# Supporting Information: A General Model <br> for the Ideal Chain Length Distributions of 

## Polymers Made with Reversible Deactivation

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## Experimental

## Materials

All materials were purchased from commercial sources and used as received unless otherwise specified.
Synthesis of phenyl vinyl ketone (PVK) was adopted from a known method and used immediately to prevent degradation. ${ }^{1}$ The synthesis of chain transfer agent 2-[[(dodecylthio)thioxomethyl]thio]-

2-methylpopanoic acid, or (isobutyric acid)yl dodecyl trithiocarbonate (iBADTC) was carried out using a known synthesis procedure in literature. ${ }^{2}$

## Synthesis of PPVK-b-PBA block polymer

In a 25 mL round bottom flask equipped with a magnetic stirrer bar, azobisisobutyronitrile (AIBN) $\left(2.49 \times 10^{-3} \mathrm{~g}, 1.51 \times 10^{-5} \mathrm{~mol}\right)$, iBADTC ( $5.51 \times 10^{-2} \mathrm{~g}, 1.51 \times 10^{-4} \mathrm{~mol}$ ), PVK ( $1.00 \mathrm{~g}, 7.57 \times 10^{-3}$ mol ) and 1.06 g of dioxane were added. The reaction mixture was capped with a rubber septum and deoxygenated with nitrogen for 20 minutes and then stirred overnight at $65^{\circ} \mathrm{C}$. The monomer conversion ( $>98 \%$ ) was confirmed by ${ }^{1} \mathrm{H}-\mathrm{NMR}$, giving the PPVK homopolymer.

To the previously prepared PPVK polymer mixture, azobisisobutyronitrile (AIBN) ( $2.49 \times 10^{-3} \mathrm{~g}$, $\left.1.51 \times 10^{-5} \mathrm{~mol}\right)$, BA $\left(9.70 \times 10^{-1} \mathrm{~g}, 7.57 \times 10^{-3} \mathrm{~mol}\right)$ and 1.00 g of dioxane was added. The mixture was mixed, and deoxygenated with nitrogen for 20 minutes and then stirred overnight at $65^{\circ} \mathrm{C}$. The monomer conversion ( $>98 \%$ ) was confirmed by ${ }^{1} \mathrm{H}-\mathrm{NMR}$.

## NMR

${ }^{1} \mathrm{H}$ were obtained on a Bruker AV500 Ultra Shield ( 500 MHz ) or Bruker Avance NEO 400i nanobay ( 400 MHz ) spectrometer.

## Size Exclusion Chromatography (SEC)

Size exclusion chromatography of the PPVK homopolymer and PPVK-PBA block copolymer was performed using an Agilent 1260 gel permeation chromatography system equipped with an isocratic pump, an autosampler, a guard and 2x PL Gel Mixed B columns, and a refractive index detector. The eluent was tetrahydrofuran running at $1 \mathrm{~mL} / \mathrm{min}$ at $30^{\circ} \mathrm{C}$. The system was calibrated with poly(methyl methacrylate) standards in the range of 617,000 to 1,010 .

## Supporting Data

Table S1. Degree of polymerization and dispersity for systems with $\mathrm{k}^{*}=0.1$ and varied $\mu_{\text {decap }}$. In all cases $[\mathrm{M}]_{0}=4 \mathrm{M},[\mathrm{P}-\mathrm{X}]=[\mathrm{D}]=0.04 \mathrm{M}$.

| $\mu_{\text {decap }}$ | $\mathrm{DP}_{\mathrm{n}}$ | Dispersity |
| :--- | :--- | :--- |
| 1 | 15.881 | 2.2078 |
| 2 | 25.9576 | 1.611 |
| 3 | 33.8272 | 1.4163 |
| 5 | 46.3431 | 1.2628 |
| 10 | 67.8898 | 1.1399 |
| 20 | 88.8193 | 1.0808 |

Table S2. Degree of polymerization and dispersity for systems with $\mu_{\text {decap }}=5$ and varied $\mathrm{k}^{*}$. In all cases $[\mathrm{M}]_{0}=4 \mathrm{M},[\mathrm{P}-\mathrm{X}]=[\mathrm{D}]=0.04 \mathrm{M}$.

| $\mathrm{k}^{*}$ | $\mathrm{DP}_{\mathrm{n}}$ | Dispersity |
| :--- | :--- | :--- |
| 0.1 | 46.3431 | 1.2628 |
| 0.2 | 71.4329 | 1.2488 |
| 0.4 | 92.6084 | 1.3106 |
| 0.8 | 100.0926 | 1.6775 |
| 0.99 | 100.3238 | 1.9838 |

Table S3. Degree of polymerization and dispersity for systems with constant product of $\mathrm{k}^{*}$ and $\mu_{\text {decap. }}$. In all cases $[\mathrm{M}]_{0}=4 \mathrm{M},[\mathrm{P}-\mathrm{X}]=[\mathrm{D}]=0.04 \mathrm{M}$.

| $\mathrm{k}^{*}$ | $\mu_{\text {decap }}$ | $\mathrm{DP}_{\mathrm{n}}$ | Dispersity |
| :--- | :--- | :--- | :--- |
| 0.1 | 10 | 67.8898 | 1.1399 |
| 0.2 | 5 | 71.4329 | 1.2488 |
| 0.33 | 3 | 74.4598 | 1.4067 |
| 0.5 | 2 | 75.8346 | 1.6649 |
| 0.99 | 1 | 64.1999 | 3.0826 |

## Comparison of Models for Dispersity

The predictions of the developed model, labeled model below are compared to those developed by Goto et al. ${ }^{3}$ using the equation below:

$$
\begin{equation*}
\mathrm{Đ}=1+\frac{1}{D P_{n}}+\left(\frac{2-\text { conversion }}{\text { conversion }}\right)\left(k^{*} \frac{[P-X]}{[D]}\right) \tag{S1}
\end{equation*}
$$



Figure S1: Comparison of dispersities $\left({ }^{\boxplus}\right)$ predicted by the developed model and the model outlined by Goto et al. ${ }^{3}$ a) A RAFT system with $[\mathrm{M}]_{0}=5.5 \mathrm{M},[\mathrm{P}-\mathrm{X}]=[\mathrm{D}]$ determined by the DP and the product of $k^{*} \times \mu_{\text {decap }}$ of 5. b) An ATRP system with $[\mathrm{M}]_{0}=5.5 \mathrm{M}, k^{*}=1.7 \times 10^{-4}$ or $5 \times 10^{-4},[\mathrm{P}-\mathrm{X}]$ determined by the DP and the product of $k^{*} \mu_{\text {decap }} /[\mathrm{D}]$ of ca. 100 for DP 100 systems and 300 for DP 300 systems. c) Cationic system with $[\mathrm{M}]_{0}=0.5 \mathrm{M},[\mathrm{D}]=1$ and $[\mathrm{P}-\mathrm{X}] \times$ $\mu_{\text {decap }}=0.05$ for $k^{*}=80$ and $[\mathrm{P}-\mathrm{X}] \times \mu_{\text {decap }}=0.165$ for $\mathrm{k}^{*}=30$.

## Convolution of two distributions

To predict the outcome of convolving two distributions, where a fraction of the chain length comes from a CTA that gives a narrow distribution and a fraction comes from a CTA that gives a broad distribution, the overall chain length is split by the fraction of CTA loading. For instance if a loading of $f$ of a narrow distribution forming CTA is used with a 1- $f$ fraction of the broad
distribution forming CTA was used, then the simulated traces would assume that of the total chain length, a fraction $f$ of the final chain length came from the narrow distribution forming CTA and $1-f$ came from the broad distribution forming CTA. In this way the final distribution at chain length n can be found by the convolution below and also in eq 29 of the main text:
$P_{\text {con }}\left(n \mu_{\text {decap }, 1}, \mu_{\text {decap }, 2}, k_{1}^{*}, k_{2}^{*},[M]_{0,1},[M]_{0,2},[P-X]_{1},[P-X]_{2},[D]_{1},[D]_{2}\right)=$
$\sum_{i=1}^{n} P_{1}\left(n-i+1 \mid \mu_{\text {decap }, 1}, k_{1}^{*},[M]_{0,1},[P-X]_{1},[D]_{1}\right) P_{2}\left(i \mid \mu_{\text {decap }, 2}, k_{2}^{*},[M]_{0,2},[P-X]_{2},[D]_{2}\right)$


Figure S2: Comparison of experiment, fitted model and convolved polymers. In the convolution one was simulated with $[\mathrm{M}]:[\mathrm{P}-\mathrm{X}]:[\mathrm{D}]=1.4: 0.02: 0.02$ using $\mathrm{k}^{*}=0.128 \& \mu_{\text {decap }}=14.7272$ to match the fraction of 0.35 CTA giving a narrow distribution and the second polymer was
simulated as $[\mathrm{M}]:[\mathrm{P}-\mathrm{X}]:[\mathrm{D}]=2.6: 0.02: 0.02$ using $\mathrm{k}^{*}=0.726 \& \mu_{\text {decap }}=3.2031$ to match the fraction of 0.65 CTA giving a broad distribution.


Figure S3: Effect of $\mu_{\text {decap }}$ on PMMA RAFT polymer of medium dispersity.


Figure S4. ATRP polymer simulated under: $[\mathrm{M}]:[\mathrm{P}-\mathrm{X}]:[\mathrm{D}]=5.5: 3.667 \times 10^{-2}: 1.482 \times 10^{-5}$, with $k^{*}=0.0004$ and $\mu_{\text {decap }}=3.6$.

Table S4: Parameters used to model complex polymers such as blended or block copolymers.

| System | Label | $[\mathrm{M}]:[\mathrm{P}-\mathrm{X}]:[\mathrm{D}]$ | $\mathrm{k}^{*}$ | $\mu_{\text {decap }}$ | $\mathrm{DP}_{\mathrm{n} \text {-Ex }}$ | $\mathrm{Đ}_{\mathrm{Ex}}$ | $\mathrm{DP}_{\mathrm{n}-\mathrm{Th}}$ | $\mathrm{Đ}_{\mathrm{Th}}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| ATRP Blended | Narrow | $250: 1: 0.02$ | 0.0015 | 13.7 | 175 | 1.09 | 17 | 1.10 |
|  | Broad | $200: 1: 0.0005$ | 0.00038 | 2.0 | 167 | 1.84 | 169 | 1.89 |
| ATRP | PMMA Block | $300: 1: 0.03$ | 0.0011 | 21 | 150 | 1.10 | 162 | 1.07 |
| PMMA-b-EA | PEA Block | $300: 1: 0.03$ | 0.0019 | 9 | $\mathrm{~N}^{\mathrm{a}}$ | $\mathrm{A}^{\mathrm{N}} / \mathrm{A}^{\mathrm{a}}$ | 142 | 1.16 |
| PhotoRAFT | PPVK block | $50: 1: 1$ | 0.22 | 9.9 | 45.6 | 1.16 | 42.9 | 1.17 |
| PPVK-b-BA | PBA block | $50: 1: 1$ | 0.15 | 25 | $\mathrm{~N} / \mathrm{A}^{\mathrm{a}}$ | $\mathrm{N} / \mathrm{A}^{\mathrm{a}}$ | 50 | 1.10 |
| PET-RAFT | PMMA Block 1 | $100: 1: 1$ | 0.44 | 10 | 103 | 1.37 | 100 | 1.29 |
| PMMA-b-MMA | PMMA Block 2 | $400: 1: 1$ | 0.5934 | 1.92 | $\mathrm{~N} / \mathrm{A}^{\mathrm{a}}$ | $\mathrm{N} / \mathrm{A}^{\mathrm{a}}$ | 113 | 3.8 |

## References:

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