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1	Supporting Information
2	Hydrodeoxygenation Reactivity of Carbonyl Group and Carboxyl
3	Group and Their Interaction: Taking 2-Pentanone, Valeric Acid, and
4	Levulinic Acid as Examples
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### 3 1. Experimental

### 4 1.1 Preparation of Ru/HZSM-5 catalyst

5 Ru/HZSM-5 was prepared by an impregnation process. HZSM-5 (industrial grade, Nankai 6 University Catalyst Plant) was calcined at 550 °C for 3 h before use. An aqueous solution of RuCl<sub>3</sub> was prepared by dissolving 0.164 g of RuCl<sub>3</sub>·xH<sub>2</sub>O (AR, Sinopharm Group Chemical 7 Reagent Co., Ltd.) in 50 mL distilled water. 4 g of the calcinated HZSM-5 and the aqueous 8 solution of RuCl<sub>3</sub> were put into a rotary flask and ultrasonically stirred for 60 min and 9 evaporated at 70 °C for 1.5 h to remove water. The resulting solid was dried at 110 °C for 12 10 h, calcinated at 550 °C for 4 h, and reduced at 450 °C for 4 h in a H<sub>2</sub>:N<sub>2</sub>=40:60 atmosphere to 11 obtain Ru/HZSM-5 catalyst. 12

### 13 1.2 HDO reaction of model compounds

14 Liquid-phase HDO reactions and kinetic experiments of 2-pentanone (99%, J&K Scientific Co., Ltd.), valeric acid (>99%, Innochem Technology Co., Ltd.), a mixture of 2-pentanone 15 and valeric acid, and levulinic acid (98%, J&K Scientific Co., Ltd.) were carried out in a 300 16 mL Parr autoclave. Taking 2-pentanone as an example, the specific operation steps were as 17 follows: 12 g of Ru/HZSM-5 catalyst and 120 g of 2-pentanone were placed in the autoclave, 18 19 sealed and replaced with hydrogen for 3 times, and then heated under stirring. When the reaction temperature was reached, the hydrogen flow was introduced for HDO reaction. After 20 21 the completion of reaction, the autoclave was cooled down to room temperature. The residual gas was collected by a gas collection bag and analyzed by gas chromatography. The liquid 22 product was separated from the catalyst by filtration and then the compositions of filtrate 23 24 were analyzed by gas chromatography.

### 25 1.3 HDO reaction product analysis

### 26 1.3.1 Qualitative analysis of liquid products

The qualitative analysis of HDO products was performed on a Shimadzu QP2010 gas chromatography-mass spectrometry (GC-MS) equipped with a RTx-WAX column (30  $m \times 0.25 \text{ mm} \times 0.25 \text{ }\mu\text{m}$ ). The temperature of column was controlled by programmed temperature as follows. For the HDO reaction products of a mixture of 2-pentanone and valeric acid: an initial temperature of 50 °C and maintained for 2 min, elevated to 53 °C at a rate of 1 °C/min, increased to 85 °C at 15 °C/min, and finally raised to 250 °C at 3 °C/min and 1 maintained for 5 min. For the LA HDO reaction products: an initial temperature of 50 °C and
2 maintained for 2 min, raised to 53 °C at 1 °C/min, increased to 85 °C at 15 °C/min, and finally
3 elevated to 250 °C at 3 °C/min and maintained for 5 min. The mass spectrometry conditions
4 are as follows: EI source temperature of 250 °C, quadrupole detector temperature of 200 °C,
5 mass range: 20-550 m/z.

### 6 1.3.2 Quantitative analysis of liquid products

(1) The composition of 2-pentanone HDO reaction solution was determined on a Shimadzu GC-2018 gas chromatograph equipped with a flame ionization detector (FID). The components were separated on a KB-1 capillary column whose temperature was controlled as following program: an initial temperature of 50 °C and maintained for 2 min, raised to 53 °C at a ramp of 1 °C/min, elevated to 85 °C at a rate of 15 °C/min, increased to 200 °C at a ramp of 3 °C/min and maintained for 5 min. The internal standard method was used for quantitative calculation and cyclohexanol was used as the internal standard.

(2) The composition of HDO reaction liquid of valeric acid, a mixture of 2-pentanone and valeric acid, and LA was separately analyzed by a Shimadzu GC-2030A gas chromatograph equipped with an FID. The internal standard method was also used for quantitative calculation. The components were separated on an SH-RTx-WAX capillary column whose temperature was controlled by the program as follows.

For valeric acid HDO reaction liquid: ethyl hexanoate was used as internal standard. The column temperature control program was as follows: an initial temperature of 50 °C and maintained for 2 min, raised to 53 °C at a rate of 1 °C/min, then increased to 200 °C at a ramp of 3 °C/min and maintained for 5 min.

For HDO reaction liquid of a mixture of 2-pentanone and valeric acid: ethyl hexanoate was used as internal standard. The column temperature control program was the same as that in GC-MS analysis.

For LA HDO reaction liquid: ethyl hexanoate as the internal standard. The column temperature control program was the same as that in GC-MS analysis.

- 28 Conversion = (amount of model compound charged amount of model compound left) /
   29 amount of model compound charged ×100%
- 30 Yield = (amount of target product *n*-pentane formed/amount of model compound
   31 charged) ×100%

### 32 1.3.3 Analysis of gaseous products

(1) The composition of the gas products was determined using a Shimadzu GC-2018 gas
 chromatograph equipped with a thermal conductivity detector (TCD). The gaseous products

such as CO, CO<sub>2</sub> and H<sub>2</sub> were separated on a TDX-01 packed column. The content of each
 gas component in the gas phase was determined by an external standard method.

3 (2) To quantitatively analyze  $C_1 \sim C_4$  components, a Shimadzu GC-2030A gas chromatograph equipped with an FID was used. The gaseous products were separated on a 4 5 KB-Al<sub>2</sub>O<sub>3</sub>/Na<sub>2</sub>SO<sub>4</sub> capillary column whose temperature was controlled according to the following program: started at 60 °C and maintained for 2 min, then raised to 200 °C at a rate 6 7 of 10 °C/min and maintained for 10 min. The internal standard method was used for 8 quantitative calculation and isobutane was used as the internal standard.

Reaction conditions Yield/% Selectivity/% Entry  $X_{MPK}$ /% Catalyst amount/wt.% temp/°C P<sub>(H2)</sub>/MPa time/h MPA Pentane Pentane MPA 190 81.6 27.9 28.2 34.2 34.6 1 4 3 6 190 82.3 52.7 2.1 64.0 2.6 2 6 3 6 190 3 79.6 50.7 0.6 63.7 0.8 3 8 6 10 190 80.2 50.6 0.8 63.1 1.0 4 3 6 5 6 150 3 6 99.5 20.9 51.0 21.0 51.3 98.9 27.2 44.1 27.5 44.6 6 170 3 6 6 210 3 44.8 18.1 0.4 40.4 0.9 7 6 6 230 40.9 11.3 0.2 27.6 0.5 8 3 6 6 190 23.8 3.1 0.1 13.0 0.4 9 6 1 6 10 6 190 2 45.0 16.3 0.2 36.2 0.4 6 11 4 86.1 59.3 1.9 68.9 2.2 190 6 6 12 91.8 71.3 2.3 77.7 2.5 190 5 6 6 13 190 6 99.4 72.3 0.4 72.7 0.4 6 6 14 190 91.4 68.1 5.8 74.5 6.3 6 5 2 15 190 5 4 91.9 67.9 4.7 73.9 5.1 6 16 5.2 60.2 5.8 6 190 5 8 90.3 54.4

 Table SI-1 Influence of reaction conditions on 2-pentanone HDO

MPK: 2-pentanone; MPA: 2-pentanol; X: conversion

		Reaction conditions			_		Amount of gas products (×10 <sup>-2</sup> mmol)						
Entry	catalyst amount/wt.%	temp/°C	P <sub>(H2)</sub> /MPa	time/h	$X_{VA}$ /%	S <sub>C5</sub> /%	СО	$H_2 \times 10^2$	CO <sub>2</sub>	$C_1$	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>
1	5	250	5	4	14.9	13.2	563.6	37.5	0	30.8	111.6	2.8	35.0
2	10	250	5	4	27.7	8.0	586.0	36.0	0	156.0	124.0	8.0	80.0
3	15	250	5	4	30.1	7.8	601.0	34.1	737.4	200.9	135.2	9.7	49.2
4	10	230	5	4	20.0	7.3	735.1	42.1	0	53.8	81.3	3.5	13.1
5	10	240	5	4	33.1	7.6	765.6	42.0	0	87.2	13.8	7.4	96.3
6	10	260	5	4	27.2	7.3	576.7	30.2	760.0	176.3	30.0	159.6	64.7
7	10	240	3	4	21.7	2.2	440.3	33.0	0	68.4	75.0	4.7	48.4
8	10	240	4	4	32.4	5.0	643.9	32.3	0	66.6	11.0	3.8	46.1
9	10	240	6	4	31.6	9.2	989.1	72.7	915.0	83.8	13.9	4.9	69.3
10	10	240	5	2	28.3	4.4	704.2	41.3	0	130.0	12.4	6.7	58.1
11	10	240	5	6	30.6	12.8	456.4	26.2	539.8	93.6	80.5	10.6	93.3

### 3. Effect of reaction conditions on valeric acid HDO

 Table SI-2 Influence of reaction conditions on valeric acid HDO

 $VA: valeric \ acid, \ C_1: \ CH_4, \ C_2: \ C_2H_4 + C_2H_6, \ C_3: \ C_3H_8, \ C_4: \ C_4H_{10} + C_4H_8, \ C_5: \ C_5H_{12}, \ X: \ conversion, \ S: \ selectivity.$ 

# 4. GC-MS analysis results of HDO reaction of the mixture of 2-pentanone and valeric acid

4		2-pentano	ne and valeric	acid	
Symbol	Retention time /min	Chemical name	Chemical formula	Constitutional formula	Similarity /%
А	1.733	<i>n</i> -Pentane	$C_{5}H_{12}$	$\sim$	93
В	1.883	<i>n</i> -Heptane	$C_{7}H_{16}$		97
С	1.997	n-Valeraldehyde	$C_5H_{10}O$		96
D	2.173	4-Methylheptane	$C_8H_{18}$		95
Е	2.392	<i>n</i> -Nonane	$C_{9}H_{20}$	$\wedge \wedge \wedge \wedge$	95
F	2.556	4-Methylnonane	$C_{10}H_{22}$		93
G	2.662	2-Pentanone	$C_5H_{10}O$		97
Н	2.864	<i>n</i> -Decane	$C_{10}H_{22}$	$\checkmark \checkmark \checkmark \land$	96
Ι	2.932	5-Decene	$C_{10}H_{20}$	$\sim\!\!\sim\!\!\sim\!\!\sim$	90
J	3.553	2-Pentanol	$C_5H_{12}O$	OH	97
K	4.877	<i>n</i> -Pentanol	$C_5H_{12}O$	ОН	95
L	5.712	Butyl 2- Methylvalerate	$C_{10}H_{20}O_2$		92
М	6.200	4-Decanone	$C_{10}H_{20}O$		94
Ν	7.119	Pentyl pentanoate	$C_{10}H_{20}O_2$		95
0	10.739	Valeric acid	$C_{5}H_{10}O_{2}$		94

3	Table SI-3 Identification of components in Ru/HZSM-5 catalyzed HDO reaction of a mixture of
4	2-pentanone and valeric acid

1	5.	GC-MS	analysis	results	of lev	ulinic	acid	HDO	reaction
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Symbol	Retention time /min	Chemical name	Chemical formula	Constitutional formula	Similarity /%
А	1.817	<i>n</i> -Pentane	$C_{5}H_{12}$	$\sim$	87
В	1.858	n-Valeraldehyde	$C_5H_{10}O$		87
С	1.917	Methyl cyclopentane	C <sub>6</sub> H <sub>12</sub>		98
D	2.108	Acetone	C <sub>3</sub> H <sub>6</sub> O	0	96
Е	3.058	Toluene	$C_7H_8$		98
F	3.358	2-Hexanone	C <sub>6</sub> H <sub>12</sub> O		96
G	4.832	<i>n</i> -Pentanol	$C_5H_{12}O$	ОН	95
Н	5.712	3-Methylcyclopentanone	$C_6H_{10}O$		92
Ι	7.225	Acetic acid	$C_2H_4O_2$	ОН	97
J	9.142	4-Methyl-3-pentenoic acid	$C_{6}H_{10}O_{2}$	OH	95
К	9.358	γ-Valerolactone	$C_5H_8O_2$		96
L	10.675	Valeric acid	$C_{5}H_{10}O_{2}$	OH	90
М	11.442	4-Methylpentanoic acid	$C_6H_{12}O_2$	OH OH	96
Ν	12.008	3-Pentenoic acid	$C_5H_8O_2$	ОН	93
0	12.600	5-isobutyl-5- Methyldihydrofuran- 2(3H)-one	$C_{9}H_{16}O_{2}$		92
Р	16.567	Levulinic acid	$C_5H_8O_3$	ОН	96

2 Table SI-4 Identification of reaction components in levulinic acid HDO catalyzed by Ru/HZSM-5

### 1 6. Calculation of carbon balance in HDO reactions

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### Table SI-5 Carbon balance of HDO reactions

	Reaction substrate					
	2-pentanone	valeric acid	2-pentanone & valeric acid	levulinic acid		
carbon balance/%	94.1	71.3	76.9	92.7		

### 3 7. 2-Pentanone HDO reaction kinetics

### 4 7.1 Effect of internal and external diffusion at different reaction temperatures

5 2-Pentanone HDO catalyzed by Ru/HZSM-5 is a gas-liquid-solid three-phase reaction 6 system and the mass transfer resistance will have a certain effect on the reaction rate. In order 7 to calculate the reaction rate constant and activation energy, the effects of internal and 8 external diffusion should be excluded firstly. The Weisz-Prater criterion and Mears criterion 9 were calculated. The specific calculation process is as follows:

10 (1) Weisz-Prater criterion is utilized to evaluate the effect of internal diffusion:

$$\Phi_{A} = \frac{-r_{A,obs}\rho_{P}R_{P}^{2}}{D_{A,e}C_{A,s}} < 1$$

11

$$\frac{-r_{A,obs}\rho_{P}R_{P}n}{k_{A}C_{A,s}} < 0.15$$

14 Where  $r_{A,obs}$  represents the observed reaction rate of component A,  $mol/kg \cdot s$ ;  $\rho_P$ 15 indicates the catalyst particle density,  $kg/m^3$ ;  $R_P$  stands for catalyst particle radius, m; *n* 16 represents reaction order;  $C_A$  indicates liquid concentration of 2-pentanone,  $mol/m^3$ ; 17  $D_A$  stands for effective diffusion coefficient,  $m^2/s$ ;  $k_A$  represents mass transfer 18 coefficient, m/s.

19 Since  $D_A$  and  $k_A$  cannot be directly measured, they were obtained by calculation. The 20 specific calculation process is as follows:

Calculation of  $D_A$ : Since the average free path of liquid molecule is much less than the pore size of catalyst <sup>[S1]</sup> in the heterogeneous system, Knudsen diffusion ( $D_k$ ) can be ignored <sup>[S2]</sup>. Total diffusion can be simplified to molecular diffusion only, i.e., the total diffusion coefficient  $D = D_{AB}$ . The above diffusion coefficient was calculated according to the Wilke1 Chang equation:

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$$D_{AB} = 7.4 \times 10^{-10} \frac{T(XM_A)^{1/2}}{\mu V_b^{0.6}} (cm^2/s)$$

3 The structure of 2-pentanone includes ketone carbonyl group, methylene group and methyl group. According to the group contribution method<sup>[S1]</sup>,  $V_{b=22.7+27.4\times2+21.3\times2=120.1.}$ 4 Similarly, according to the Van Velzen group contribution method [S3], the calculation formula 5 for  $\mu$  can be derived as  $\log \mu = 738.50 \times [(T)^{-1} - (245.38)^{-1}]$ . 6

Calculation of  $k_A$ : according to Frossling relation<sup>[S1]</sup>, 7  $Sh = 2 + 0.6Re^{1/2}Sc^{1/3} = 2 + 0.6 \times \left(\frac{Ndd_P}{\nu}\right)^{1/2} \left(\frac{\nu}{D_{AP}}\right)^{1/3}$ 8  $Sh = \frac{k_A d_P}{D_{AB}}$ 

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Where N represents stirring rate, 500 rpm; d indicates impeller diameter, 0.033 m;  $d_P$ 10 stands for particle size, mm;  $\nu$  represents the dynamic viscosity,  $m^2/s$ . 11

The effects of internal and external diffusion at 150 °C, 170 °C and 190 °C were calculated 12 13 using the above criteria and the results are shown in Table SI-6. It can be seen that the Weisz-Prater criterion value is less than 1 and the Mears criterion value is less than 0.15, indicating 14 that there is no mass transfer effect under the experimental conditions. 15

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Table SI-6 Effect of internal and external diffusion at different reaction temperatures

T/°C	r <sub>A,obs/</sub> mol/kg/s	k <sub>A</sub> / m/s	$D_{A,e}/$ cm <sup>2</sup> /s	C <sub>A,S</sub> / mol/m <sup>3</sup>	$\frac{-r_{A,obs}\rho_P R_P n}{k_A C_{A,s}}$	$\Phi_A = \frac{-r_{A,obs}\rho_P R_P^2}{D_{A,e}C_{A,s}}$
150	6.20×10 <sup>-4</sup>	1.25×10-7	3.02×10-8	1.39×10 <sup>6</sup>	0.000193	0.000999
170	6.16×10 <sup>-4</sup>	1.20×10-7	3.80×10 <sup>-8</sup>	1.39×10 <sup>6</sup>	0.000199	0.000791
190	5.13×10-4	1.16×10 <sup>-7</sup>	4.68×10-8	1.39×10 <sup>6</sup>	0.000172	0.000534

#### 7.2 Kinetic experiment data 17





Figure SI-1 Concentration of each component vs reaction time at different temperatures (a):150 °C, (b): 170 °C, (c):190 °C

#### 7.3 Comparison of experimentally measured concentrations with those predicted 4 5 by Langmuir-Hinshelwood models





#### 8. Valeric acid HDO reaction kinetics 10

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#### 8.1 Effect of internal and external diffusion at different reaction temperatures 11

12 The Weisz-Prater criterion and the Mears criterion were also used to calculate the effects of 13 internal and external diffusion at 220 °C, 230 °C, and 240 °C, respectively. The results are

- shown in Table SI-7. The Weisz-Prater criterion value is less than 1 and the Mears criterion 1
- value is less than 0.15, indicating that there is no mass transfer effect under the experimental 2
- 3 conditions.

4	Table SI-7 Effect of internal and external diffusion at different reaction temperatures								
	T/°C	r <sub>A,obs/</sub> mol/kg/s	k <sub>A</sub> / m/s	$D_{A,e}/m^2/s$	C <sub>A,S</sub> / mol/m <sup>3</sup>	$\frac{-r_{A,obs}\rho_P R_P n}{k_A C_{A,s}}$	$\Phi_A = \frac{-r_{A,obs}\rho_P R_P^2}{D_{A,e}C_{A,s}}$		
	220	1.13×10-4	4.54×10 <sup>-8</sup>	0.99×10 <sup>-8</sup>	1.12×10 <sup>5</sup>	0.000102	6.91×10 <sup>-6</sup>		
	230	1.50×10-4	4.49×10 <sup>-8</sup>	1.09×10 <sup>-8</sup>	1.12×10 <sup>5</sup>	0.000137	8.39×10 <sup>-6</sup>		
_	240	1.87×10 <sup>-4</sup>	4.44×10-8	1.18×10-8	1.12×10 <sup>5</sup>	0.000173	9.62×10-6		

Table SI-7 Effect of internal and external diffusion at different reaction temperatures

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### 6 8.2 Kinetic experiment data



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9. HDO reaction kinetics of the mixture of 2-pentanone and valeric acid

#### 12 9.1 Effect of internal and external diffusion at different reaction temperatures

The Weisz-Prater criterion and the Mears criterion were used to calculate the effects of 13 internal and external diffusion at 190 °C, 215 °C, and 240 °C, respectively. The results are 14 shown in Table SI-8. It can be seen that the Weisz-Prater criterion value is less than 1 and the 15

- Mears criterion value is less than 0.15, indicating that there is no mass transfer effect under 1
- 2 this experimental condition.

3	Table SI-8 Effect of internal and external diffusion at different reaction temperatures									
T/°C		r <sub>A,obs/</sub> mol/kg/s	k <sub>A</sub> / m/s	D <sub>A,e</sub> / cm <sup>2</sup> /s	C <sub>A,S</sub> / mol/m <sup>3</sup>	$\frac{-r_{A,obs}\rho_P R_P n}{k_A C_{A,S}}$	$\Phi_A = \frac{-r_{obs}\rho_P R_P^2}{D_{A,e} C_{A,S}}$			
	190	2.37×10-4	4.96×10-8	7.71×10-7	$1.02 \times 10^{6}$	0.000256	2.05×10-5			
	215	3.13×10-4	4.76×10-8	1.05×10-6	$1.02 \times 10^{6}$	0.000351	1.99×10 <sup>-5</sup>			
	240	3.53×10 <sup>-4</sup>	4.59×10-8	1.39×10-6	$1.02 \times 10^{6}$	0.000411	1.69×10-5			
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### 6 9.2 Kinetic experiment data



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# (a):190 °C, (b): 215, (c):240 °C

#### 10. Levulinic acid HDO reaction kinetics 11

#### 10.1 Effect of internal and external diffusion at different reaction temperatures 12

The Weisz-Prater criterion and the Mears criterion were used to calculate the effects of 13 14 internal and external diffusion at 190 °C, 215 °C, and 240 °C, respectively. The results are

- 1 shown in Table SI-9. It can be seen that the Weisz-Prater criterion value is less than 1 and the
- 2 Mears criterion value is less than 0.15, indicating that there is no mass transfer effect under
- 3 the experimental condition.

4_		Table SI-9 Effect of internal and external diffusion at different reaction temperatures										
T/°C		r <sub>A,obs/</sub> mol/kg/s	k <sub>A</sub> / m/s	$D_{A,e}/\ cm^2/s$	C <sub>A,S</sub> / mol/m <sup>3</sup>	$\frac{-r_{A,obs}\rho_P R_P n}{k_A C_{A,S}}$	$\Phi_A = \frac{-r_{obs}\rho_P R_P^2}{D_{A,e} C_{A,S}}$					
	190	2.37×10-4	4.96×10-8	7.71×10-7	$1.02 \times 10^{6}$	0.000256	2.05×10-5					
	215	3.13×10-4	4.76×10 <sup>-8</sup>	1.05×10-6	$1.02 \times 10^{6}$	0.000351	1.99×10 <sup>-5</sup>					
_	240	3.53×10-4	4.59×10 <sup>-8</sup>	1.39×10-6	$1.02 \times 10^{6}$	0.000411	1.69×10-5					

 Table SI-9 Effect of internal and external diffusion at different reaction tempe

#### 10.2 Kinetic experiment data 6



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# **11. HDO reaction kinetic model statistics**

Table SI-10 Model Statistic
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	Reaction	Experim	Free	Regression	Residual	Correlation	
Model	temperature	ent	variation	square sum	squares sum	index	F
	/°C	No.	No.	square sum	squares sum	Index	
	150	10		27.13	0.0506	0.9992	
	170	10	3	13.46	0.0162	0.9996	1199
	190	10		2.55	0.0146	0.9993	
	150	10		23.77	0.0518	0.9985	
2-Pentanone	170	10	3	13.18	0.0251	0.9991	955
	190	10		2.58	0.0106	0.9983	
	150	10		22.75	0.0513	0.9986	
	170	10	3	9.62	0.0169	0.9985	849
	190	10	U	1.74	0.0223	0 9741	0.17
	220	12		12.02	0.0341	0.9983	
	230	12	3	11.11	0.0262	0.9972	1753
	240	12	5	9.69	0.0099	0.9943	1700
	220	12	3	10.17	0.0082	0.9957	1910
	230	12		15.00	0.0547	0.9790	
	240	12		11.78	0.0302	0.9854	
	220	12	3	11.38	0.0270	0.9865	1126
Valeric acid	230	12		12.16	0.0325	0.9843	
	240	12		16.67	0.0505	0.9824	
	220	12		17.41	0.0749	0.9747	
	230	12	3	19.69	0.0695	0.9792	679
	240	12		23.13	0.1413	0.9651	
	220	12		15.28	0.0316	0.9986	
	230	12	3	12.91	0.0763	0.9998	1199
	240	12		11.89	0.0217	0.9969	
	190	12		12.72	0.0104	0.9907	
	215	12	3	11.89	0.0135	0.9912	2466
	240	12		10.88	0.0299	0.9880	
Mixture of	190	12	2	10.32	0.0694	0.9847	510
2-pentanone	215	12	3	2.87	0.0090	0.9965	519
and valeric	240	12		1.03	0.0325	0.996/	
acid	190	12	2	5.54	0.0143	0.99/8	710
	213	12	3	4.09	0.0113	0.9988	/19
	240 100	12		0.04	0.0120	0.9655	
	215	12	3	2.51	0.0030	0.9899	2488

240	12		2.46	0.0025	0.9996	
190	12		13.75	0.0226	0.9965	
215	12	3	14.57	0.0357	0.9979	1355
240	12		10.89	0.0322	0.9986	
190	12		11.15	0.0198	0.9993	
215	12	3	8.34	0.0159	0.9989	2212
240	12		12.43	0.0111	0.9992	
190	12		9.99	0.0322	0.9991	
215	12	3	2.26	0.0175	0.9968	1017
 240	12		2.04	0.0035	0.9985	

Table SI-10 Model Statistics (Continuation)

Model	Reaction temperature /°C	Experiment No.	Free variation No.	Regression square sum	Residual squares sum	Correlation index	F
	190	12		12.79	0.0402	0.9852	
	215	12	3	12.38	0.0298	0.9877	1017
	240	12		16.35	0.0575	0.9832	
	190	12		19.14	0.1031	0.9731	
	215	12	3	11.10	0.0412	0.9808	912
	240	12		9.88	0.0216	0.9893	
	190	12		10.55	0.0312	0.9852	
	215	12	3	18.73	0.0786	0.9793	1427
Levulinic	240	12		11.23	0.0132	0.9998	
acid	190	12		8.94	0.0015	0.9987	
	215	12	3	12.11	0.0112	0.9984	7332
	240	12		13.91	0.0478	0.9896	
	190	12		5.68	0.0064	0.9968	
	215	12	3	13.09	0.0190	0.9987	1760
	240	12		10.78	0.0604	0.9979	
	190	12		11.12	0.0263	0.9991	
	215	12	3	10.83	0.0491	0.9924	948
	240	12		7.70	0.0253	0.9962	

# 3 12. NH<sub>3</sub>-TPD analysis results of Ru/HZSM-5 catalysts with different Si/Al ratios

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Table SI-11 Acid properties of Ru/HZSM-5 catalysts with different Si/Al ratio

	NH <sub>3</sub> desorption peak at lower temperature		NH <sub>3</sub> desorption peak at medium temperature		NH <sub>3</sub> desorption peak at higher temperature		Total acid
Catalyst	Peak top temperature/ °C	Weak acid amount/ μmol·g <sup>-1</sup>	Peak top temperature/ °C	Strong acid amount/ µmol·g <sup>-1</sup>	Peak top temperature/ °C	Strong acid amount/ µmol·g <sup>-1</sup>	amount∕ µmol∙g <sup>-1</sup>
Ru/HZSM-5(21)	190.9	319.2	263.9	231.6	347.1	143.8	694.6
Ru/HZSM-5(61)	184.6	130.4			303.4	194.3	324.7
Ru/HZSM-5(130)	180.7	101.0			283.3	191.9	292.9
Ru/HZSM-5(360)	162.1	26.5			260.0	75.3	101.8

# 5 13. Py-IR analysis results of Ru/HZSM-5 catalysts with different Si/Al ratios



**Fig. SI-6** Py-IR spectra of Ru/HZSM-5 with different Si/Al ratios a: HZSM-5(21); b: HZSM-5(60); c: HZSM-5(130); d: HZSM-5(360)

### 4 Reference

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