.82 \times 10^{-11}$	$4.82 \times 10^{-11}$
	290	$4.18 \times 10^{-11}$	$4.23 \times 10^{-11}$	$4.23 \times 10^{-11}$	$4.24 \times 10^{-11}$	$4.24 \times 10^{-11}$
	298	$3.74 \times 10^{-11}$	$3.79 \times 10^{-11}$	$3.79 \times 10^{-11}$	$3.80 \times 10^{-11}$	$3.80 \times 10^{-11}$
	300	$3.63 \times 10^{-11}$	$3.68 \times 10^{-11}$	$3.68 \times 10^{-11}$	$3.69 \times 10^{-11}$	$3.69 \times 10^{-11}$
	310	$3.13 \times 10^{-11}$	$3.18 \times 10^{-11}$	$3.18 \times 10^{-11}$	$3.19 \times 10^{-11}$	$3.19 \times 10^{-11}$
	320	$2.76 \times 10^{-11}$	$2.80 \times 10^{-11}$	$2.80 \times 10^{-11}$	$2.84 \times 10^{-11}$	$2.84 \times 10^{-11}$
$k_{\text{c-SA}}$	280	$1.48 \times 10^{-11}$	$1.60 \times 10^{-11}$	$1.62 \times 10^{-11}$	$1.63 \times 10^{-11}$	$1.64 \times 10^{-11}$
	290	$1.19 \times 10^{-11}$	$1.28 \times 10^{-11}$	$1.30 \times 10^{-11}$	$1.31 \times 10^{-11}$	$1.31 \times 10^{-11}$
	298	$8.50 \times 10^{-12}$	$1.03 \times 10^{-11}$	$1.06 \times 10^{-11}$	$1.08 \times 10^{-11}$	$1.09 \times 10^{-11}$
	300	$7.89 \times 10^{-12}$	$9.76 \times 10^{-12}$	$1.01 \times 10^{-11}$	$1.03 \times 10^{-11}$	$1.04 \times 10^{-11}$
	310	$5.13 \times 10^{-12}$	$7.22 \times 10^{-12}$	$7.66 \times 10^{-12}$	$8.00 \times 10^{-12}$	$8.18 \times 10^{-12}$
	320	$3.69 \times 10^{-12}$	$4.50 \times 10^{-12}$	$5.47 \times 10^{-12}$	$5.66 \times 10^{-12}$	$6.40 \times 10^{-12}$

**Table S8** Effective rate constants ( $k'$ ) for the  $\text{HO}_2 + \text{SO}_3$  reaction with  $X$  ( $X = \text{H}_2\text{O}, (\text{H}_2\text{O})_2, \text{H}_2\text{SO}_4, \text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  and  $(\text{H}_2\text{SO}_4)_2$ ) within the temperature range of 280-320 K (at 0 km altitude)

Channels	$T$ (K)	280	290	298	300	310	320
Channel WM1	$k'_{\text{WM1}}$	$6.48 \times 10^{-14}$	$6.28 \times 10^{-14}$	$6.10 \times 10^{-14}$	$6.09 \times 10^{-14}$	$5.75 \times 10^{-14}$	$5.26 \times 10^{-14}$
Channel WM2	$k'_{\text{WM2}}$	$5.92 \times 10^{-21}$	$8.51 \times 10^{-21}$	$1.13 \times 10^{-20}$	$1.20 \times 10^{-20}$	$1.65 \times 10^{-20}$	$2.16 \times 10^{-20}$
Channel WM3	$k'_{\text{WM3}}$	$3.33 \times 10^{-14}$	$3.09 \times 10^{-14}$	$2.96 \times 10^{-14}$	$2.89 \times 10^{-14}$	$2.62 \times 10^{-14}$	$2.32 \times 10^{-14}$
Channel WD1	$k'_{\text{WD1}}$	$3.39 \times 10^{-14}$	$3.68 \times 10^{-14}$	$3.80 \times 10^{-14}$	$3.96 \times 10^{-14}$	$4.06 \times 10^{-14}$	$4.11 \times 10^{-14}$
Channel <i>c</i> -SA	$k'_{\text{c-SA}}$	$5.27 \times 10^{-20}$	$1.94 \times 10^{-20}$	$8.98 \times 10^{-21}$	$7.29 \times 10^{-21}$	$2.92 \times 10^{-21}$	$9.91 \times 10^{-22}$
Channel <i>t</i> -SA	$k'_{\text{t-SA}}$	$1.23 \times 10^{-20}$	$3.49 \times 10^{-21}$	$1.53 \times 10^{-21}$	$1.21 \times 10^{-21}$	$4.89 \times 10^{-22}$	$1.53 \times 10^{-22}$
Channel <i>c</i> -SW	$k'_{\text{c-SW}}$	$1.05 \times 10^{-19}$	$4.00 \times 10^{-20}$	$1.92 \times 10^{-20}$	$1.56 \times 10^{-20}$	$6.38 \times 10^{-21}$	$2.63 \times 10^{-21}$
Channel <i>t</i> -SW	$k'_{\text{t-SW}}$	$5.02 \times 10^{-19}$	$1.68 \times 10^{-19}$	$7.38 \times 10^{-20}$	$5.87 \times 10^{-20}$	$2.18 \times 10^{-20}$	$8.30 \times 10^{-21}$
Channel SD	$k'_{\text{SD}}$	$2.85 \times 10^{-26}$	$3.82 \times 10^{-27}$	$8.20 \times 10^{-28}$	$5.69 \times 10^{-28}$	$9.36 \times 10^{-29}$	$1.57 \times 10^{-29}$
$k'_{\text{WM1}}/k_{\text{tot}}$ (%)		0.31%	0.32%	0.33%	0.34%	0.34%	0.34%
$k'_{\text{WD1}}/k_{\text{tot}}$ (%)		0.16%	0.19%	0.21%	0.22%	0.24%	0.27%

**Table S9** Equilibrium constants ( $K_{eq}$ ,  $\text{cm}^3 \cdot \text{molecules}^{-1}$ ) for the formation of  $\text{HO}_2 \cdots \text{H}_2\text{O}$ ,  $\text{HO}_2 \cdots (\text{H}_2\text{O})_2$ ,  $c\text{-HO}_2 \cdots \text{H}_2\text{SO}_4$  and  $c\text{-HO}_2 \cdots \text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  complexes, concentrations (molecules $\cdot\text{cm}^{-3}$ ) of  $\text{H}_2\text{O}$ ,  $(\text{H}_2\text{O})_2$ ,  $\text{H}_2\text{SO}_4$  and  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$ , and rate constants ( $\text{cm}^3 \cdot \text{molecules}^{-1} \cdot \text{s}^{-1}$ ) of the  $\text{HO}_2 + \text{SO}_3$  reaction with  $\text{H}_2\text{O}$ ,  $(\text{H}_2\text{O})_2$ ,  $\text{H}_2\text{SO}_4$  and  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  at different altitudes in troposphere

Altitude	$T(\text{K})$	$P(\text{atm})$	$k_{\text{WM1}}$	$K_{eq}(\text{HO}_2 \cdots \text{H}_2\text{O})$	$[\text{H}_2\text{O}]$
5 km	259.3	0.535	$1.22 \times 10^{-11}$	$3.26 \times 10^{-20}$	$2.41 \times 10^{16}$
10 km	229.7	0.266	$2.85 \times 10^{-11}$	$2.83 \times 10^{-19}$	$4.92 \times 10^{15}$
15 km	212.6	0.120	$2.26 \times 10^{-11}$	$1.18 \times 10^{-18}$	$1.96 \times 10^{13}$
Altitude	$T(\text{K})$	$P(\text{atm})$	$k_{\text{WD1}}$	$K_{eq}(\text{HO}_2 \cdots (\text{H}_2\text{O})_2)$	$[(\text{H}_2\text{O})_2]$
5 km	259.3	0.535	$6.64 \times 10^{-12}$	$2.56 \times 10^{-17}$	$2.70 \times 10^{12}$
10 km	229.7	0.266	$4.20 \times 10^{-11}$	$7.39 \times 10^{-16}$	$2.30 \times 10^{11}$
15 km	212.6	0.120	$6.02 \times 10^{-11}$	$8.06 \times 10^{-15}$	$6.30 \times 10^6$
Altitude	$T(\text{K})$	$P(\text{atm})$	$k_{c\text{-SA}}$	$K_{eq}(c\text{-HO}_2 \cdots \text{H}_2\text{SO}_4)$	$[\text{H}_2\text{SO}_4]$
5 km	259.3	0.535	$2.68 \times 10^{-11}$	$4.81 \times 10^{-17}$	$6.00 \times 10^7$
10 km	229.7	0.266	$2.63 \times 10^{-11}$	$9.49 \times 10^{-16}$	$8.30 \times 10^6$
15 km	212.6	0.120	$1.90 \times 10^{-11}$	$8.03 \times 10^{-15}$	$2.40 \times 10^5$
Altitude	$T(\text{K})$	$P(\text{atm})$	$k_{c\text{-SW}}$	$K_{eq}(c\text{-HO}_2 \cdots \text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O})$	$[\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}]^a$
5 km	259.3	0.535	$3.45 \times 10^{-11}$	$9.79 \times 10^{-17}$	$1.02 \times 10^6$
10 km	229.7	0.266	$3.54 \times 10^{-11}$	$1.88 \times 10^{-15}$	$2.34 \times 10^5$
15 km	212.6	0.120	$2.42 \times 10^{-11}$	$1.56 \times 10^{-14}$	$1.21 \times 10^2$

<sup>a</sup> The concentrations of  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  at 5, 10 and 15 km altitudes were respectively calculated to be  $1.02 \times 10^5$ ,  $2.34 \times 10^5$  and  $1.21 \times 10^2$  molecules $\cdot\text{cm}^{-3}$  by using the above concentration of  $\text{H}_2\text{SO}_4$  and  $\text{H}_2\text{O}$ .

The average concentration<sup>2,17</sup> of  $\text{H}_2\text{SO}_4$  at 5, 10 and 15 km altitudes were known to be  $6.00 \times 10^7$ ,  $8.30 \times 10^6$  and  $2.40 \times 10^5$  molecules $\cdot\text{cm}^{-3}$ , respectively. Meanwhile, the concentration for  $\text{H}_2\text{O}$  was respectively found to be  $2.41 \times 10^{16}$ ,  $4.92 \times 10^{15}$  and  $1.96 \times 10^{13}$  molecules $\cdot\text{cm}^{-3}$ , whereas the concentration of  $(\text{H}_2\text{O})_2$  was respectively found to be  $2.70 \times 10^{12}$ ,  $2.30 \times 10^{11}$  and  $6.30 \times 10^6$  molecules $\cdot\text{cm}^{-3}$ , in the same order considering temperatures (259 K, 230 K and 213 K, respectively) and pressures (0.533, 0.266 and 0.120 atm, respectively) at those altitudes (Table S9). Using the above concentrations of  $\text{H}_2\text{SO}_4$  and  $\text{H}_2\text{O}$  along with the equilibrium constants for the  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  complex formation, the concentrations of  $\text{H}_2\text{SO}_4 \cdots \text{H}_2\text{O}$  complex were calculated to be  $1.2 \times 10^6$ ,  $2.34 \times 10^5$  and  $1.21 \times 10^2$  molecules $\cdot\text{cm}^{-3}$  at 5, 10 and 15 km altitudes, respectively.

**Table S10** Coordinates stationary points for the HO<sub>2</sub> + SO<sub>3</sub> reaction without and with X (X = H<sub>2</sub>O, (H<sub>2</sub>O)<sub>2</sub>, H<sub>2</sub>SO<sub>4</sub>, H<sub>2</sub>SO<sub>4</sub>···H<sub>2</sub>O and (H<sub>2</sub>SO<sub>4</sub>)<sub>2</sub>) at the M06-2X/6-311+G(2df,2pd) level of theory

<b>HO<sub>2</sub></b>			<b>SO<sub>3</sub></b>		
O	0.05495900	0.70692200	0.00000000	S	0.00000000
O	0.05495900	-0.59859000	0.00000000	O	0.00000000
H	-0.87934600	-0.86666200	0.00000000	O	0.00000000
<b>IM</b>			<b>TS</b>		
S	-0.65103500	0.09510600	-0.00000300	S	-0.56835000
O	-1.12311500	-0.41905700	1.23336900	O	-1.13555000
O	-1.12315800	-0.41921800	-1.23329100	O	-1.13538100
O	0.00168700	1.38229700	-0.00009700	O	0.16647700
O	2.13179700	0.02563700	0.00000200	O	2.01351200
H	1.62474200	0.89379400	-0.00004500	H	1.31450400
O	1.21176700	-0.87159600	0.00003000	O	1.06333000
<b>HOSO<sub>4</sub></b>			<b>H<sub>2</sub>O···HO<sub>2</sub></b>		
S	0.45817600	-0.03289000	0.08694800	O	1.06875500
O	0.30730800	1.14735200	-0.92649700	O	0.97910600
H	-0.22081500	1.85697100	-0.53058500	H	0.00981000
O	0.42856000	0.45974200	1.41365000	O	-1.61563500
O	1.40805100	-0.94165100	-0.41900500	H	-2.29743800
O	-2.01578900	-0.01185900	0.00414500	H	-1.17018200
O	-1.01688000	-0.81992500	-0.17986600	O	0.83118700
<b>IM_WM1</b>			<b>TS_WM1</b>		
S	0.84128700	-0.27789400	0.00003400	S	0.78614400
O	0.27117000	-0.76843600	-1.21913900	O	2.14203000
O	0.27136100	-0.76822600	1.21935000	O	0.01771000
O	2.15628900	0.24655900	-0.00016300	O	-1.26219800
H	-1.85551700	-1.27871600	-0.76258100	O	0.26120700
O	-2.27583700	-0.85682300	-0.00020000	O	0.13418400
H	-1.85793200	-1.27845000	0.76360600	H	-1.43929500
H	-1.71652500	0.45822900	-0.00001400	O	-2.19846000
O	-1.35554200	1.46470300	-0.00000800	H	-1.80870600
O	-0.07126800	1.50037700	-0.00003700	H	-2.08608300
<b>IMF_WM1</b>			<b>HO<sub>2</sub>···(H<sub>2</sub>O)<sub>2</sub></b>		
S	0.70762400	-0.29202900	0.07272100	H	0.96147100
O	2.06630600	-0.51595600	-0.23279600	O	0.69884900
O	0.56536600	1.40799600	-0.10103400	H	1.28314500
O	-0.66345900	1.79447300	0.00416100	O	1.62710600
O	0.11893800	-0.59163700	1.33280000	H	0.67954700
O	-0.19801700	-0.75394700	-1.07129400	H	2.05172900
H	-1.17567100	-0.74675600	-0.75352700	O	-1.22190200
O	-2.52983000	-0.56791900	-0.09738200	O	-1.62729500
H	-2.46339300	0.34331600	0.21494700	H	-0.78995100
H	-2.55735600	-1.10817800	0.69939800	O	0.84556600
<b>IM_WD1</b>			<b>TS_WD1</b>		
H	-3.00639900	1.43058400	-0.04638800	H	-2.95846900
O	-2.26708100	0.99072600	0.38472500	O	-2.25225900
H	-2.36411200	0.01607300	0.20550100	H	-2.30565000
O	-2.39950600	-1.56507300	-0.30322400	O	-2.29574600
H	-1.48892100	-1.64268600	-0.63691900	H	-1.38094900
H	-2.49279900	-2.23560800	0.37971400	H	-2.35456400
O	-0.17953800	2.15482400	-0.27571300	O	-0.21673600
H	-0.99995600	1.53911900	0.04937500	H	-1.15589000
O	0.92813000	1.49505500	-0.46284500	O	0.91284100
S	1.04201500	-0.49497600	0.11159500	S	1.02594300
O	0.30852500	-1.07493500	-0.99527800	O	0.32238600

O 0.34936300 -0.38021100 1.36590900	O 0.29290600 -0.35633000 1.34324800	
O 2.47010000 -0.51887000 0.06932700	O 2.45416200 -0.49614800 0.11183500	
<b>IMF_WD1</b>		
H -2.97400100 1.57263500 0.60601700	<i>c</i> -HO <sub>2</sub> ···H <sub>2</sub> SO <sub>4</sub>	
O -2.72452300 0.69442700 0.90787600	S 0.86352900 -0.05995800 -0.11832700	
H -2.46852500 -0.50261200 -0.25498400	O -0.08301400 -1.13466900 0.09686400	
O -2.10214700 -1.20102900 -0.85703600	O 0.09131500 1.27394300 0.03787000	
H -0.67323700 -1.20733200 -0.74367900	O 1.68049500 -0.04915700 -1.26888200	
H -2.53432000 -2.03093000 -0.63479100	O 1.84003100 -0.02503700 1.11109800	
O 0.08313000 1.65186700 -1.14737700	H -0.90156600 1.09729300 0.04687500	
H -1.81496600 0.76998800 1.23712400	H 1.35788200 -0.17442100 1.93504400	
O 1.22524100 1.16881200 -0.73762100	O -2.64478700 -0.60725900 -0.02748700	
S 1.00929700 -0.23944800 0.29475300	H -1.73331000 -1.01138800 -0.02578800	
O 0.38371900 -1.23141000 -0.69072600	O -2.45147400 0.67315900 0.04267400	
O 0.07244300 0.16593500 1.30966300		
O 2.35167300 -0.59492400 0.59950400		
<b>c-IM_SA</b>		
S 1.80737200 -0.51138300 0.00060700	<b><i>c</i>-TS_SAI</b>	
O 0.99691000 -0.61240900 1.18438400	S -1.80491600 -0.48149200 0.00180900	
O 3.16063400 -0.90880800 0.04465200	O -3.15560300 -0.88749100 0.04342100	
O 1.08679400 -0.58665900 -1.24480000	O -0.98857200 -0.60726400 1.18315100	
O 1.06947500 2.09552600 -0.00707200	O -1.07684200 -0.58621700 -1.24268100	
H 0.13170600 1.54254000 -0.05261600	O -1.02126600 2.05951200 -0.00359000	
O 2.11447300 1.35780000 0.03186000	H -0.00582500 1.49025000 -0.05736800	
S -2.02253800 0.00463000 -0.01800300	O -2.08243400 1.34644400 0.02763000	
O -1.71700800 -0.67505200 1.34241800	S 2.00664100 -0.01424500 -0.01906100	
O -3.41437500 0.17672500 -0.12452900	O 1.48615700 -1.01229000 -1.06783800	
O -1.17481000 1.18941100 -0.12947000	O 3.39978800 0.13097400 -0.13210900	
O -1.54321900 -1.00913500 -1.08399400	O 1.20661800 1.21580600 -0.14758000	
H -0.74691900 -0.74053500 1.47989900	O 1.67872400 -0.65053600 1.35092900	
H -0.57311500 -0.91314100 -1.25651700	H 0.50364700 -0.90391000 -1.22553100	
<b><i>c</i>-IMF_SA1</b>		
S -1.88461100 -0.39379400 -0.06357400	<b><i>t</i>-HO<sub>2</sub>···H<sub>2</sub>SO<sub>4</sub></b>	
O -3.17887800 -0.93045200 -0.18791400	S -0.87225200 -0.07063300 -0.11654600	
O -1.29789100 -0.62414400 1.31756300	O 0.06468000 -1.14580700 -0.30637300	
O -0.87620200 -0.54185000 -1.06998400	O -1.23478000 -0.13395700 1.41776000	
O -1.09358400 1.98081600 -0.00125600	O -2.06980600 -0.00092100 -0.87004800	
H 0.66920700 1.41080400 -0.49069400	O -0.11377400 1.26925900 -0.25306100	
O -2.18323500 1.29155000 -0.00462100	H -2.06234800 0.33982400 1.57606600	
S 2.07510800 -0.06567200 0.09050200	H 0.87071300 1.11957400 -0.09540900	
O 1.83296100 -1.16851900 -0.98233500	O 2.61864700 -0.59087800 -0.01361900	
O 3.45909700 -0.00258400 0.33451900	H 1.71770800 -0.99478200 -0.14704200	
O 1.62469800 1.24858500 -0.61594500	O 2.41377800 0.68549400 0.09173100	
O 1.17164800 -0.29524300 1.20439000		
H 0.88448600 -1.22341600 -1.20433600		
H -0.27055300 -0.50119800 1.30884100		

<b><i>t</i>-IM_SA1</b>				<b><i>t</i>-TS_SA1</b>			
S	-1.85438500	-0.55024600	0.03784300	S	1.84564300	-0.47141800	-0.04303900
O	-1.12156200	-0.68421500	-1.20222500	O	1.12965200	-0.64618400	1.22547300
O	-3.21691500	-0.92518800	0.05174600	O	3.19822200	-0.87852800	-0.06742300
O	-1.06537600	-0.53904800	1.22279800	O	0.99905500	-0.56051500	-1.18810100
O	-1.13762200	2.12011300	0.01354900	O	1.02720300	2.02289500	-0.02163500
H	-0.26014700	1.56180500	0.06127300	H	-0.06080600	1.42628100	-0.07994100
O	-2.18038200	1.38108500	-0.08111600	O	2.10554100	1.33881800	0.04318900
S	2.04783200	0.03119900	-0.05891000	S	-1.99982700	-0.01242400	0.07020600
O	1.95670900	-0.60690900	1.37262800	O	-1.93019100	-0.66786200	-1.34821700
O	1.44454600	-1.03371700	-0.99137500	O	-1.28249600	-0.95283500	1.00046100
O	1.15964300	1.16786000	-0.00621100	O	-1.21697700	1.22621300	-0.09002900
O	3.40744400	0.22292400	-0.40198400	O	-3.34870300	0.16582500	0.45137600
H	2.74227200	-1.14635600	1.53841500	H	-2.70097100	-1.23671300	-1.48553700
H	0.45082400	-0.93393200	-1.08508100	H	-0.22173900	-0.83069500	1.09006500
<b><i>t</i>-IMF_SA1</b>				<b><i>c</i>-HO<sub>2</sub>…H<sub>2</sub>SO<sub>4</sub>…H<sub>2</sub>O</b>			
S	-1.88641100	-0.41523400	0.07964800	O	-2.48491800	-1.43855800	-0.01619600
O	-1.22053400	-0.65080700	-1.26518200	H	-1.51436400	-1.31289800	-0.18059200
O	-3.20690300	-0.90321300	0.09858300	O	-2.98980400	-0.24352000	0.01048900
O	-0.95669700	-0.55531800	1.14865400	S	1.15682400	-0.18805500	0.09533300
O	-1.09721600	1.98877500	0.01926800	O	2.32702200	-0.22800700	-0.95662900
H	0.37734400	1.30876700	0.20987600	O	1.00524700	1.31434900	0.37022500
O	-2.17290500	1.29315300	-0.03599800	O	-0.04573500	-0.63535800	-0.57850900
S	2.04605200	-0.05279500	-0.10265900	O	1.62833100	-0.88728100	1.23023600
O	1.95969100	-0.77547200	1.29257000	H	2.03415100	0.14344700	-1.79925300
O	1.23931200	-0.80428400	-1.05158800	H	0.02834100	1.62464000	0.19878800
O	1.37441300	1.27835500	0.23832500	O	-1.35883700	1.96917300	-0.07801100
O	3.39979900	0.17255000	-0.44778100	H	-1.91445300	1.16090500	-0.11227400
H	2.70291100	-1.44014800	1.36722900	H	-1.79331300	2.58640700	0.51517400
<b><i>c</i>-IM_SW1</b>				<b><i>c</i>-TS_SW1</b>			
S	2.09585100	-0.40893100	-0.38124200	S	-2.08169800	-0.33004800	0.40833400
O	0.71201500	-0.76900300	-0.53593700	O	-0.70412500	-0.68126800	0.64331500
O	3.05265400	-1.42644300	-0.15619500	O	-3.05976500	-1.35278300	0.39542400
O	2.49922500	0.81204500	-1.01260400	O	-2.45420400	0.99177600	0.82570600
O	0.85866200	0.46263000	1.94015000	O	-0.84104000	0.13475300	-1.97468400
H	-0.01098500	0.21288200	1.34593600	H	0.11639600	0.00693200	-1.34644600
O	2.00446200	0.26195000	1.41132500	O	-1.99005700	-0.01145700	-1.43660600
S	-2.26260300	-0.19860600	0.02443900	S	2.23537300	-0.20442500	0.00954700
O	-1.89386700	0.79325900	-1.09178500	O	1.86634900	0.90024900	0.99993300
O	-1.88437500	-1.58997100	-0.56672700	O	1.83559300	-1.52287400	0.72712300
O	-1.39356300	0.06872400	1.16615100	O	1.38423500	-0.04795900	-1.17882000
O	-3.65428600	-0.20833800	0.25014000	O	3.62374600	-0.25331700	-0.22447700
H	-1.05843600	1.33133200	-0.88180300	H	1.04299300	1.45212500	0.72108700
H	-0.92003100	-1.64298600	-0.69844300	H	0.87154600	-1.53673100	0.88610000
O	0.14917900	2.18363100	-0.49076400	O	-0.09879600	2.26298100	0.25241900
H	1.00609800	1.97302300	-0.89445400	H	-0.00575000	3.21741800	0.20924300
H	0.05055900	3.13846200	-0.47241400	H	-0.97946000	2.05099900	0.60927200

<b>c-IMF_SW1</b>	<b>t-HO<sub>2</sub>…H<sub>2</sub>SO<sub>4</sub>…H<sub>2</sub>O</b>
S 2.05083200 -0.18668600 -0.42419100	O -2.35841800 -1.43097900 0.10205900
O 0.67236200 -0.47370300 -0.74694400	H -1.42070200 -1.28014700 0.39257400
O 3.09817900 -0.81484900 -1.13456100	O -2.84391400 -0.25179600 -0.13719600
O 2.24361200 1.24915200 -0.14074200	S 1.17701000 -0.16074200 0.11443500
O 1.17608200 -0.69641800 1.88152100	O 0.86833400 -0.60983200 -1.37604300
H -0.58298100 -0.58096600 1.09779900	O 1.12726400 1.36837300 0.05140800
O 2.22598000 -0.87041500 1.15591600	O 0.03790500 -0.63826700 0.85430000
S -2.32052200 -0.13574100 -0.08388600	O 2.48970200 -0.57396400 0.45523000
O -1.81198000 1.18331500 -0.42038100	H 1.68790400 -0.60968200 -1.88807400
O -1.90771600 -1.11275400 -1.22205500	H 0.14312500 1.69230400 0.04752900
O -1.55894000 -0.64956300 1.17154800	O -1.29126700 2.00981700 0.07033000
O -3.70135100 -0.29066000 0.14621400	H -1.64543400 2.58965200 -0.60745000
H -0.62024900 1.90420800 0.03854200	H -1.83390300 1.19291700 0.06374800
H -0.95253900 -1.02407100 -1.40886600	
O 0.20511200 2.43135900 0.34859200	
H 1.15777500 1.89778400 0.11463800	
H 0.18231500 3.31817100 -0.02574400	
<b>t-IM_SW1</b>	<b>t-TS_SW1</b>
S -2.08435400 0.23073000 0.29679100	S -2.05785600 0.17667000 0.27278900
O -0.98828400 0.05890700 1.19341700	O -0.95794800 0.09134000 1.18077700
O -3.42023700 0.12605500 0.75280000	O -3.39371500 0.07734300 0.73048900
O -1.82010600 0.99937000 -0.89277100	O -1.80457500 0.97200400 -0.91389000
O -0.90616100 -1.93301700 -0.99456000	O -0.82554000 -1.89476200 -0.94663800
H -0.14897100 -1.21224300 -0.86058000	H 0.01952700 -1.11374500 -0.85053100
O -2.04202900 -1.54873000 -0.54198300	O -1.97241200 -1.53530900 -0.50792400
S 1.98268300 -0.27246400 0.17196700	S 1.97355200 -0.22393900 0.18632900
O 3.37429500 -0.28960900 -0.57323400	O 3.41038600 -0.24056900 -0.46207600
O 1.90144800 1.12578500 0.75230000	O 1.89068000 1.18119700 0.66050200
O 1.02951300 -0.37936900 -0.92390200	O 1.04042100 -0.38252000 -0.95638400
O 1.99403400 -1.26205700 1.18780000	O 1.90238900 -1.23136400 1.18227400
H 4.06210100 -0.57821000 0.04146700	H 3.76887500 -1.13704400 -0.41905400
H 1.26802900 1.76319600 0.19077700	H 1.09815900 1.82732100 0.10959900
O 0.39027800 2.57071700 -0.55019100	O 0.25952500 2.50739100 -0.48813400
H 0.74707100 2.90717500 -1.37629900	H 0.60291000 2.87821700 -1.30656900
H -0.40352200 2.04341000 -0.77289600	H -0.53428800 1.94355000 -0.71131200
<b>t-IMF_SW1</b>	<b>HO<sub>2</sub>…(H<sub>2</sub>SO<sub>4</sub>)<sub>2</sub></b>
S 2.18473000 -0.32088600 -0.29349800	O 0.03126700 2.61618200 0.54548600
O 1.03199000 -0.34898700 -1.15516200	H 0.74230500 2.04042100 0.91997500
O 3.32788100 -1.09826900 -0.57304200	O -0.20630600 2.13819900 -0.63613900
O 2.51084600 1.08901700 0.10746300	S 2.08790100 -0.38737900 0.07232200
O 0.57445400 -0.32351200 1.58668200	O 1.44562500 -1.74738200 -0.28014000
H -0.50831100 -0.87535600 -0.90614800	O 1.97744100 0.44678800 -1.24186400
O 1.62283000 -0.96925800 1.17721700	O 1.23205100 0.28370400 1.04983400
S -2.34696500 -0.08537000 -0.17600900	O 3.44688700 -0.59239300 0.37758100
O -2.29015000 -0.41414500 1.36415500	H 0.50562400 -1.60691300 -0.56708200
O -1.70270300 1.19039700 -0.29885000	H 1.12100100 0.92171000 -1.26081300
O -1.45012700 -1.17403800 -0.81305900	S -2.01508300 -0.53162200 -0.02230600
O -3.67173300 -0.28036200 -0.64028100	O -2.71131100 0.79521700 -0.46174700
H -2.92652200 -1.11133100 1.57295300	O -3.03273900 -1.49391400 0.13430900
H -0.26325500 1.99521700 0.06823700	O -0.90374900 -0.77080800 -0.92290100
O 0.56304000 2.52344100 0.14626700	O -1.40963700 -0.18371000 1.37059300
H 1.62543200 1.75193100 0.11662700	H -2.05920900 1.48162000 -0.68731200
H 0.53779000 3.18536300 -0.55065600	H -0.43103800 -0.06788500 1.31488400

<b>IM_SD1</b>			<b>TS_SD1</b>		
S -2.27613700	-1.07355100	-0.48583600	S -1.73923000	-1.56256100	-0.45273800
O -2.74031700	0.28519300	-0.44802300	O -2.55426300	-0.44528500	-0.85977800
O -3.19573000	-2.10544800	-0.76836300	O -2.19311500	-2.86970100	-0.73218300
O -0.88342500	-1.25049400	-0.77529500	O -0.32683200	-1.29245300	-0.39438500
O -1.38261400	-0.59438500	2.06476500	O -1.70358600	-0.49489700	1.99934500
H -0.84024700	0.07754600	1.43922900	H -1.06715900	0.27844900	1.39231600
O -2.19003000	-1.35794600	1.42691600	O -2.11942000	-1.52975600	1.37164400
S -0.01274300	2.13703500	-0.01204000	S -0.63630000	2.15865600	-0.07727000
O 0.17119700	1.55301500	-1.41642400	O -0.04028600	1.58964400	-1.35725100
O -1.48140100	2.59206300	-0.04465000	O -2.14263300	2.05861000	-0.33340000
O 0.11278200	1.00544200	0.93679700	O -0.30081300	1.18786200	1.01583200
O 0.81676400	3.24204000	0.26872700	O -0.27224700	3.48826300	0.20470000
H 0.89610700	0.84320900	-1.40890000	H 0.84806700	1.09744700	-1.20603500
H -2.06900700	1.83251300	-0.27664900	H -2.38851800	1.13126000	-0.62269600
S 2.59225900	-0.94690300	-0.13247300	S 2.78415800	-0.45562400	-0.02703900
O 1.49742300	-1.96360100	0.32205900	O 2.31742500	-1.89988300	-0.35249900
O 3.82055900	-1.61302500	-0.30816300	O 4.18723300	-0.47884000	0.08437900
O 2.03354700	-0.17715800	-1.22445100	O 2.16050900	0.46251100	-0.96050900
O 2.74355000	-0.02658600	1.11775500	O 2.15911400	-0.17541200	1.37895900
H 0.65823100	-1.80750200	-0.15666400	H 1.34595900	-1.93099300	-0.46797700
H 1.92241000	0.47606000	1.27536200	H 1.35491500	0.37101500	1.29829400
<b>IMF_SD1</b>					
S -2.29571100	-1.13970700	-0.37430100			
O -2.96228700	0.17936800	-0.69434800			
O -3.03687100	-2.23598300	-0.84998600			
O -0.87278900	-1.03817300	-0.51593900			
O -1.73153800	-0.44747600	1.97377900			
H -0.25226000	0.47763800	1.24093700			
O -2.53607400	-1.21948500	1.32636200			
S -0.11543800	2.15880400	-0.07092700			
O 0.26691200	1.52035700	-1.40896800			
O -1.56344500	2.11241200	0.01307500			
O 0.44037800	1.12933200	1.00092200			
O 0.53566900	3.38891800	0.15534200			
H 1.04452600	0.87425100	-1.34401100			
H -2.37082500	1.00458300	-0.45348700			
S 2.72061900	-0.94344200	-0.11236800			
O 1.55595600	-1.78489600	0.50412600			
O 3.83993900	-1.76143700	-0.35921200			
O 2.16075100	-0.15897200	-1.19198000			
O 3.09661700	0.00148800	1.07069700			
H 0.72080800	-1.65420100	0.01280900			
H 2.36046900	0.60363200	1.27432400			

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