

## Electronic supplementary information

### Survival of newly formed particles in haze conditions

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## Summary

This electronic supplementary information (ESI) document describes the CLOUD chamber and details of experimentation and instrumentation used at CLOUD, CERN. Details of the parameters calculated from CLOUD results (such as growth rates) and details of the kinetic model set up and equations used are also presented.

## Methods

### The CLOUD chamber at CERN

The CLOUD chamber is 26.1 cubic meters, is made of stainless steel, and the inside surface is electro-polished<sup>1,2</sup>. The chamber concentrations are kept homogeneous via turbulence created by two magnetically coupled stainless steel fans at the top and bottom of the chamber<sup>3</sup>, with mixing times typically on the order of a few minutes. The dilution (ventilation) lifetime is 1.3 hours. Wall loss rates of gases and different sized particles are also well characterised<sup>4</sup>. Precursor gases are injected via a state-of-the-art gas system that allows us to control dilution and injection flows to control the gas concentrations with great accuracy. The trace gases are injected into the chamber along with dry air, formed by mixing 79% boil-off nitrogen and 21% boil-off oxygen (both Messer, 99.999%) and water is added from an evaporator using ultrapure water (18 M $\Omega$  cm, Millipore Corporation) in order to control the relative humidity. Note that in this study experiments were done without use of the 3.5 GeV/c secondary pion beam ( $\pi$  beam) from the CERN PS.

The experiments presented in this paper involved varying mixtures of gases capable of nucleation and growth; sulfuric acid, ammonia, dimethylamine, nitric acid, and HOMs generated from toluene and  $\alpha$ -pinene. Experiments started when lights were turned on and condensable gases were formed by photolysis (and further reactions). The various lights used in these experiments resulted in a homogeneous illumination of the chamber. These different sources were: three UV sources including four 200 W Hamamatsu Hg-Xe lamps (UVH), a 170 W quartz-clad high intensity Hg lamp (saber, LS1), and a 4 W KrF 248 nm excimer UV laser (UVX); further, UVA was generated at 385 nm by a 400 W UVA LED saber (LS3). LS1, UVH, and UVX were used to photolyse ozone, and LS3 was used to photolyse HONO, both in order to generate OH radicals. After each experiment, the particles and condensable gases were cleaned from the chamber by increasing the fan speed and thus the loss rates of particles, and gas concentrations were set up for the subsequent experiment.

The high condensation sink runs were extremely challenging to perform. For example, in instances where the condensation sink was decreasing over time, the gas phase NH<sub>3</sub> was constantly increasing, although the injection rate was constant. The large amount of HNO<sub>3</sub> generated in building up the condensation sink was also the cause of depletion of reagent ions in the Br<sup>-</sup> CIMS, and so the HNO<sub>3</sub> was modelled for certain experiments (see modelling nitric acid).

### Instrumentation

To measure gas-phase nitric acid, a Br<sup>-</sup> chemical ionisation atmospheric pressure interface time of flight mass spectrometer (CI-API-TOF-MS) was deployed in the CLOUD chamber at CERN. We used a commercially available inlet from Airmodus for the mass spectrometer, which is optimised for minimum wall loss. The details of measurements can be found in the Methods section of Wang *et al.* (2020). During some experiments, the Br<sup>-</sup> ion was depleted in the Br<sup>-</sup> CIMS due to high levels of HNO<sub>3</sub>, and so HNO<sub>3</sub> was modelled from other time-series (see modelling nitric acid).

74 H<sub>2</sub>SO<sub>4</sub> and HOMs were also measured by a CI-API-TOF-MS but with nitrate reagent ions. There were  
75 two NO<sub>3</sub><sup>-</sup> CIMS present, one was equipped with an inlet from Airmodus, and the other used a home-  
76 made inlet and corona discharge for ion generation<sup>5</sup>. Both instruments were equipped with an  
77 electrostatic filter so as not to measure naturally formed ions from the CLOUD chamber. The  
78 detection limit of the condensable gases measured by the NO<sub>3</sub><sup>-</sup> CIMS was approximately 5 x 10<sup>4</sup> cm<sup>-3</sup>.  
79 Calibration techniques for H<sub>2</sub>SO<sub>4</sub> and HOMs have been described previously <sup>6,7</sup>.

80 Volatile organic compounds (VOCs) were measured by two different custom built proton transfer  
81 reaction time of flight mass spectrometers, a selective reagent ionization time of flight mass  
82 spectrometer (SRI-ToF-MS) described in Canaval *et al.* (2019)<sup>8</sup> and the PTR3-ToF-MS described in  
83 Breitenlechner *et al.* (2017)<sup>9</sup>. Both instruments used H<sub>3</sub>O<sup>+</sup> ions to charge compounds of the sample  
84 gas. Humidity dependent calibrations of toluene were performed by directly measuring a gas  
85 standard (Apel Riemer Environmental Inc) at specific conditions of the respective experiments.  
86 These instruments were also used to analyze the cleanliness of the chamber in between  
87 experiments.

88 Ammonia and DMA were measured by a water cluster CI-API-TOF-MS, this instrument is described in  
89 detail in Pfeifer *et al.* (2020)<sup>10</sup>. The instrument introduced a newly designed cross-flow ion source.  
90 The authors report the limit of detection of ammonia to be ~ 0.5 pptv and predict the detection limit  
91 of DMA to be lower.

92 A suite of instruments covering different size ranges measured the particle number and size  
93 distribution between 1.5 nm and 487 nm. Starting with the smallest size, the instruments used were:  
94 a nano condensation nucleus counter (nCNC) <sup>11</sup>; a differential mobility analyser train (DMA-Train) <sup>12</sup>;  
95 a nano-scanning electrical mobility spectrometer (nSEMS) <sup>13</sup>; a nano-scanning mobility particle sizer  
96 (nano-SMPS); and a long SMPS.

97 The A11 nano Condensation Nucleus Counter is composed of a particle size magnifier (PSM)  
98 connected in series with a condensation particle counter (CPC). The PSM is an aerosol pre-  
99 conditioner that uses diethylene glycol (DEG) to grow aerosol particles to a size that is easily  
100 detected by the CPC. The saturator flow rate inside the PSM can be adjusted so aerosol particles of  
101 different sizes are activated. During CLOUD13, the PSM saturator flow was set to scanning, meaning  
102 it measured the particle size distribution between 1.5 and 2.5 nm <sup>14,15</sup>.

103 The DMA train is built up of 6 different DMAs in parallel, measuring the range 1.8 - 4.3 nm each with  
104 different fixed voltages, to allow different size ranges, and the particles are counted by either a PSM  
105 or CPC depending on the size <sup>12</sup>; Stolzenburg *et al.* (2017) describe the instrument in detail.

106 The nSEMS is a newly developed instrument that operates in the range of 1.5 – 25 nm. For  
107 classification of particle size, the nSEMS uses a radial opposed migration ion and aerosol classifier  
108 (ROMIAC), which is capable of measuring particle diameters down to the nanometer level with less  
109 degradation and less sensitivity to diffusional resolution degradation than the DMAs. A full  
110 description of the instrument can be found in Kong *et al.* (2021)<sup>13</sup>.

111 The nano and long SMPS are commercially available instruments and have been fully characterised  
112 and described in previous studies <sup>16–18</sup>. Together, the nano-SMPS and long-SMPS scan range spanned  
113 from 4 to 487 nm. Particles larger than 487 nm were formed during runs with high condensation

sinks. For these experiments, a multi-peak fitting routine was applied to deconvolve the observable size distribution into component modes, which were assumed to be lognormal in shape. The fitting results were then used to estimate the particle size distribution from 487 nm to 1036 nm. This was necessary for us to better calculate the condensation sinks and  $J$  rates, since the existence of larger particles will influence these parameters.

Ozone (O<sub>3</sub>, Thermo Environmental Instruments, TEI 49C), sulfur dioxide (SO<sub>2</sub> Thermo Fischer Scientific Inc. 42i-TLE), and nitric oxide (NO, ECO Physics, CLD 780TR) were measured by gas monitors. Nitrogen dioxide was also measured but by a cavity attenuated phase shift NO<sub>2</sub> monitor (CAPS NO<sub>2</sub>, Aerodyne Research Inc.). A custom-made cavity-enhanced differential optical absorption spectrometry instrument (CE-DOAS) was also used to measure NO<sub>2</sub> and HONO. Relative humidity of the chamber was measured by two instruments, dew point mirrors (EdgeTech) and an in situ-TDL-Hygrometer (KIT, CERN). Temperature was measured by mid-plane internal PT100 temperature sensors placed at 5 different distances from the chamber wall. The sensor that was closest to the midpoint of the chamber, 1.2 m from the wall, was used as the chamber's reference temperature.

## Growth rates

Growth rates were calculated using the 50 % appearance time method<sup>19</sup>. This method works best in chamber or flow tube experiments, as it relies on the identification of a growing particle distribution easily differentiated from other particles. Since the CLOUD chamber is cleaned before each experiment, and new particles are nucleated from gases rather than injected, it is easy to differentiate the growing particles. This was more difficult in the case of the high condensation sink runs, as there were many pre-existing particles of different sizes, and thus the reason why growth rates are not reported for these runs. The model was set up to give output of different size bin concentrations at every time step (0.1 s) and so growth rates could be calculated in the same way as experimental data, where the sizing instrument output also gives size-distributed particle concentrations. Each size bin concentration over time is fit to the following function using a least-squares solver:

$$S_{d_p}(t) = \frac{a - b}{1 + (t/t_{app})^d} + b \quad (\text{S.1})$$

Size and time dependent growth rates calculated using the INSIDE method were presented in Figure 2.<sup>20</sup> This method is based on the adapted, size-integrated GDE, where the growth rate is solved for using experimental inputs for other variables. Full details of this method can be found in Pichelstorfer *et al.* (2018).<sup>20</sup> GDE-based GR methods might suffer from statistical fluctuations in the size-distribution measurement that may cause significant error. However, Ozon *et al.* (2021)<sup>21</sup> showed that for well-controlled chamber experiments, the INSIDE method agrees well with a fixed interval Kalman smoother which estimates the GR error for similar experiments to those in Figure 2a-e) to be roughly 1 nm hr<sup>-1</sup>, or at maximum 50% for more dynamic situations such as in Figure 2f-j).

Where  $S_{d_p}$  is the signal or concentration of a particular diameter ( $d_p$ ) bin,  $a$  and  $b$  are the background and plateau concentrations respectively,  $d$  is a free parameter which relates to the steepness of the sigmoidal increasing curve, and  $t_{app}$  is the 50 % appearance time, which is equal to the time at which 50% of the concentration (in between background and plateau) has been reached. The appearance time for each bin is then plotted against the particle diameter and a linear fit is made to present

153 growth rates in nm hr<sup>-1</sup>. For a full description see the Supporting Information of Stolzenburg *et al.*  
 154 (2018)<sup>19</sup>.

### 155 Formation rates

156 Formation rates were determined using the balance equation between the particle sources and sinks  
 157 as per Dada *et al.* (2020)<sup>22</sup> shown in equation (S.2):

$$J_x = \frac{dN_{\geq x}}{dt} + S_{dil} + S_{wall} + S_{coag} \quad (S.2)$$

158

159 Where the units of  $J$  are (particles) cm<sup>-3</sup> s<sup>-1</sup> and  $S_{dil}$ ,  $S_{wall}$ , and  $S_{coag}$  are terms for dilution loss, wall loss,  
 160 and coagulation loss, respectively.

161 Formation rates of particles of diameter 2.5 nm were reported as a 2.5 nm particle is  
 162 thermodynamically stable and larger than the critical radius<sup>23</sup>. 2.5 nm particles are also commonly  
 163 measured in ambient campaigns and thus it is valuable for comparison. The total number  
 164 concentration of particles with diameters 2.5 nm and above was measured using the nCNC.

### 165 Activation diameter

166 During the CLOUD experiments, when there was an activation event, the particle size bins just above  
 167 the activation diameter tended to have low concentrations, due to fast growth after activation  
 168 (faster than the time resolution of the instrument). The activation diameter was therefore  
 169 determined by identifying the first time step where a bimodal distribution occurred, and the largest  
 170 size bin of the smaller mode, where the concentration dropped, was identified as the activation  
 171 diameter. For further information on this technique see the supporting information of Wang *et al.*  
 172 (2020)<sup>24</sup>.

### 173 Modelling ammonium nitrate

174 The flux of ammonia and nitric acid to a certain size particle is calculated using the following  
 175 equation.

$$\phi_{i,p} = N_p^s \pi d_p^2 \underbrace{\left( \frac{E_{i,p}^\mu \epsilon_{i,p} e_{i,p} \alpha_{i,p} \bar{S}_i B_{i,p}}{4} \right)}_{\text{Area: } A_p^s} \underbrace{\left[ c_i^v - \alpha_{i,p} K_{i,p} c_i^o \right]}_{\text{Collision speed: } \bar{S}_{i,p}^\perp} \underbrace{\left[ c_i^v - \alpha_{i,p} K_{i,p} c_i^o \right]}_{\text{Driving force: } F_{i,p}^{v,s}} \quad (S.3)$$

Flux per unit surface area:  $\phi_{i,p}^{v,s}$

$$\bar{S}_i = \sqrt{\frac{8k_b T}{\pi m_i}} \quad (S.4)$$

176

177 The subscript  $i$  denotes the gas species, i.e. NH<sub>3</sub> or HNO<sub>3</sub> (depending on which is limiting), and the  
 178 subscript  $p$  refers to the particle size. Where  $N_p^s$  is the particle number and  $d_p$  is the diameter. The  
 179 collision speed is derived from the average molecular speed (Equation (S.4)), and includes terms  
 180 reflecting Van der Waals interactions between the vapour and particle (charge - dipole, dipole -

181 induced dipole, and induced dipole - induced dipole),  $E_{i,p}^{\mu} = E^{\mu}(H_{i,p})$  where  $H_{i,p}$  is the Hamaker  
 182 constant in Joules; the non-zero size of the vapour,  $\varepsilon_{i,p} = (d_i^2 + d_p^2)/d_p^2$ ; and the non-infinite mass of  
 183 small clusters,  $e_{i,p} = \sqrt{(m_i + m_p)/m_p}$ . A term for gas-phase diffusion limitations is  $B_{i,p} \approx 1$  for large  
 184 Knudsen numbers. The mass accommodation coefficient,  $\alpha_{i,p}$ , can also be included, this was assumed  
 185 to be 1 for these calculations. The driving force depends on vapour concentration,  $c_i^v$ , and saturation  
 186 concentration,  $c_i^o$ , as well as the activity in the solid phase and the kelvin term. Since the Hamaker  
 187 constant for ammonia is 0, the enhancement from Van der Waals interaction is only relevant in acid-  
 188 limiting conditions, and has the greatest effect at lower sized particles. This enhancement was not  
 189 included in the thermodynamic model for this paper, but it may explain some of the difficulty in  
 190 duplicating the experiment in Figure 2 Run 2, since the enhancement of growth at small sizes would  
 191 have the small particles grow faster than the large particles in the CS.

192 We simplify the flux per unit surface area calculation to

$$\varphi_{i,p}^{v,s} = s_{i,p}^{\perp} c_i^v \gamma_{i,p} \quad (\text{S.5})$$

$$\gamma_{i,p} = \left[ 1 - \frac{a_{i,p}^s}{a_i^v} K_{i,p} \right] \quad (\text{S.6})$$

193 where  $\gamma_{i,p}$  is defined as the uptake coefficient and can be defined in terms of the saturation ratio of  
 194 the gas, where the saturation ratio is equal to the activity in the vapour phase divided by the activity  
 195 in the solid phase times the kelvin term to account for the curvature of the surface of a particle.

$$\gamma_{i,p} = \left( 1 - \frac{1}{S_{i,p}} \right) = \frac{S_{i,p} - 1}{S_{i,p}} = \frac{S_{i,p}^{XS}}{S_{i,p}} \quad (\text{S.7})$$

$$S_{i,p} = \frac{a_i^v}{a_{i,p}^s K_{i,p}} \quad (\text{S.8})$$

196 We can consider the flux as equal due to the 1:1 stoichiometry of condensation of ammonium  
 197 nitrate, and thus we define a collision ratio,  $r_{AB}^v$ , which is the concentration ratio scaled by the  
 198 collision speed of each molecule. The subscripts A and B are now used for acid and base.

$$\varphi_{A,p}^{v,s} = \varphi_{B,p}^{v,s} \quad (\text{S.9})$$

$$s_{A,p}^{\perp} c_A^v \gamma_{A,p} = s_{B,p}^{\perp} c_B^v \gamma_{B,p} \quad (\text{S.10})$$

$$\gamma_{B,p} = \frac{s_{A,p}^{\perp} c_A^v}{s_{B,p}^{\perp} c_B^v} \gamma_{A,p} \quad (\text{S.11})$$

$$\gamma_{B,p} = r_{AB}^v \gamma_{A,p} \quad (\text{S.12})$$

$$r_{AB}^v = \frac{s_{A,p}^{\perp} c_A^v}{s_{B,p}^{\perp} c_B^v} \quad (\text{S.13})$$

199

200

201

202 In the case of base limiting experiments,  $S_{B,p}$  is then found iteratively using the following equation,  
 203 solved by combining Equations (S.7), (S.9) and (S.10). If the experiment is acid limiting, the difference  
 204 in solving for  $S_{A,p}$  is to replace  $r_{AB}^v$  with  $1/r_{AB}^v$ .

$$S_{B,p} = \frac{S_{AB,p}}{2} \left[ \left( \frac{r_{AB}^v - 1}{r_{AB}^v} \right) + \sqrt{\left( \frac{r_{AB}^v - 1}{r_{AB}^v} \right)^2 + \frac{4}{r_{AB}^v S_{AB,p}}} \right] \quad (\text{S.14})$$

205

206 Where  $S_{AB,p}$  is the saturation of ammonium nitrate

$$S_{AB,p} = \frac{a_A^v a_B^v K_{AB}^{eq}}{K_{AB,p}} = \frac{x_A^v x_B^v}{K_{AB,p} K_p} \quad (\text{S.15})$$

$$K_p = \frac{p_B^o p_A^o}{K_{AB}^{eq}} \quad (\text{S.16})$$

207 Where  $x_A^v$  and  $x_B^v$  are the mixing ratios of nitric acid and ammonia respectively,  $K_{AB}^{eq}$  is the  
 208 equilibrium constant for  $\text{NH}_3(\text{s}) + \text{HNO}_3(\text{s}) \rightleftharpoons \text{NH}_4\cdot\text{NO}_3(\text{s})$ ,  $K_p$  is an overall dissociation constant for  
 209 ammonium nitrate condensation, i.e.  $\text{NH}_3(\text{v}) + \text{HNO}_3(\text{v}) \rightleftharpoons \text{NH}_4\cdot\text{NO}_3(\text{s})$ ,<sup>25</sup>, and  $K_{AB,p}$  is the Kelvin term  
 210 for ammonium nitrate, correcting for the curvature effect of different sized particles.

$$K_{AB,p} = 10^{\left( \frac{d_{K10}}{d_p} \right)} \quad (\text{S.17})$$

211

212 The Kelvin diameter for ammonium nitrate at 5 °C was calculated by fitting the data from CLOUD  
 213 experiments (Figure S2) according to the relationship shown in Equation (S.18).

$$S_{AB,p} = 10^{\left( \frac{d_{K10}}{d_{act}} \right)} \quad (\text{S.18})$$

214

## 215 Modelling nitric acid

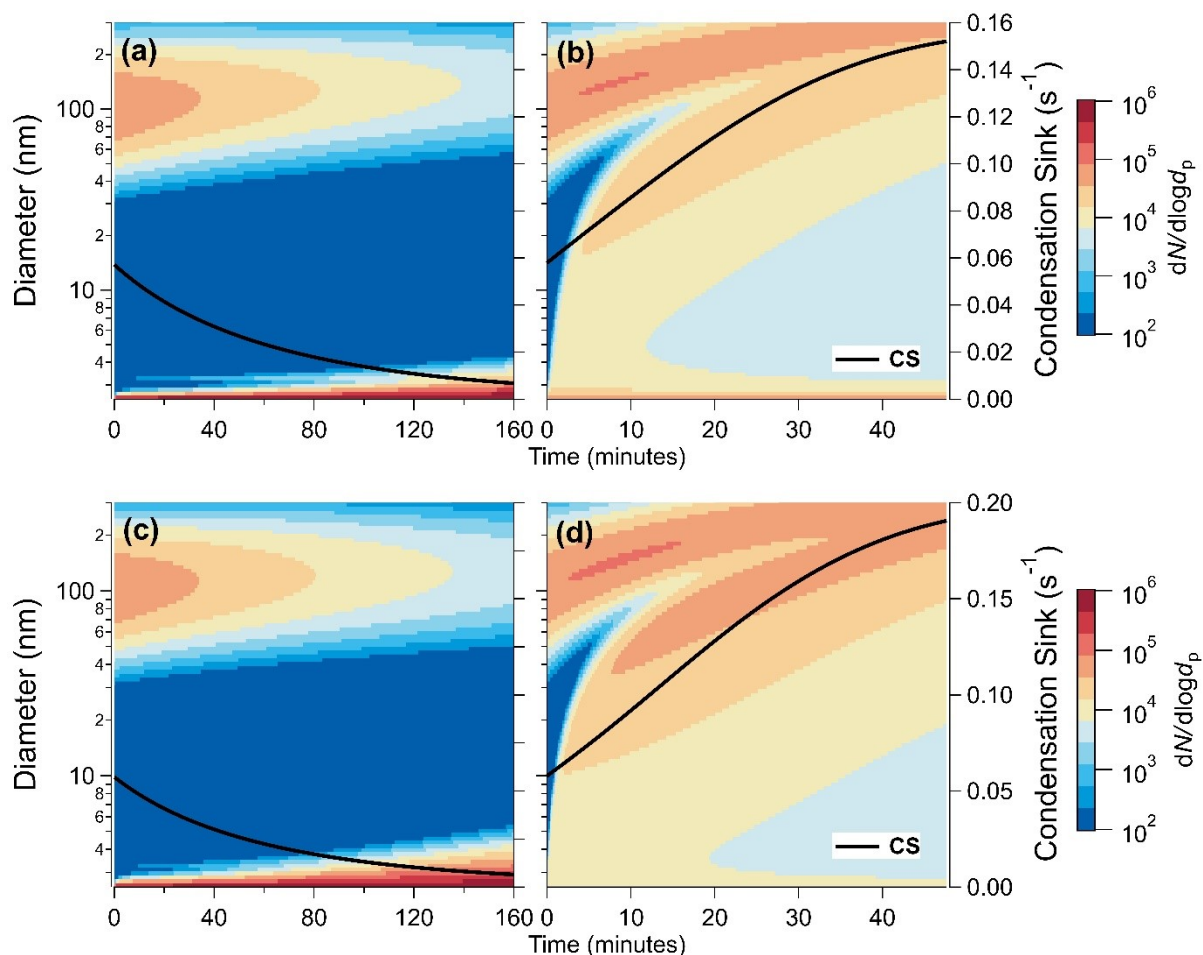
216 In the two CLOUD experiments with high condensation sink (Figure 2), there were no accurate  
 217 measurements of  $\text{HNO}_3$  due to depleted reagent ions, and therefore the time-series presented are  
 218 modelled concentrations. A box model was set up where  $\text{HNO}_3$  was solved for based on sums of  
 219 production and losses at each time step.

$$\frac{\partial \text{HNO}_3}{\partial t} = \text{source}_{\text{injection}} + \text{source}_{\text{NO}_2 + \text{OH}} - \text{loss}_{\text{wall} + \text{dilution}} - \text{loss}_{\text{condensation sink}} \quad (\text{S.19})$$

220

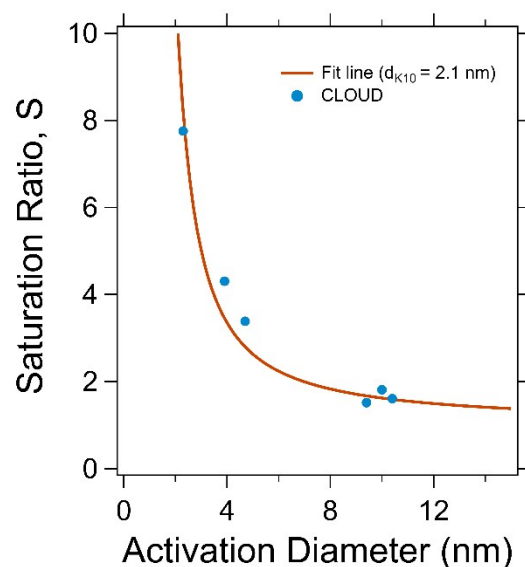
221 This model was tested on other CLOUD experiments and agreed with the measurements from the  
 222 Br<sup>-</sup> CI-API-TOF-MS within a factor of two.

223 OH was modelled in a similar way using the AtChem online solver where the chemical mechanistic  
 224 information was taken from the Master Chemical Mechanism, MCM v3.3.1<sup>26,27</sup>. Inputs were  
 225 measured time series of various trace gases, photolysis rates of ozone and HONO, and chamber wall  
 226 and dilution losses specific to CLOUD.



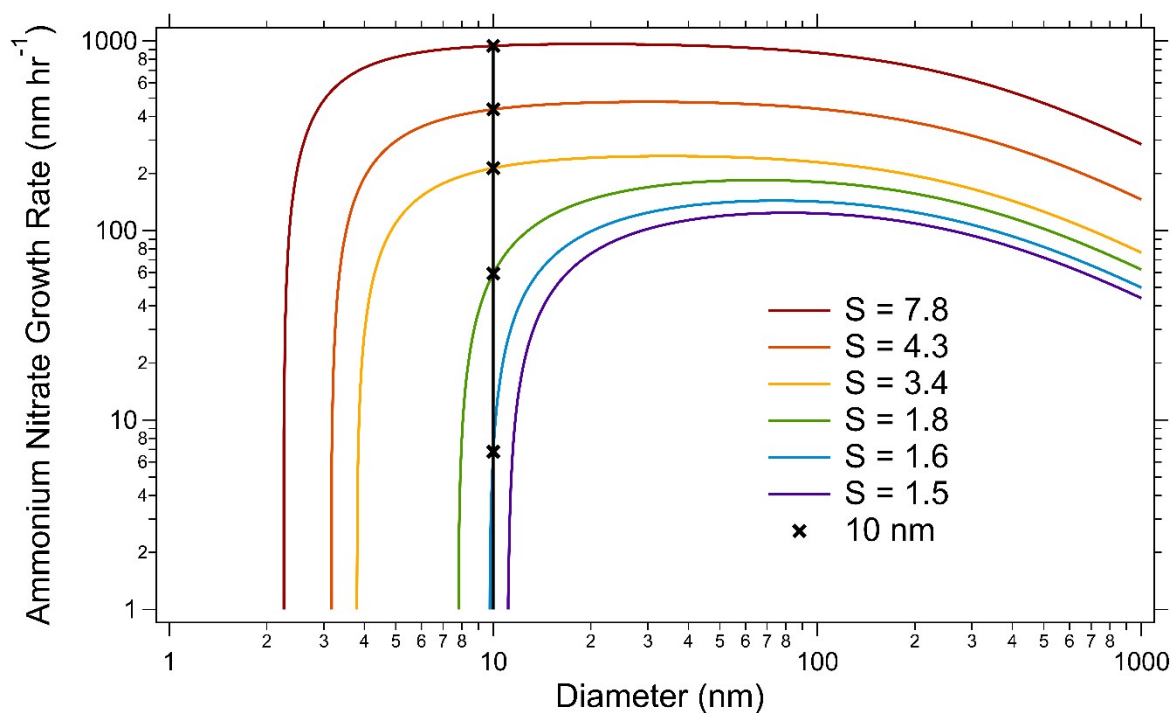
229 **Figure S1: Sensitivity tests on gas phase concentrations and formation rates on modelled results of Figure 2:** This figure is  
 230 a repeat model of the runs in Figure 2 d and i of the main text but with **a-b)**  $J_{2.5}$  constrained to  $10 \text{ cm}^3 \text{ s}^{-1}$ , and **c-d)**  $J_{2.5}$   
 231 constrained to  $10 \text{ cm}^3 \text{ s}^{-1}$  as well as  $\text{H}_2\text{SO}_4$  and  $\text{NH}_3$  concentrations switched between the two experiments. All other  
 232 experimental conditions are the same. The model results are similar to those in Figure 2 panels d and i, with little to no growth  
 233 in the low  $\text{HNO}_3$  case (a,c), and the “smear” of particles of all sizes in the high  $\text{HNO}_3$  case (b, d).





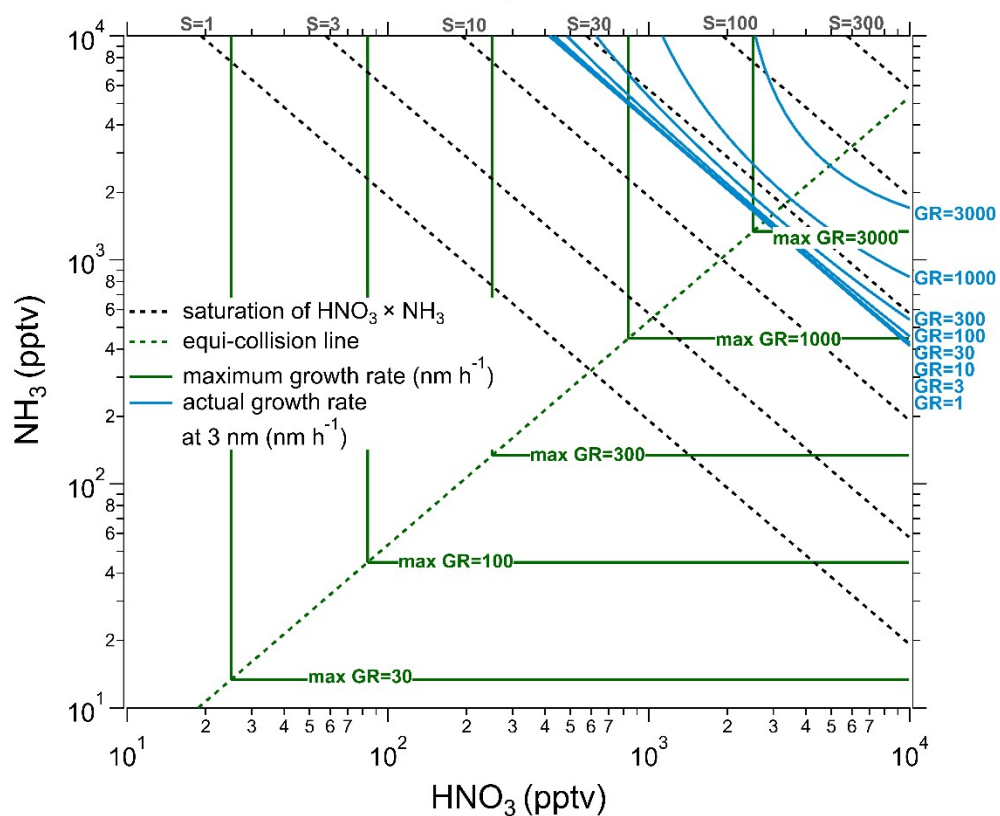
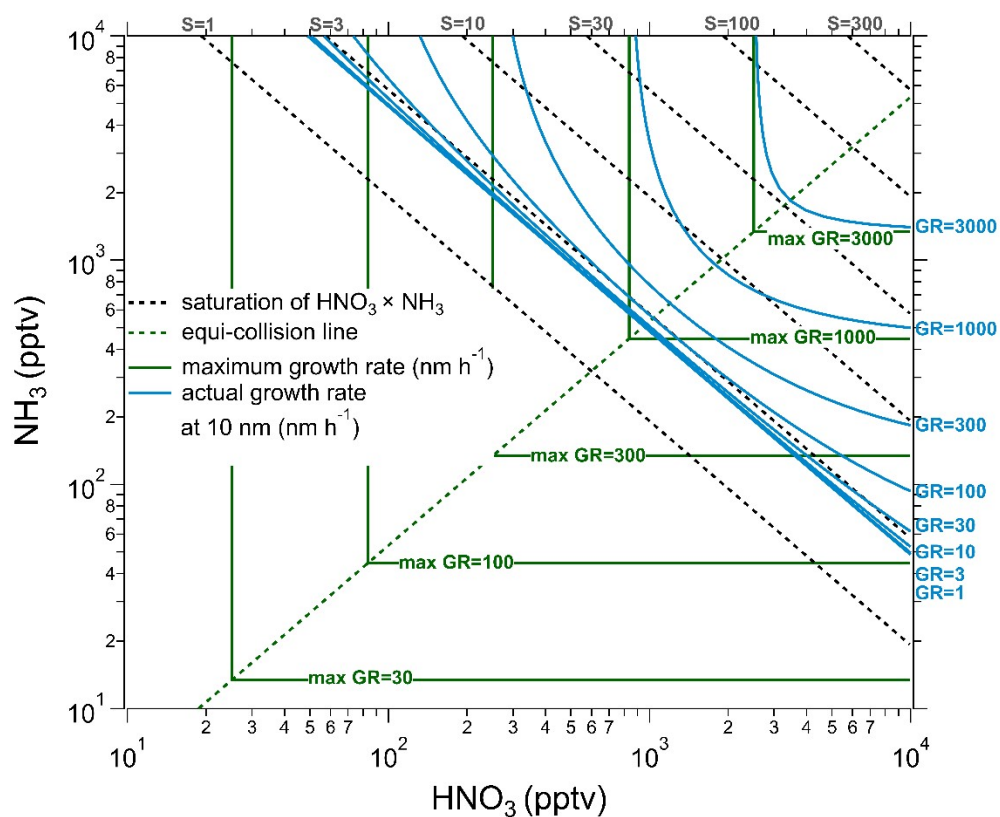
235

236 **Figure S2: Saturation ratio vs activation diameter:** Blue markers represent measured activation diameters from CLOUD  
 237 experiments and saturation ratios calculated from measured  $\text{HNO}_3$  and  $\text{NH}_3$  gas phase concentrations. The red fit line is fit to  
 238 this data and then used to calculate the Kelvin diameter for use in the model.



239

240 **Figure S3: Diameter vs calculated growth rates from flux equations –** The curves are calculated using the equations in the  
 241 section “Modelling ammonium nitrate”. The six  $S$  curves plotted are using  $S$  calculated from the  $\text{HNO}_3$  and  $\text{NH}_3$  gas  
 242 concentrations from the six CLOUD experiments shown in Figure 1. It is apparent that at low diameters the growth varies  
 243 dramatically, around the activation diameter for each  $S$  value.



**Figure S4: Calculated growth rates of condensation of ammonium nitrate:** The phase space shown is between 1 pptv and 10,000 pptv (10 ppbv) at 5 °C. The top panel shows growth rates for a particle of 10 nm and the bottom panel shows growth rates for a particle of 3 nm (the same size used for calculating growth rates in Figure 2) The calculations for growth rate include the Kelvin effect using the Kelvin diameter calculated (see modelling ammonium nitrate).

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