

Electronic Supplementary Material (ESI) for Materials Horizons.

Mineral Plastic Foams

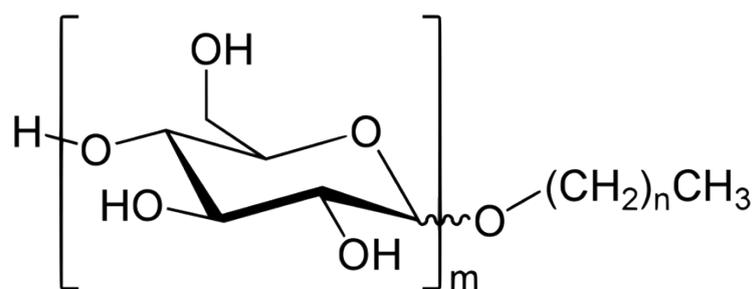
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Scheme S1: Molecular structure of alkyl polyglucosides (C_nG_m). In our case $m = 1.5$, $n = 8-16$.

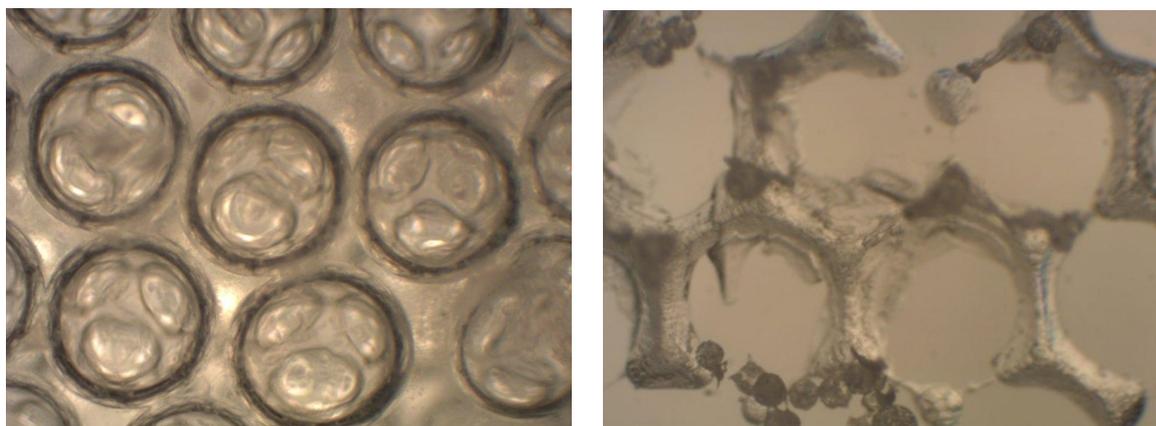


Figure S1: (left) Optical microscope image of the foamed liquid precursor, which was foamed via microfluidics and consisted of 0.1 M PAA, 0.1 M $CaCl_2$, and 0.5 wt% Plantacare® 2000 UP. The separation of the bubbles (round shape) can be clearly seen. (right) Optical microscope image of the dried solid foam, so-called mineral plastic foam. For solidification a 0.1 M sodium carbonate solution was added to the liquid foam and subsequently dried in air. A homogeneous solid foam cannot be formed due to the low amount of PAA.

Powder X-Ray Diffraction: Powder X-Ray Diffraction (PXRD) measurements were carried out on a Bruker D8 Discover device equipped with a Vantec detector.

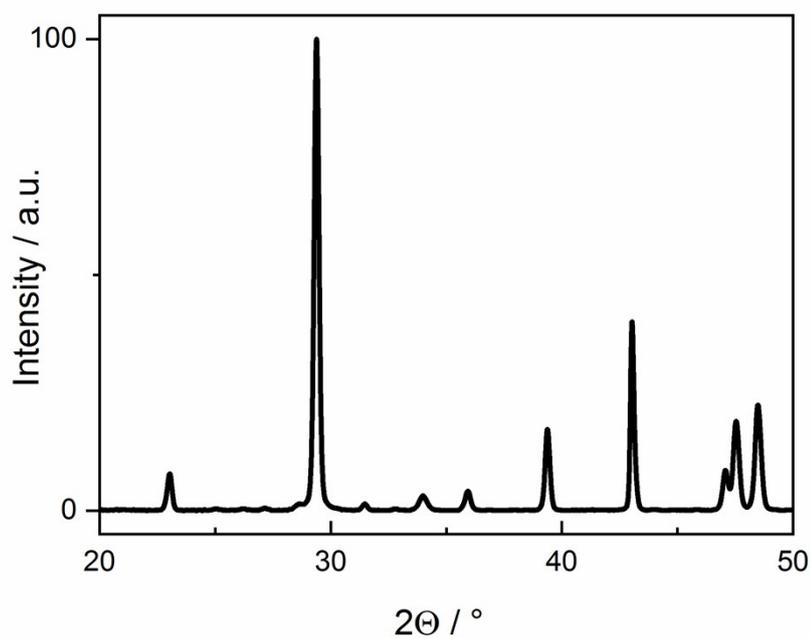


Figure S2: X-ray diffractogram of the white precipitate formed instead of mineral plastic. The precipitate was obtained by using a 1:10 mass ratio between sample and 4.0 M lithium hydroxide solution for the deprotonation of the PAA. The XRD pattern with peaks at 2Θ of 23.1° , 29.3° , 35.9° , 39.4° , 43.2° , 47.4° , and 48.4° , indicates that the sample is calcite. ¹

Mechanical Properties: Mechanical compression tests were carried out with the zwickiLine 5 kN universal testing machine from Zwick / Roell, which was equipped with a 5 kN force transducer and was regulated by the testXpert III software. The stress-strain curves were obtained with normal forces and a test speed of 1 mm min^{-1} . A pre-force of 5.0 N was chosen to obtain a flat sample surface that was uneven from cutting with a scalpel. The slope of the linear part at the beginning of the stress-strain curve (cf. dashed regression line in Fig. S3) was used to determine the Young's modulus E . It holds

$$E = \frac{\sigma}{\varepsilon} = \frac{F \cdot I_0}{A \cdot \Delta I} \quad (1)$$

with σ being the stress (force F acting on a cross-sectional area A) and ε being the strain (difference ΔI between the sample height before compression I_0 and after compression I).² We obtained $E = 48.26 \pm 0.19 \text{ MPa}$ for a cube-shaped mineral plastic foam sample with a density of $327 \pm 31 \text{ kg m}^{-3}$.

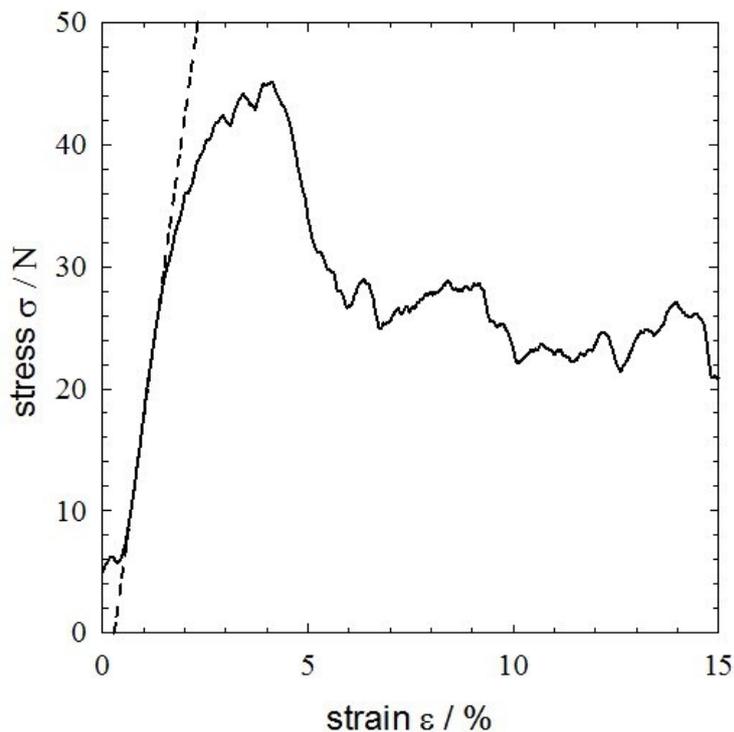


Figure S3: Stress (σ) - strain (ε) curve with a pre-set force of 5.0 N for a cube-shaped mineral plastic foam sample with a density of $(327 \pm 31) \text{ kg m}^{-3}$. The Young's modulus of $(48.3 \pm 0.2) \text{ MPa}$ was determined from the slope of the linear part (dashed curve) at the beginning of the stress-strain curve.

Solid foams have been studied extensively and there is general agreement that the relative Young's modulus ($E_{foam}/E_{polymer}$) is proportional to the squared relative density ($\rho_{foam}/\rho_{polymer}$)². It holds for open-pore systems

$$\frac{E_{foam}}{E_{polymer}} = C_c \cdot \left(\frac{\rho_{foam}}{\rho_{polymer}} \right)^2 \quad (2)$$

with $C_c \sim 1$ according to Gibson and Ashby.²⁻⁴ Using $E_{polymer} = (380 \pm 2)$ MPa (experimental stress-strain curve not shown) and $\rho_{polymer} = (1117 \pm 4)$ kg m⁻³, one obtains a relative elastic modulus ($E_{foam}/E_{polymer}$) of 0.127 and a relative squared density ($\rho_{foam}/\rho_{polymer}$)² of 0.086. The resulting proportionality factor $C_c \sim 1.5$ is in the usual range.

References

1. C. G. Kontoyannis and N. V. Vagenas, *Analyst*, 2000, **125**, 251.
2. L. J. Gibson, M. F. Ashby, *Cellular Solids, Structures and Properties*, Cambridge University Press, Cambridge 1999.
3. L. J. Gibson, *J. Biomech.* 2005, 38, 377.
4. M. Ashby, R. M. Medalist, *Metall. Trans. A* 1983, 14A, 1755.