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Supporting Information for

The Construction of Palladium-Hydrogen Accelerated Catalytic Fenton System

Enhanced by UiO-66(Zr)

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Detailed Characterization information of the synthesized UiO-66(Zr)

The FT-IR spectrum of terephthalic acid, which was different from that of the synthesized UiO-66(Zr), was displayed in Fig.S1. The C=C stretch (at 1678 cm⁻¹), the C=O stretching vibration (at 1573 cm⁻¹), O-H in-plane bending vibrations (at 1440-1260 cm⁻¹), C-C aromatic stretch (at 1423 cm⁻¹), C-H in plane ring bending vibrations (at 1300-1000 cm⁻¹), C-O stretch (at 1282 cm⁻¹) and C-H out of plane bending vibration (at 935 and 779 cm⁻¹) were observed. This was consistent with the previous reports. ¹⁻³ Compared with the FT-IR spectrum of synthesized UiO-66(Zr), these typical peaks were not obvious. The peaks of 663 cm⁻¹ and 746 cm⁻¹ corresponded to the vibration of carbon-hydrogen bond and oxygen-hydrogen bond, respectively. The peaks of 1018 cm⁻¹, 1106 cm⁻¹ and 1157 cm⁻¹ corresponded to the stretching vibration of zirconium-oxygen bond, respectively. The peaks of 1506 cm⁻¹ and 1658 cm⁻¹ corresponded to the vibration of carbon-carbon double bond in benzene ring and the carboxyl group, respectively. The peaks of 1398 cm⁻¹ and 1585 cm⁻¹ corresponded to the symmetric/asymmetric stretching vibrations of carboxyl group. It indicated that the terephthalic acid PTA undoubtedly participated in the reaction of preparing UiO-66(Zr). It constituted the skeleton structure of UiO-66(Zr).



Fig.S1 The FT-IR spectrums of synthesized UiO-66(Zr) and terephthalic acid
The XRD pattern of the synthesized UiO-66(Zr) was displayed in Fig.S2. The
characteristic diffraction peaks at 7.29°, 8.42°, 11.92°, 13.99°, 14.61°, 23.98°, 25.46°,
30.40°, 36.31° and 43.98° could be observed. It matched well with the theoretical one
of UiO-66(Zr) produced by using Diamond software with versatile Crystallographic
Information Framework file. ⁴



Fig.S2 The simulated ref. XRD pattern of UiO-66(Zr) and XRD pattern of synthesized UiO-66(Zr)

Control Tests

The adsorption of UiO-66(Zr) for the removal of SMT and 4-CP was displayed in Fig.S3(a). Only 8.17 % of 4-CP and 9.90 % of SMT could be adsorbed by UiO-66(Zr), respectively. After the UiO-66(Zr) was substituted by Pd/UiO-66(Zr), the removal of 4-CP and SMT was lower to 7.54 % and 6.92 %, respectively. According to the characterization of these two materials, after the nano Pd⁰ particle was loaded on the outer surface of UiO-66(Zr), the surface area was reduced. That may be attributed to the occupation of cavities or blocking of the outer surfaces of UiO-66(Zr) by the Pd⁰ particle. Therefore, the adsorption of Pd/UiO-66(Zr) was weaker than that of UiO-66(Zr).

In the current Fenton reaction project in actual operation, the molar ratio of ferrous to hydrogen peroxide is usually 1:2 to 1:20. In this work, the molar ratio of ferrous iron to hydrogen peroxide was 1:800. The molar ratio1:4 of ferrous to hydrogen peroxide were chosen to conduct a controlled experiment. As seen in Fig.S3(b), increasing the dosage of ferrous can promote the production of \cdot OH. And the degradation efficiency of pollutants could be further promoted. Under the condition of 1:4 molar ratio of ferrous to H₂O₂, the SMT could be thoroughly removed in 90 min and the 4-CP could be thoroughly removed in 60 min, while in the MHACF-UiO-66(Zr) system, about 95 % SMT could be removed, and the 4-CP could be thoroughly removed in 120 min. Although under the condition of 1:4 molar ratio, both of the removal efficiency of organics in Fenton reaction system were higher than that of MHACF system, the addition of ferrous in former was 200 times that of the latter. In order to maintain the production of \cdot OH, the ferrous salt must be

continuously added into the Fenton system. The TFe in MHACF-UiO-66(Zr) system was about 25 μ M. It is in accordance with the emission limits for TFe in most countries.⁵ According to the law of conservation of mass and dissolution balance, when the solution pH is adjusted to 6-9 to meet the effluent discharge standard, except a small amount of iron element dissolved in the solution could discharge from the system with the effluent, most of the iron element will form iron sludge precipitation. Therefore, the iron sludge derived from the MHACF-UiO-66(Zr) system was much less than that in Fenton system.





Fig.S3 (a) The Control tests of adsorption; (b) The Control tests of Fenton reaction. The initial parameter was UiO-66(Zr) 2 g·L⁻¹ Pd/UiO-66(Zr) 2 g·L⁻¹, Pd content 0.536 % (W_{Pd} : $W_{Pd/UiO-66(Zr)}$), pH 3, SMT 15 mg·L⁻¹ and 4-CP 10 mg·L⁻¹.

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