# Modelling of a CH<sub>4</sub>-producing microbial electrosynthesis system for energy recovery and wastewater treatment

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#### Section 1: experimental operation of CH<sub>4</sub>-producing MESs

A glass bottle with 350 mL was used as the bioreactor for a single-chamber MES, and two carbon clothes (12 cm<sup>2</sup>, TMIL Ltd., Ibaraki, Japan) were used as the anode and cathode, respectively. The distance between the anode and cathode was 2 cm, and the electrodes were connected to a power source (Array 3645 A, Array Electronics, Nanjing, China) by titanium wires. To cultivate the MES, the effluent (100 mL) from a CH<sub>4</sub>-producing MES operated for 6 months and medium (150 mL) were added into the reactor, and the output voltage of the power source was set at 0.82 V. The medium mainly contained 15 mmol L<sup>-1</sup> acetate, 50 mmol L<sup>-1</sup> PBS (19 mmol L<sup>-1</sup> KH<sub>2</sub>PO<sub>3</sub>, 31 mmol  $L^{-1}$  Na<sub>2</sub>HPO<sub>3</sub>) and other microelements [1]. Before operation, the reactor was flushed by pure N<sub>2</sub> to remove oxygen. The solution in reactor was exchanged by fresh medium when the current density decreased to 0.5 A m<sup>-2</sup>. The gaseous and liquid products were analyzed per day by a gas chromatography and an ion chromatography, respectively according to our previous studies [1-3]. The pH of solution was detected using a pH-meter (PHS-2F, INESA scientific instrument Co., Ltd, Shanghai, China) by extracting 1 mL of the electrolyte from the reactor per day.

# Section 2: operation and electron transfer of a CH<sub>4</sub>-producing MES

A voltage of  $0.7 \sim 1.0$  V is usually applied to a CH<sub>4</sub>-producing MES. Fig. S1 shows the variation of the current and electrode potential of a MES operated under 0.7 V. As shown in this figure, the cathode potential is kept at ~ -1.15 V vs. Ag/AgCl during the stable operation of the MES, indicating that the cathode potential is always lower than -1.0 V vs. Ag/AgCl during the operation of MESs under typical applied voltages. In this condition, electrons are mainly transferred from cathode surfaces to cathode biofilms through the indirect electron transfer pathway [2].



Fig. S1 Variation of the current and electrode potential of a  $CH_4$ -producing MES operated under 0.7 V

#### Section 3: kinetics of biocathodes

As shown in Fig. S2, when the biocathode operated at the potential higher than -0.8 V vs. Ag/AgCl, nearly no current was generated on it. When it operated at the potential lower than -0.8 V vs. Ag/AgCl, the generated current was mainly contributed to indirect electron transfer, indicating that H<sub>2</sub> was first generated on the biocathode, and then H<sub>2</sub> was further conversed to CH<sub>4</sub> in biofilms or bulk solution [1, 2]. In this case, we used a piecewise function to describe the kinetics current generation with -0.8 V vs. Ag/AgCl as the critical point.

Furthermore, as the conversion of  $H_2$  to  $CH_4$  ( $CO_2 + 4H_2 \rightarrow CH_4 + 2H_2O$ ) was not an electrochemical reaction and methane was the main products observed in our experiments, thus we assumed the conversion of  $H_2$  to  $CH_4$  as a non-limiting step. Therefore, we only considered the electrochemical kinetics of hydrogen generation using the Bulter-Volmer-Monod equation.



Fig. S2 Current generation of the biocathode under different potentials.

#### Section 4: equation construction of pH factor

The original equations used to illustrate the influence of pH on bioanode activities was illustrated as Eq. S1 [4]:

$$r_{ut} = \begin{cases} 0, & pH < pH_{opt} - W \\ \frac{\hat{q}X_f}{2} \left( 1 + \cos\left(\frac{\pi}{W}(pH - pH_{opt})\right) \right), pH_{opt} - W < pH < pH_{opt} (S1) \\ \hat{q}X_f, & pH > pH_{opt} \end{cases}$$

where,  $r_{ut}$  indicated the rate of substrate utilization,  $\hat{q}X_f$  indicated the maximum rate of substrate utilization in the biofilm, W indicated a parameter for pH inhibition, and  $pH_{opt}$  indicated the optimum pH for anode biofilm.

As the microorganism activity was proportional to the substrate utilization rate which was proportional to the current density generated by bioelectrodes, we defined <u>**pH factor**</u> (dimensionless) as the value of  $r_{ut}$  divided by  $\hat{q}X_f$ , thus the pH factor of bioanodes was shown as Eq. S2:

$$\alpha_{pH,a} = \begin{cases} 0, & pH < pH_{opt,a} - W_{a} \\ 1 + \cos\left(\frac{\pi}{W_{a}} \cdot (pH - pH_{opt,a})\right) \\ \hline 2 \\ 1, & pH > pH_{opt,a} \end{cases}$$

To construct the equation of cathode pH factor, we first experimentally tested the variation of biocathode current under different pH [5]. Then, we modified Eq. S2 according to our experimental data and constructed Eq. S3.

$$\alpha_{pH,c} = \begin{cases} 1 + \cos\left(\frac{\pi}{W_{c}} \cdot (pH - pH_{opt,c})\right) \\ \hline \\ \hline \\ 0, & pH < pH_{opt,c} - W_{c} \le pH \le pH_{opt,c} + W_{c} \end{cases} (S3) \end{cases}$$

# Section 5: illustrations of $D_{i}^{eff}$ and $S_{i}$

species *i* 

Species i	Š <sub>i</sub>	D <sup>eff</sup> <sub>i</sub>		Value of $S_i$ in biofilms	
		In biofilm	In diffusion layer	Anode biofilm	Cathode biofilm
$CO_2(aq)$	$\dot{S}_{CO_2(aq)}$	$\epsilon_p^{1.5} D_{CO_2(aq)}$	$D_{CO_2(aq)}$	0	0
<i>HCO</i> <sup>-</sup> <sub>3</sub>	; нсо <sub>3</sub>	$\epsilon_p^{1.5} D_{HCO\overline{3}}$	D <sub>HCO3</sub>	0	0
$CO_{3}^{2-}$	S <sub>co<sup>2</sup>3</sub>	$\epsilon_p^{1.5} D_{CO^2_3}^{-}$	$D_{CO^2_3}$	0	0
0H <sup>-</sup>	S <sub>OH</sub> -	$\epsilon_p^{1.5} D_{OH^{-}}$	D <sub>OH</sub> -	0	$\frac{i_c}{2FL_{B,c}}$
$H^+$	S <sub>H</sub> +	$\epsilon_p^{1.5} D_{H^+}$	$D_{H^+}$	$\frac{7i_a}{8FL_{B,a}}$	0
$H_2PO_4^-$	: <sup>Н</sup> 2 <sup>РО</sup> 4	$\epsilon_p^{1.5} D_{H_2^{PO} \overline{4}}$	$D_{H_2PO_4}$	0	0
$HPO_{4}^{2}$	'S <sub>HP0<sup>2</sup>-4</sub>	$\epsilon_p^{1.5} D_{HPO^2_4^-}$	$D_{HPO^2_4}$	0	0
Ac <sup>-</sup>	S <sub>Ac</sub>	$\epsilon_p^{1.5} D_{Ac}$	D <sub>Ac</sub>	$-rac{i_a}{8FL_{B,a}}$	0

Table S1. Illustrations of the efficient diffusion coefficient and bioelectrochemical source item of

where  $D_i$  and  $\epsilon_p$  indicate the diffusion coefficient of species *i* and the porosity of biofilm, respectively. The efficient diffusion coefficient is calculated according to the Bruggeman mode.

# Section 6: calculation for the resistance of biofilms and solution

The resistance of biofilms is calculated by the following equation:

$$R = \frac{k_{bio}(L_{B,a} + L_{B,c})}{A}$$

where  $k_{bio}$  is the conductivity of the biofilms (the conductivity of the anode biofilm is thought to be equal to that of the cathode biofilm);  $L_{B,a}$  and  $L_{B,c}$  are the thickness of the anode and cathode biofilms, respectively; A is the area of the electrode.

The resistance of biofilms is calculated by the following equation:

$$R = \frac{k_l L_{Bulk}}{A}$$

where  $k_l$  is the conductivity of the solution;  $L_{Bulk}$  is the distance of the electrodes; A is the area of the electrode.

Section 7: variation of pH and acetate concentration during the operation of a



### **CH<sub>4</sub>-producing MES**

Fig. S3 pH value under typical operation conditions. (A): MESs are operated with 15 mmol  $L^{-1}$  initial concentration of acetate and 50 or 100 mmol  $L^{-1}$  PBS; (B): MESs are operated with 25 mmol  $L^{-1}$  initial concentration of acetate and 50 or 100 mmol  $L^{-1}$  PBS. mM indicates mmol  $L^{-1}$ 

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