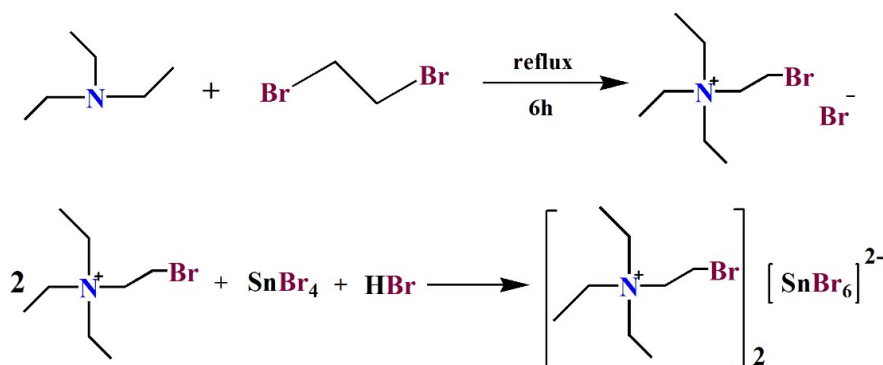


Multisequential reversible phase transition materials with Semiconducting and fluorescence properties : $(C_8H_{18}BrN)_2SnBr_6$

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Scheme 1. Schematic diagrams of synthesis of compound 1

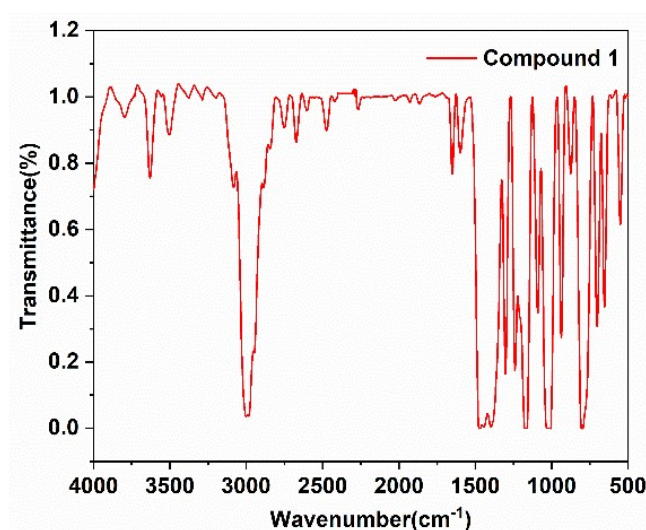


Fig. S1 Infrared spectrum of compound 1

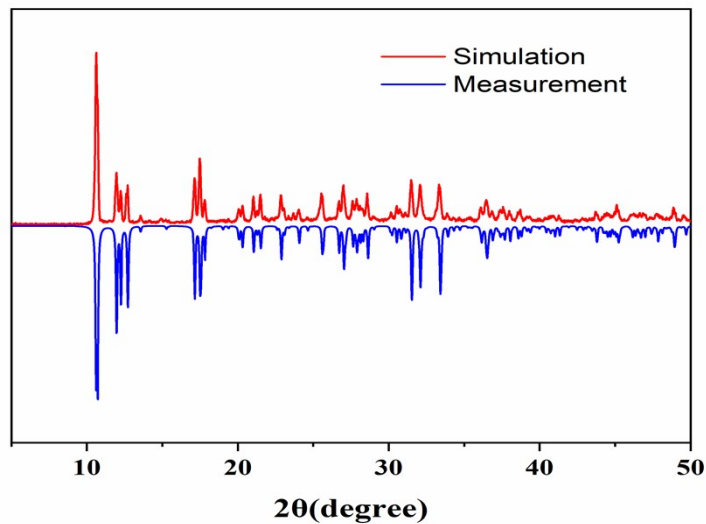


Fig. S2 The powder XRD of 1.

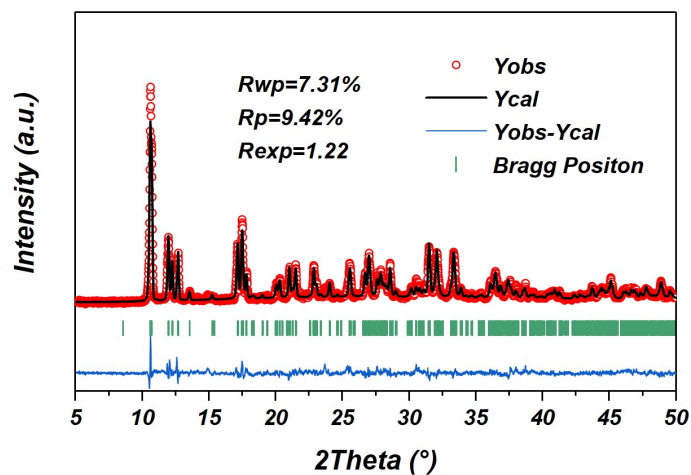


Fig. S3 Powder X-ray diffractograms of 1 collected in 300 K (LTP), refined by Le Bail method using the FULLPROF program. The lattice parameters obtained from the fitting: $a=14.4563(9)$, $b=14.7985(3)$, $c=13.9563(5)$ Å ($R_p=7.31\%$, $R_{wp}=9.42\%$, $R_{exp}=1.22\%$).

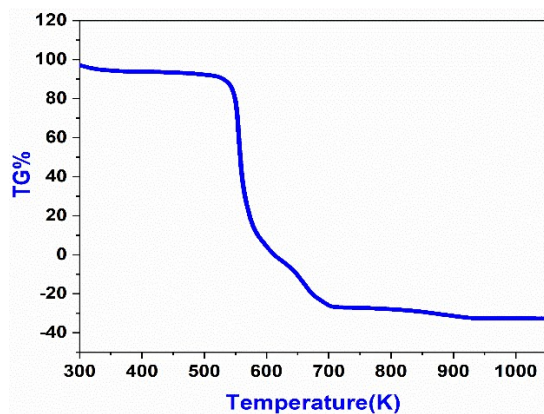


Fig. S4 TG-DTA curves for 1.

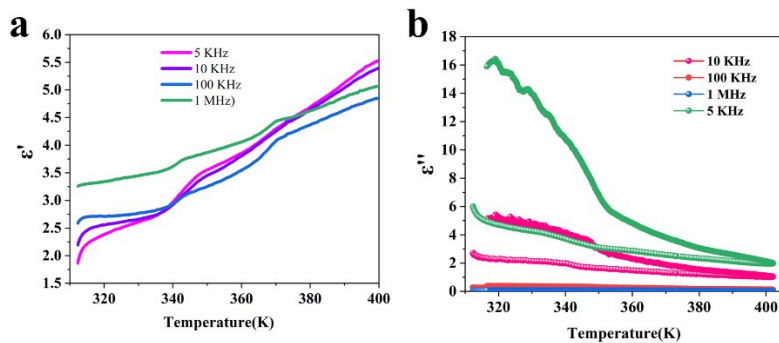


Fig. S5 (a) The frequency dependence of the dielectric of compound **1** during heating. (b) Temperature-dependent imaginary part (ϵ'') of the permittivity of **1** measured at selected frequencies in heating and cooling modes

Table.S1 Crystal data and refinement parameters for **1**

Compound	1
Empirical formula formula	$C_{16}H_{36}Br_8N_2Sn$
Temperature (K)	300 K
Crystal system	monoclinic
Space group	$C2/c$
a (Å)	14.4401(14)
b (Å)	14.7764(13)
c (Å)	13.9147(12)
$\alpha/^\circ$	90
$\beta/^\circ$	90.855(3)
$\gamma/^\circ$	90
V (Å ³)	2968.7(5)
Z	4
ρ calcg/cm ³	2.270
μ /mm ⁻¹	11.636
F(000)	1904.0
$R_1, wR_2[I > 2\sigma(I)]$	$R_1 = 0.0655, wR_2 = 0.1322$
$R_1, wR_2(\text{all data})$	$R_1 = 0.1151, wR_2 = 0.1596$

Calculation of ΔS and N

The first stage :

In the heating cycle mode

$$\Delta S_H = R \ln N$$

$$\Delta S_H = \int_{T_2}^{T_1} \frac{Q}{T} dT$$

$$\approx \frac{\Delta H}{T_c}$$

$$= \frac{4.300 \text{ J}^{-1} \text{ mol} \times 1014.44 \text{ g}^{-1} \text{ mol}}{353 \text{ K}}$$

$$= 12.36 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$$

$$N_I = \exp\left(\frac{\Delta S_I}{R}\right) = \exp\left(\frac{12.36 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}{8.314 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}\right)$$

$$= 4.410$$

In the cooling cycle mode

$$\Delta S_C = R \ln N$$

$$\Delta S_C = \int_{T_2}^{T_1} \frac{Q}{T} dT$$

$$\approx \frac{\Delta H}{T_c}$$

$$= \frac{4.104 \text{ J}^{-1} \text{ mol} \times 1014.44 \text{ g}^{-1} \text{ mol}}{345 \text{ K}}$$

$$= 12.07 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$$

$$N_2 = \exp\left(\frac{\Delta S_C}{R}\right) = \exp\left(\frac{12.07 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}{8.314 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}\right)$$

$$= 4.263$$

$$\Delta S_H = R \ln N_I$$

$$\Delta S_H = \int_{T_2}^{T_1} \frac{Q}{T} dT$$

$$\approx \frac{\Delta H}{T_c}$$

$$= \frac{4.300 \text{ J}^{-1} \text{ mol} \times 1014.44 \text{ g}^{-1} \text{ mol}}{353 \text{ K}}$$

$$= 12.36 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$$

$$N_I = \exp\left(\frac{\Delta S_H}{R}\right) = \exp\left(\frac{12.36 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}{8.314 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}\right)$$

$$=4.410$$

In the heating cycle mode

$$\Delta S_H = R \ln N_1$$

$$\Delta S_H = \int_{T_2}^{T_1} \frac{Q}{T} dT$$

$$\approx \frac{\Delta H}{T_c}$$

$$= \frac{0.854 \text{ J}^{-1} \text{ mol} \times 1014.44 \text{ g}^{-1} \text{ mol}}{384 \text{ K}}$$

$$= 2.25 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$$

$$N_1 = \exp\left(\frac{\Delta S_H}{R}\right) = \exp\left(\frac{2.25 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}{8.314 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}\right)$$

$$= 1.310$$

In the cooling cycle mode

$$\Delta S_C = R \ln N_2$$

$$\Delta S_C = \int_{T_2}^{T_1} \frac{Q}{T} dT$$

$$\approx \frac{\Delta H}{T_c}$$

$$= \frac{0.975 \text{ J}^{-1} \text{ mol} \times 1014.44 \text{ g}^{-1} \text{ mol}}{374 \text{ K}}$$

$$= 2.645 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$$

$$N_2 = \exp\left(\frac{\Delta S_C}{R}\right) = \exp\left(\frac{2.645 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}{8.314 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}}\right)$$

$$= 1.374$$