Supporting Information for

Rapid Fabrication of MOF-based Mixed Matrix Membranes through Digital Light Processing

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Figure S1. Chemical schemes and corresponding codes for photopolymerizable oligomers used in this study: (A) ethoxylated-4-bisphenol-A-dimethacrylate (E-component), (B) aliphatic urethane dimethacrylate (U-component), (C) trimethylolpropane trimethacrylate (Tcomponent) and (D) amine modified polyether acrylate (**P**-component).



Figure S2. Chemical scheme of photoinitiator Irgacure®-819.

Table S1. Summary of photopolymerizable systems and MIL-53(A1)-NH₂/MMA containing ink formulations.

Entry	Sample code	Commercial oligomer ^{a)}		Photoinitiator	MIL-53-NH ₂ /MMA
		1 st [wt.%]	2 nd [wt.%]	Irgacure [®] -819 [wt.%]	[wt.%]
1	T-comp.	98	_	2	-
2	P-comp.	98	-	2	-
3	U-comp.	98	-	2	-
4	E-comp.	98	_	2	-
5	2/3 T +1/3U -comps.	65	33	2	-
6	2/3 T +1/3 E -comps.	65	33	-	-
7	T / MIL-53-NH ₂ /MMA	86	_	2	12
8	P / MIL-53-NH ₂ /MMA	86	_	2	12
9	U / MIL-53-NH ₂ /MMA	86	_	2	12
10	E / MIL-53-NH ₂ /MMA	86	_	2	12
11	2/3 T +1/3E / MIL-53-NH ₂ /MMA	58	28	2	12

^{a)} Acrylate systems contain 4-methoxyphenol as a stabilizer (~ 500-600 ppm)



Figure S3. Scheme of 3D printer with DLP configuration.

The DLP printer setup consists of three main components: the projector, the resin basin (vat) and the build platform. The projector is placed under the transparent vat. The build platform enters the vat from the top and can be moved upwards to "pull" the print out of the vat layer by layer.

The build platform is positioned one layer height above the vat floor	Then, the projector exposes the first layer projection	The build platform moves up to separate the freshly cured laye from the vat floor	After the build platform has moved back by one layer + height	The projector exposes the next layer projection	The steps 1-5 will continue until the model is finished

Figure S4. The six-step printing process using 3D DLP printer.

Specifications		DLP Kudo3D Titan 2	
	Machine size	40.9 cm × 34.8 cm × 85.3 cm	
	Weight	13.6 kg	
Hardware	Resin container	Flexible PSP	
Haluwale	Linear stage module	THK's high precision	
	Projector	ACER H5360 LED DLP projector with a 2 cm native 1920 × 1080 DMD chip by Texas Instruments	
	XY resolution	38 – 92 μm	
	Finest Z resolution	5 µm	
Printing properties	Maximum build size	XY: 92 μm resolution 17.5 cm × 9.6 cm × 24.9 cm XY: 100 μm resolution 19.0 cm × 10.9 cm × 24.9 cm	
	Maximum print speed (for XY = 50 μm and Z = 100 μm)	6.86 cm/h	
	Control software	Web-based	
Control	Connectivity	LAN cable	
	Printer control	PC	
Collibration and assembly	Pre-calibration	At 50 μm / 75 μm	
	Assembly	Fully assembled body	

 Table S2. Technical characteristics of 3D DLP printer Kudo3D model Titan 2.



Figure S5. (A) Spectral irradiance of the 3D printer light source as a function of the distance (B) between the printer light source and resin vat.

Table S3. Typical operative parameters for DLP 3D printing used in this study.

Parameter	Value
Exposure time	10 [s]
Layer thickness	50 [µm]
Lifting height	3.5 [mm]
Lifting speed	10 [mm·min ⁻¹]
Projected width	28 [mm]
Projected length	49.8 [mm]
Projected area	1393.7 [mm ²]
Temperature	RT
Light intensity	212.5 [mW⋅cm ⁻²]

d [cm]	P [mW⋅cm²]
2	566.6
3	240.3
4	212.5
5	164.3
6	137.3

Table S4. Summary of power density of the 3D printer light source as a function of the separation distance between the printer light source and resin vat.



Figure S6. TEM images of MIL-53(Al)-NH₂ (A) and MIL-53(Al)-NH₂/MMA (B). Thermogravimetric curves in air atmosphere (C) and N₂ adsorption isotherms (D) for MIL-53(Al)-NH₂ and MIL-53(Al)-NH₂/MMA.



Figure S7. Particle size distributions of MIL-53(Al)-NH₂ nanoparticles measuring (A) length (mean of 95 ± 24 nm) or (B) width (mean of 28 ± 13 nm). Measurements were performed on several TEM images accounting of more than 100 particles.



Figure S8. Solid-state one-dimensional ¹H MAS NMR spectrum of MIL-53(Al)-NH₂ before post-synthetic modification.



Figure S9. Solid state 2D 1 H MAS DQ-SQ NMR correlation spectrum for MIL-53(A1)-NH₂ before post-synthetic modification.



Figure S10. Solid-state one-dimensional ¹³C CP-MAS NMR spectrum of MIL-53(Al)-NH₂ before post-synthetic modification.



Figure S11. Solid-state two-dimensional (2D) ¹³C-¹H heteronuclear single quantum correlation NMR spectrum of MIL-53(Al)-NH₂ before post-synthetic modification.



Figure S12. Solid-state ¹H MAS NMR spectrum of MIL-53(Al)-NH₂/MMA after postsynthetic modification. Characteristic resonances expected to be in PSM material with MMA moiety are shown in color.



Figure S13. Solid-state 2D ¹H MAS DQ-SQ NMR correlation spectrum of MIL-53(Al)-NH₂/MMA after post-synthetic modification.



Figure S14. Solid-state ¹³C CP-MAS NMR spectrum of MIL-53(Al)-NH₂/MMA after post-synthetic modification.



Figure S15. Solid-state two-dimensional (2D) ¹³C-¹H heteronuclear single quantum spectrum of MIL-53(Al)-NH₂/MMA after post-synthetic modification.



Figure S16. Solid-state DNP enhanced ¹H NMR spectrum of MIL-53(Al)-NH₂ before postsynthetic modification with and without DNP microwave applied.



Figure S17. Solid-state DNP enhanced ¹⁵N NMR spectrum of MIL-53(Al)-NH₂ before post-synthetic modification.



Figure S18. Solid-state DNP enhanced ¹H NMR spectrum of MIL-53(Al)-NH₂/MMA after post-synthetic modification with and without DNP microwave applied.



Figure S19. Solid-state DNP enhanced ¹⁵N NMR spectrum of MIL-53(Al)-NH₂/MMA after post-synthetic modification.



Figure S20. Solid-state DNP enhanced ¹⁵N-¹H CP-MAS HETCOR NMR spectrum of MIL-53(Al)-NH₂/MMA after post-synthetic modification.

Sample	Surface area [m ² ·g ⁻¹]			TGA
Sample	SBET	Smicro	S _{ext} ^{a)}	∆ <i>m/m</i> ₀ [%] ^{♭)}
MIL-53(AI)-NH ₂	370	150	220	68
MIL-53(AI)-NH ₂ /MMA	303	43	260	80

Table S5. TGA and Ar physisorption data for MIL-53(Al)-NH₂ and MIL-53(Al)-NH₂/MMA.

^{a)} Mesopore surface area is obtained from the *t*-plot applied to the Ar isotherm; ^{b)} Value corresponds to the mass loss step observed on thermogravimetric curve in region 350-600 $^{\circ}$ C



Figure S21. FTIR spectra of MIL-53(Al)-NH $_2$ before (a) and after (b) post-synthetic modification with MMA group.



Figure S22. Liquid state ¹H NMR spectrum of MIL-53(Al)-NH₂/MMA digestion crude in DMSO-d6.



Figure S23. Schematic representation of MIL-53(Al)-NH₂ nanoparticle with ~95 nm × 28 nm × 28 nm dimensions (Figure S7) and unit cell arrangement of *np*-form of the framework with respect to the crystal faces. Image showing the surface fraction of the linkers (20%) exposed to PSM and structure orientation within unit cell respective to the nanocrystal facets.

Component	Sample code	Viscosity [cP]
SR350D	Т	65.7
CN501	Р	65
SR540	E	575
CN1963	U	1740

Table S6. Viscosity of commercial photopolymerizable methacrylic systems at 25 °C.



Figure S24. ATR-FTIR spectra for T-, P-, E- and U-components with the highlight of characteristic C=C stretching (\sim 1640 cm⁻¹) of methacrylic group.

Components		Sample code	V total ro/ 1	14
Comm.	MOF	Sample code	∧MMA [70]	VXMMA*** [76'S]
SR350D	-	Т	27	1.50
CN501	-	Р	25	2.40
SR540	-	Е	24	1.55
CN1963	-	U	15	0.75
SR350D	MIL-53-NH ₂ /MMA	T/MIL-53-NH ₂ /MMA	30	0.55
CN501	MIL-53-NH ₂ /MMA	P/MIL-53-NH ₂ /MMA	27	0.50
SR540	MIL-53-NH ₂ /MMA	E/MIL-53-NH ₂ /MMA	25	0.39

Table B7. Data of kinetic characteristics of photopolymerizable systems with and without MOF additive.



Figure S25. Methacrylate group conversion (X_{MMA} , %) curves for formulations containing MIL-53(Al)-NH₂/MMA and different oligomers.



Figure S26. Raman map with the selected (A) and (B) pixels on the color scaled confocal microscopy map (inset) and Raman spectra (A) and (B) corresponding to these pixels. Dashed lines indicate the analyzed intensities: for the map shown in Figure 4A, the intensity corresponding to C-(C=O)-O (~ 600 cm⁻¹) symmetric stretching (D) in the MMA moieties involved in copolymerization was considered, whereas the map depicted on Figure 4B (and top left in above figure) was build based on relative intensities of the aromatic ring C-C chain vibration (1450 cm⁻¹) of the MOF's linker and C=O symmetric stretching (1730 cm⁻¹) (C) of the copolymerized moieties in the composite.



Figure S27. CO_2 adsorption isotherms of (A) membranes 3D printed from T-, P-, E- and Ucommercial oligomers and T+U mixture, and (B) of membranes 3D printed from MIL-53(Al)-NH₂/MMA containing ink mixtures acquired at 273 K. Filled symbols correspond to the adsorption branch and open symbols to the desorption.

Sample code	ε _R [%] ^{a)}	σ _R [MPa] ^{b)}	Young's modulus [GPa]	tan δ [–] $^{\circ)}$	δ [°] ^{d)}
U -comp	0.67	50.6	7.6	0.092	5.25
T-comp	1.82	47.8	2.7	0.081	4.66
T / MIL-53-NH ₂ /MMA	1.20	26.0	2.2	0.076	4.36
P-comp	2.15	68.3	3.3	0.112	6.42
P / MIL-53-NH ₂ /MMA	1.25	44.4	3.6	0.091	5.20
E-comp	2.75	30.2	1.1	0.120	6.86
E / MIL-53-NH ₂ /MMA	0.80	11.9	1.6	0.113	6.47
2/3T+1/3E-comps	1.58	31.3	2.0	0.080	4.59
2/3T+1/3E / MIL-53-NH ₂ /MMA	1.04	25.9	2.5	0.071	4.06

Table S8. Mechanical data of photopolymerizable systems and MIL-53(Al)-NH₂/MMA contained ink formulations.

^{a)} Strain at break (ε_R , %); ^{b)} Stress at break (σ_R , MPa); ^{c)} Phase difference in stress and strain (δ , degrees); ^{d)} Damping factor (tan δ).

Mechanical analyses were performed on stress-strain data curves determining the strain at break (ε_R) and stress at break (σ_R) values by extrapolating the last point of the curve on abscise and ordinate axes, respectively.

Young's modulus was determined from corresponding stress-strain curves as a slope coefficient on the linear fits.

The damping properties of the composites during tension or compression were expressed in terms of the stress and strain relations, and defined by following Equation S1:

$$\tan \delta = \frac{E''}{E'} \tag{S1}$$

where tan δ is so-called damping factor, E'' and E' are loss modulus and storage modulus, respectively.



Figure S28. Micrographs of 3D printed composites containing MIL-53(Al)-NH₂/MMA in T-(A), P- (C) and E-matrix (E) under reflected light and (B, D, F) the same under crossed polarizers.



Figure S29. SEM-EDX maps of T/MIL-53(Al)-NH₂/MMA 3DP composite: (A) top view survey image and corresponding to Al (C), O (D), P (E), C (F) *K*-edges maps. (B) SEM image of the membrane and two locations used for the elemental analysis. (G) Cross-section view of the membrane and (H) survey image with the analyzed region for Al (I), N (J), C (K) and O (L) mappings.

	Relative m	nass [%]
Element	Point 1 (P1)	Point 2 (P2)
AI	1.42	1.81
С	76.81	69.54
0	21.47	28.49
Ρ	0.30	0.16

Table S9. Elemental analysis data derived obtained by EDX from the two locations of 3DP membrane according to Figure S29B.

Table S10. Degree of the crosslinking (DC, %) of photopolymerizable systems with and without MOF additive.

Components			
Comm.	MOF	- Sample code	DC [%]
SR350D	-	т	96.2
CN501	-	Ρ	97.4
SR540	-	E	99.7
CN1963	-	U	93.6
SR350D	MIL-53-NH ₂ /MMA	T/MIL-53-NH ₂ /MMA	93.9
CN501	MIL-53-NH ₂ /MMA	P/MIL-53-NH ₂ /MMA	94.7
SR540	MIL-53-NH ₂ /MMA	E/MIL-53-NH ₂ /MMA	92.8

	Components				
Components		- Sample code	T _d [°C]	T_g [°C]	∆ <i>m/m</i> ₀ [%]
Comm.	MOF				
SR350D	_	т	461.0	155.7	96.5
CN501	_	Ρ	432.5	84.4	98.0
SR540	-	E	428.0	180.4	97.3
CN1963	-	U	387.5	173.6	99.4
SR350D	MIL-53-NH ₂ /MMA	T/MIL-53-NH ₂ /MMA	438.0	145.3	87.3
CN501	MIL-53-NH ₂ /MMA	P/MIL-53-NH ₂ /MMA	429.5	79.5	89.7
SR540	MIL-53-NH ₂ /MMA	E/MIL-53-NH ₂ /MMA	432.5	190.3	86.3

Table S11. Thermogravimetric (TGA) and differential scanning calorimetry (DSC) data for photopolymerizable inks with and without MOF additive.

 T_d - temperature at which a maximum mass loss velocity is observed; T_g – glass transition temperature; Δm – total mass loss in air atmosphere.

Table S12. Summary of gas separation performance obtained with 3DP polymer and 3DP MOF-polymer composite membranes (12 wt.% MOF loading) under several operation conditions.

Membrane	T-comp.		T + MIL-53-NH₂/MMA	
Thickness (µm)	48 ± 2		57 ± 1	
Temperature	323 K	373 K	323 K	373 K
ΔP (bar)	1	1	1	1
P _{H2} (Barrer)	9.4 ± 0.4	42 ± 13	229 ± 79	501 ± 82
P _{CO2} (Barrer)	4.8 ± 1.4	40 ± 9	120 ± 14	346 ± 87
H ₂ /CO ₂ selectivity (-)	1.9 ± 0.5	1.1 ± 0.1	1.9 ± 0.6	1.5 ± 0.2