Supplementary information

Eco-friendly and techno-economic conversion of CO₂ into calcium formate, a valuable resource

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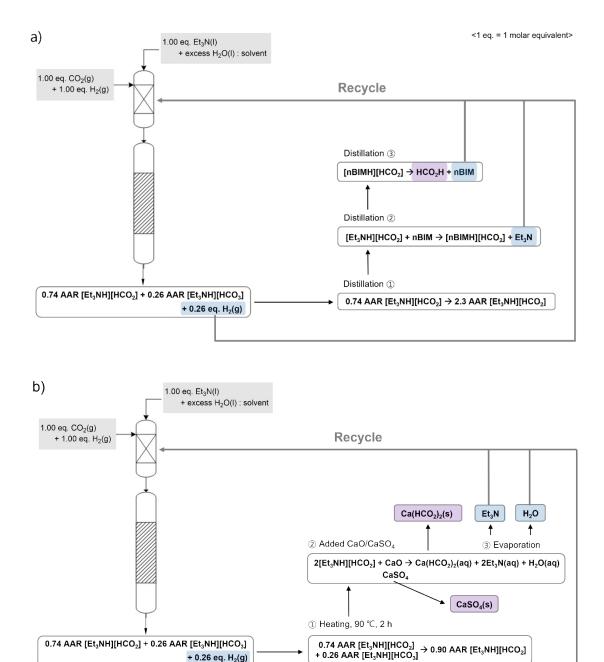
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Conventional HCO₂H production process and proposed Ca(HCO₂)₂ production process 1.

*Flue-gas desulfurization ash (CaO/CaSO₄) consists of 23.4 wt% of CaO

+ 0.26 eq. H₂(g)

Figure S1. Detailed schematics of CO₂ conversion into value-added chemicals: a) conventional HCO₂H production process and b) proposed Ca(HCO₂)₂ production process. (AAR: acid to amine ratio)

 $CO_2(g)$

2. composition analysis of CO₂ hydrogenation adduct

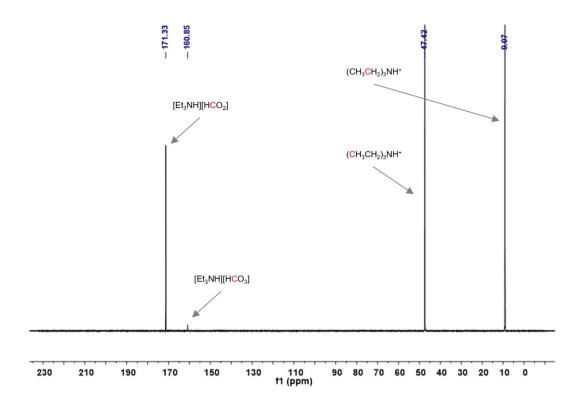


Figure S2. ¹³C NMR analysis of the [Et₃NH][HCO₂] adduct generated by CO₂ hydrogenation.

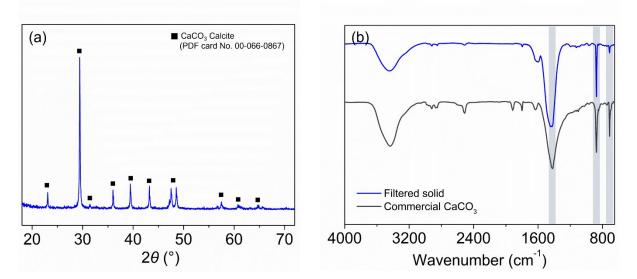


Figure S3. (a) XRD and (b) FT-IR analyses of filtered solid (blue) and commercial CaCO₃ (black) in a stirred solution obtained by adding CaO to the adduct containing bicarbonate.

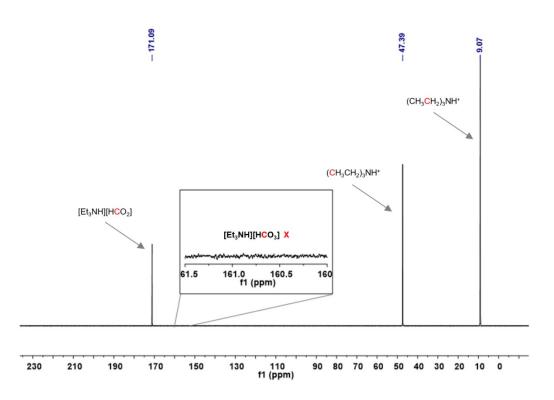


Figure S4. ¹³C NMR analysis of the adduct produced by CO₂ hydrogenation after degassing at 90 °C for 2 h.

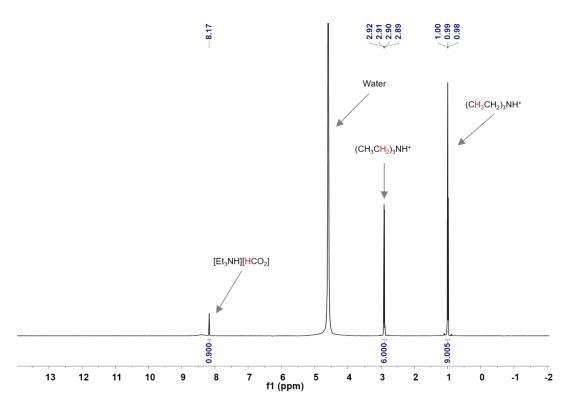


Figure S5. ¹H NMR analysis of the adduct produced by CO₂ hydrogenation after degassing at 90 °C for 2 h.

3. Analysis of substances generated during separation of Ca(HCO₂)₂ production

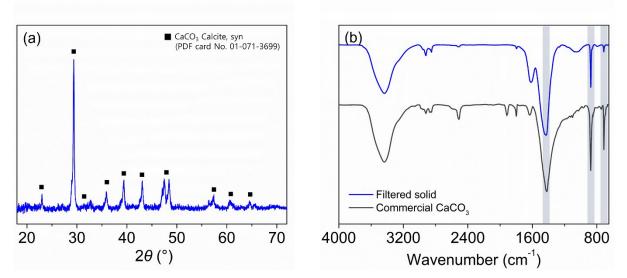


Figure S6. (a) XRD and (b) FT-IR analyses of the filtered solid produced during the synthesis of $Ca(HCO_2)_2$ from [Et₃NH][HCO₂] by using CaO.

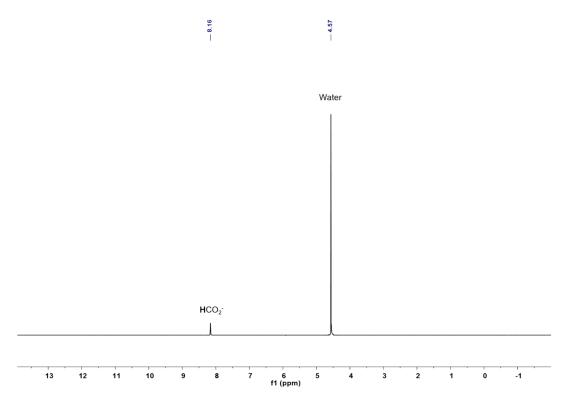


Figure S7. ¹H NMR analysis of the evaporated solid produced during the synthesis of $Ca(HCO_2)_2$ from [Et₃NH][HCO₂] by using CaO.

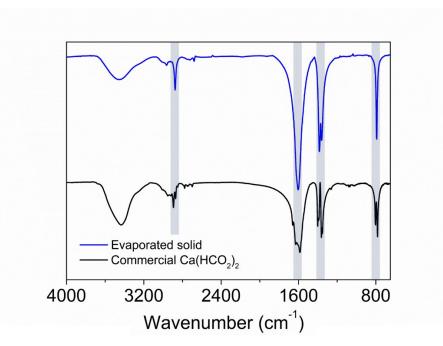


Figure S8. FT-IR analysis of the evaporated solid produced during the synthesis of $Ca(HCO_2)_2$ from $[Et_3NH][HCO_2]$ by using CaO.

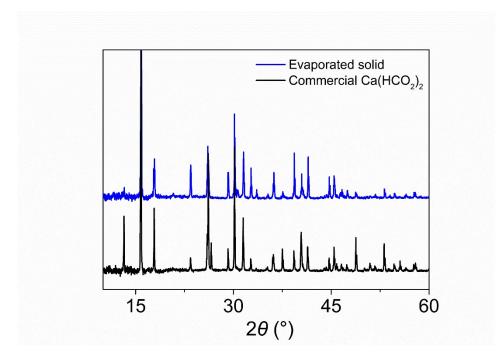


Figure S9. XRD image of Ca(HCO₂)₂ obtained from [Et₃NH][HCO₂] by using CaO.

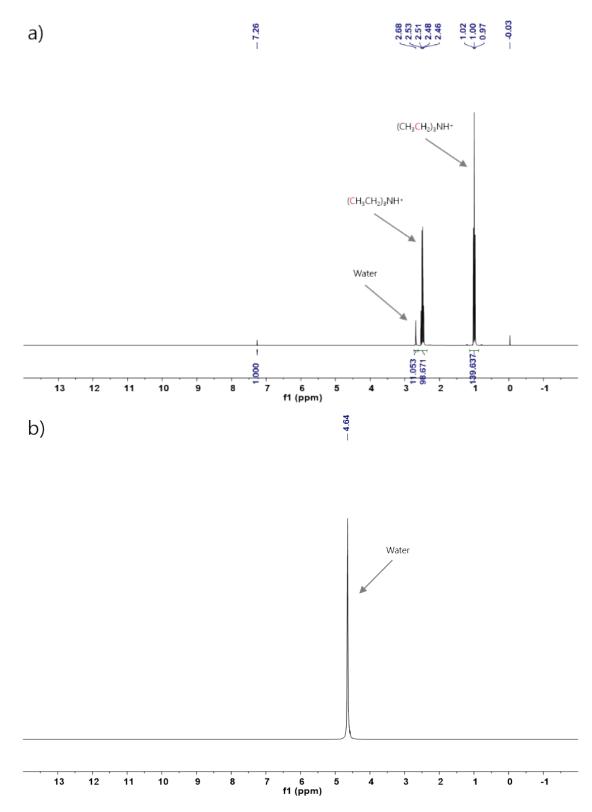


Figure S10. ¹H-NMR data of a) Et₃N and b) H₂O obtained by evaporating the filtrate at 100 and 130 °C.

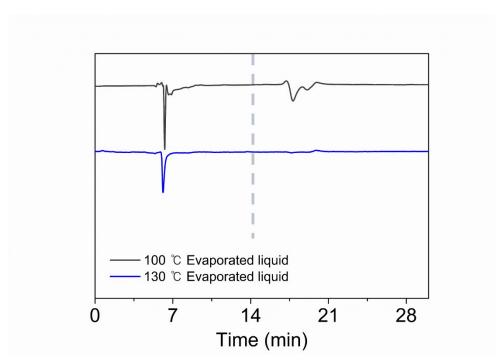


Figure S11. HPLC data of Et₃N (black) and H₂O (blue) obtained by evaporating the filtrate at 100 and 130 °C.

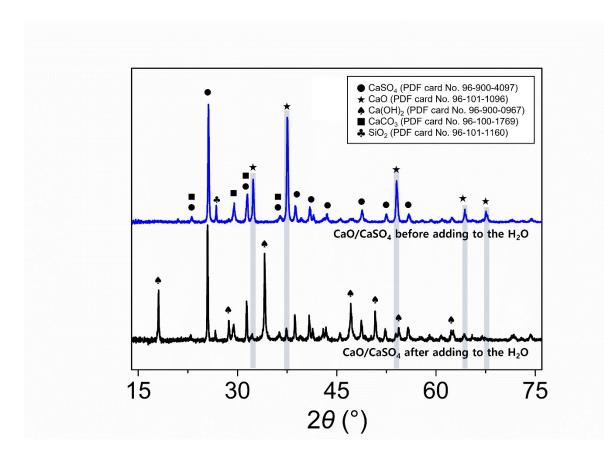


Figure S12. XRD image before and after adding CaO/CaSO₄ to the H₂O.

4. Ca(HCO₂)₂ yield and amine loss according to the change of additives containing CaO

| Entry | Temp. | Time | Et ₃ N | HCO ₂ H | Added CaO | Reacted CaO | Reacted CaO | Produced Ca(HCO ₂) ₂ | Produced Ca(HCO ₂) ₂ |
|-------|-------|--------|-------------------|--------------------|--------------|----------------|----------------|--|--|
| - | [°C] | [h] | [M] | [M] | [M] | [M] | | [M] | |
| 1 | 30 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8547 | 99.93% | 0.8434 | 98.60% |
| 2 | 30 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8518 | 99.58% | 0.8559 | 100.06% |
| 3 | 30 | 0.5 | 1.9008 | 1.7107 | 0.8554 | 0.8510 | 99.50% | 0.8551 | 99.97% |
| 4 | 30 | 0.5 | 1.9008 | 1.7107 | 0.8554 | 0.8516 | 99.56% | 0.8453 | 98.83% |
| 5 | 30 | 2 | 1.9008 | 1.7107 | 0.8554 | 0.8526 | 99.68% | 0.8735 | 102.13% |
| 6 | 30 | 2 | 1.9008 | 1.7107 | 0.8554 | 0.8521 | 99.62% | 0.8618 | 100.75% |
| 7 | 30 | 15 | 1.9008 | 1.7107 | 0.8554 | 0.8543 | 99.88% | 0.8677 | 101.44% |
| 8 | 30 | 15 | 1.9008 | 1.7107 | 0.8554 | 0.8484 | 99.19% | 0.8603 | 100.58% |
| 9 | 30 | 60 | 1.9008 | 1.7107 | 0.8554 | 0.8395 | 98.15% | 0.8394 | 98.13% |
| 10 | 30 | 60 | 1.9008 | 1.7107 | 0.8554 | 0.8171 | 95.53% | 0.8329 | 97.37% |
| 11 | 45 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8539 | 99.83% | 0.8584 | 100.36% |
| 12 | 45 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8521 | 99.62% | 0.8411 | 98.33% |
| 13 | 60 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8521 | 99.62% | 0.8664 | 101.29% |
| 14 | 60 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8527 | 99.69% | 0.8432 | 98.57% |
| 15 | 75 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8520 | 99.61% | 0.8536 | 99.79% |
| 16 | 75 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8536 | 99.79% | 0.8657 | 101.21% |
| 17 | 90 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8536 | 99.79% | 0.8217 | 96.06% |
| 18 | 90 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8533 | 99.76% | 0.8210 | 95.98% |

Table S1. $Ca(HCO_2)_2$ yields from the reaction between $[Et_3NH][HCO_2]$ and CaO for various reaction times and temperatures.

| Entry | Temp. | Time | Et ₃ N | HCO ₂ H | Added CaSO ₄ | Added CaO | Reacted CaO | Reacted CaO | Produced Ca(HCO ₂) ₂ | Produced Ca(HCO ₂) ₂ |
|-------|-------|--------|-------------------|--------------------|----------------------------|--------------|----------------|----------------|--|--|
| - | [°C] | [h] | [M] | [M] | [M] | [M] | [M] | | [M] | |
| 1 | 30 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.9034 | 105.62% | 0.8852 | 103.49% |
| 2 | 30 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.9014 | 105.38% | 0.8606 | 100.61% |
| 3 | 30 | 0.5 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8959 | 104.74% | 0.8464 | 98.96% |
| 4 | 30 | 0.5 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8821 | 103.13% | 0.8310 | 97.16% |
| 5 | 30 | 2 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8993 | 105.14% | 0.8396 | 98.16% |
| 6 | 30 | 2 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8864 | 103.63% | 0.8553 | 99.99% |
| 7 | 30 | 15 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8987 | 105.06% | 0.8727 | 102.03% |
| 8 | 30 | 15 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8332 | 97.41% | 0.8530 | 99.72% |
| 9 | 30 | 60 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.9183 | 107.36% | 0.8859 | 103.57% |
| 10 | 30 | 60 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8946 | 104.59% | 0.8676 | 101.43% |
| 11 | 45 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8819 | 103.11% | 0.8474 | 99.07% |
| 12 | 45 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8736 | 102.14% | 0.8634 | 100.94% |
| 13 | 60 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8973 | 104.90% | 0.8629 | 100.89% |
| 14 | 60 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8899 | 104.04% | 0.8540 | 99.84% |
| 15 | 75 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.9084 | 106.20% | 0.9053 | 105.84% |
| 16 | 75 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8887 | 103.89% | 0.8722 | 101.97% |
| 17 | 90 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.9037 | 105.65% | 0.8669 | 101.35% |
| 18 | 90 | 0.0833 | 1.9008 | 1.7107 | 0.8554 | 0.8554 | 0.8843 | 103.39% | 0.8650 | 101.12% |

Table S2. $Ca(HCO_2)_2$ yields from the reaction between $[Et_3NH][HCO_2]$ and the CaO-CaSO₄ mixture for various reaction times and temperatures.

| Temp. | Time | Et ₃ N | HCO ₂ H | Added CaO | Reacted CaO | Reacted CaO | Produced Ca(HCO ₂) ₂ | Produced Ca(HCO ₂) ₂ |
|-------|-------|-------------------|--------------------|--------------|----------------|----------------|--|--|
| [°C] | [min] | [M] | [M] | [M] | [M] | | [M] | |
| 30 | 5 | 1.9008 | 1.7107 | 0.9593 | 0.8529 | 99.71% | 0.8624 | 100.83% |

Table S3. $Ca(HCO_2)_2$ yields from the reaction between $[Et_3NH][HCO_2]$ and the ash in the desulfurization process (CaO 23.4wt%).

Table S4. Amine loss during synthesis of $Ca(HCO_2)_2$ from $[Et_3NH][HCO_2]$ by using (1) CaO, (2) CaO+CaSO₄ and (3) ash in desulfurization process.

| Entry | HCO ₂ H | Et ₃ N | Temp. | Time | Added CaO | Produced Ca(HCO ₂) ₂ | Produced Ca(HCO ₂) ₂ | Produced amine | Amine loss |
|-------|--------------------|-------------------|-------|-------|--------------|--|--|----------------|------------|
| - | [M] | [M] | [°C] | [min] | [M] | [M] | % | | |
| 1 | 1.7107 | 1.9008 | 30 | 5 | 0.8554 | 0.8559 | 100.06% | 100.06% | 0% |
| 2 | 1.7107 | 1.9008 | 30 | 5 | 0.8554 | 0.8606 | 100.61% | 100.61% | 0% |
| 3 | 1.7107 | 1.9008 | 30 | 5 | 0.8554 | 0.8624 | 100.82% | 100.82% | 0% |

5. Techno-economic analysis

| | Parameter | Value |
|-------------|--|-----------------|
| Assumptions | (1) Annual Ca(HCO ₂) ₂ production (t Ca(HCO ₂) ₂ /yr) | 38,500 |
| | (2) Economic life of the plant (yr) | 20 |
| | (3) Annual operating hours (hr/yr) | 8,000 |
| | (4) Interest rate (%) | 8 |
| | (5) Tax rate (%) | 35 |
| | (5) Depreciation method | Straightforward |
| | (6) Direct supervisory and clerical labor(% of operating labor cost) | 17 |
| | (7) Maintenance and repairs(% of fixed capital investment cost) | 6 |
| | (8) Operating supplies(% of maintenance and repairs cost) | 15 |
| | (9) Laboratory charges(% of operating labor cost) | 15 |
| | (10) Patents and royalties(% of total operating cost) | 3 |
| | (11) Taxes and insurance(% of fixed capital investment cost) | 2 |
| | (12) Plant overhead costs(% of operating labor, (6) and (7)) | 60 |
| | (13) Administration costs(% of operating labor, (6) and (7)) | 15 |
| | (14) Distribution and selling cost(% of total operating cost) | 11 |
| | (15) Research and development(% of total operating cost) | 5 |
| Utilities | (16) Low-pressure steam (USD/GJ) | 13.28 |
| | (17) Electricity (Conventional) (USD/kWh) | 0.07 |
| | (18) Electricity (Renewable) (USD/kWh) | 0.14 |
| | (19) Cooling water (USD/ton) | 0.354 |

Table S5. Parameters used and assumptions made for the economic analysis^{1, 2}

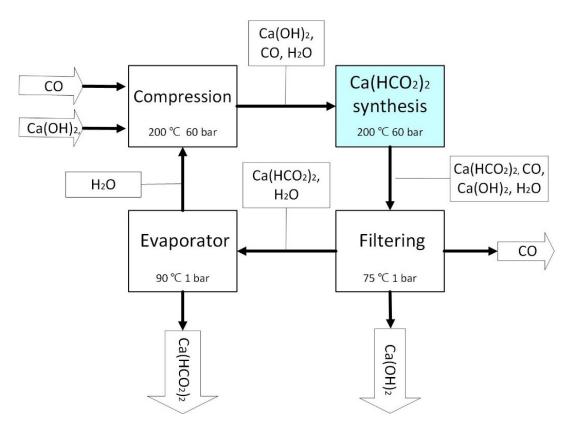


Figure S13. Block flow diagram of the process of Ca(HCO₂)₂ production from CO and Ca(OH)₂.

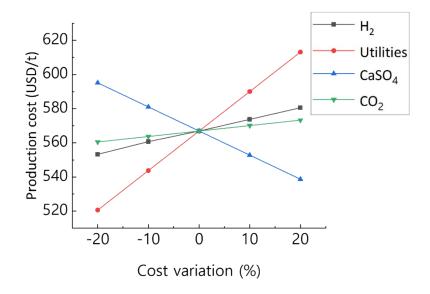


Figure S14. Sensitivity analysis of the Ca(HCO₂)₂ production cost for the fluctuation of H₂ from SMR(black), utilities (red), CO₂ (green), and CaSO₄ (blue).

6. Life-cycle assessment

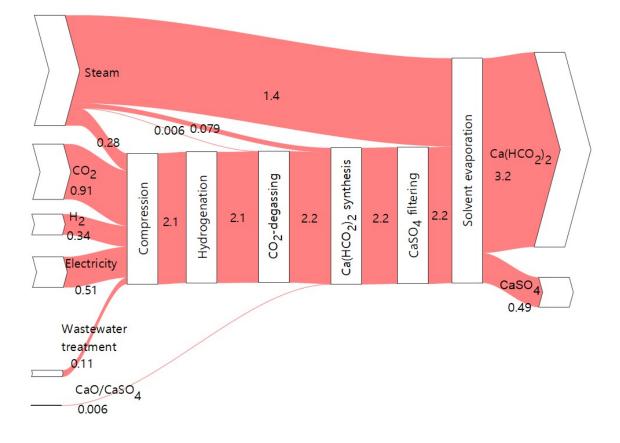


Figure S15. Sankey diagram for the GW index of the proposed process (H₂ from SMR) (unit: kg CO_2 -eq/kg $Ca(HCO_2)_2$).

| Inflows | Database | Note |
|----------------------------------|---|-------------------------------------|
| Material | | |
| ${\rm H_2}^3$ | Hydrogen (reformer) E | H ₂ from SMR |
| CO_2^4 | Carbon dioxide, liquid market for Cut-off, S | |
| CaO/CaSO44 | Waste gypsum market for Cut-off, S | |
| $\rm CO^4$ | Carbon monoxide market for Cut-off. S | |
| Ca(OH) ₂ ⁴ | Lime, hydrated, packed market for Cut-off, S | |
| H_2O^4 | Water, completely softened market for Cut-off, S | |
| Et ₃ N | Triethyl amine {GLO} market for Cut-off, S | |
| Utilities | | |
| Steam ⁴ | Heat, from steam, in chemical industry market for Cut-off, S | |
| Electricity ⁴ | Electricity, high voltage $^2\vert$ heat and power co-generation, hard coal \vert Cut-off, S | |
| Electricity ^{4, 5} | Electricity, low voltage ² electricity production, photovoltaic, 570kWp open Cut-off, S | H ₂ from Electrolysis |
| Electricity ^{4, 5} | Electricity, high voltage ² electricity production, wind, >3MW turbine, onshore Cut-off, S | H ₂ from Electrolysis |
| Outflows | | |
| Wastewater ⁴ | Wastewater, average treatment of, capacity 1E9l/year Cut-off, S | |
| Inert waste ⁴ | Inert waste treatment of, sanitary landfill Cut-off, S | |

Table S6. Parameters used for the environmental analysis.

5. A. Al-Qahtani, B. Parkinson, K. Hellgardt, N. Shah and G. Guillen-Gosalbez, *Applied Energy*, 2021, **281**, 115958.

^{1.} R. Turton, R. C. Bailie, W. B. Whiting and J. A. Shaeiwitz, *Analysis, synthesis and design of chemical processes*, Pearson Education, 2008.

^{2.} L. a. K.-H. G-D, Kim, Establishment and operation of mid- to long-term unit cost (LCOE) forecasting system for expanding renewable energy supply, <u>https://www.keei.re.kr/main.nsf/index.html?open&p=%2Fweb_keei%2Fd_results.nsf%2Fmain_all%2F</u> <u>A10FCB3438C55F4349258669004FC436&s=%3FOpenDocument%26menucode%3DS0%26category%3</u> D%25EA%25B8%25B0%25EB%25B3%25B8%25EC%2597%25B0%25EA%25B5%25AC.

^{3.} Eco-profiles, <u>https://www.plasticseurope.org/en/resources/eco-profiles</u>, 2005.

^{4.} G. Wernet, C. Bauer, B. Steubing, J. Reinhard, E. Moreno-Ruiz and B. Weidema, *The International Journal of Life Cycle Assessment*, 2016, **21**, 1218-1230.