## Supporting Information

# Engineering of platinum-oxygen vacancy interfacial sites in confined catalysts for enhanced hydrogenation selectivity

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#### **Experimental section**

### 1.1 Synthesis of catalysts.

Synthesis of CNCs and the ALD process. The carbon nanocoils (CNCs) were synthesized by chemical vapor deposition using acetylene as a carbon source and copper nanoparticles as catalysts at 250 °C followed by a heat treatment at 900 °C in an Ar atmosphere for 2 h. Raw CNCs were refluxed in HNO<sub>3</sub> (15 wt %) for 4 h at 100 °C in an oil bath to remove the copper catalysts, then filtered and washed with deionized water and ethanol until there was no further change in pH (around pH = 7).

The atomic layer deposition (ALD) process was carried out in a hot-wall closed chamber-type ALD reactor. Prior to ALD, 15 mg CNCs were dispersed onto a quartz wafer (5 cm×10 cm) with ethanol. After the samples were dried at ambient temperature, they were transferred to the ALD chamber. Pt nanoparticles were deposited at 250 °C with trimethyl (methylcyclopentadienyl) platinum (MeCpPtMe<sub>3</sub>) and ozone (O<sub>3</sub>) as precursors. MeCpPtMe<sub>3</sub> was kept at 65 °C. The pulse, exposure, and purge times for the MeCpPtMe<sub>3</sub> were 0.5, 12, and 25 s, respectively, and for the O<sub>3</sub>, 0.1, 12, and 25 s, respectively. The TiO<sub>2</sub> film was deposited at 125 °C with titanium tetraisopropoxide (TTIP) and deionized H<sub>2</sub>O as precursors. The pulse, exposure, and purge times for the TTIP were 1, 8, and 25 s, respectively, and for the H<sub>2</sub>O, 0.1, 8, and 25 s, respectively.

Synthesis of TiO<sub>2</sub>/Pt. CNCs were firstly decorated with Pt nanoparticles (20 cycles) by Pt ALD and then coated with a TiO<sub>2</sub> layer (300 cycles) by TiO<sub>2</sub> ALD, producing TiO<sub>2</sub>/Pt/CNCs. The TiO<sub>2</sub>/Pt/CNCs was calcinated at 500 °C for 2 h to remove the CNC templates, obtaining a TiO<sub>2</sub>/Pt catalyst, in which Pt nanoparticles were confined in TiO<sub>2</sub> nanotubes.

Synthesis of TiO<sub>2</sub>/Pt-T-Ar. The TiO<sub>2</sub>/Pt/CNCs prepared by the above method was firstly heated under argon atmosphere at different temperatures (T=500 °C, 600 °C, 700 °C, and 800 °C) for 2 h. After the thermal treatment, the obtained sample was calcinated at 500 °C for 2 h to remove the CNC templates, obtaining a TiO<sub>2</sub>/Pt-T-Ar catalyst.

Synthesis of Pt/TiO<sub>2</sub> and Pt/TiO<sub>2</sub>-700-Ar. CNCs were firstly coated with a TiO<sub>2</sub> layer (300 cycles) by TiO<sub>2</sub> ALD and then decorated with Pt nanoparticles (20 cycles) by Pt ALD, producing Pt/TiO<sub>2</sub>/CNCs. Next, the Pt/TiO<sub>2</sub>/CNCs was calcined at 500 °C for 2 h, obtaining a Pt/TiO<sub>2</sub> catalyst, in which Pt nanoparticles were supported on the outer surfaces of TiO<sub>2</sub> nanotubes. When the Pt/TiO<sub>2</sub>/CNCs was firstly heated under argon atmosphere at 700 °C for 2 h and then calcined at 500 °C for 2 h, the Pt/TiO<sub>2</sub>-700-Ar was obtained.

### **1.2 Catalyst characterizations.**

Transmission electron microscopy (TEM) images, high-angle annular dark field scanning transmission electron microscopy (HAADF-STEM) images, and energydispersive X-ray spectroscopy (EDS) mapping profiles were acquired with a JEM-2100F field-emission transmission electron microscope operated at 200 kV. X-ray diffraction (XRD) patterns were collected on a Bruker D8 Advance X-ray diffractometer using a Cu K $\alpha$  source ( $\lambda = 1.540$  Å) in the 2 $\theta$  range from 10° to 90°. The  $N_2$  sorption measurements were performed using Micromeritics Tristar II (3020) at 77 K. The contents of Pt metal in the catalysts were determined by inductively coupled plasma atomic emission spectrometry (ICP-AES, Thermo iCAP 6300).

X-ray photoelectron spectra (XPS) were recorded on an AXIS ULTRA DLD spectrometer (Shimadzu/Kratos) to characterize the surface composition with the Al K $\alpha$  line as the excitation source. The C 1s peak at 284.8 eV was used as a reference for calibration. XPS spectra of the catalysts without exposure to air were obtained based on the assistance of a pretreatment chamber. The carbon-assisted thermal treatment under argon atmosphere for TiO<sub>2</sub>/Pt/CNCs was performed in tubular furnace. The calcination under flowing air (500 °C, 2 h) for TiO<sub>2</sub>/Pt/CNCs and TiO<sub>2</sub>/Pt/CNCs-700-Ar was performed in the pretreatment chamber. Therefore, the samples treated in the pretreatment chamber connected by an in-vacuum sample transfer system to the surface analysis chamber. Therefore, the samples treated in the pretreatment chamber can be transferred to the analysis chamber without exposure to air.

Electron paramagnetic resonance (EPR) spectra were recorded using a Brucker EMX spectrometer (EMXplus-10/12) operating at 100 kHz field modulation. The signal intensities of EPR spectra for different catalysts were quantified using a double integration method of the peaks based on the area under the curve.

The X-ray absorption near-edge structure (XANES) and extended X-ray absorption fine structure (EXAFS) spectra of the Ti K-edge were measured on the BL11B beamline of the Shanghai Synchrotron Radiation Facility (SSRF), Shanghai Advanced Research Institute, Chinese Academy of Sciences. A Si (111) double-crystal monochromator was used to reduce the harmonic component of the monochrome beam. Anatase TiO<sub>2</sub> was used as the reference sample and measured in the transmission mode, and all the catalysts were measured in the transmission mode. IFEFFIT software was used to calibrate the energy scale, to correct the background signal and to normalize the intensity. The theoretical paths for Ti–O and Ti–Ti species used for fitting two coordination shells of the experimental data were generated using the FEFF7 program. The coordination number, bond distance, Debye–Waller factor, and inner potential correction were used as variable parameters for the fitting procedures.

Diffuse reflectance infrared Fourier transform spectroscopy (DRIFTS) spectra were recorded using a Bruker Tensor II spectrometer with a resolution of 2 cm<sup>-1</sup>. The IR spectrum of TiO<sub>2</sub>/Pt-700-Ar without exposure to air was obtained based on in-situ calcination in a DRIFTS cell. TiO<sub>2</sub>/Pt/CNCs was firstly heated under argon atmosphere in tubular furnace. Then the obtained TiO<sub>2</sub>/Pt/CNCs-700-Ar was placed into the DRIFTS cell and calcinated under oxygen flow for the removal of CNCs. After calcination, the spectrum was recorded in argon atmosphere. Temperature-programmed desorption of *p*-nitrobenzyl chloride (*p*-NBC) over different catalysts was also performed in a DRIFTS cell. As a typical run, the sample was placed in the DRIFTS cell and treated under Ar flow at 200 °C for 1 h. After that, 20 µL methanol solution of *p*-NBC was injected into the cell by a homemade window at 55 °C. The heating rate was 10 °C/min. The spectra at different temperatures (55, 65, 75, 85, 100, 150, and 200 °C) were collected when *p*-NBC was not desorbed from the catalyst surfaces.

#### **1.3 Catalytic hydrogenation tests.**

*p*-NBC hydrogenation reactions over the catalysts were carried out in a 50 mL stainless-steel autoclave reactor. The reaction was carried out at 55 °C and 1 MPa H<sub>2</sub> with 10 mg of catalyst, 0.5 mmol of *p*-NBC and 20 mL of anhydrous methanol. After the reaction, the reactor was cooled and then slowly depressurized. Finally, the reaction mixture was separated by centrifugation in order to remove the solid catalysts. The reaction products were analyzed and quantified by gas chromatographic mass spectrometry (GC-MS, Agilent Technologies 7890A-5975C). The reaction conversion and selectivity were determined by the product analysis.



Figure S1. TEM images of (a)  $TiO_2/Pt-500$ -Ar, (b)  $TiO_2/Pt-600$ -Ar, and (c)  $TiO_2/Pt-800$ -Ar.



**Figure S2.** (a) The N<sub>2</sub> adsorption-desorption isotherms and (b) the corresponding pore size distributions for  $TiO_2/Pt$  and  $TiO_2/Pt$ -T-Ar. Brunauer-Emmett-Teller (BET) surface areas, pore volumes, and average pore diameters of the catalysts are listed in Table S1.



**Figure S3.** The EXAFS spectra and their  $k^3$ -weighted fitting spectra of anatase TiO<sub>2</sub>, TiO<sub>2</sub>/Pt, and TiO<sub>2</sub>/Pt-700-Ar. Lines indicate experimental data and open circles indicate fitted results.



**Figure S4.** (a) The IR spectra of TiO<sub>2</sub>/Pt-700-Ar with exposure (blue line) and without exposure (red line) to air. (b) The XPS O 1s spectra of TiO<sub>2</sub>/Pt and TiO<sub>2</sub>/Pt-700-Ar without exposure to air. The spectrum (Figure S4a, blue line) shows a broad adsorption band at 3000~3700 cm<sup>-1</sup> corresponding to the surface-adsorbed water and the hydroxyl groups. For the TiO<sub>2</sub>/Pt-700-Ar without exposure to air, no OH stretching features in the range 3700–3300 cm<sup>-1</sup> is observed (Figure S4a, red line), meaning few surface hydroxyls. In Figure S4b, only a peak at ~530.0 eV is observed and no shoulder peak is observed at 531.8 eV. This may be because the catalysts were not exposed to air and there are no hydroxyl groups formed by dissociative adsorption of H<sub>2</sub>O on oxygen vacancies of TiO<sub>2</sub> surfaces.



**Figure S5.** The evolution of *p*-nitrobenzyl chloride conversion and product selectivities with reaction time over (a)  $TiO_2/Pt$  and (b)  $TiO_2/Pt$ -700-Ar. The *p*-ABC and *p*-ATL represent *p*-aminobenzyl chloride and *p*-aminotoluene, respectively. Others include *p*-nitrotoluene, *p*-nitrosotoluene, and *p*-hydroxyamine toluene.



Figure S6. TEM images of (a)  $TiO_2/15Pt-700$ -Ar and (b)  $TiO_2/10Pt-700$ -Ar.



Figure S7. (a) TEM images of  $Pt/TiO_2$ -700-Ar. (b) The EPR spectra of  $Pt/TiO_2$ -700-Ar and  $TiO_2/Pt$ -700-Ar.



Figure S8. The recycling stability of  $TiO_2/Pt$ -700-Ar in the hydrogenation of *p*-NBC.



Figure S9. (a) TEM image of  $TiO_2/Pt-700$ -Ar after four consecutive runs. (b) EPR spectra of  $TiO_2/Pt-700$ -Ar before and after reaction.

Catalysts  $S_{BET}\left(m^2~g^{\text{--}1}\right)$  $V_{total} \left( cm^3 \ g^{\text{--}1} \right)$ D (nm)  $TiO_2/Pt$ 40.5 0.14 49.3 TiO<sub>2</sub>/Pt-500-Ar 46.2 0.18 48.8  $TiO_2/Pt-600-Ar$ 45.0 0.16 43.6 TiO<sub>2</sub>/Pt-700-Ar 48.0 0.15 41.5

0.09

37.0

36.0

TiO<sub>2</sub>/Pt-800-Ar

Table S1. The specific surface areas and pore structure parameters of  $TiO_2/Pt$  and  $TiO_2/Pt$ -T-Ar.

Sample	Pt contents (wt.%)
TiO <sub>2</sub> /Pt	0.46
TiO <sub>2</sub> /Pt-700-Ar	0.49
TiO <sub>2</sub> /15Pt-700-Ar	0.42
TiO <sub>2</sub> /10Pt-700-Ar	0.32
Pt/TiO <sub>2</sub>	1.56
Pt/TiO <sub>2</sub> -700-Ar	1.32

 Table S2. Loading amounts of Pt for different catalysts.

Shell	CN	R (Å)	$\Delta\sigma^2 \times 10^3$ (Å <sup>2</sup> )	R-factor(%)	
Ti-O	6	1.96	5.7±0.2	0.6	
Ti-Ti 4 3.05	5.5±0.3	- 0.6			
Ti-O	5.9	1.95	1.8±0.4	0.2	
Ti-Ti	3.0	3.05	1.9±0.5	0.3	
Ti-O	5.0	1.95	3.0±0.6	- 07	
Ti-Ti	3.5	3.05	1.4±0.7	- 0.7	
	Shell Ti-O Ti-Ti Ti-O Ti-Ti Ti-O Ti-Ti	Shell         CN           Ti-O         6           Ti-Ti         4           Ti-O         5.9           Ti-Ti         3.0           Ti-O         5.0           Ti-Ti         3.5	Shell         CN         R (Å)           Ti-O         6         1.96           Ti-Ti         4         3.05           Ti-O         5.9         1.95           Ti-Ti         3.0         3.05           Ti-O         5.0         1.95           Ti-Ti         3.5         3.05	ShellCNR (Å) $\Delta\sigma^2 \times 10^3$ (Å2)Ti-O61.965.7±0.2Ti-Ti43.055.5±0.3Ti-O5.91.951.8±0.4Ti-Ti3.03.051.9±0.5Ti-O5.01.953.0±0.6Ti-Ti3.53.051.4±0.7	

Table S3. EXAFS data fitting results of anatase  $TiO_2$ ,  $TiO_2/Pt$ , and  $TiO_2/Pt$ -700-Ar.

Table 51. The under the curve (Teoc) of Errespectation unterent cutarysis.				
Catalysts	AUC			
TiO <sub>2</sub> /Pt	0			
TiO <sub>2</sub> /Pt-500-Ar	0			
TiO <sub>2</sub> /Pt-600-Ar	0			
TiO <sub>2</sub> /Pt-700-Ar	14.2			
TiO <sub>2</sub> /Pt-700-Ar (after reaction)	17.9			
TiO <sub>2</sub> /Pt-800-Ar	95.6			
Pt/TiO <sub>2</sub> -700-Ar	4.1			

 Table S4. Area under the curve (AUC) of EPR spectra for different catalysts.

Catalyata	$O_{I}$		(	Area ratio	
Catalysts	P <sub>peak</sub>	A <sub>peak</sub>	P <sub>peak</sub>	A <sub>peak</sub>	$(O_{II}/O_{I})$
TiO <sub>2</sub> /Pt	530.0	112702.6	531.8	3811.9	0.03
TiO <sub>2</sub> /Pt-700-Ar	530.1	117108.7	531.8	12403.6	0.11

**Table S5.** The position ( $P_{peak}$ ), area ( $A_{peak}$ ), and  $O_{II}/O_I$  area ratio of XPS O 1s peak for TiO<sub>2</sub>/Pt and TiO<sub>2</sub>/Pt-700-Ar.

	Catalysts	Time (min)	Conv. (%)	Sel. (%) <sup>[a]</sup>		
		Time (mm)		<i>p</i> -ABC	<i>p</i> -ATL	others
	TiO <sub>2</sub> /15Pt-700-Ar	110	99.5	73.3	17.8	8.9
	TiO <sub>2</sub> /10Pt-700-Ar	140	95.8	75.7	11.7	12.6

**Table S6.** Catalytic performances of the  $TiO_2/Pt-700$ -Ar catalysts with different Pt ALD cycles for *p*-nitrobenzyl chloride hydrogenation.

<sup>[a]</sup>The *p*-ABC and *p*-ATL represent *p*-aminobenzyl chloride and *p*-aminotoluene, respectively. Others include *p*-nitrotoluene, *p*-nitrosotoluene, and *p*-hydroxyamine toluene.

Catalysts	s Time (min) Co	Conv (%)	Sel. (%) <sup>[a]</sup>		
Catalysts		Conv. (70)	<i>p</i> -ABC	<i>p</i> -ATL	others
Pt/TiO <sub>2</sub>	30	92.4	2.0	93.8	4.2
Pt/TiO <sub>2</sub> -700-Ar	90	94.5	4.4	93.6	2
$TiO_2/Pt\text{-}500\text{-}H_2^{[b]}$	90	93.8	56.2	32.9	10.9

**Table S7.** Catalytic performances of unconfined  $Pt/TiO_2$  and  $Pt/TiO_2$ -700-Ar and confined  $TiO_2/Pt$ -500-H<sub>2</sub> for *p*-nitrobenzyl chloride hydrogenation.

<sup>[a]</sup>The *p*-ABC and *p*-ATL represent *p*-aminobenzyl chloride and *p*-aminotoluene, respectively. Others include *p*-nitrotoluene, *p*-nitrosotoluene, and *p*-hydroxyamine toluene.

<sup>[b]</sup>Reducing TiO<sub>2</sub>/Pt at 500 °C for 1 h.

Notes: Compared to hydrogen reduction to create oxygen vacancies by gas-solid reaction ( $H_2$  and  $TiO_2$ ), the carbon-assisted thermal treatment creates oxygen vacancies by solid-solid reaction (carbon and  $TiO_2$ ). The gas-solid reaction forms oxygen vacancies on the whole  $TiO_2$ , while the solid-solid reaction can selectively generate oxygen vacancies in the interfacial region between carbon and  $TiO_2$ . This provides more alternative means for regulation of interfacial sites, which will contribute to further interfacial site optimization and performance improvement. Moreover, from the perspective of safety, the carbon-assisted thermal treatment also shows the superiority.

Compared to hydrogen reduction, additional calcination in air for the carbon-assisted thermal treatment is required to remove the carbon templates after oxygen vacancies are generated.