

## Supporting Information

# Silica-decorated Ni–Zn alloy as a highly active and selective catalyst for acetylene semihydrogenation

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## Experimental details

### Catalyst Preparation

Ni and Ni–Zn alloy nanoparticles supported on silica (Ni/SiO<sub>2</sub> and Ni–Zn/SiO<sub>2</sub>, Ni loading: 2 wt%) were prepared by pore-filling impregnation method. Aqueous solution of Ni (NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O (Wako, 99%) alone or Ni (NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O and Zn (NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (Wako, 99%) with molar ratio 1:1 were added to dried silica gel (CARiACT G-6, Fuji Silysia,  $S_{\text{BET}} = 470 \text{ m}^2\text{g}^{-1}$ ) so that the solutions filled the silica pores. The mixtures were sealed overnight at room temperature and dried over liquid nitrogen under vacuum overnight followed by drying at 90°C. The reduction under flowing H<sub>2</sub> at 600 °C for 1 h was then performed. Silica decorated Ni (Si–Ni/SiO<sub>2</sub>) and Ni–Zn nanoparticles supported on silica (Si–Ni–Zn/SiO<sub>2</sub>) were prepared by adding ethanol solution of C<sub>18</sub>H<sub>16</sub>OSi (Mr = 276.40 g mol<sup>-1</sup>, Tokyo Chemical Industry Co., Ltd) and Ni (NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O (Wako, 99%) with Zn (NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (Wako, 99%) in a similar fashion to that of Ni/SiO<sub>2</sub> or Ni–Zn/SiO<sub>2</sub> except drying over the hot plate. The specific surface area of the prepared catalysts were as follows: Ni–Zn/SiO<sub>2</sub>,  $S_{\text{BET}} = 454 \text{ m}^2\text{g}^{-1}$ ; Si–Ni–Zn/SiO<sub>2</sub>,  $S_{\text{BET}} = 451 \text{ m}^2\text{g}^{-1}$ , indicating that the silica-decoration did not decrease the surface area.

### Reaction condition

The catalytic activities of the prepared catalysts were tested in hydrogenation of acetylene. The mixture of Ni-based catalysts (15 mg) and quartz sand (Miyazaki Chemical Co., 250 ~ 420 μm, 2 g) was filled into a quartz glass tube (internal diameter, 10 mm) and put in a fixed bed continuous reactor. Prior to the activity test, the catalyst was reduced under flowing H<sub>2</sub> (10 mL min<sup>-1</sup>) at 500°C for 0.5 h and the temperature was cooled down to the reaction temperature. The reaction was initiated by flowing the gas mixture: (C<sub>2</sub>H<sub>2</sub>:H<sub>2</sub>:He = 2:20:10 mL min<sup>-1</sup>: GHSV = 128,000 mL h<sup>-1</sup> g<sup>-1</sup>). The gas phase was analyzed by an online thermal conductivity detector (TCD) gas chromatography (Shimadzu GC-8A) equipped downstream connected to the Unipack S packed column. The catalytic performance (C<sub>2</sub>H<sub>2</sub> conversion and C<sub>2</sub>H<sub>4</sub> selectivity) at 15 min on stream was reported. For the stability test, 60 mg of catalyst was used. C<sub>2</sub>H<sub>2</sub> conversion and C<sub>2</sub>H<sub>4</sub> selectivity were calculated using the following equations:

$$\text{C}_2\text{H}_2 \text{ conversion (\%)} = (F_{\text{C}_2\text{H}_2,\text{in}} - F_{\text{C}_2\text{H}_2,\text{out}}) / F_{\text{C}_2\text{H}_2,\text{in}} \times 100$$

$$\text{C}_2\text{H}_4 \text{ selectivity (\%)} = F_{\text{C}_2\text{H}_4,\text{out}} / (F_{\text{C}_2\text{H}_2,\text{in}} - F_{\text{C}_2\text{H}_2,\text{out}}) \times 100$$

### Characterization

The crystal structure of the prepared catalyst was examined by powder X-ray diffraction (XRD) using

a Rigaku MiniFlex II/AP diffractometer with Cu K $\alpha$  radiation.

High-angle annular dark field scanning transmission electron microscopy (HAADF-STEM) was carried out using a JEOL JEM-ARM200 M microscope equipped with an energy dispersive X-ray (EDX) analyzer (EX24221M1G5T). STEM analysis was performed at an accelerating voltage of 200 kV. To prepare the TEM specimen, all samples were sonicated in ethanol and then dispersed on a Mo grid supported by an ultrathin carbon film.

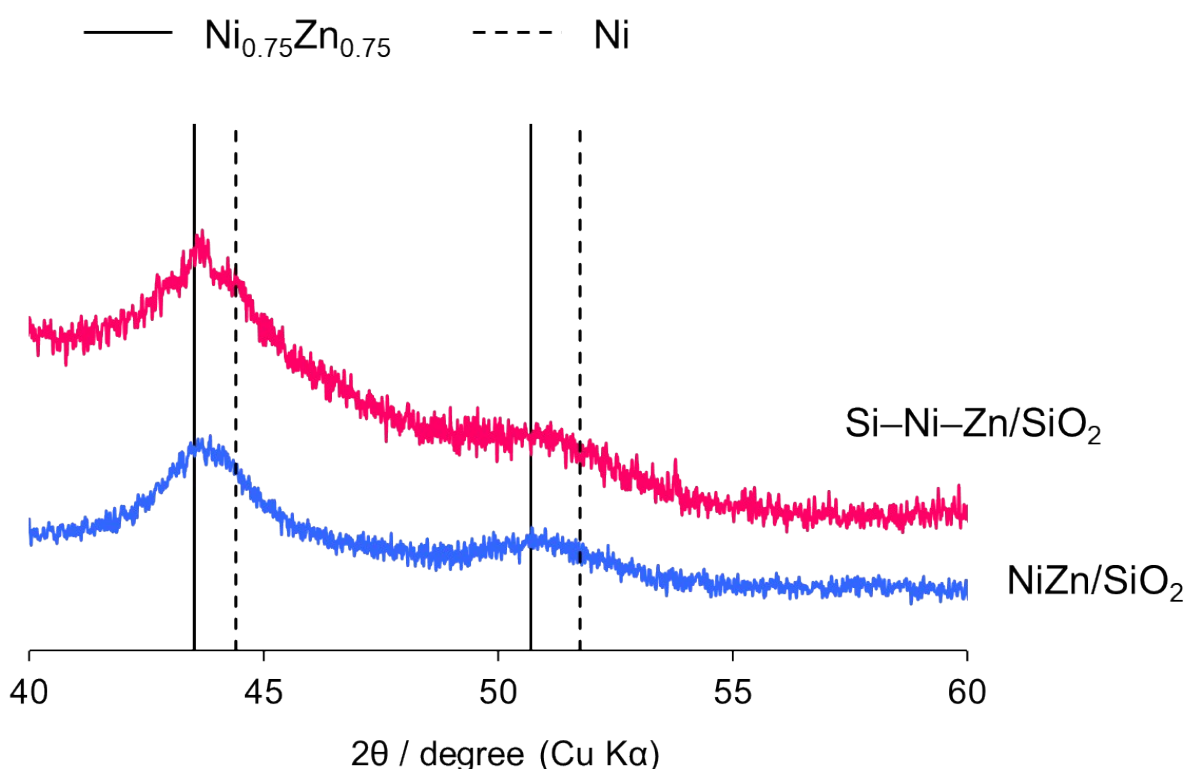
Reduction properties of the as-prepared catalyst were analyzed by temperature programmed reduction method by H<sub>2</sub> (H<sub>2</sub>-TPR) by using a BELCAT- II instrument. Prior to analysis, 30 mg of catalyst was pretreated at 150°C for 1 h under inert He flow to remove absorbed water, then the sample was heated under H<sub>2</sub> flow (5v% H<sub>2</sub> balanced with Ar 30 sccm) in the temperature from 50°C to 900°C at a ramping rate of 2°C/min<sup>-1</sup>.

### **Computational Details**

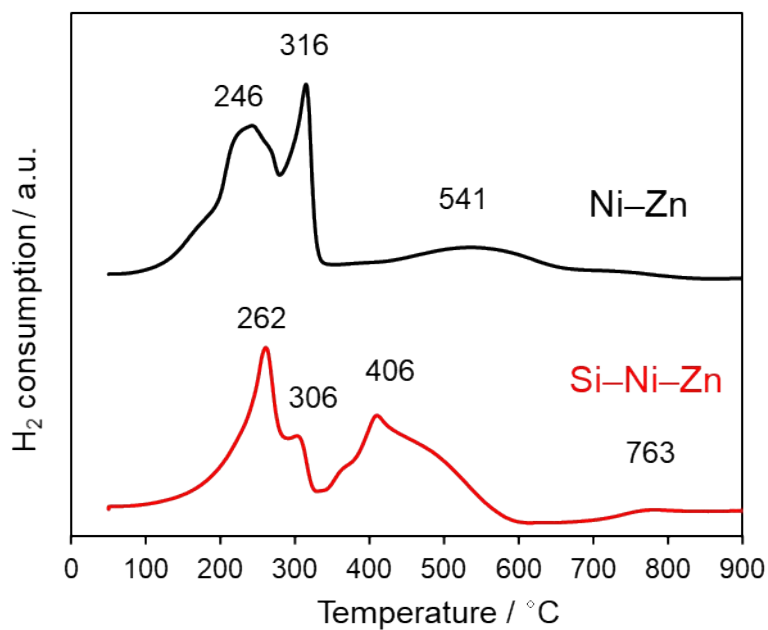
Periodic density functional theory (DFT) calculations, except frequency calculations, were performed using the CASTEP code<sup>1</sup> with Vanderbilt-type ultrasoft pseudopotentials<sup>2</sup> and a revised Perdew–Burke–Ernzerhof exchange-correlation functional (RPBE)<sup>3</sup> based on the generalized gradient approximation (GGA). The plane-wave basis set was truncated at a kinetic energy of 370 eV. A Fermi smearing of 0.1 eV was utilized. The reciprocal space was sampled using a *k*-point mesh with a typical spacing of 0.04 Å<sup>-1</sup> generated by the Monkhorst–Pack scheme.<sup>4</sup> Geometry optimizations were performed in supercell structures using periodic boundary conditions. Surfaces were modeled using 4 atomic layer-thick metallic slabs. An L1<sub>2</sub>-type Ni<sub>3</sub>Zn structure was considered as the model of the Ni<sub>0.75</sub>Zn<sub>0.25</sub> alloy. The surface was modeled using Ni<sub>3</sub>Zn(111) and Ni<sub>3</sub>Zn(211) planes for the terrace and step sites of Ni–Zn, respectively, with a 13 Å vacuum region. Convergence criteria comprised a) a self-consistent field (SCF) tolerance of 1.0×10<sup>-6</sup> eV/atom, b) an energy tolerance of 1.0×10<sup>-5</sup> eV/atom, c) a maximum force tolerance of 0.05 eV Å<sup>-1</sup>, and d) a maximum displacement tolerance of 1.0×10<sup>-3</sup> Å for structure optimization and energy calculation. Frequency calculations of adsorbed CO

molecules were conducted by the DMol<sup>3</sup> code<sup>5</sup> based on the aforementioned optimized structures. These calculations involved the RPBE functional, a double-numeric quality basis set with polarization functions (DNP, comparable to Gaussian 6-311G<sup>\*\*</sup>)<sup>6</sup> with a real-space cutoff of 4.2 Å, DFT semi-core pseudopotential core treatment,<sup>7</sup> and a Fermi smearing of 0.1 eV. The SCF convergence was accelerated using the iterative scheme proposed by Kresse and Furthmüller.<sup>8</sup> The partial Hessian matrix including C and O atoms was computed to evaluate the harmonic frequencies for adsorbed CO. All computed harmonic frequencies were scaled by an empirical factor of 1.056, which corresponds to the ratio of experimental<sup>9</sup> and computed values for gas-phase CO (2143 cm<sup>-1</sup>/2028.7 cm<sup>-1</sup>).

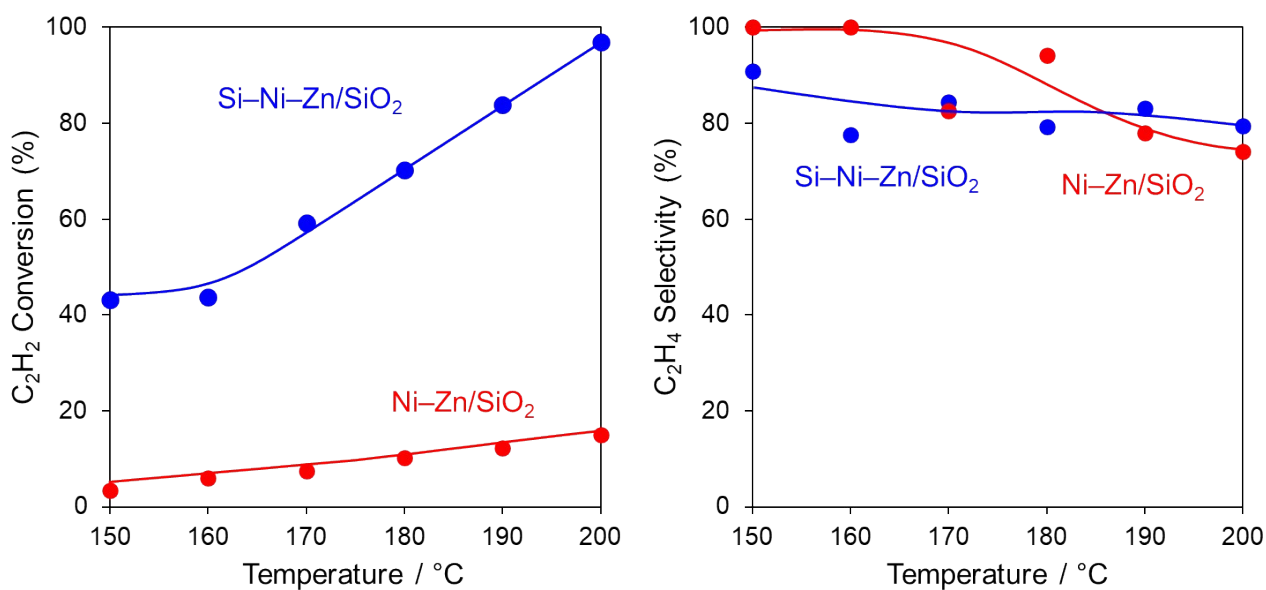
### Supplementary Figures



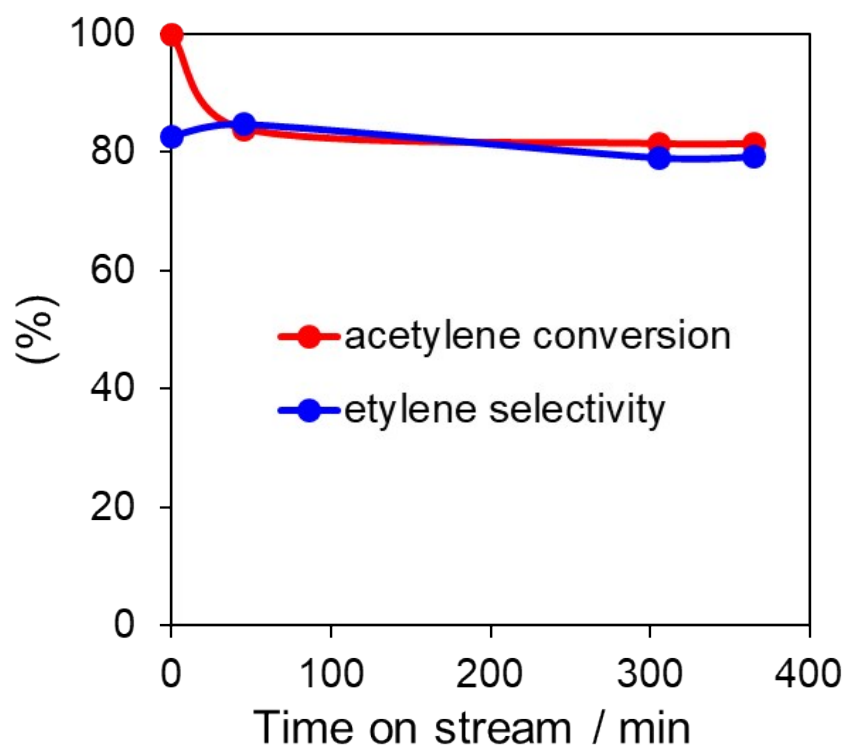
**Fig. S1.** XRD patterns of Ni-Zn/SiO<sub>2</sub> and Si-Ni-Zn/SiO<sub>2</sub>. References are shown as black vertical lines.



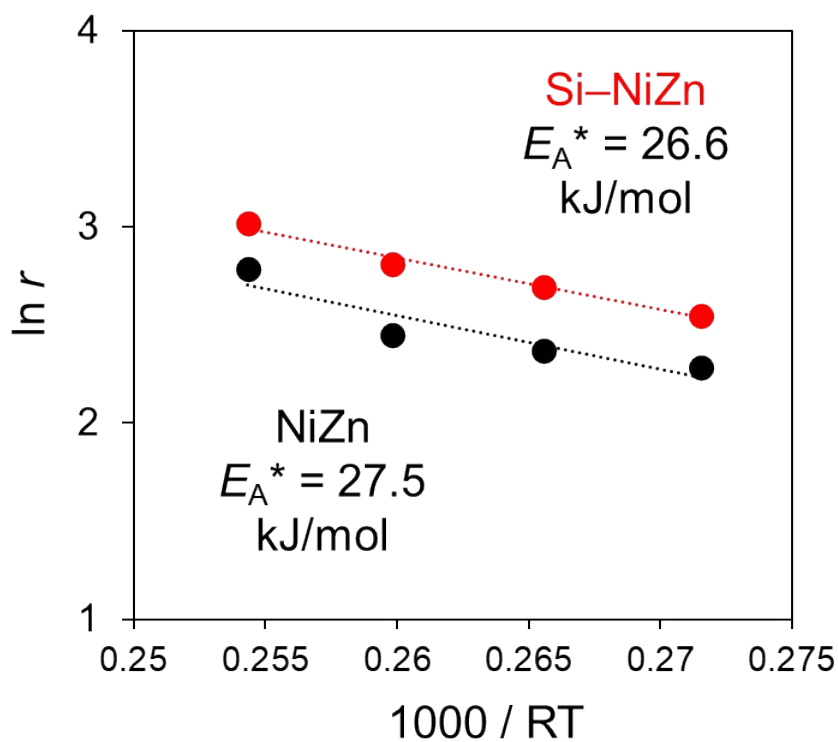
**Fig. S2.** H<sub>2</sub>-TPR profiles of Ni-Zn/SiO<sub>2</sub> and Si-Ni-Zn/SiO<sub>2</sub>.



**Fig. S3.** Temperature-dependences of C<sub>2</sub>H<sub>2</sub> conversion and C<sub>2</sub>H<sub>4</sub> selectivity for Ni-Zn/SiO<sub>2</sub> and Si-Ni-Zn/SiO<sub>2</sub> catalysts.



**Fig. S4.** Stability test for acetylene semihydrogenation using Si-Ni-Zn/SiO<sub>2</sub>.



**Fig. S5.** Arrhenius-type plots obtained in acetylene semihydrogenation on Ni-Zn/SiO<sub>2</sub> and Si-Ni-Zn/SiO<sub>2</sub>.

**Table S1.** Summary of the catalytic performance of Ni-based catalyst in acetylene semihydrogenation.

entry	catalyst	Ni wt%	amount / mg	C <sub>2</sub> H <sub>2</sub> flow / mLmin <sup>-1</sup>	C <sub>2</sub> H <sub>2</sub> :H <sub>2</sub> :C <sub>2</sub> H <sub>4</sub> :He(Ar) / mLmin <sup>-1</sup>	GHSV / mLg <sup>-1</sup> h <sup>-1</sup>	conv. (%)	sel. (%)	temp. / °C	specific rate / mL <sub>C<sub>2</sub>H<sub>2</sub></sub> min <sup>-1</sup> g <sub>Ni</sub> <sup>-1</sup>	ref
1	Si-Ni-Zn/SiO <sub>2</sub>	2	15	2	2:20:0:10	128,000	97	80	200	6,467	this work
2	NiCu <sub>0.125</sub> /MCM-41	1	100	3.3	3.3:10:0:0	8,000	100	63	250	3,333	10
3	AgNi <sub>0.125</sub> /SiO <sub>2</sub>	0.37	30	0.3	0.3:6:6:17.7	60,000	98	25	200	2,649	11
4	Ni <sub>3</sub> Ge/MCM-41	3.2	15.6	3.9	3.9:8.1:0:17	111,360	30	87	250	2340	12
5	Ni-Zn/SiO <sub>2</sub>	2	15	2	2:20:0:10	128,000	15	80	200	1,007	this work
6	NiGa	10	50	1.2	1.2:12:24:82.5	144,000	90	82	190	216	13
7	Ni <sub>3</sub> Ga/MgAl <sub>2</sub> O <sub>4</sub>	2	100	0.33	0.33:6.7:33.3:26.67	40,000	92	77	220	153	14
8	Ni/MCM-41	25	100	3.7	3.7:7.4:0:55.5	40,000	96	87	240	142	15
9	Ni-CeO <sub>2</sub>	1.54	200	0.35	0.35:24.5:1.4:43.75	21,000	100	100	200	114	16
10	Ni <sub>6</sub> In/SiO <sub>2</sub>	8	500	3	3:30:0:267	36,000	100	64	200	75	17
11	Na-Ni/CHA	3.5	200	0.5	0.5:8:0:41.5	15,000	100	97	170	71	18
12	Ni-SAs/N-C	5.67 <sup>a</sup>	400	0.2	0.2:4:20:15.8	6,000	96	91	200	8	19

<sup>a</sup> Although the loading amount of Ni was not reported, it was estimated from the original Ni content<sup>20</sup> and the weight loss by TG.

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