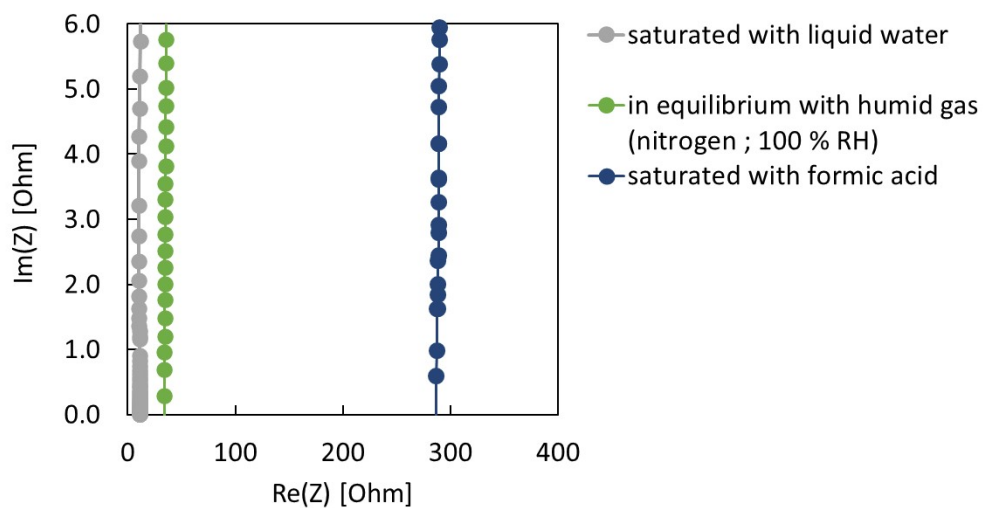
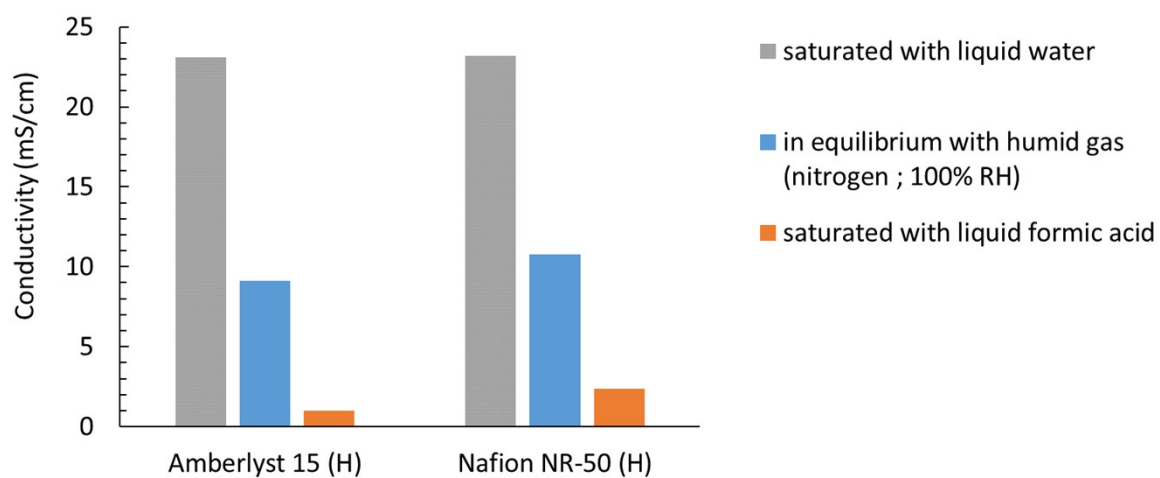


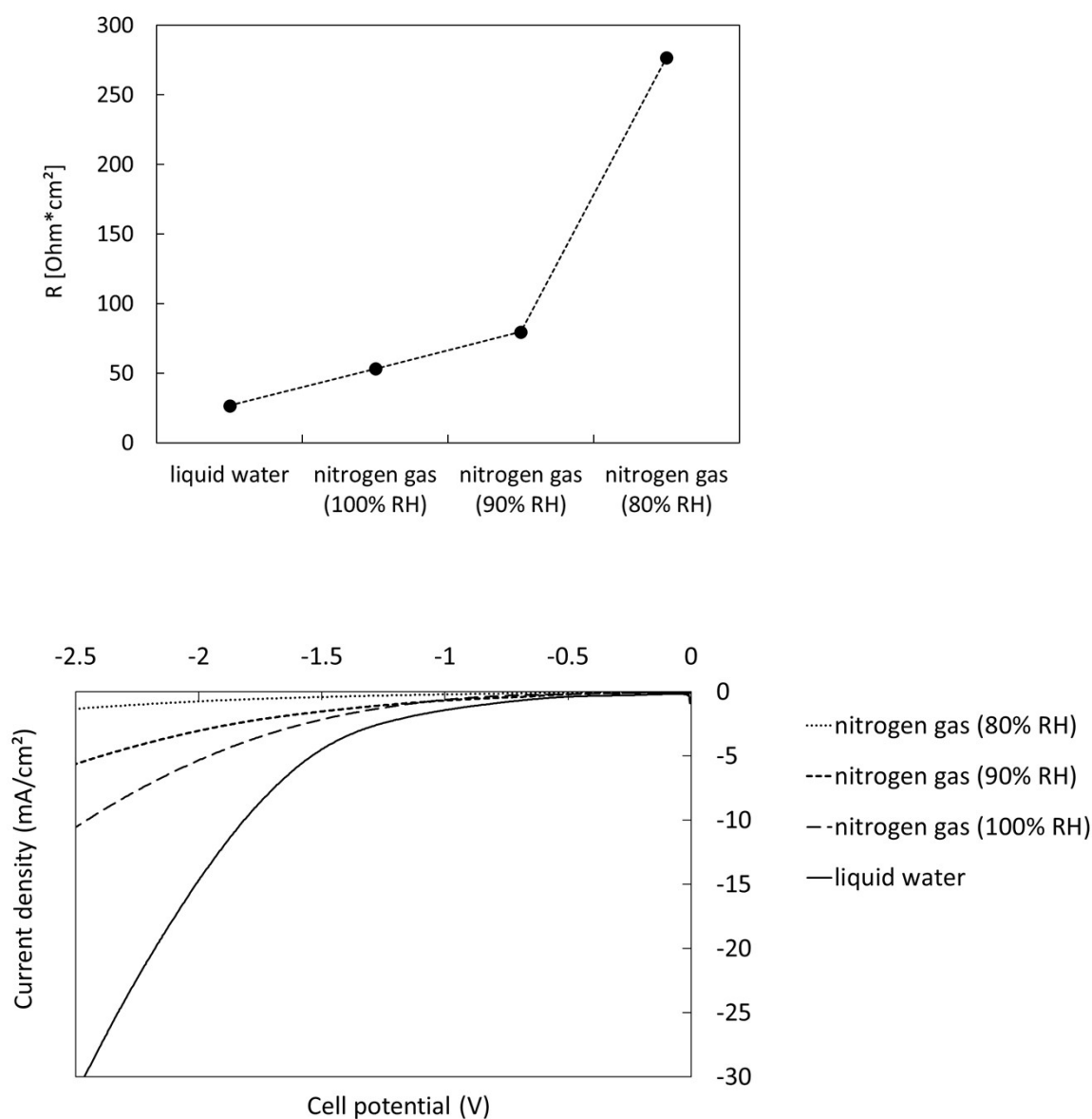
## Supplementary information

# Matching emerging formic acid synthesis processes with application requirements

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**Fig. S1 : Top** : Conductivity of two types of proton exchange solid state electrolyte ('PE-SSE') resin beads saturated either with liquid water, concentrated formic acid or after equilibration with a humid N<sub>2</sub> gas flow at a relative humidity of 100% at room temperature. A 5 mm thick layer of resin beads was pressed between two stainless steel plates and the resistance was determined from Nyquist plots obtained with potentiostatic electrochemical impedance spectroscopy (pEIS ; 0V). **Bottom** : Nyquist plots for Amberlyst 15 (H) PE-SSE resin beads.



**Fig. S2** : Resistance measurements (**top**) and cyclic voltammetry (CV) measurements (**bottom**) for a three-compartment electrolyser for CO<sub>2</sub> reduction to formic acid at different humidity conditions. The membrane electrode assembly consisted of a Pt on C-cloth anode, a PEM (Nafion 117), SSE resin (Amberlyst-15H ; 3 mm thick layer), AEM (Fumasep FAD-PET-75) and Sn/Cu cathode coated with Pention D35 ionomer. In the middle compartment, either a liquid water flow or a humid gas flow was used. **Top** : The resistance was measured with potentiostatic electrochemical impedance spectroscopy (pEIS ; 0V) after exposing the MEA to the operating conditions until an equilibrium value was reached for the resistance, which is depicted here. **Bottom** : The CV curves were measured at equilibrium at a scan rate of 5 mV/s.

**Table S1** : additional information for the determination of the round-trip efficiencies for various energy storage media. Transport is not taken into account.

	Li-ion battery	Pumped hydro	Hydrogen *1		Methane *2	Ammonia *3	Formic acid *4
			Compressed (350 - 700 bar)	Liquefied	Compressed	Liquefied	
Energy to fuel (kWh/kg)			50 – 55				2.6 - 5.7
Fuel processing (kWh/kg)			2 – 6	7 - 13			2.3 – 9.6
Energy content (LHV)			33.3			5.2	1.72
Conversion efficiency (%)			55 - 64	49 - 58		43 - 52	11 - 35
Reconversion efficiency (%)			50 - 70			45	45
Round-trip efficiency (%)	<b>80 – 95</b>	<b>70 – 80</b>	<b>34 - 45</b>	<b>25 - 41</b>	<b>30 - 38</b>	<b>19 - 23</b>	<b>5 - 16</b>

#### \*1 : Hydrogen

Assuming H<sub>2</sub> formation from renewable energy with a PEM electrolyser with an energy efficiency of ca.70%,<sup>1</sup> followed by compression or liquefaction<sup>2</sup> and reconversion to energy in a hydrogen fuel cell with an energy efficiency of 50-70%.<sup>3</sup>

#### \*2 : Methane

Assuming H<sub>2</sub> formation from renewable energy by an electrolyser, catalytic CO<sub>2</sub> methanation by the Sabatier-Senderens reaction and compression to 80 bar.<sup>4</sup>

#### \*3 : Ammonia

Assuming one kg of ammonia production requires 9–15 kWh of energy.<sup>5</sup> For reconversion, ammonia is cracked into high-purity hydrogen, compressed and used in a PEMFC.<sup>5</sup>

#### \*4 : Formic acid

Assuming electrochemical production of formic acid from CO<sub>2</sub> and H<sub>2</sub>O in a CO<sub>2</sub> electrolyzer. Post-processing is done by distillation and reconversion to energy by reforming of formic acid to H<sub>2</sub> followed by a H<sub>2</sub> fuel cell (“HYFORM-PEMFC”, as described by Ma *et al.*<sup>6</sup>). Fuel processing of formic acid refers to the concentration process. A feed concentration of 10 wt.% is assumed, which requires 2.3-9.6 kWh/kg depending on the concentration method, as derived from Ramdin *et al.* (Fig. S4 from <sup>7</sup>), calculated from given operational cost in \$/kg, assuming energy cost is biggest contributor to the operating costs with an electricity price of 50 \$/MWh.<sup>7</sup>

## References

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