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Supporting information for

**2 High-sensitivity and field analysis of lead by portable optical emission spectrometry using
3 microplasma trap**

4 Yaru Zhang^{†,§}, Jixin Liu^{*,†,||}, Xuefei Mao^{*,†}, Xing Na^{||}, Di Tian[§], Yongzhong Qian[†]

5 † Institute of Quality Standard and Testing Technology for Agro-products, Chinese Academy of Agricultural
6 Sciences, and Key Laboratory of Agro-food Safety and Quality, Ministry of Agriculture and Rural Affairs,
7 Beijing 100081, China

8 § College of Instrumentation & Electrical Engineering, Jilin University, Changchun 130023, China

9 || Beijing Ability Technique Company, Limited, Beijing 100081, China

10 **Corresponding authors:**

11 *X. F. Mao. Phone & Fax: +86 10 82106523. E-mail: mxmf08@163.com & maoxuefei@caas.cn.

12 *J. X. Liu. Phone & Fax: +86 10 82106540. E-mail: ljx2117@gmail.com.

13 1. Picture of HG-*in situ* DBD trap-OES



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Fig. S1 Picture of HG-*in situ* DBD trap-OES.

16 2. The operational parameters of ICP-MS

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Table S-1 Operational parameters of ICP-MS

Parameters	Values
Incident RF power	1150 W
Sampling depth	120 mm
Nebulizer Ar gas flow rate	0.8 L min ⁻¹
Cooling Ar gas flow rate	14 L min ⁻¹
Auxiliary Ar gas flow rate	1.2 L min ⁻¹
Peristaltic pump rate	30 rpm
Dwell time	10 ms
Isotopes	²⁰⁸ Pb
Internal standard isotopes	¹⁷⁵ Lu

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19 3. Background correction method

20 In this paper, an iteratively modified moving average algorithm is employed to eliminate the influence of
21 background fluctuation. In this method, a baseline is fitted according to Equation (1), in which $f_{Base}(i)$
22 indicates the intensity of point i on baseline curve, $f(i)$ indicates the intensity of point i on initial spectrum and

23 $dAver(i)$ indicates the average intensity of point i and its surrounding points on initial spectrum, which is
 24 calculated as Equation (2). In Equation (2), d indicates the number of point on one side on point i (in this
 25 experiment, d is set as 13). After the baseline curve ($fBase$) is obtained, another baseline ($fbase2$) is calculated
 26 by replacing $f(i)$ in Equation (1) and Equation (2) with $fbase(i)$. The final baseline curve is obtained by iterate
 27 n times like this (in this experiment, n is set as 8). The spectrum after background correction is obtained by
 28 subtracting the final baseline curve from the initial spectrum.

$$29 \quad fBase(i) = \begin{cases} f(i) & f(i) < dAver(i) \\ dAver(i) & f(i) > dAver(i) \end{cases} \quad (1)$$

$$30 \quad dAver(i) = \left(\sum_{j=-d}^{j=d} f(i+j) \right) / (2*d+1) \quad (2)$$

31 4. Peak volume, linear range, precision and sensitivity

32 In this article, a peak volume algorithm is used for the OES quantification of Pb. Regarding OES, peak
 33 height and area have been usually utilized to calculate the signals for quantitative analysis. Herein, for HG-*in*
 34 *situ* DBD trap OES, the complete release of Pb occupies a certain amount of time by means of the intensity-
 35 wavelength spectrum. So, Pb signals can be calculated by combination of intensity, wavelength and time,
 36 which become a group of 3-dimensional data, namely peak volume. The calculation equations of peak volume
 37 are described as Equation 1 and Equation 2. The effects of these calculation methods including peak height,
 38 area, and volume on linear range and sensitivity were evaluated and results were summarized in Table S1. As
 39 can be seen, the peak volume have a great effect on improving the sensitivity and precision of Pb.

$$40 \quad I_{area}(t) = \sum_{\lambda=\lambda_{start}}^{\lambda=\lambda_{end}} I_t(\lambda) \quad (1)$$

$$41 \quad I_{volume} = \sum_{t=t_{start}}^{t=t_{end}} I_{area}(t) \quad (2)$$

42 In Eq. (1), $I_{area}(t)$ is the intensity calculated by peak area of the intensity-wavelength spectrum collected
 43 at t time. $I_t(\lambda)$ refers to the intensity-wavelength spectrum collected at t time. λ_{start} and λ_{end} refer to the
 44 wavelength of starting point and ending point of the peak. In Eq. (2), I_{volume} is the intensity calculated by peak
 45 volume. t_{start} and t_{end} refer to the time index of starting intensity-wavelength spectrum and ending intensity-
 46 wavelength spectrum.

47 It is worth mentioning that the background correction was performed for each intensity-wavelength
 48 spectrum to reduce errors caused by baseline fluctuation before the comparison.

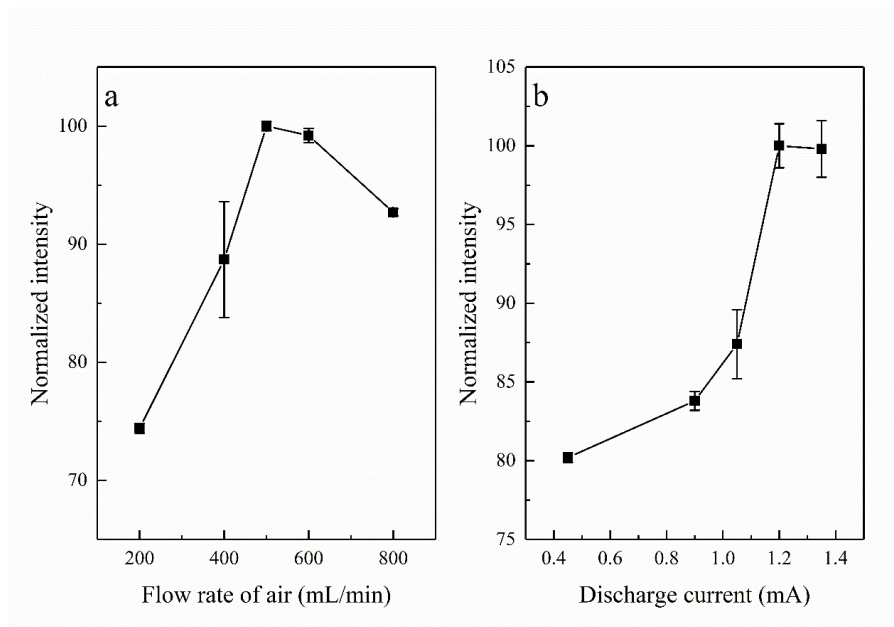
49 **Table S1** Linear range and sensitivity achieved by different signal calculation methods.

Calculated method	Sensitivity (L μg^{-1})	Linear range ($\mu\text{g L}^{-1}$)	RSD (%)
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Peak height	48	1-100	4
Peak area	595	1-100	3.5
Peak volume	3775	1-100	1.4

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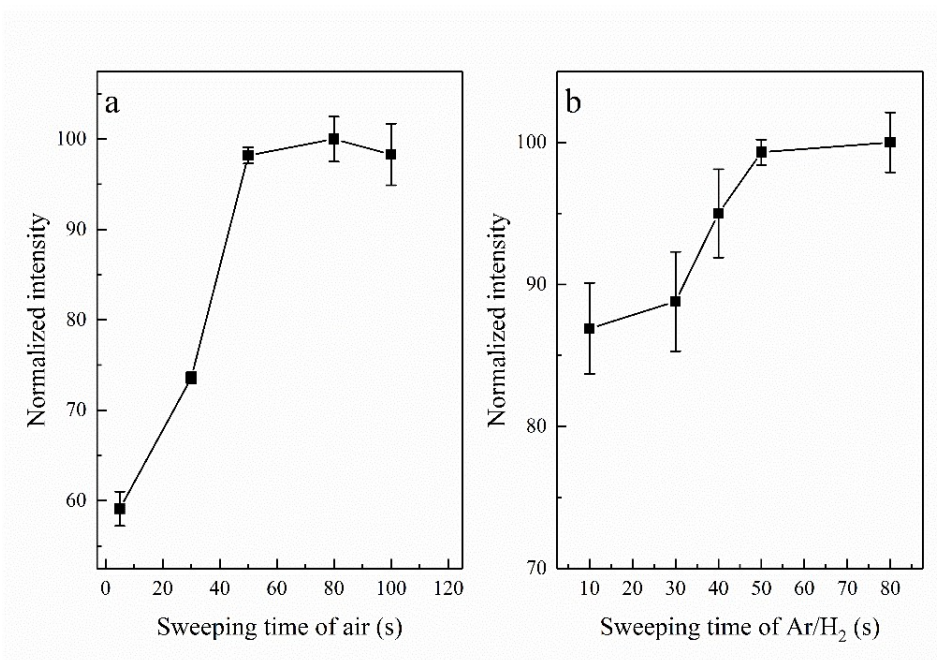
51 **5. Optimization of trap conditions**



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53 **Fig.S2 Dependence of DBD trapping on air flow rate and discharge current.** In Fig. S1a, intensities are
54 normalized with the Pb signal at 500 mL/min set at 100 for. In Fig. S1b, intensities are normalized with the
55 Pb signal at 1.2 mA set at 100.

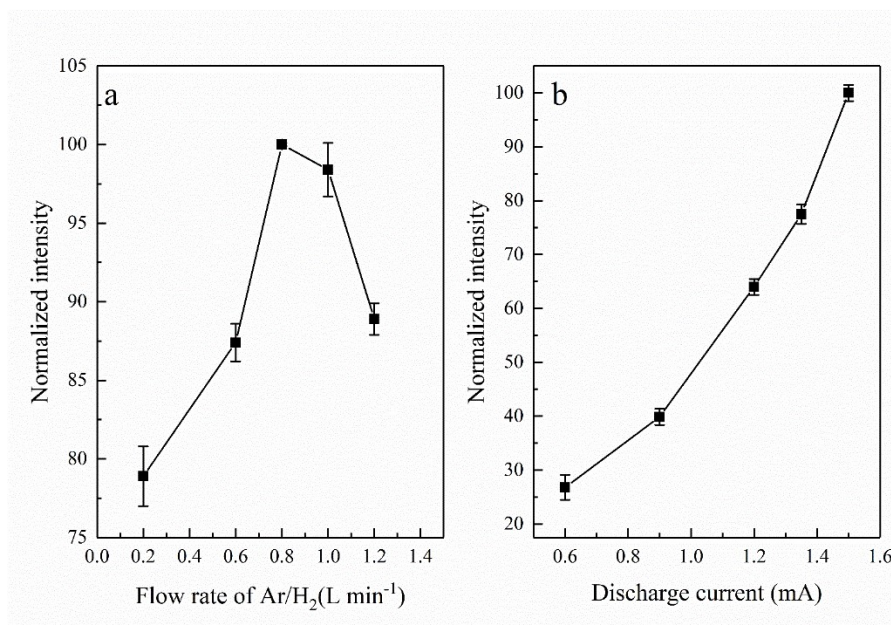
56 **6. Optimization of sweeping conditions**



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58 **Fig. S3 Effect of air and Ar/H₂ sweeping duration on moisture interference.** Fig. S2a shows the effect of
 59 air sweeping duration on Pb intensities without subsequent Ar/H₂ sweeping. The intensities are normalized
 60 with the Pb intensity at 80 s set at 100. Fig. S2b shows the effect of Ar/H₂ sweeping on Pb intensities after 50
 61 s air sweeping. The intensities are normalized with the Pb intensity at 80 s set at 100.

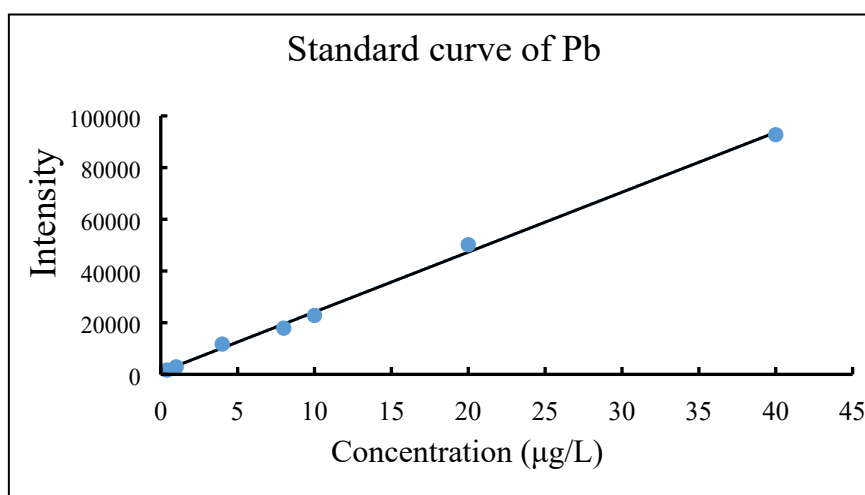
62 **7. Optimization of releasing condition**



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64 **Fig. S4 The effect of Ar/H₂ flow rate and discharge current on Pb intensities for DBD release.** In Fig.S3a,
 65 the Pb intensity at 800 mL/min is set as 100, and the others are normalized. In Fig.S3b, the Pb intensity at 1.5
 66 mA is set as 100, and the others are normalized to this value.

67 **8. Standard curve of Pb**



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Fig.S5 Standard curve of Pb.

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