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Electronic Supplementary Information

## Oxidative coupling of methane over sodium zirconate catalyst

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## Simplified kinetic model and parameter fitting

The kinetic model and rate equations are shown in Scheme S1. As it was demonstrated that the addition of CO<sub>2</sub> decreased the CH<sub>4</sub> consumption rate, we assumed that CO<sub>2</sub> competes with hydrocarbon species for active sites, thus the CO<sub>2</sub> adsorption term was included in all steps. In some simplified reaction networks, CO and CO<sub>2</sub> are lumped into one pseudocomponent CO<sub>x</sub>, but for a more accurate description of O<sub>2</sub> consumption, it was necessary to explicitly treat the oxidation of CO to CO<sub>2</sub>, especially in the case of Na<sub>2</sub>ZrO<sub>3</sub> which has a known activity for CO oxidation. The O<sub>2</sub> reaction orders of the primary reactions (r1, r2, and r3) were considered as independent parameters, but to limit the degree of freedom in the model, the rates of secondary reactions (r4, r5, r6, and r7) were assumed to follow the kinetics of dissociatively adsorbed O<sub>2</sub> (i.e. to vary with O<sub>2</sub> to 0.5 order). To allow for fitting to experimental data from different temperatures, each rate constant was assumed to have an Arrhenius-type temperature dependence (k = Aexp(-E<sub>a</sub>/RT), where A is the pre-exponential factor and E<sub>a</sub> is the apparent activation energy). The adsorption equilibrium constant of CO<sub>2</sub> (K<sub>CO2</sub>) was also considered to vary with temperature: K = K<sub>∞</sub>exp(-ΔH/RT), where K<sub>∞</sub> is the equilibrium constant in the high-temperature limit and ΔH is the enthalpy of CO<sub>2</sub> adsorption, assumed to be constant over the experimental temperature range of 700 – 800 °C.

In preliminary model fitting, the adsorption term for CH<sub>4</sub> was also included, but the obtained value was close to zero, indicating that it was negligible. As the experimental selectivity of  $C_2H_2$  was <0.2 % in all runs,  $C_2H_2$  was not included in the kinetic modelling.  $C_3$  and  $C_4$  species were <3 %, and these were bundled with  $C_2H_4$  selectivity for modelling purposes. Additional reaction pathways were also considered (the nonoxidative dehydrogenation of  $C_2H_6$ , the oxidation of  $C_2H_6$  and  $C_2H_4$  to CO, the backwards reaction of CO<sub>2</sub> to CO) but their contributions were negligible under the selected conditions.

Figure S1 demonstrates the fit at 750 °C between the model and the experimental product distributions,  $CH_4$  conversion, and  $C_2$  yield, under various contact times (defined as the weight of the catalyst divided by the total flow rate, with the



Scheme S1. Simplified reaction scheme and rate equations for OCM.

dimensions of  $g_{cat}$  s mL<sup>-1</sup>). These results show that the simplified reaction network, with 19 degrees of freedom (7 rate constants, 7 apparent activation energies, 3 O<sub>2</sub> reaction orders, the adsorption equilibrium constant of CO<sub>2</sub>, and the enthalpy of adsorption of CO<sub>2</sub>), fit well with the experimental dataset across a wide range of conditions. The average error of a product partial pressure was 12.1 % (calculated from averaging the percentage differences between experimental and calculated C<sub>2</sub>H<sub>6</sub>, C<sub>2</sub>H<sub>4</sub>, CO, and CO<sub>2</sub> pressures at each of the 150 datapoints).

The fitted parameters are shown in Table S1. The fitted  $O_2$  reaction orders for the CO and  $CO_2$  forming reactions were higher than 1, which is higher than that of the  $C_2H_6$  forming reaction (r<sub>1</sub>), indicating that the primary  $C_2$  selectivity is strongly dependent on the concentration of  $O_2$ .

**Table S1.** Fitted kinetic parameters of Na<sub>2</sub>ZrO<sub>3</sub>. n is the total reaction order in the reaction steps 1-3. \* denotes parameters that were kept constant.

Step number	O <sub>2</sub> reaction	Pre-exponential factor A	Apparent activation energy $E_{a}$	rate constant k at 750 °C (s <sup>-1</sup> kPa <sup>-n</sup> )
	order	(S <sup>-1</sup> KPa <sup>-11</sup> )	(kJ mol <sup>-1</sup> )	
1	0.31	9.10E+08	185	0.31
2	1.32	2.15E+00	32	0.053
3	1.48	4.30E+00	33	0.092
4	0.5*	1.07E+08	144	4.8
5	0.5*	2.23E+06	110	5.5
6	0.5*	2.40E+05	100	1.8
7	0.5*	2.64E+06	126	1.0
CO <sub>2</sub> adsorption		High-temperature limit adsorption equilibrium constant K∞ (kPa <sup>-1</sup> )	Enthalpy of adsorption ∆H (kJ mol <sup>-1</sup> )	adsorption equilibrium constant K at 750 °C (kPa <sup>-1</sup> )
-	-	5.77E-11	-228	24



**Figure S1.** Experimental (points) and fitted model (dashed lines) product partial pressures, CH<sub>4</sub> conversion, and C<sub>2</sub> yield at various contact times. C<sub>2</sub>H<sub>6</sub>: blue, C<sub>2</sub>H<sub>4</sub>: red, CO: green, CO<sub>2</sub>: brown, CH<sub>4</sub> conversion: black, C<sub>2</sub> yield: purple. Reaction conditions: catalyst 0.5 g, 750 °C, CH<sub>4</sub> 10 kPa, O<sub>2</sub> 1.0 – 5.0 kPa, total pressure 101 kPa (Ar balance), total flow rate 30 – 200 mL min<sup>-1</sup>.

## OCM performance of ZrO<sub>2</sub>



**Figure S2.** The OCM performance of ZrO<sub>2</sub>. Reaction conditions: catalyst 0.2 g, 800 °C, CH<sub>4</sub> 10 kPa, O<sub>2</sub> 1.7 kPa, total pressure 101 kPa (Ar balance), total gas flow 30 - 150 mL min<sup>-1</sup>.