

Supplementary Information

Microfluidic Generation of ATPS Droplets by Transient Double Emulsion Technique

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I Supplementary Figures

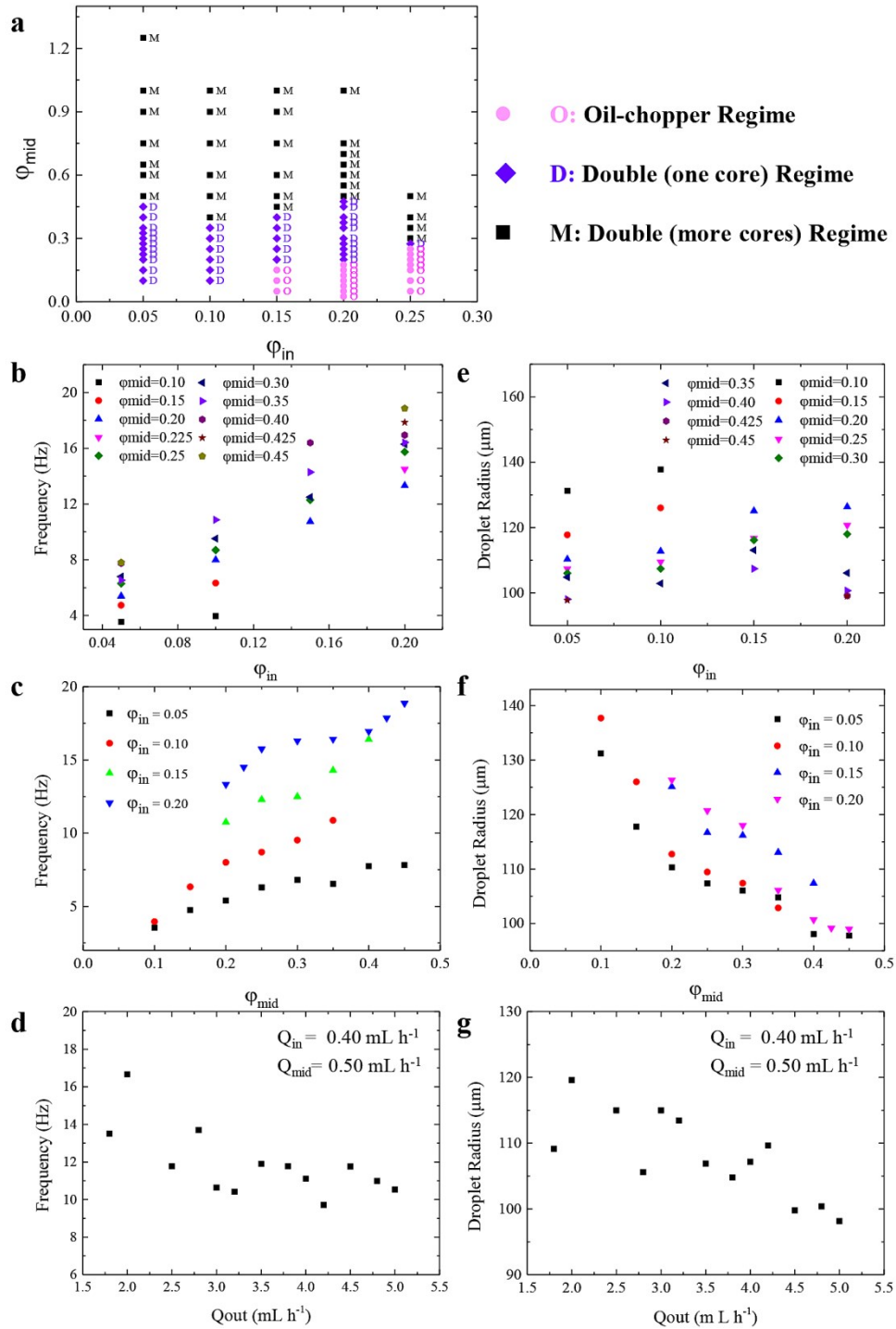


Fig. S1 ATPS droplets generated by using System II (see Table S1). (a) Phase diagram for dextran-in-PEG ATPS droplet generation by changing the flow rate ratio of the inner ($\phi_{in} = Q_{in}/Q_{out}$) and middle oil phases ($\phi_{mid} = Q_{mid}/Q_{out}$), while keeping the flow rate of outer PEG-rich phase constant at $Q_{out} = 2.00 \text{ mL h}^{-1}$. (b-d) Controlling the generation frequency of ATPS droplets by tuning the inner phase flow rate ratio $\phi_{in} = Q_{in}/Q_{out}$ (b), the middle phase flow rate ratio $\phi_{mid} = Q_{mid}/Q_{out}$ (c), and the outer phase flow rate Q_{out} (d). (e-g) Controlling the radius of ATPS droplets by tuning ϕ_{in} (e), ϕ_{mid} (f), and Q_{out} (g). In (b), (c), (e), and (f), $Q_{out} = 2.00 \text{ mL h}^{-1}$. In (d) and (g), $Q_{in} = 0.40$, $Q_{mid} = 0.50 \text{ mL h}^{-1}$.

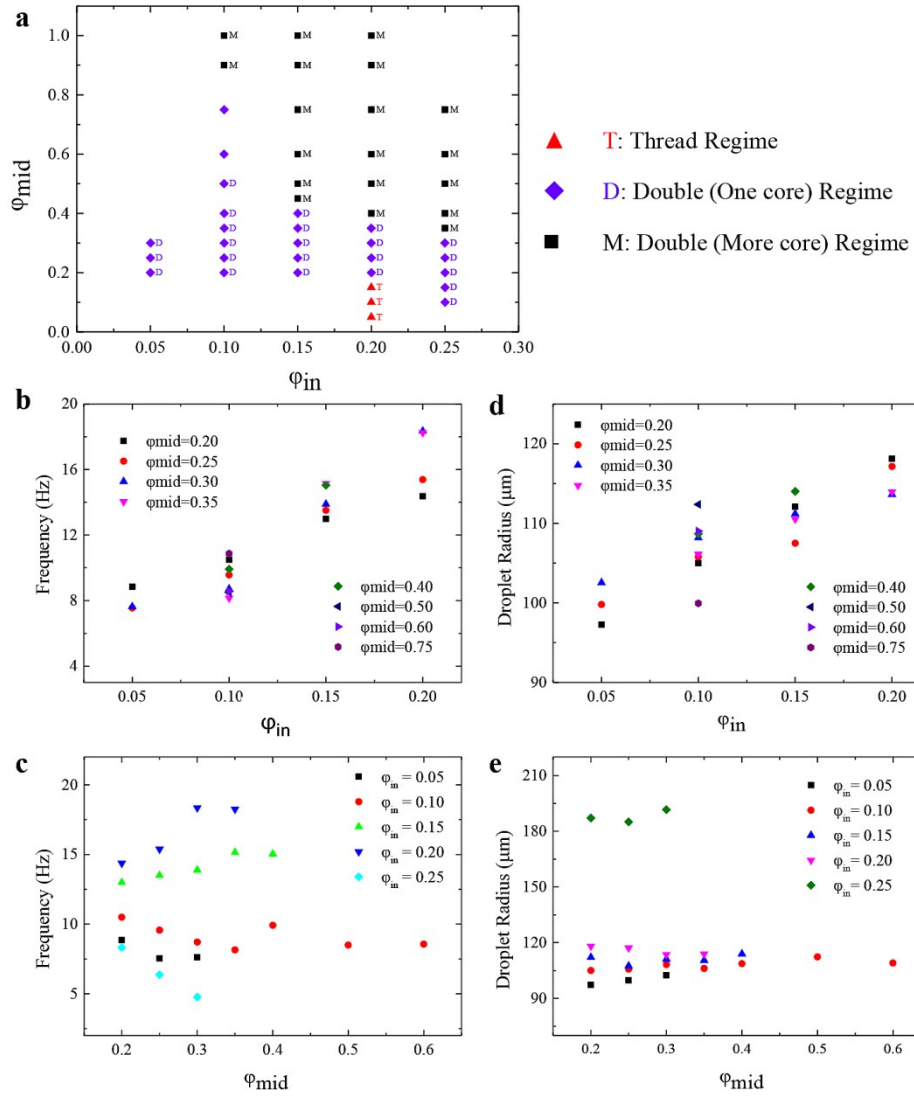


Fig. S2 ATPS droplets generated by using System III (see Table S1). (a) Phase diagram for dextran-in-PEG ATPS droplet generation by changing the flow rate ratio of the inner ($\phi_{in} = Q_{in}/Q_{out}$) and middle oil phases ($\phi_{mid} = Q_{mid}/Q_{out}$), while keeping the flow rate of outer PEG-rich phase constant at $Q_{out} = 2.00 \text{ mL h}^{-1}$. (b-c) Controlling the generation frequency of ATPS droplets by tuning the inner phase flow rate ratio $\phi_{in} = Q_{in}/Q_{out}$ (b), and the middle phase flow rate ratio $\phi_{mid} = Q_{mid}/Q_{out}$ (c). (d-e) Controlling the radius of ATPS droplets by tuning ϕ_{in} (d), and ϕ_{mid} (e). In (b)-(e), $Q_{out} = 2.00 \text{ mL h}^{-1}$.

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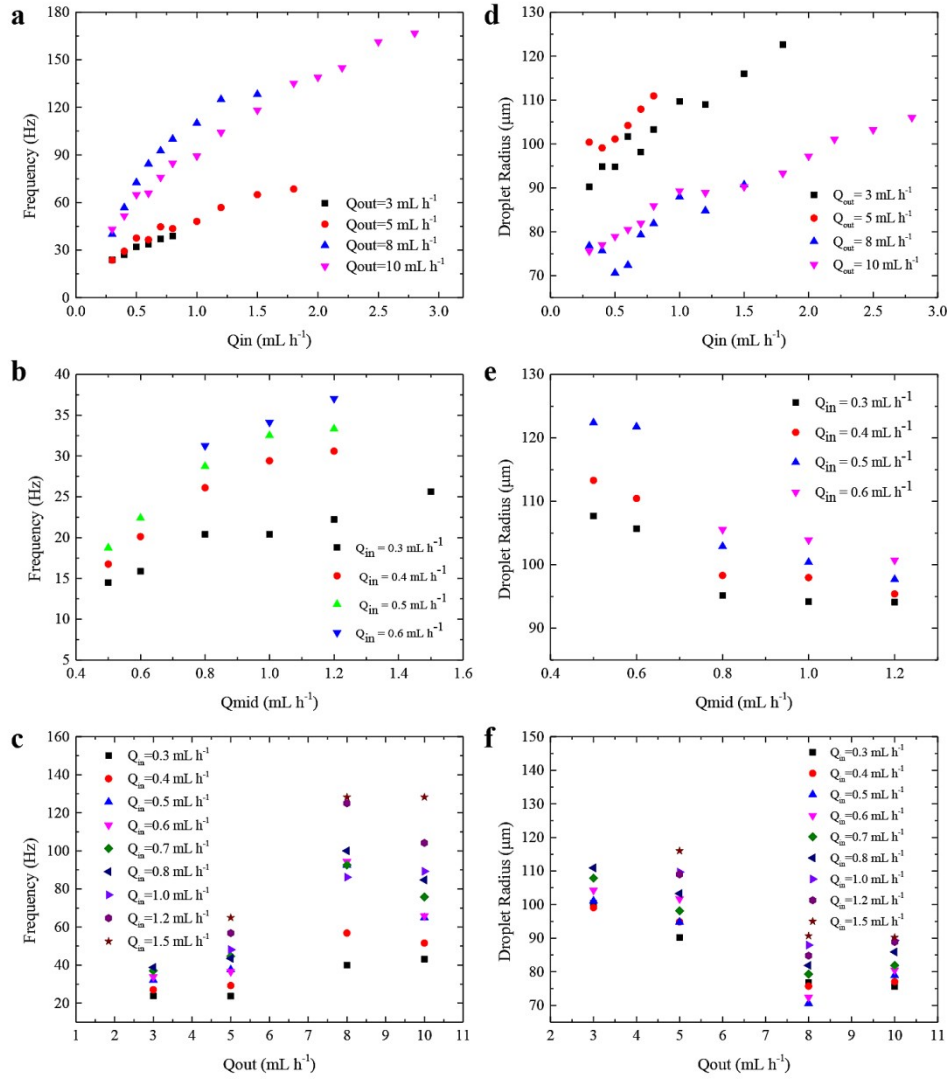


Fig. S3 The generation frequency and radius of PEG-in-dextran ATPS droplets by using System IV (see **Table S1**). (a-c) Controlling the generation frequency of PEG-in-dextran ATPS droplets by tuning the inner phase flow rate Q_{in} (a), the middle phase flow rate Q_{mid} (b), and the outer phase flow rate Q_{out} (c). (d-f) Controlling the radius of PEG-in-dextran ATPS droplets by tuning Q_{in} (d), Q_{mid} (e), and Q_{out} (f). In (a) and (d), $Q_{mid} = 1.00 \text{ mL h}^{-1}$. In (b) and (e), $Q_{out} = 3.00 \text{ mL h}^{-1}$. In (c) and (f), $Q_{mid} = 1.00 \text{ mL h}^{-1}$.

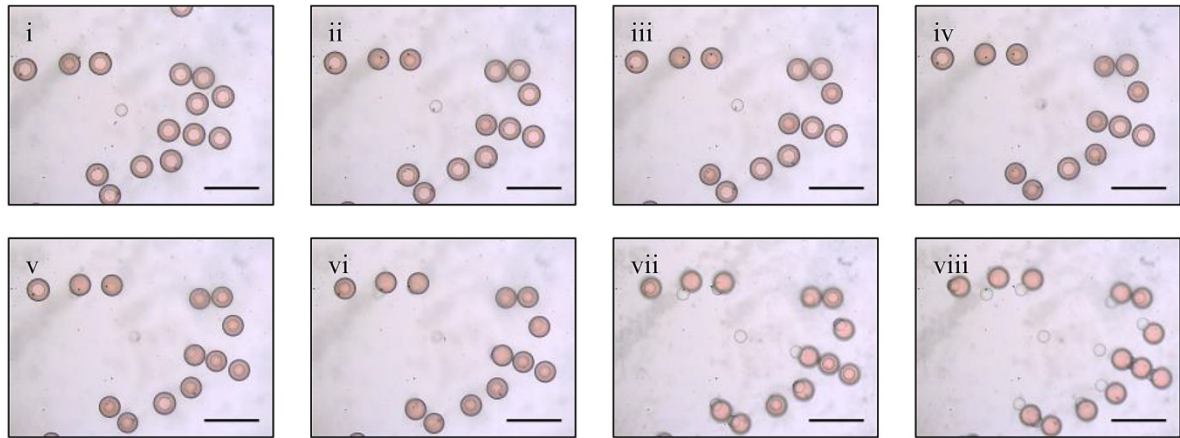


Fig. S4 Off-chip releasing process for double emulsion droplets with an average density smaller than the density of the continuous phase ($\rho_{\text{Double}} < \rho_{\text{PEG}}$), the lighter double emulsion droplets rise up to the air-liquid surface and then separate into oil-in-water (O/W2) droplets and ATPS (W1/W2) droplets ($Q_{\text{in}} = 0.20 \text{ mL h}^{-1}$, $Q_{\text{mid}} = 1.00 \text{ mL h}^{-1}$, and $Q_{\text{out}} = 3.00 \text{ mL h}^{-1}$). Scale bars, 500 μm .

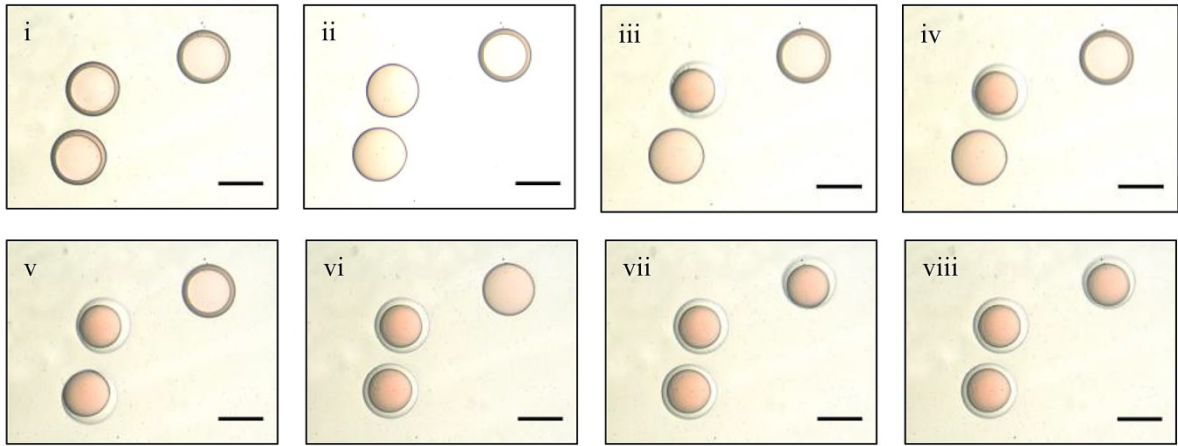


Fig. S5 Off-chip releasing process for double emulsion droplets with an average density equal to the density of the continuous phase ($\rho_{\text{Double}} = \rho_{\text{PEG}}$), the double emulsion droplets suspend in the continuous phase, keep stable for longer time and then separate ($Q_{\text{in}} = 0.50 \text{ mL h}^{-1}$, $Q_{\text{mid}} = 0.50 \text{ mL h}^{-1}$, and $Q_{\text{out}} = 1.00 \text{ mL h}^{-1}$). Scale bars, 500 μm .

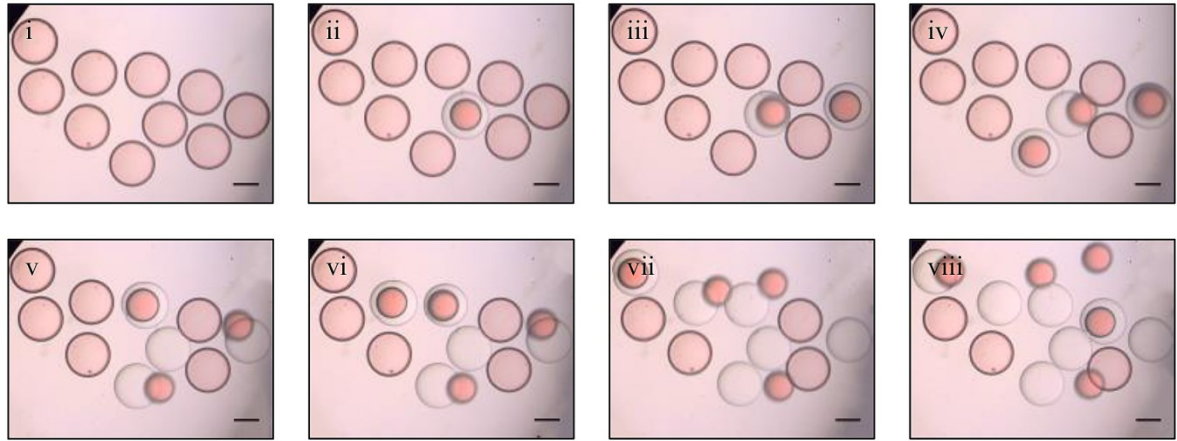


Fig. S6 Off-chip releasing process for double emulsion droplets with an average density higher than the density of the continuous phase, the heavier double emulsion droplets sink to the bottom of the collection container and then separate into oil-in-water (O/W2) droplets and ATPS (W1/W2) droplets at the bottom surface of the container ($Q_{in}= 2.00 \text{ mL h}^{-1}$, $Q_{mid}= 1.00 \text{ mL h}^{-1}$, and $Q_{out}= 5.00 \text{ mL h}^{-1}$). Scale bars, 500 μm .

II Supplementary Tables

Table S1 Properties of the ATPS systems and middle oil phases used in the experiments.

System	Inner Phase	Middle Oil Phase	Outer Phase	Interfacial tension	Spreading Parameter
System I	Dextran-rich phase (25%)		PEG-rich phase (15%)	$\gamma_{W1/W2} = 0.103 \text{ mN m}^{-1}$	
	$\rho = 1138.9 \text{ kg m}^{-3}$		$\rho = 1062.6 \text{ kg m}^{-3}$	$\gamma_{W1/O} = 26 \text{ mN m}^{-1}$	$S_0 = -57.757 \text{ mN m}^{-1} < 0$
	$\mu = 44.05 \text{ mPa s}$		$\mu = 11.043 \text{ mPa s}$	$\gamma_{W2/O} = 25.86 \text{ mN m}^{-1}$	
System II	Dextran-rich phase (25%)		PEG-rich phase (20%)	$\gamma_{W1/W2} = 0.164 \text{ mN m}^{-1}$	
	$\rho = 1155 \text{ kg m}^{-3}$	Silicone oil	$\rho = 1059 \text{ kg m}^{-3}$	$\gamma_{W1/O} = 26.05 \text{ mN m}^{-1}$	$S_0 = -51.906 \text{ mN m}^{-1} < 0$
	$\mu = 69.54 \text{ mPa s}$	$\rho = \sim 960.2 \text{ kg m}^{-3}$	$\mu = 13.29 \text{ mPa s}$	$\gamma_{W2/O} = 26.02 \text{ mN m}^{-1}$	
System III	Dextran-rich phase (20%)		PEG-rich phase (15%)	$\gamma_{W1/W2} = 0.064 \text{ mN m}^{-1}$	
	$\rho = 1130.3 \text{ kg m}^{-3}$	$\mu = \sim 100 \text{ mPa s}$	$\rho = 1057.1 \text{ kg m}^{-3}$	$\gamma_{W2/O} = 26.49 \text{ mN m}^{-1}$	$S_0 = -55.596 \text{ mN m}^{-1} < 0$
	$\mu = 32.12 \text{ mPa s}$		$\mu = 8.2625 \text{ mPa s}$	$\gamma_{W1/O} = 29.17 \text{ mN m}^{-1}$	
System IV	PEG-rich phase (15%)		Dextran-rich phase (25%)	$\gamma_{W1/W2} = 0.103 \text{ mN m}^{-1}$	
	$\rho = 1062.6 \text{ kg m}^{-3}$		$\rho = 1138.9 \text{ kg m}^{-3}$	$\gamma_{W1/O} = 25.86 \text{ mN m}^{-1}$	$S_0 = -57.757 \text{ mN m}^{-1} < 0$
	$\mu = 11.043 \text{ mPa s}$		$\mu = 44.05 \text{ mPa s}$	$\gamma_{W2/O} = 26 \text{ mN m}^{-1}$	
System V	Dextran-rich phase (25%)	Silicone oil	PEG-rich phase (15%)	$\gamma_{W1/W2} = 0.103 \text{ mN m}^{-1}$	
	$\rho = 1138.9 \text{ kg m}^{-3}$	$\rho = \sim 960.2 \text{ kg m}^{-3}$	$\rho = 1062.6 \text{ kg m}^{-3}$	$\gamma_{W2/O} = 25.18 \text{ mN m}^{-1}$	$S_0 = -52.057 \text{ mN m}^{-1} < 0$
	$\mu = 44.05 \text{ mPa s}$	$\mu = \sim 10 \text{ mPa s}$	$\mu = 11.043 \text{ mPa s}$	$\gamma_{W1/O} = 26.98 \text{ mN m}^{-1}$	
System VI	Dextran-rich phase (25%)	PDMS oil (1:1)	PEG-rich phase (15%)	$\gamma_{W1/W2} = 0.103 \text{ mN m}^{-1}$	
	$\rho = 1138.9 \text{ kg m}^{-3}$	$\rho = \sim 960.2 \text{ kg m}^{-3}$	$\rho = 1062.6 \text{ kg m}^{-3}$	$\gamma_{W2/O} = 22.75 \text{ mN m}^{-1}$	$S_0 = -43.837 \text{ mN m}^{-1} < 0$
	$\mu = 44.05 \text{ mPa s}$	$\mu = \sim 275 \text{ mPa s}$	$\mu = 11.043 \text{ mPa s}$	$\gamma_{W1/O} = 21.19 \text{ mN m}^{-1}$	

III Supplementary Movies

Movie S1: ATPS thread without the middle oil phase.

The video shows the formation of a stable ATPS thread without introducing the middle oil phase. The ATPS thread generates at the flow rates of $Q_{in}=0.50$, $Q_{mid}=0.00$ and $Q_{out}= 5.00$ mL h⁻¹. The Video is recorded at 500 frames per second (fps) and played at 10 fps.

Movie S2: The transient W1/O/W2 double emulsion generation.

The video shows the transient W1/O/W2 double emulsion generation when introducing a middle oil phase. The W1/O/W2 double emulsion droplets are generated at the flow rates of $Q_{in}=0.50$, $Q_{mid}=0.50$ and $Q_{out}= 5.00$ mL h⁻¹, respectively. The Video is recorded at 500 fps and played at 10 fps.

Movie S3: The four generation regimes with transient double emulsion technique.

The video shows the four generation regimes: oil-chopper regime, thread regime, double emulsion (with one core) regime and double emulsion (with more cores) regime by varying the flow rate of the middle oil phase from 0.20 to 1.80 mL h⁻¹ while keeping the inner and outer phases flow rates at $Q_{in}=0.50$ and $Q_{out}= 3.00$ mL h⁻¹, respectively. The Video is recorded at 500 fps and played at 10 fps.

Movie S4: ATPS droplets generation by on-chip separation of the transient W1/O/W2 double emulsion for low viscous middle oil phase.

The video shows the on-chip dewetting process of the generated transient W1/O/W2 double emulsion droplets when using low viscous oil (~10 mPa s silicone oil) as the middle oil phase. The flow rates of the inner, middle and outer phases are $Q_{in}=0.50$, $Q_{mid}=0.50$ and $Q_{out}= 3.00$ mL h⁻¹, respectively. The Video is recorded at 1500 fps and played at 10 fps.

Movie S5: ATPS droplets generation by off-chip dewetting of the transient W1/O/W2 double emulsion (State 1: rising).

The video shows the off-chip dewetting process of the collected W1/O/W2 double emulsion for ~100 mPa s silicone oil system, where the W1/O/W2 double emulsion droplets are generated at the flow rates of $Q_{in}=0.20$, $Q_{mid}=1.00$ and $Q_{out}= 3.00$ mL h⁻¹, respectively. The Video is recorded at 24 fps and played at 96 fps.

Movie S6: ATPS droplets generation by off-chip dewetting of the transient W1/O/W2 double emulsion (State 2: suspending).

The video shows the off-chip dewetting process of the collected W1/O/W2 double emulsion for ~100 mPa s silicone oil system, where the W1/O/W2 double emulsion droplets are generated at the flow rates of $Q_{in}=0.50$, $Q_{mid}=0.50$ and $Q_{out}= 1.00$ mL h⁻¹, respectively. The Video is recorded at 24 fps and played at 96 fps.

Movie S7: ATPS droplets generation by off-chip dewetting of the transient W1/O/W2 double emulsion (State 3: sinking).

The video shows the off-chip dewetting process of the collected W1/O/W2 double emulsion for ~100 mPa s silicone oil system, where the W1/O/W2 double emulsion droplets are generated at the flow rates of $Q_{in}=2.00$, $Q_{mid}=1.00$ and $Q_{out}= 15.00$ mL h⁻¹, respectively. The Video is recorded at 24 fps and played at 96 fps.

Movie S8: Dewetting process of the transient W1/O/W2 double emulsion for high viscous PDMS oil system.

The video shows the dewetting process of the collected W1/O/W2 double emulsion for PDMS oil system. The Video is recorded and played at 25 fps.