

Supporting Information

Co₃O₄/TiO₂ Catalysts Studied *In Situ* During the Preferential Oxidation of Carbon Monoxide: *The Effect of Different TiO₂ Polymorphs*

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On-line gas chromatography

Table S1: Parameters set for achieving gas separation in the different modules of the micro-GC.

| Channel | 1 | 2 | 3 |
|----------------------------|--|-------------------------------------|----------------------------------|
| Detector type | TCD | TCD | TCD |
| Column type and length | Molecular Sieve 5Å PLOT, 20 m | PoraPLOT Q, 10 m | Molecular Sieve 5Å PLOT, 10 m |
| Injection temperature (°C) | 100 | 100 | 100 |
| Injection time (msec) | 40 | 40 | 40 |
| Carrier gas | H ₂ | H ₂ | Ar |
| Column temperature (°C) | 80 | 60 | 80 |
| Column pressure (kPa) | 150 | 80 | 150 |
| Duration (sec) | 270 | 270 | 270 |
| Gas(es) analysed | O ₂ , N ₂ , and CO | CH ₄ and CO ₂ | H ₂ |

The micro-GC (Varian CP-4900) was calibrated using two calibration gas cylinders – one having a mixture of 39.8% H₂, 18.5% CO, 15.9% CH₄, 10.1% CO₂, 9.9% Ar, and 5.8% N₂ (AFROX), and the other gas cylinder had synthetic air (21% O₂ in N₂, Air Products). From the chromatograms, response factors for each gas (except for N₂ and Ar) were calculated (see Equation S1) using N₂ as the reference, since it was present in both gas cylinders and was the only gas that would not get consumed under reaction conditions. To calculate the volumetric flow rate for each gas, Equation S2 was used.

$$F_i = \frac{A_{N_2} \cdot v_{i, in}}{A_i \cdot v_{N_2, in}} \quad (S1)$$

$$v_{i, out}(mL/min) = F_i \cdot \frac{A_i \cdot v_{N_2, in}}{A_{N_2}} \quad (S2)$$

F_i is the response factor of gas component i with reference to N_2 . A_{N_2} is the calculated peak area of nitrogen, and A_i is the calculated peak area of gas component i . $v_{N_2, in}$ is the volumetric gas flow rate of nitrogen, and $v_{i, in}$ is the volumetric gas flow rate of gas component i entering the system during the GC calibrations or the CO-PrOx experiments. Finally, $v_{i, out}$ is the volumetric gas flow rate of gas component i exiting the reactor during CO-PrOx.

The performance of the catalyst was assessed by calculating normalised gas outlet flow rates (Equation S3), conversions/yields (Equations S4 and S5), and selectivities (Equation S6).

$$v_{j,out}^- = \frac{v_{j, out}}{v_{i, in}} \quad (S3)$$

$$X_{CO \rightarrow CO_2} \text{ or } Y_{CO_2} (\%) = \frac{v_{CO, in} - v_{CO, out} - v_{CH_4, out}}{v_{CO, in}} \times 100 = \frac{v_{CO_2, out}}{v_{CO, in}} \times 100 \quad (S4)$$

$$X_{CO \rightarrow CH_4} \text{ or } Y_{CH_4} (\%) = \frac{v_{CO, in} - v_{CO, out} - v_{CO_2, out}}{v_{CO, in}} \times 100 = \frac{v_{CH_4, out}}{v_{CO, in}} \times 100 \quad (S5)$$

$$S_{O_2 \rightarrow CO_2} (\%) = \frac{v_{CO, in} - v_{CO, out} - v_{CH_4, out}}{2 \cdot (v_{O_2, in} - v_{O_2, out})} \times 100 = \frac{v_{CO_2, out}}{2 \cdot (v_{O_2, in} - v_{O_2, out})} \times 100 \quad (S6)$$

$v_{j,out}^-$ is the normalised gas outlet flow rate of gas j .

***Ex situ* catalyst characterisation**

Powder X-ray diffraction (PXRD) measurements on the fresh supported catalysts were carried out in a Bruker D8 Advance Laboratory X-ray diffractometer equipped with a Co X-ray source ($\lambda_{\text{K}\alpha 1} = 0.178897 \text{ nm}$) and a position-sensitive detector (LYNXEYE XE, Bruker AXS). The diffractometer was operated at 35 kV and 40 mA, and the optics were set to Bragg-Brentano geometry. A 2θ measurement window of $20 - 120^\circ$ (or a $1/d$ range of $1.9 - 9.7 \text{ nm}^{-1}$, where “d” is the d-spacing), a step size of 0.043° ($4.2 \times 10^{-3} \text{ nm}^{-1}$), and a time per step of 0.75 s were applied (total scan time: 29 min and 50 s). We note that two different X-ray sources (one on each diffractometer) were used in the current work, *i.e.*, Co for the *ex situ* measurements and Mo ($\lambda_{\text{K}\alpha 1} = 0.07093 \text{ nm}$) for the *in situ* measurements (see section 2.2. of the main paper and the section “*In situ* catalyst characterisation” in the Supporting Information). This can result in dissimilar 2θ positions (or values) for the reflections of the same crystalline phase. Therefore, we chose to plot all *ex situ* and *in situ* diffraction patterns as a function of $1/d$ instead of 2θ to eliminate this effect (see example in Figure S1 and the Bragg Law equation¹ (Equation S7)).

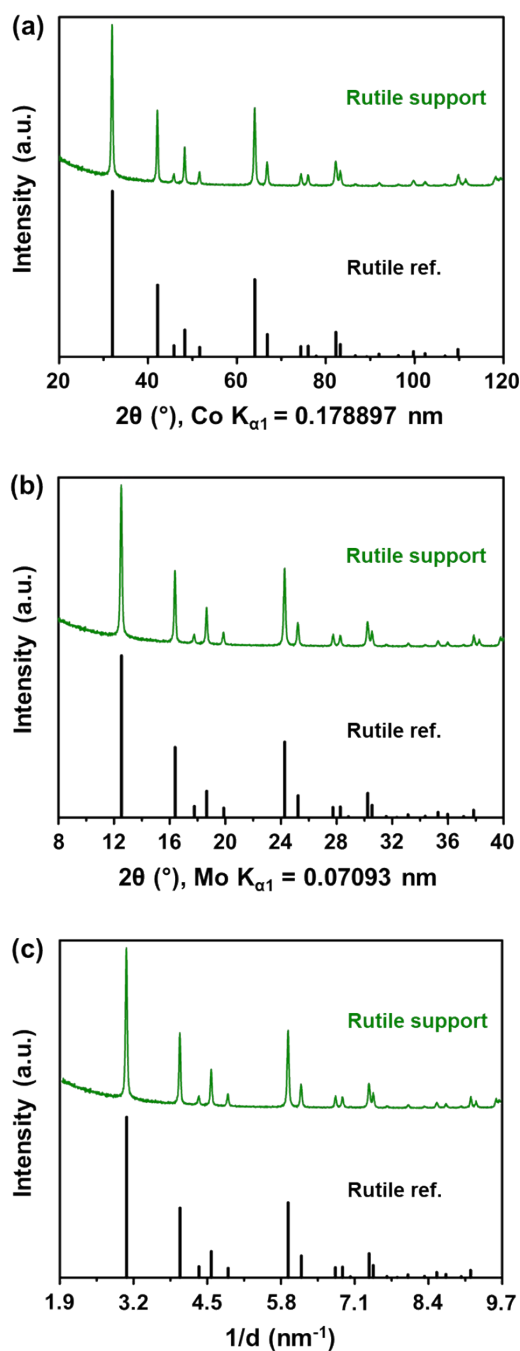


Figure S1: (a) *Ex situ* PXRD pattern of the bare Rutile support recorded using a Co X-ray source. The same PXRD pattern is replotted (b) as a function of the expected 2θ positions from a Mo X-ray source, and (c) as a function of the unifying parameter, $1/d$ (also see Bragg Law equation¹ - Equation S7). Note that all reflections from Rutile (see Table S2 for the ICDD PDF-2 entry) are expected to be at much lower diffraction angles when using a Mo source than when using a Co source.

$$\frac{1}{d} (nm^{-1}) = \frac{2 \sin \theta_{Co}}{\lambda_{Co}} = \frac{2 \sin \theta_{Mo}}{\lambda_{Mo}} \quad (S7)$$

d is the interplanar distance or d-spacing, θ_{Co} and θ_{Mo} are the measured diffraction angles (normally reported as 2θ) from a PXRD instrument equipped either with a cobalt source of X-ray wavelength λ_{Co} or a molybdenum source of X-ray wavelength λ_{Mo} , respectively.

All recorded *ex situ* diffraction patterns were compared with known diffraction patterns found in the International Centre for Diffraction Data (ICDD) Powder Diffraction File-2 (PDF-2) database² to determine the chemical and crystallographic phases present. A summary of the PDF entries accessed can be found in Table S2. Rietveld refinement was carried out using the TOPAS 5.0 software package³ (Bruker AXS) to quantify the Co-based phases present in terms of their relative weight fraction and volume-based average crystallite size.

Table S2: ICDD PDF-2 entries of all chemical/crystal phases relevant to the current study.

| Chemical formula | Chemical name | PDF entry |
|-----------------------------------|--|-------------|
| α -Co | α -Cobalt (hexagonal) | 01-071-4239 |
| β -Co | β -Cobalt (cubic) | 00-015-0806 |
| CoO (cubic) | Cobalt(II) oxide (cubic) | 00-043-1004 |
| Co ₃ O ₄ | Cobalt(II,III) oxide | 01-073-1701 |
| CoTiO ₃ (rhombohedral) | Cobalt(II) titanium(IV) oxide (rhombohedral) | 00-029-0516 |
| CoTiO ₃ (cubic) | Cobalt(II) titanium(IV) oxide (cubic) | 00-015-0866 |
| TiO ₂ (anatase) | Titanium(IV) oxide (anatase) | 01-089-4921 |
| TiO ₂ (rutile) | Titanium(IV) oxide (rutile) | 01-089-4202 |

Scanning transmission electron microscopy (STEM) was performed on all fresh and spent catalysts in a JEM-ARM200F microscope (JEOL) equipped with a field emission cathode and an integrated correction of the spherical aberrations of the objective and condenser lenses. The instrument is fitted with an advanced GIF (Gatan Image Filter) electron spectrometer with electron energy loss spectroscopy (EELS) capabilities. Lacey carbon sample grids (Agar Scientific) were utilised for the STEM analysis. Particle size measurements were carried out using the freeware ImageJ 1.15a.⁴ Thereafter, the number- and volume-based average particle sizes, and the associated standard deviations were calculated using Equations S8 – S11. The STEM-derived volume-based average particle sizes can be compared with the PXRD-derived average crystallite sizes since they are also volume-based.

$$\text{number - based average } (\bar{d}_{c,n}) = \frac{\sum_{i=1}^N n_i d_i}{N} \quad (S8)$$

$$\text{volume - based average } (\bar{d}_{c,v}) = \frac{\sum_{i=1}^N n_i d_i^4}{\sum_{i=1}^N n_i d_i^3} \quad (S9)$$

$$\text{number - based standard deviation } (sd_n) = \sqrt{\frac{\sum_{i=1}^N n_i (d_i - \bar{d}_{c,n})^2}{N - 1}} \quad (S10)$$

$$\text{volume - based standard deviation } (sd_v) = \sqrt{\frac{\sum_{i=1}^N n_i d_i^3 (d_i - \bar{d}_{c,v})^2}{\frac{N-1}{N} \sum_{i=1}^N n_i d_i^3}} \quad (S11)$$

d_i is the diameter of particle i , n_i is the number of particles of size d_i , and N is the total number of particles counted. The above equations can also be found in the book chapter by Bergeret and Gallezot.⁵

Nitrogen physisorption was conducted on all bare supports and fresh supported catalysts in a Micromeritics TriStar II 3020 after degassing the samples (*ca.* 0.3 g each) at 200 °C overnight. The mass-specific surface area of each sample was calculated using the Brunauer–Emmett–Teller (BET) method. The mass-specific pore volume was calculated by applying the Barrett–Joyner–Halenda (BJH) method.

The fresh catalysts (*ca.* 0.05 g each) for elemental analysis, performed using inductively coupled plasma-optical emission spectroscopy (ICP-OES), were pre-treated overnight in a 3:1:1 mixture of HCl:HNO₃:HF. Subsequently, the mixture was heated at a rate of 6.4 °C/min to 180 °C for 40 min for digestion in a MARS-5 microwave digester to ultimately obtain the Co loadings/concentrations in a Varian ICP-OES 730 instrument (Agilent).

X-ray absorption spectroscopy (XAS) measurements were performed at the Co K-edge (7709 eV) on beamline B18 at Diamond Light Source (United Kingdom), operating with a ring energy of 3 GeV and a ring current of 300 mA.⁶ A Co foil was used for energy calibration. The scans were performed in quick extended X-ray absorption fine structure (QEXAFS) mode from 7509 to 8559 eV, with a resolution of 0.3 eV/point, and each scan was approximately 3 min. Three scans were recorded for each sample to check reproducibility and to obtain a good signal-to-noise ratio. The samples were diluted with cellulose and pressed into discs prior to being measured in transmission mode. The data processing was performed using the Athena software, which is part of the open-source software package Demeter⁷ (based on the IFEFFIT library⁸). Linear combination fitting (LCF) was performed between 7675 and 7825 eV (*i.e.*, -50 eV before the edge and +100 eV after the edge). The reference spectra considered for the LCF were of Co₃O₄,⁹ CoO,¹⁰ CoTiO₃,¹¹ and Co foil.⁶ These reference samples were synthesised according to the procedures outlined in the cited literature.

***In situ* catalyst characterisation**

Reduction studies

The reduction of the supported catalysts (*ca.* 0.012 g each) was carried out in a gas flow of 50% H₂ in N₂ (1.2 mL(NTP)/min) at atmospheric pressure using a capillary-based reaction cell (developed at the University of Cape Town (UCT), South Africa).^{12–14} The cell was mounted on a Bruker D8 Advance Laboratory X-ray diffractometer, equipped with a Mo X-ray source ($\lambda_{\text{K}\alpha 1} = 0.07093$ nm) and a position-sensitive detector (VANTEC, Bruker AXS), to allow for PXRD patterns to be recorded during the reduction. The diffractometer was operated at 50 kV and 35 mA, and the optics were set to parallel beam geometry to minimise possible peak shifts due to sample height differences.

The cell uses a fixed-bed capillary reactor (made of borosilicate glass, length: 75 mm, wall thickness: 0.02 mm, and O.D.: 1.0 mm (Capillary Tube Supplies LTD, UK)), through which gas can be flowed using a mass flow controller (Brooks Instruments). The loaded reactor was heated from 50 to 450 °C (at a rate of 1 °C/min), and thereafter, the temperature was held at 450 °C for 2 h. A 2θ measurement window of 15 – 30° (or a $1/d$ range of 3.7 – 7.3 nm⁻¹), a step size of 0.019° (4.7 x 10⁻³ nm⁻¹), and a time per step of 0.20 s were applied (total scan time: 4 min and 2 s, with an added 58-s delay between scans). PXRD patterns were recorded every 5 min throughout each reduction experiment. All recorded *in situ* diffraction patterns were compared with known diffraction patterns in the ICDD PDF-2 database², and Rietveld refinement was carried out using the TOPAS 5.0 software package³ (Bruker AXS).

Conventional H₂-TPR was conducted on the bare supports and supported Co₃O₄ catalysts. A sample of 0.1 g was placed between two pieces of quartz wool in a U-shaped quartz reactor. The reduction was carried out in a Micromeritics AutoChem 2920 instrument, equipped with

a thermal conductivity detector (TCD) for measuring the H₂ consumption. The sample was firstly dried by heating the reactor from room temperature to 120 °C at a rate of 10 °C/min under a flow of Ar (10 mL(NTP)/min), and then keeping the temperature at 120 °C for 60 min. Thereafter, the temperature was decreased to 60 °C before switching the gas flow to 5% H₂ in Ar (50 mL(NTP)/min). Under this reducing gas mixture, the reactor was heated to 920 °C at a rate of 10 °C/min, which was kept for 10 min before cooling to room temperature. The H₂ consumption was measured every 0.1 min (6 s) between 60 and 920 °C after introducing the reducing gas. The degree of reduction (DoR) of Co₃O₄ to Co⁰ in the TiO₂-supported catalysts was calculated based on the instrument calibration performed using different known amounts of Ag₂O (also see Equations S12 – S14).



$$\text{H}_2 \text{ consumption (mmol)} = 2.8 \cdot 10^{-2} + A_{\text{peak}} \cdot 2.3 \cdot 10^{-1} \quad (\text{S13})$$

$$\text{Degree of reduction (\%)} = \frac{\text{H}_2 \text{ consumption}}{x \cdot n_{\text{metal oxide loaded}}} \times 100 \quad (\text{S14})$$

A_{peak} is the area of the peak in the chromatogram. x is the H₂:metal oxide molar ratio as shown in Equation S12. $n_{\text{metal oxide loaded}}$ is the amount (in mmol) of Co₃O₄ in the supported catalysts loaded in the H₂-TPR quartz reactor.

Catalytic evaluation

The magnetometer uses a ½-inch stainless steel fixed-bed reactor (I.D.: 9.7 mm) that is placed vertically between two pole caps of a current-controlled electro-magnet (maximum external field strength: 2 T (or 20 kOe), Bruker Analytik GmbH). PXRD patterns and magnetisation measurements (at 2 T) were recorded every 5 min in the separate *in situ* instruments. The scan parameters (*i.e.*, 2θ (or 1/d) range, step size, and time per step) used for the PXRD-based reduction studies (section 2.2.1.) were also applied for the PXRD-based CO-PrOx reactions. The data from the magnetisation measurements were used to calculate the DoR of Co₃O₄ to

Co⁰ using Equation S15, which is based on quantities from a pre-determined calibration curve (Figure S2).

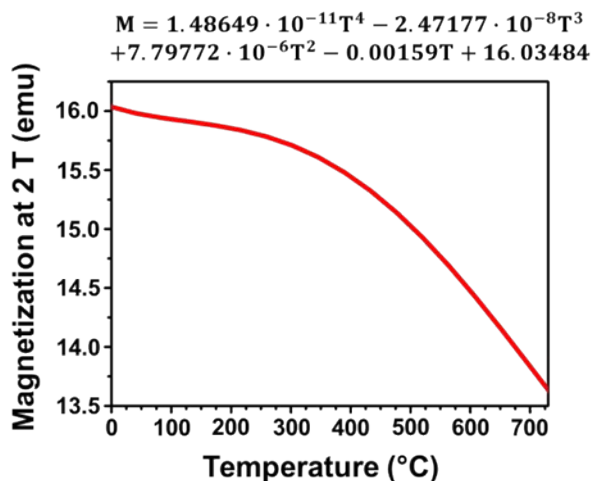


Figure S2: Calibration curve for the magnetometer based on a 0.1 g pre-reduced unsupported Co⁰ sample.

$$DoR(\%) = \frac{M_{sample} \cdot 0.1}{M_{calibration} \cdot X_{loading} \cdot m_{unreduced\ sample}} \times 100 \quad (S15)$$

M_{sample} is the sample magnetisation (in emu) at any temperature within the temperature window used in this study and $M_{calibration}$ is the corresponding magnetisation of Co⁰ (in emu) from the calibration curve in Figure S2 at the same temperature. $X_{loading}$ is the metal loading as determined from ICP-OES and $m_{unreduced\ sample}$ is the mass of the unreduced supported sample (in g) loaded into the reactor.

***Ex situ* PXRD and STEM-EELS results for the bare supports and fresh supported catalysts**

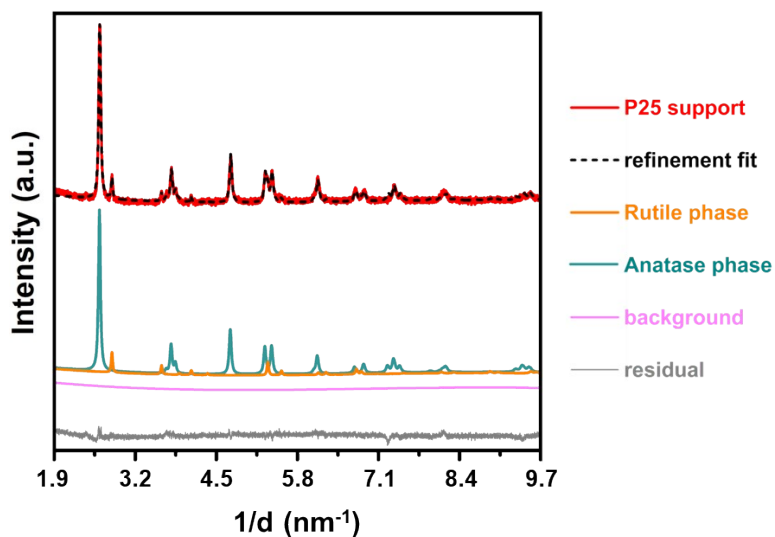


Figure S3: *Ex situ* PXRD pattern (radiation source: Co K α 1 = 0.178897 nm) of the bare P25 support. Also included are the Rietveld refinements results in terms of the fitted crystallographic phases. The Rwp value can be found in Table S3.

Table S3: Rietveld refinement results for the bare P25 support.

| Sample name | Rutile | | Anatase | | Rwp (%) |
|-------------|--------------------------|----------------------------|--------------------------|----------------------------|---------|
| | Crystallite size (nm) | Weight fraction (wt.-%) | Crystallite size (nm) | Weight fraction (wt.-%) | |
| P25 support | 42.1 \pm 1.8 | 14.7 \pm 0.4 | 25.8 \pm 1.6 | 85.3 \pm 0.4 | 3.7 |

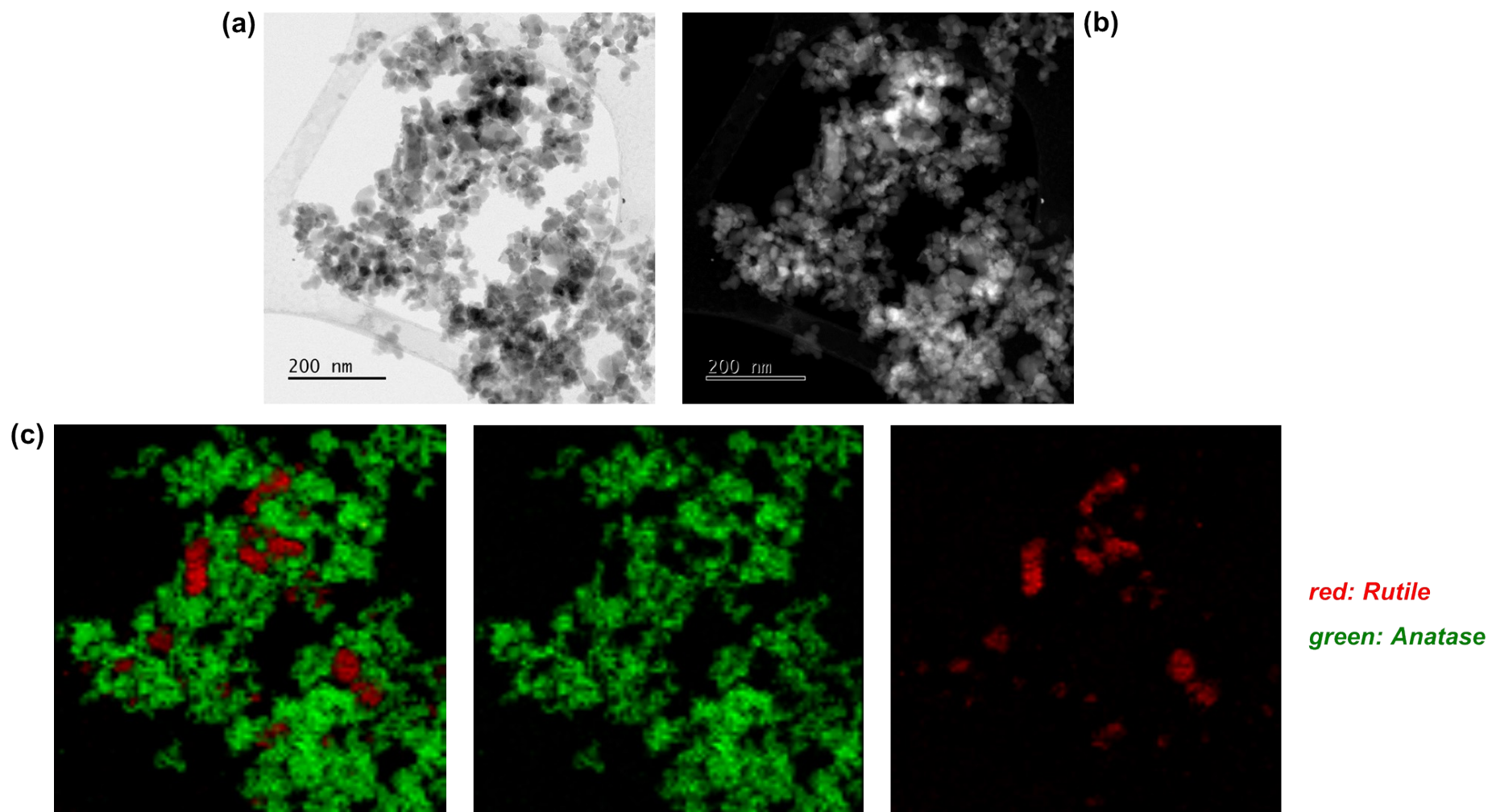


Figure S4: (a) Bright- and (b) dark-field STEM micrographs of the fresh $\text{Co}_3\text{O}_4/\text{P25}$ catalyst. (c) Phase composition maps derived using EELS showing the Anatase and Rutile regions in the fresh catalyst.

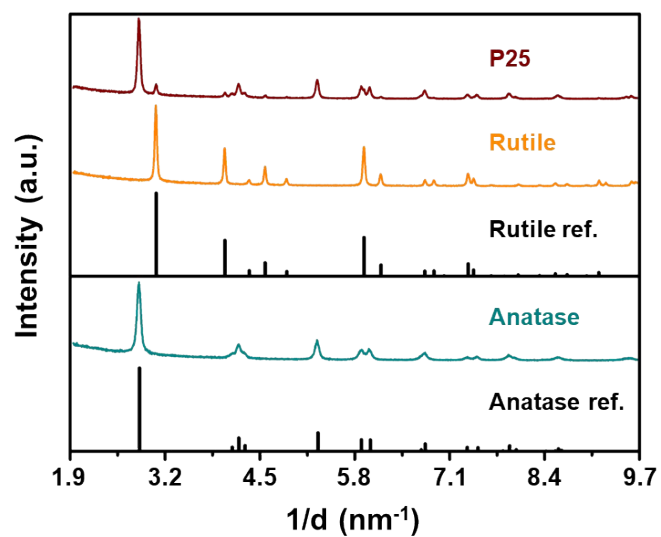


Figure S5: *Ex situ* PXRD patterns (X-ray source: Co K α 1 = 0.178897 nm) of the bare support materials and the corresponding reference reflection lines. See Table S2 for the ICDD PDF-2 entries of Rutile and Anatase.

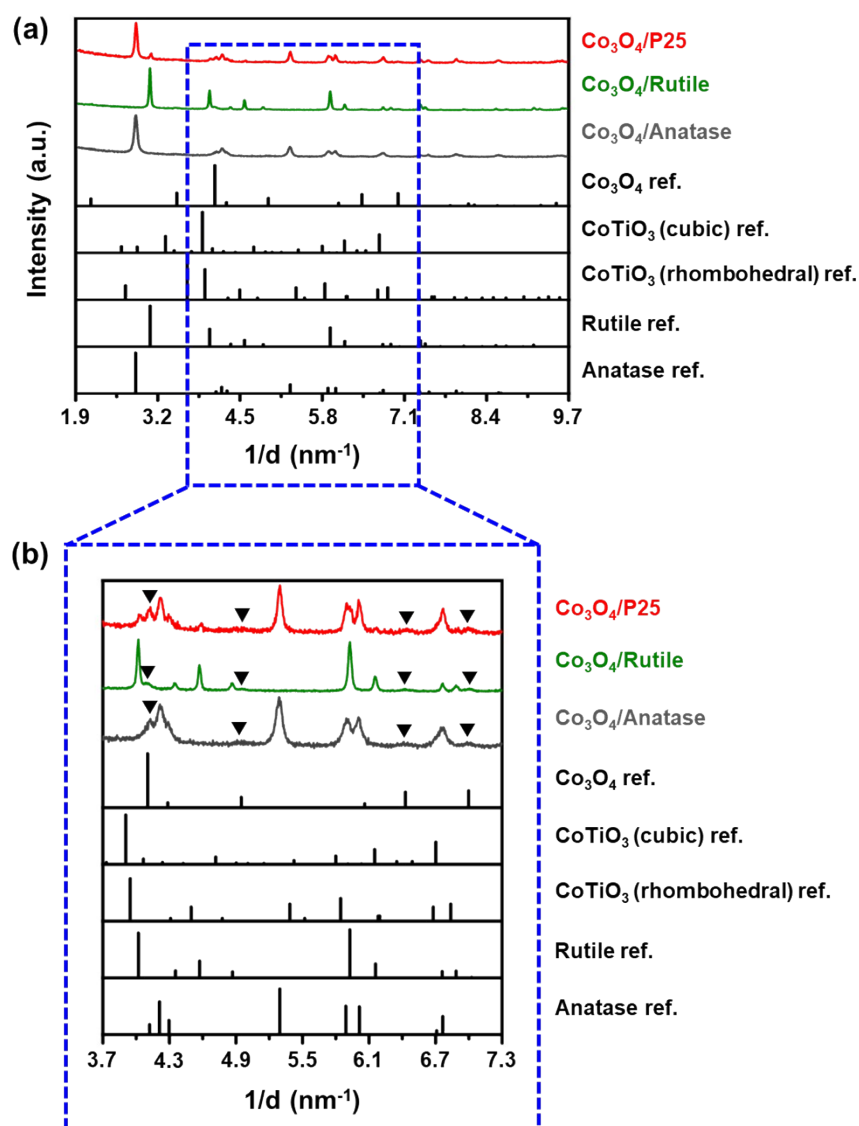


Figure S6: (a) PXRD patterns (X-ray source: Co K α 1 = 0.178897 nm) of the supported fresh samples as well as the reference reflection lines for Co₃O₄, CoTiO₃ (cubic and rhombohedral), Rutile, and Anatase as recorded in the ICDD PDF-2 database (see Table S2 for the PDF entries). (b) Magnified short 1/d range of the recorded PXRD patterns enhancing the visibility of the Co₃O₄ reflections. The black triangles indicate the identified Co₃O₄ reflections in each diffraction pattern.

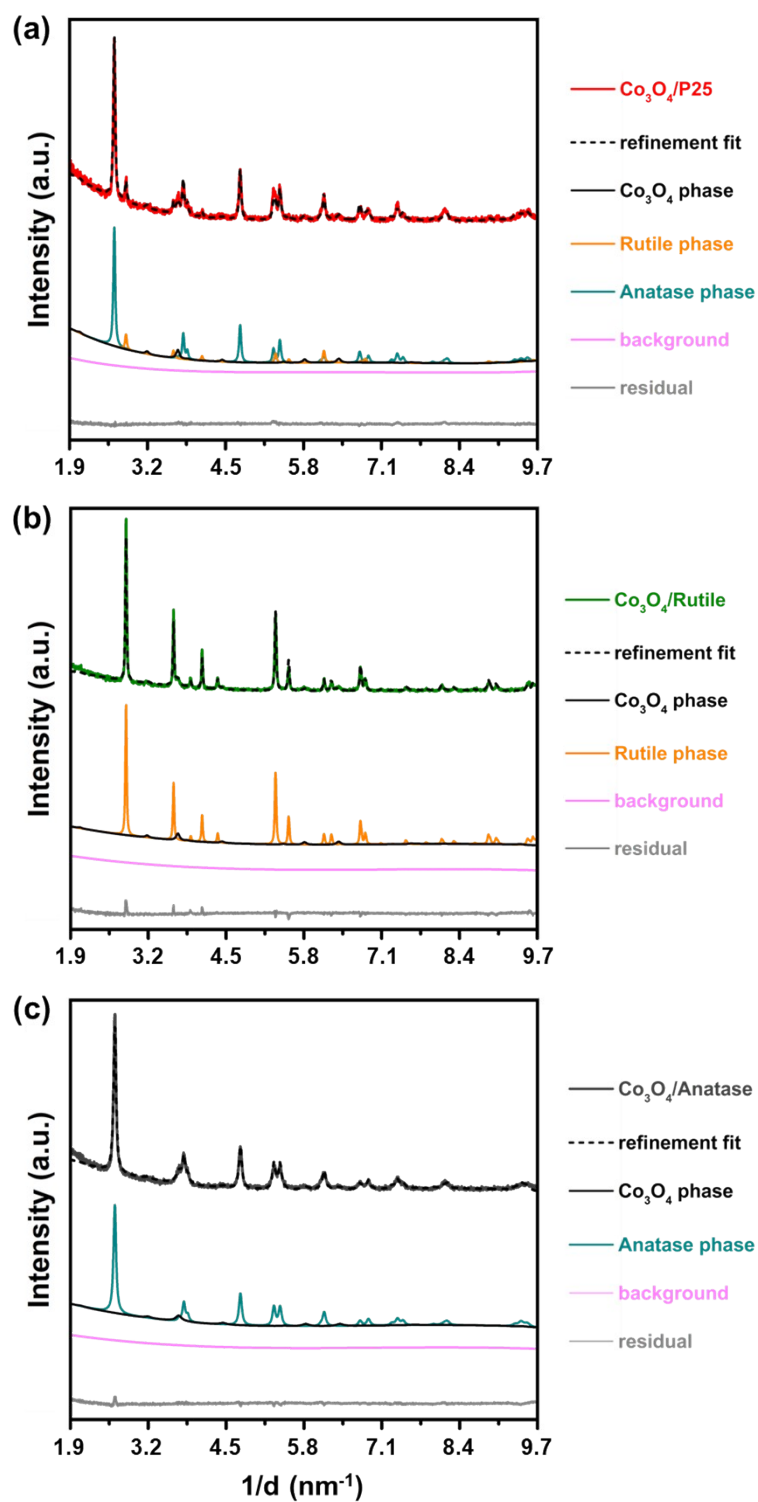


Figure S7: *Ex situ* PXRD pattern (X-ray source: Co $K\alpha 1 = 0.178897$ nm) of (a) $\text{Co}_3\text{O}_4/\text{P25}$, (b) $\text{Co}_3\text{O}_4/\text{Rutile}$, and (c) $\text{Co}_3\text{O}_4/\text{Anatase}$. Also included are the Rietveld refinements results in terms of the fitted crystallographic phases. The R_{wp} values can be found in Table S3.

Table S4: Rietveld refinement results for the fresh supported catalysts.

| Sample name | Rutile | | Anatase | | Co ₃ O ₄ | | Rwp (%) |
|---|-----------------------|-------------------------|-----------------------|-------------------------|--------------------------------|-------------------------|---------|
| | Crystallite size (nm) | Weight fraction (wt.-%) | Crystallite size (nm) | Weight fraction (wt.-%) | Crystallite size (nm) | Weight fraction (wt.-%) | |
| Co ₃ O ₄ /P25 | 30.1 ± 2.1 | 10.5 ± 0.3 | 27.9 ± 0.5 | 79.2 ± 0.3 | 11.8 ± 0.3 | 10.3 ± 0.3 | 10.1 |
| Co ₃ O ₄ /Rutile | 47.9 ± 0.8 | 89.7 ± 0.5 | - | - | 14.7 ± 0.3 | 10.3 ± 0.5 | 11.4 |
| Co ₃ O ₄ /Anatase | - | - | 18.1 ± 0.3 | 91.5 ± 0.3 | 9.8 ± 0.2 | 8.5 ± 0.3 | 10.8 |

In situ PXRD-based reduction results

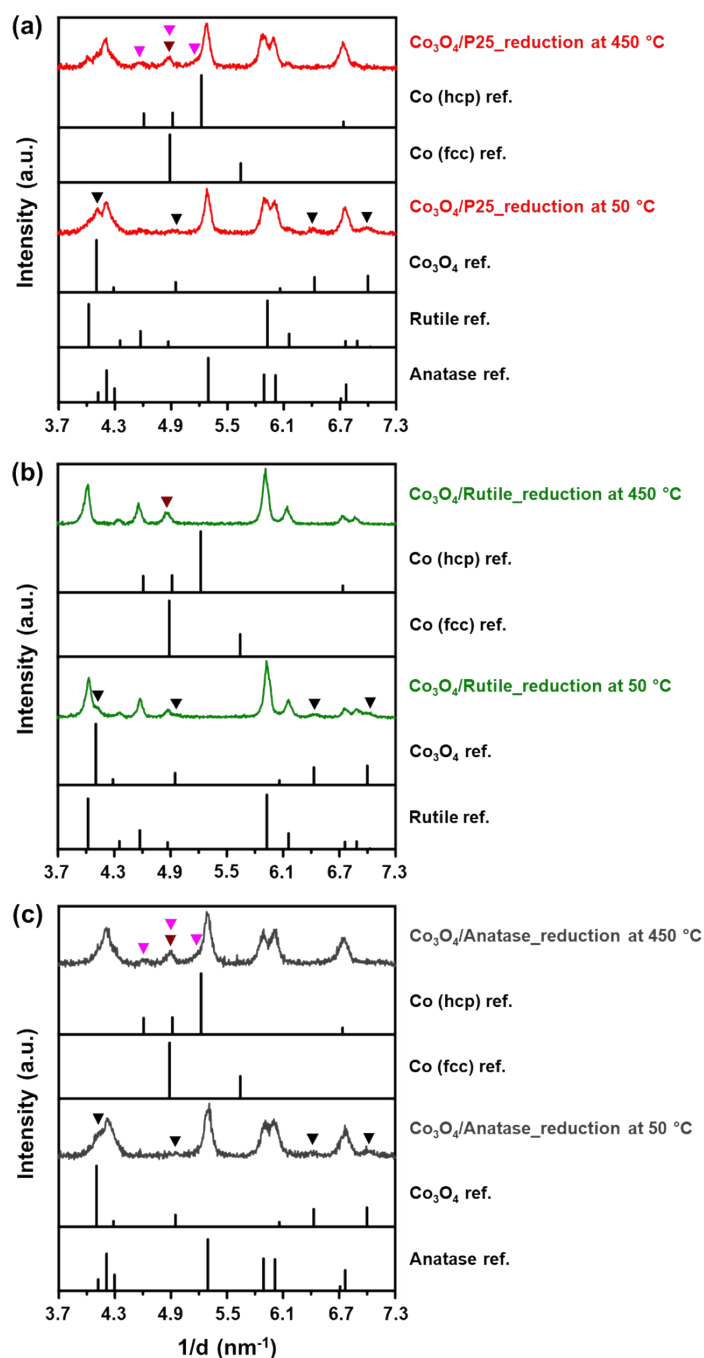


Figure S8: *In situ* PXRD patterns of (a) Co₃O₄/P25, (b) Co₃O₄/Rutile, and (c) Co₃O₄/Anatase recorded at 50 and 450 °C during reduction in a 50:50 H₂:N₂ mixture at atmospheric pressure. The reference reflection lines of metallic Co (fcc and hcp Co⁰), Co₃O₄, Rutile, and Anatase are also included. The brown, magenta and black triangles indicate the reflections of fcc Co⁰, hcp Co⁰, and Co₃O₄, respectively. Note that there exists some overlap between the reflections of the Co-based phases and those of the Rutile and/or Anatase crystal phases.

H₂-TPR profile of Co₃O₄/Anatase and equations for calculating the degree of reduction

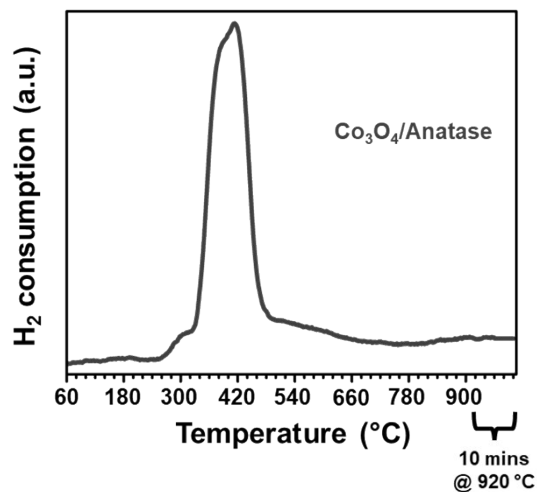


Figure S9: Reduction profile of Co₃O₄/Anatase derived from H₂-TPR performed in a 5:95 H₂:Ar mixture at atmospheric pressure.

***In situ* PXRD patterns obtained during dry CO-PrOx and magnetometer calibration**

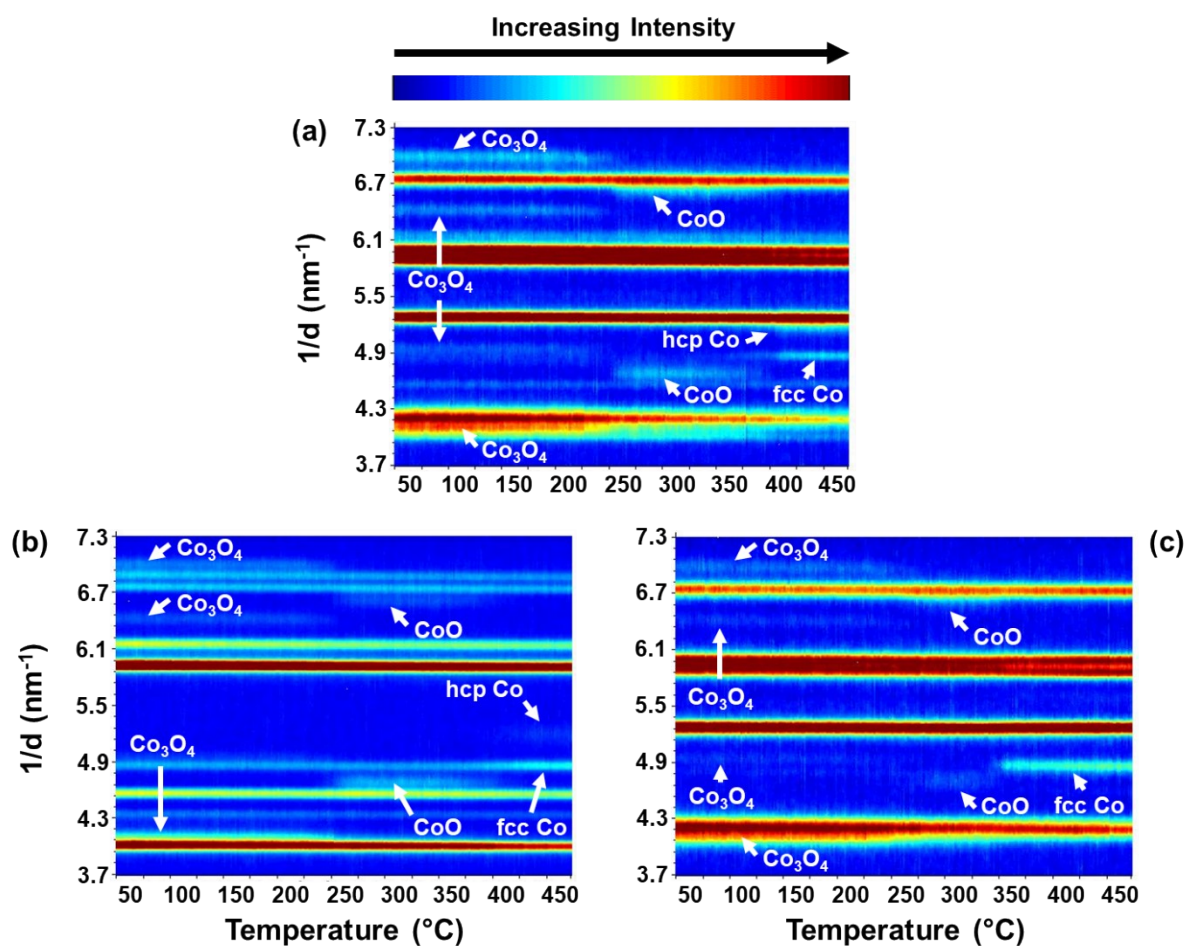


Figure S10: On-top view of the PXRD patterns recorded during dry CO-PrOx over (a) Co₃O₄/P25, (b) Co₃O₄/Rutile, and (c) Co₃O₄/Anatase. (Gas composition: 1% CO, 1% O₂, 50% H₂, 48% N₂; pressure: atmospheric; GHSV: 60000 mL(NTP)/g_{Co₃O₄}/h).

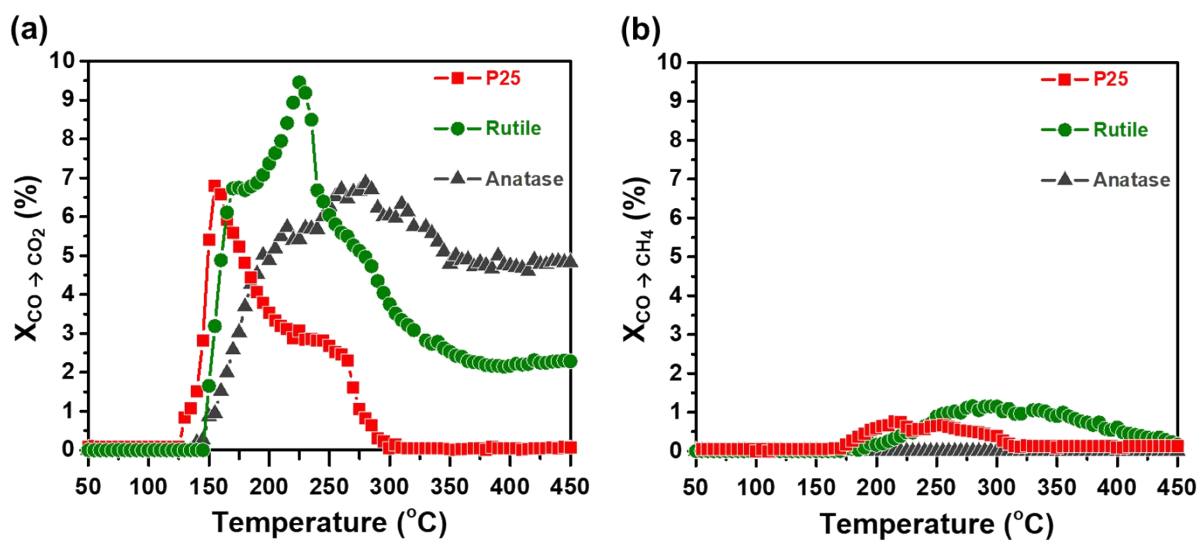


Figure S11: (a) CO conversion to CO₂ ($X_{\text{CO} \rightarrow \text{CO}_2}$), and (b) CO conversion to CH₄ ($X_{\text{CO} \rightarrow \text{CH}_4}$) during CO-PrOx for all bare supports. (Gas composition: 1% CO, 1% O₂, 50% H₂, and 48% N₂; pressure: atmospheric; GHSV: 60000 mL(NTP)/g_{TiO₂}/h).

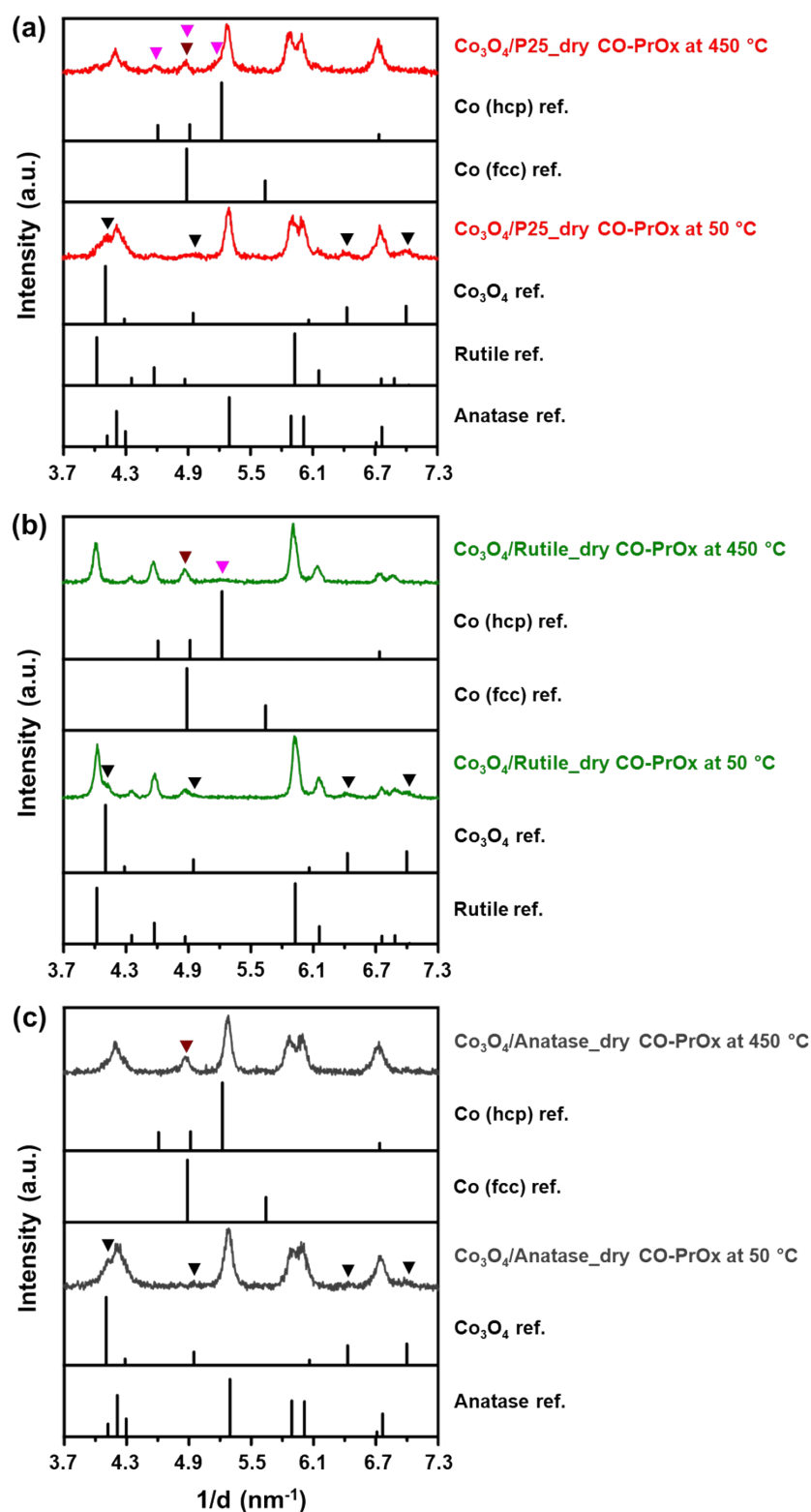


Figure S12: *In situ* PXRD patterns of (a) $\text{Co}_3\text{O}_4/\text{P25}$, (b) $\text{Co}_3\text{O}_4/\text{Rutile}$, and (c) $\text{Co}_3\text{O}_4/\text{Anatase}$ recorded at 50 and 450 °C during dry CO-PrOx. The reference reflection lines of metallic Co (fcc and hcp Co^0), Co_3O_4 , Rutile, and Anatase are also included. The brown, magenta, and black triangles indicate the reflections of fcc Co^0 , hcp Co^0 , and Co_3O_4 , respectively. Note that there exists some overlap between the reflections of the Co-based phases and those of the Rutile and/or Anatase crystal phases.

Results from thermodynamic calculations: Gibbs free energy and $p_{\text{H}_2}/p_{\text{H}_2\text{O}}$ as a function of temperature

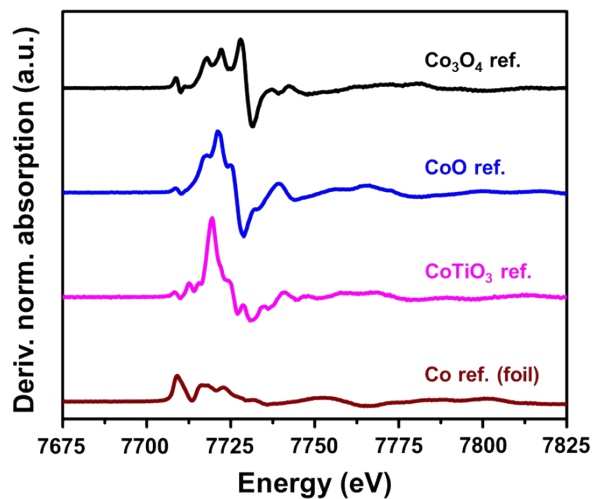


Figure S13: Normalised first derivative XANES spectra of the reference compounds.

Results from thermodynamic calculations: Gibbs free energy and p_{H_2}/p_{H_2O} as a function of temperature

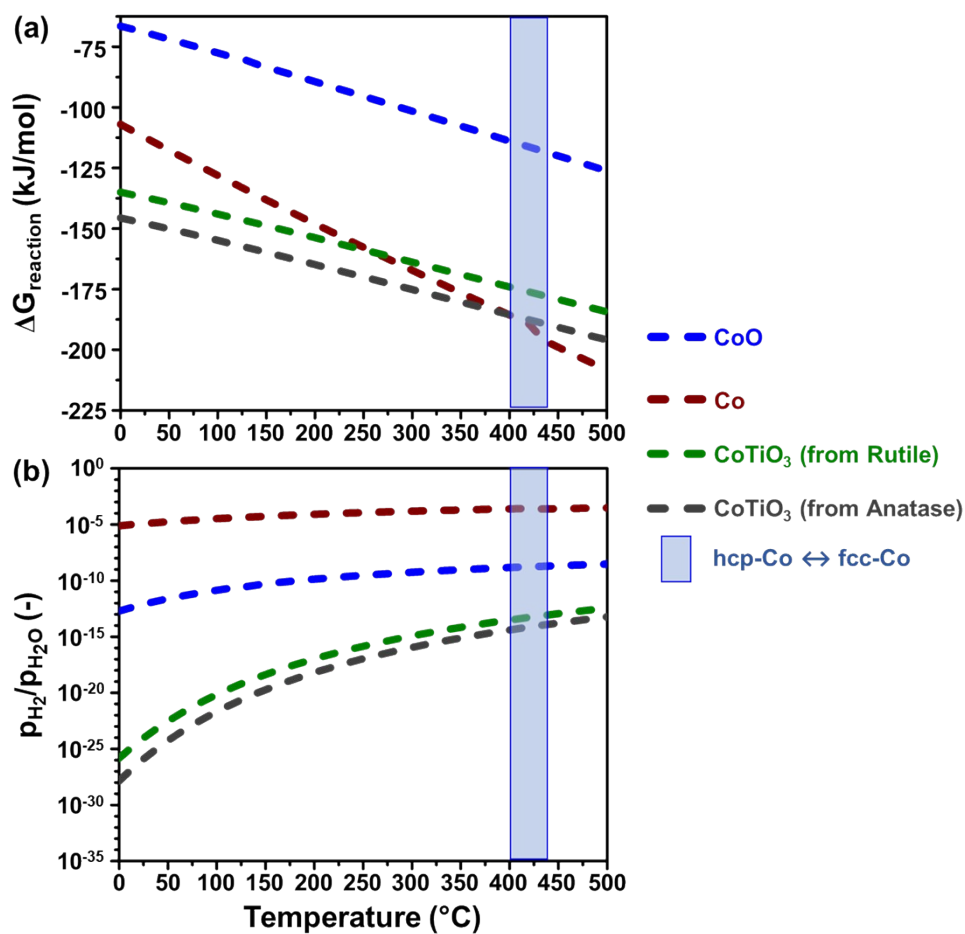
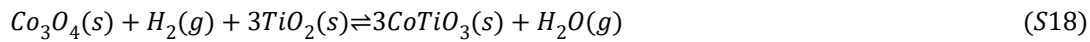


Figure S14: (a) Gibbs free energy and (b) p_{H_2}/p_{H_2O} as a function of temperature at 1.013 bar during the reduction of bulk Co_3O_4 to CoO , Co^0 , or $CoTiO_3$ (the latter would involve either of the two TiO_2 crystal phases, *viz.*, Anatase or Rutile – see Equation S18), respectively. The light blue shaded area indicates the temperature region where bulk hcp Co^0 transforms into bulk fcc Co^0 . Thermodynamic data used in the calculations were obtained from Knacke *et al.*¹⁵

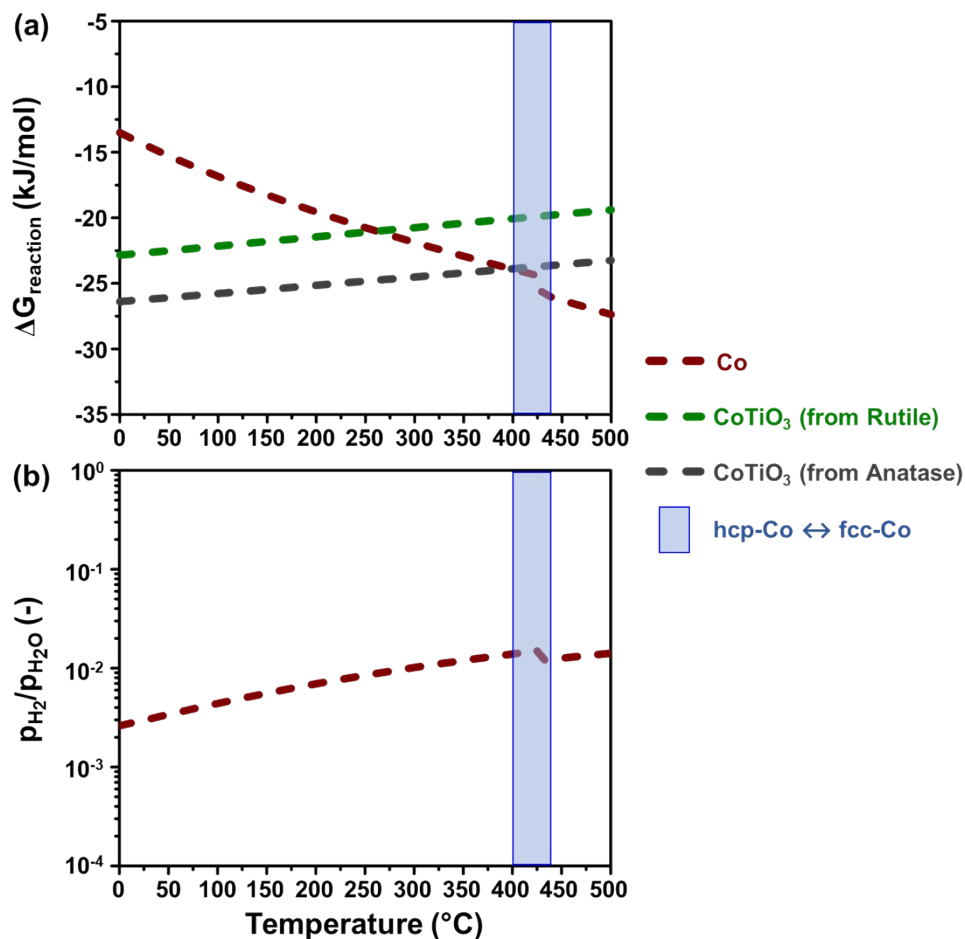


Figure S15: (a) Gibbs free energy as a function of temperature at 1.013 bar during the reduction of bulk CoO forming Co⁰ as well as during the solid state-reaction between CoO and TiO₂ (Anatase or Rutile, respectively) forming CoTiO₃. Note that the formation of CoTiO₃ from CoO does not require H₂ or H₂O (see Equation S20). (b) $p_{\text{H}_2}/p_{\text{H}_2\text{O}}$ as a function of temperature at 1.013 bar during the reduction of CoO to Co⁰.

Ex situ STEM-EELS analysis of spent catalysts

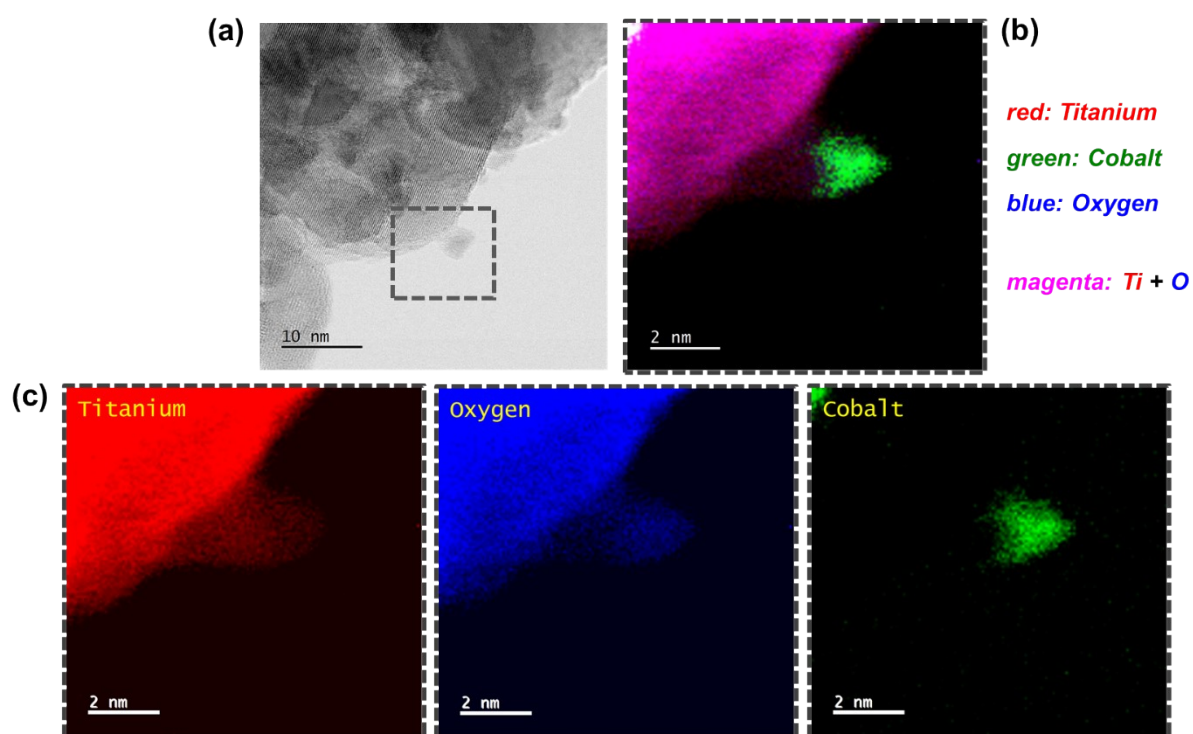


Figure S16: (a) Bright-field STEM micrograph, (b) magnified STEM-EELS composite map showing the regions with Ti, O, and Co, and the (c) corresponding magnified STEM-EELS maps of the individual elements present in the spent $\text{Co}_3\text{O}_4/\text{Anatase}$ catalyst.

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