

Supporting information

Understanding catalyst deactivation during the direct cracking of crude oil

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Calculations for catalytic performance and coke analysis:

Catalytic cracking of AL performance:

$$\text{Total flow rate:} = \frac{F_{He}}{\%V_{He}} \times 100 \text{ ml} \cdot \text{min}^{-1} \quad (\text{Equation S1})$$

$$\text{Flow rate of internal standard He: } F_{He} \text{ ml} \cdot \text{min}^{-1}$$

$$\text{Percentage of gas volume: } \%V_x$$

$$\text{Flow of each component } F_x = \frac{\text{Total flow} \times \%V_x}{100} \times 100 \text{ ml} \cdot \text{min}^{-1} \quad (\text{Equation S2})$$

$$\text{Mass flow of each component } M_x = \frac{F_x \times MW_x}{R \times T} \text{ g} \cdot \text{min}^{-1} \quad (\text{Equation S3})$$

$$\text{Molecular weight of each component} = MW_x \text{ g} \cdot \text{mol}^{-1}$$

R is the gas constant and T is temperature in Kelvin

$$\text{yield wt. \%} = \frac{M_x}{\text{mass flow of AL (g.min}^{-1})} \times 100 \quad (\text{Equation S4})$$

Thermo-gravimetric analysis (TGA):

Hard coke and coke precursors are defined as following equation related to Figure S1

$$\text{Coke precursors (wt.\%)} = \frac{m_0 - m_e}{m_z} \times 100 \quad (\text{Equation S5})$$

$$\text{Hard coke (wt.\%)} = \frac{m_e - m_z}{m_z} \times 100 \quad (\text{Equation S6})$$

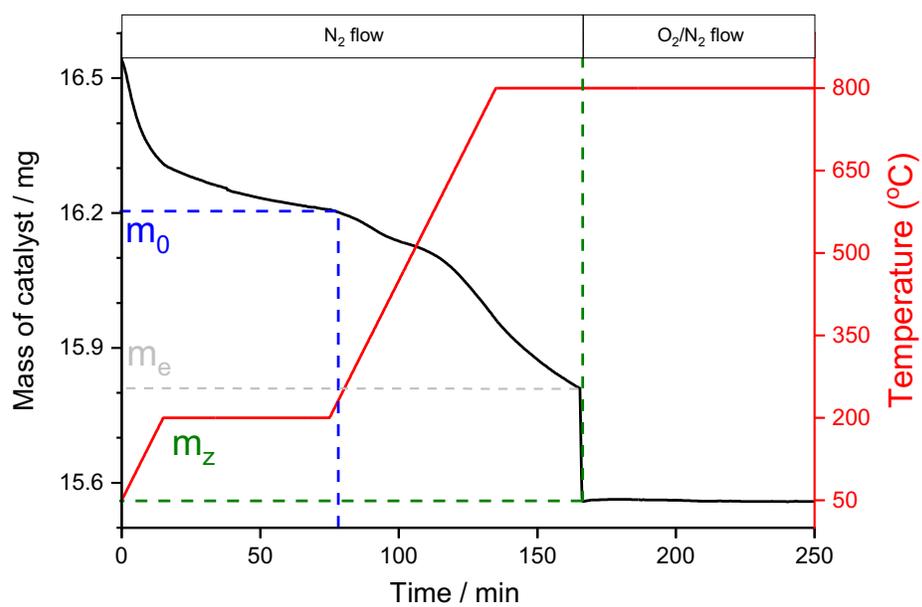


Figure. S1: Coke quantification method by thermo-gravimetric analysis. TGA of spent catalysts in MZFBR after catalytic cracking.

Calculations for determination of aluminium content (molar fraction) in zeolite framework and levels of dealumination using unit cell size (UCS) parameters derived from powder X-ray diffraction data:

The quantitative evaluation of the migration of aluminum from the framework during thermal, hydrothermal treatment and after being acted in the cracking process can be achieved by linking a unique unit cell size (UCS) parameter with the effective framework composition.⁵⁸ The unit cell parameters of a zeolite are directly correlated with the framework composition. As such, increasing the content of aluminum atoms in the frameworks induces an expansion of the UCS parameters because of relative longer tetrahedral Al-O bonds (~ 1.74 Å) compared to Si-O (~ 1.63 Å) ones. Thus, the UCS parameter well represents a “framework” tetrahedral aluminum centers associated with Brønsted acidity and can be derived from acidity evaluation applying NH₃ chemisorption at high temperature region (below 300 °C). Therefore, the framework aluminum mole fraction (x_{Al})^{58,59} can be derived through calculations involving:

$$\text{Stoichiometric acidity } [mol \cdot g^{-1}] = \frac{1}{M_w^{zeolite}} \quad (\text{Equation S7})$$

$$M_w^{zeolite} = M_w^{SiO_2} \cdot SAR + M_w^{Al_2O_3} + A_r^H \quad (\text{Equation S8})$$

where stoichiometric acidity is strong acidity population, Brønsted acidity, (mol·g⁻¹) determined from NH₃ chemisorption; $M_w^{zeolite}$ - molecular weight of zeolite with the formula (SiO₂)_{SAR}(Al₂O₃)H where SAR represents framework SiO₂:Al₂O₃ molar ratio; $M_w^{SiO_2}$, $M_w^{Al_2O_3}$ and A_r^H are molecular weights of SiO₂, Al₂O₃ and atomic weight of hydrogen, respectively. Derived SAR value can be transformed to aluminum mole fraction (x_{Al}) to express aluminum content in the framework by using Equation S9:

$$x_{Al} = \frac{[Al]}{[Al]+[Si]} = \frac{1}{1+SAR/2} \quad (\text{Equation S9})$$

The extend of dealumination and framework aluminum content can be estimated applying Equation S10:

$$V_x = V_{Si} - V_{Si} \cdot \left(1 - \left(\frac{d_{Al-O}}{d_{Si-O}}\right)^3\right) \cdot x_{Al} \quad (\text{Equation S10})$$

where V_x is experimentally determined unit cell volume of the framework with x_{Al} mole fraction and V_{Si} is unit cell volume of purely siliceous zeolite framework. Considering the tetrahedral Al-O and Si-O bond length ($\sim 1.74 \text{ \AA}$ and $\sim 1.63 \text{ \AA}$, respectively), the Equation S10 transforms to:

$$V_x = V_{Si} \cdot (1 - (1 - 1.2842) \cdot x_{Al}) = V_{Si} \cdot (1 + 0.2842 \cdot x_{Al}) \quad (\text{Equation S11})$$

V_{Si} for purely siliceous zeolite FAU and MFI can be calculated employing the V_x of the zeolite with known framework x_{Al} . The data for H-FAU/30 and H-ZSM-5/23 used in the present study for UCS- x_{Al} correlation are detailed in Table S1.

Table S1. Acidity analysis (based on NH_3 physisorption) of individual zeolite components in ACM-101 formulation

Zeolite	SAR	$T_{\text{peak}} / ^\circ\text{C}$		Acidity / $\text{mmol}\cdot\text{g}^{-1}$			$V_{Si} / \text{\AA}^3$	Framework	
		Weak	Strong	Weak	Strong	Total		$x_{Al} / -$	Si:Al
H-FAU/30	30	110	328	0.66	0.42	1.08	14204	0.050	19
H-ZSM-5/23	23	124	402	1.69	0.57	2.26	5331	0.062	15

SAR - $\text{SiO}_2:\text{Al}_2\text{O}_3$ mole ratio

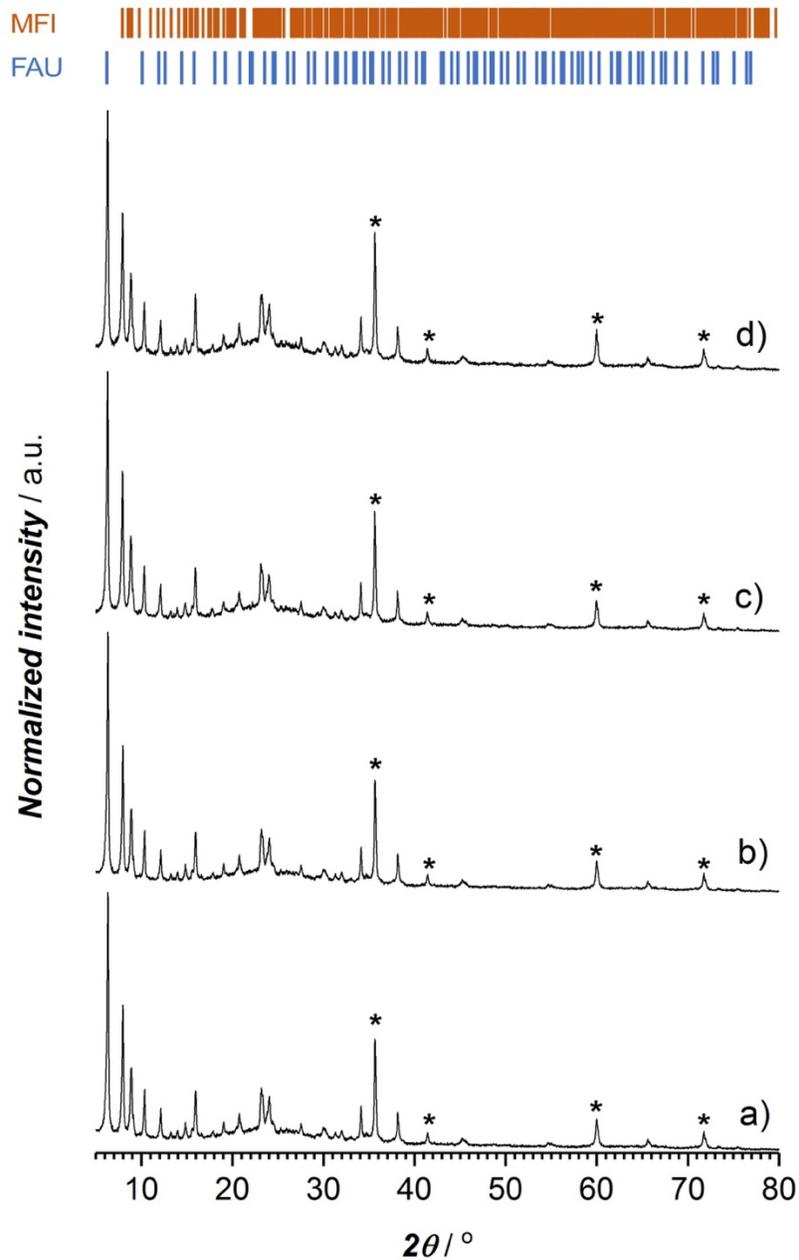


Figure S2. X-ray diffraction patterns of ACM-101 catalyst after calcination (a), steaming (b) and metal deposition steps, ACM-101-M-200 (c) and ACM-101-M-400 (d). Above on the graph expected reflection positions for FAU and MFI zeolite topologies. * marks diffractions attributed to cubic SiC.

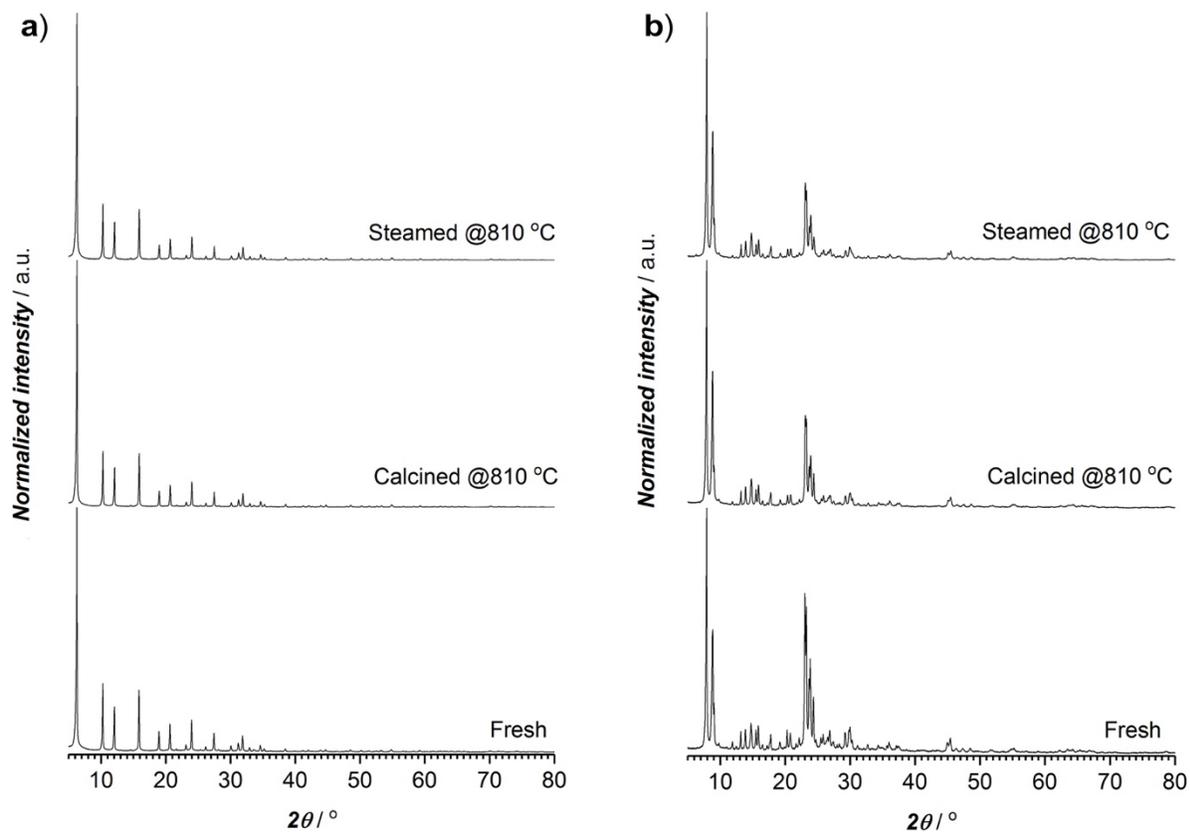


Figure S3. X-ray diffraction patterns of FAU/30 (a) and ZSM-5/23 (b) zeolites fresh, after calcination and steaming.

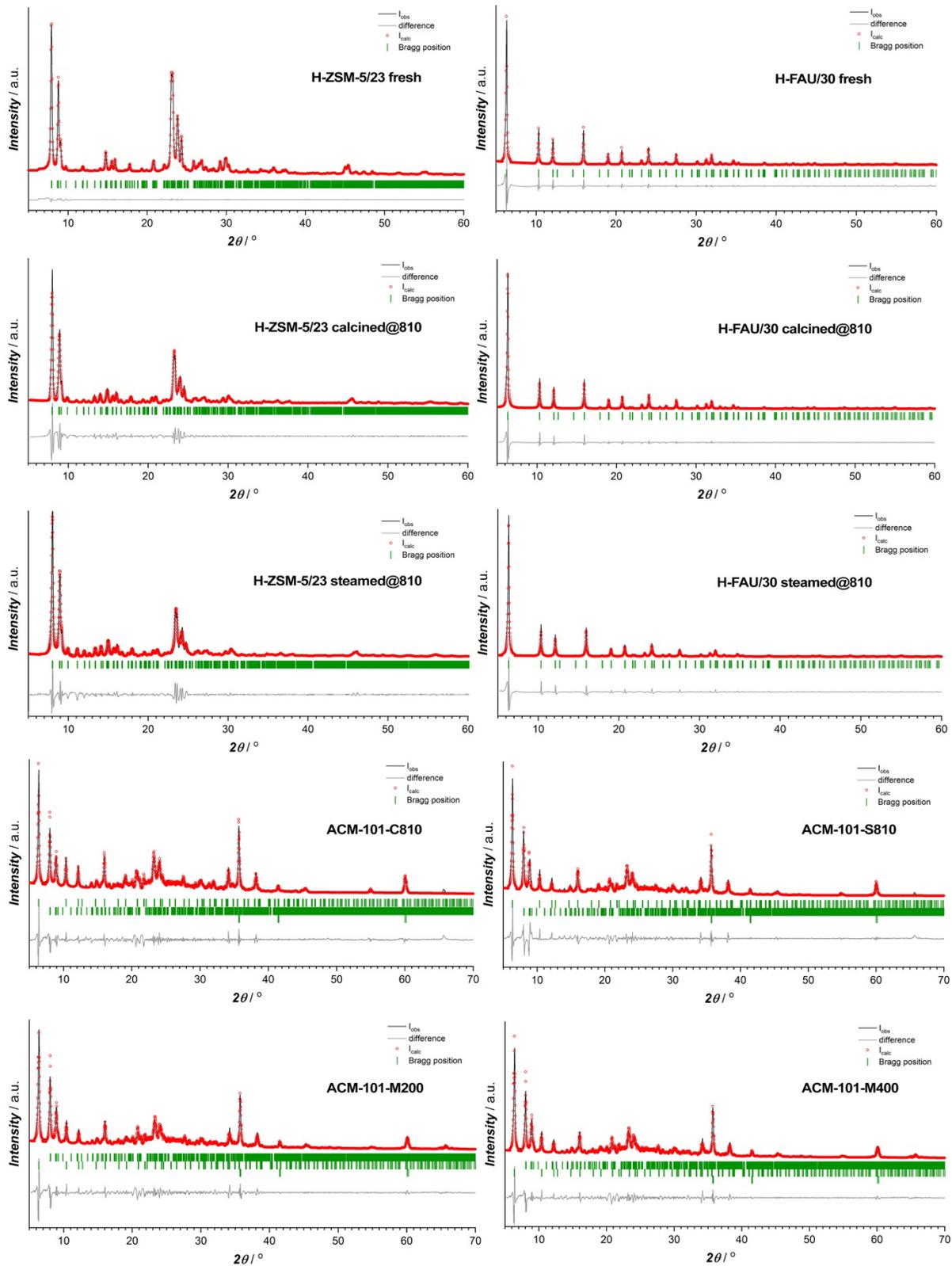


Figure S4. Pawley refinement plots for H-ZSM-5/23, H-FAU/30 fresh and ACM-101 after calcination and steaming treatments together with the same but after poison deposition steps.

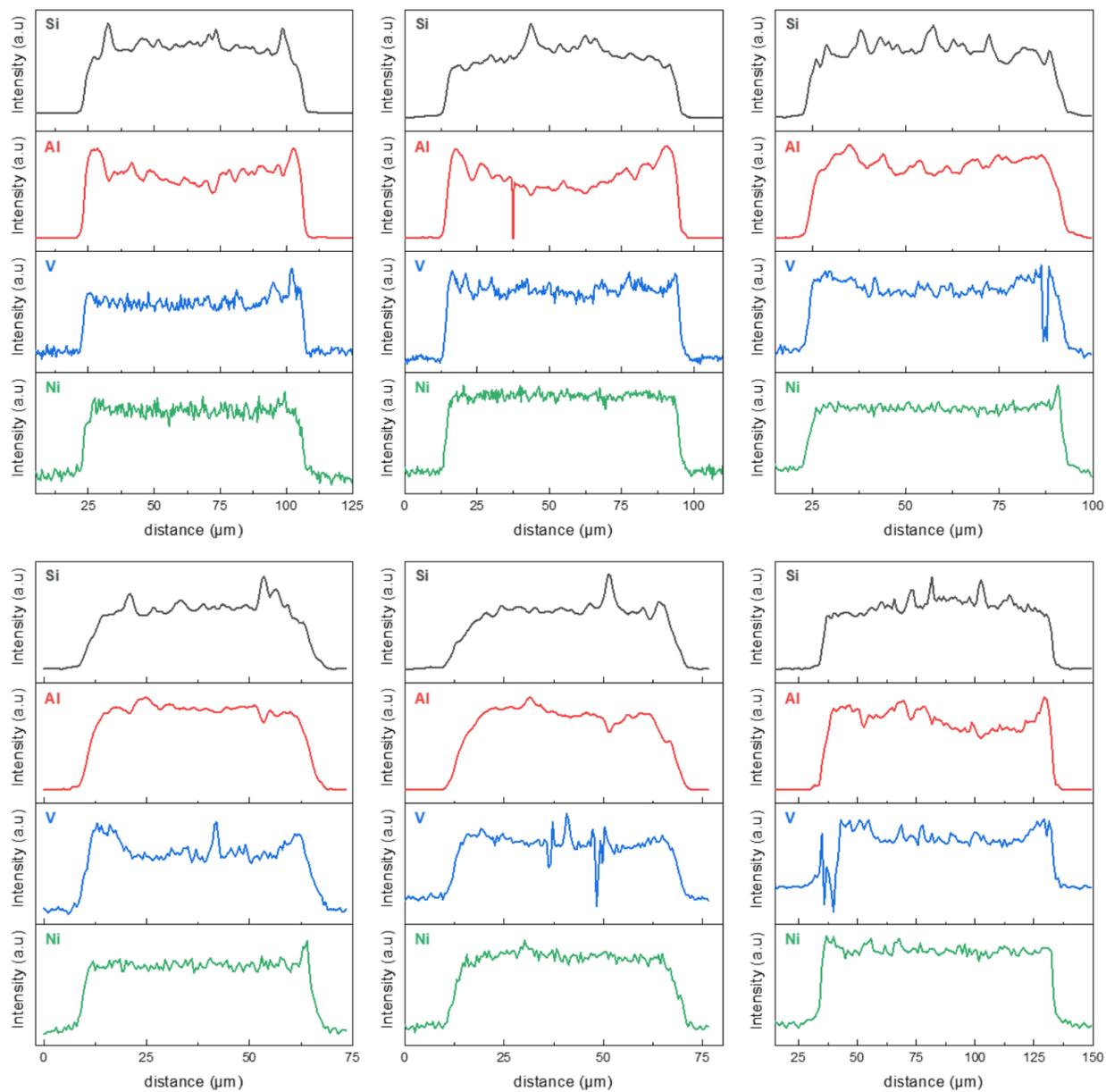


Figure S5. One dimensional analysis of the variation of X-ray intensities from $K\alpha$ fluorescence lines of Si, Al, V, and Ni elements across particle diameters.

Numerical data for distillation curves for Arabian light and liquid product after the catalytic cracking reaction:

Table S2. Distillation temperature of the Arabian Light crude and the liquid products after the catalytic cracking reaction at different mass recovery.

Product	Boiling Point / °C					
	5 wt.%	10 wt.%	30 wt.%	60 wt.%	80 wt.%	90 wt.%
Arabian Light	69	116	232	391	521	614
ACM-101-C800	131	152	205	277	360	430
ACM-101-S800	50	144	198	266	337	401
ACM-101-M200	187	244	198	266	336	397
ACM-101-M400	126	151	197	265	335	398

Table S3. Chemical composition of the Arabian Light crude and the liquid products after the catalytic cracking reaction.

Product	n-Paraffins / %	iso-Paraffins / %	Naphthenes / %	Aromatics / %
Arabian Light	47.6	28.1	17.6	6.8
ACM-101-C800	19.6	12.5	13.6	54.3
ACM-101-S800	22.8	16.8	15.3	45.1
ACM-101-M200	25.0	18.2	16.1	40.8
ACM-101-M400	23.7	15.5	17.8	43.0