# Supplementary Information

Stretchable thermogalvanic hydrogel thermocell with record-high specific output power density enabled by ion-induced crystallization

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**Fig. S1.** SEM characterization of the PAAm-SA hydrogel. (a,b) The surface (a) and cross-section (b) images of the PAAm-SA hydrogel.



**Fig. S2.** The mechanical performance analysis of the PAAm-SA hydrogel. (a) The optical image of the hydrogel supporting a heavy Al block. (b) The brightness change of a LED with the hydrogel as a conducting wire at different stretched strains. (c) The brightness change of a LED with the hydrogel soaked into  $[Fe(CN)_6]^{3-/4-}$  solution, indicating the excellent conductivity of the soaked hydrogel. (d) The optical image of an Al block supported by a soaked hydrogel. (e,f) The measurement for excellent torsional and tensile performance (e) and adhesion property (f) of the soaked hydrogel.



**Fig. S3.** (a) The schematic diagram of the working mechanism based on thermogalvanic effect. (b) The thermopower and conductivity change of the STHTC with 0.05-0.4 mol/L  $[Fe(CN)_6]^{3-4/4}$ .



Fig. S4. The performance comparison of different PAAm-SA hydrogels. (a,b) The transmittance (a) and stretchability (b) comparison of different PAAm-SA hydrogels. (c) The variation of the thermal conductivity of the PAAm-SA hydrogel with 0-4.0 mol/L CH<sub>6</sub>ClN<sub>3</sub> and 0.3 mol/L  $[Fe(CN)_6]^{3-/4-}$  as different soaking solutions.



Fig. S5. The UV-Vis absorbance spectra change of the soaked solution with 0-4.0 mol/L  $CH_6ClN_3$  and 0.3 mol/L  $[Fe(CN)_6]^{3-/4-}$ .



**Fig. S6.** (a) The comparison of three individual UV-Vis absorbance spectra corresponding to  $K_4Fe(CN)_6$ ,  $K_3Fe(CN)_6$  and  $CH_6ClN_3$ . (b) The dissolution situations of the soaking solution with different combinations among  $K_4Fe(CN)_6$ ,  $K_3Fe(CN)_6$  and  $CH_6ClN_3$ .



**Fig. S7.** The dissolution comparison of the solutions containing  $K_4Fe(CN)_6$  and  $CH_6ClN_3$ . (ac) The optical images (a), UV-Vis absorbance spectra (b), and the relative concentration change (c) of  $[Fe(CN)_6]^{4-}$  in the solution with 3 mol/L  $K_4Fe(CN)_6$  and 0.5-4.0 mol/L  $CH_6ClN_3$ .



**Fig. S8.** The dissolution comparison of the solutions containing  $K_3Fe(CN)_6$  and  $CH_6ClN_3$ . (ac) The optical images (a), UV-Vis absorbance spectra (b), and the relative concentration change (c) of  $[Fe(CN)_6]^{3-}$  in the solution with 3 mol/L  $K_3Fe(CN)_6$  and 0.5-4.0 mol/L  $CH_6ClN_3$ .



Fig. S9. The relative concentration change of  $[Fe(CN)_6]^{3-}$  and  $[Fe(CN)_6]^{4-}$  in different initial solutions.



**Fig. S10** (a) The schematic diagram of solvation situations of  $[Fe(CN)_6]^{3-/4-}$  in CH<sub>6</sub>ClN<sub>3</sub> solution. (b) The comparison of the effect of other species on the crystallization of  $[Fe(CN)_6]^{4-}$  ion.



**Fig. S11.** The thermopower retention rate of two STHTCs after being wrapped in a cling film and placed in the air for 10 days.



Fig. S12. The comparison of thermal conversion efficiency calculated by ion-type and electrontype methods. (a,b) The comparison of thermal energy conversion efficiency (a) and Carnotrelative efficiency (b) of the STHTC under different  $\Delta T$ .



**Fig. S13.** The performance measure of the STHTC at low-temperature. (a) The conductivity changes of the STHTC under a large temperature span between -60 to 60 °C. (b) The comparison of the stress-strain curves of the STHTC under an ultra-low cold (-35 °C) environment and room temperature (*RT*).



**Fig. S14.** The stability measure of the STHTC at three groups of small deformation operations. (a,b) The optical images of the STHTC being periodically pressed, bent, and stretched (a) and corresponding electrical output change (b).



**Fig. S15.** The cubic STHTC block and the 5×5 STHTC array device. (a) Optical images of cubic STHTC. (b-d) Optical images of fabricated 5×5 STHTC array device (b), showing good flexibility (c) and bendability (d).

#### **Supplementary Note**

## Note S1:

With the increase of CH<sub>6</sub>CIN<sub>3</sub> from 0.5 to 2.0 mol/L, the concentration of  $[Fe(CN)_6]^{4-}$  quickly decreases while the concentration of  $[Fe(CN)_6]^{3-}$  decreased slightly (**Fig. 2**b), which will promote the reversible redox, thus increasing the *S*<sub>c</sub>. Meanwhile, the Cl<sup>-</sup> ions from CH<sub>6</sub>CIN<sub>3</sub> can increase the electrical conductivity to a certain extent. When the CH<sub>6</sub>CIN<sub>3</sub> increases over 2.0 mol/L, there is a relatively large concentration reduction for  $[Fe(CN)_6]^{3-}$  than  $[Fe(CN)_6]^{4-}$ . The reduction of  $[Fe(CN)_6]^{3-}$  will inhibit the redox and decrease the *S*<sub>c</sub> slightly (**Fig. 2**b). At the same time, the increase of crystalline precipitate may hinder the ions transport, thus reducing the conductivity.<sup>1</sup>

## Note S2:

For the STHTC, the Power Factor (*PF*) and Figure of merit (*ZT*) can be calculated according to the calculation method for the traditional thermoelectrical materials, which can be expressed  $as^{2,3}$ :

$$PF = \alpha^2 \sigma \tag{1}$$
$$ZT = \alpha^2 \sigma T/\kappa \tag{2}$$

Where the  $\alpha$ ,  $\sigma$ , T,  $\kappa$  are the seebeck coefficient, electrical conductivity, Kelvin temperature, and thermal conductivity. Owing to the appearance of the  $\Delta T$ , there is a temperature gradient across the STHTC, therefore the average ZT can be changed as:

$$ZT_{\text{average}} = \alpha^2 \sigma (T_{\text{c}} + T_{\text{h}})/2\kappa$$
(3)

The thermal conversion efficiency ( $\eta$ ) of the traditional thermoelectrical materials can be expressed as<sup>4,5</sup>:

$$\eta = \frac{\Delta T}{T} \frac{\sqrt{1+ZT}-1}{\sqrt{1+ZT} + \frac{T_c}{T_h}}$$
(4)

Where the  $\Delta T$ , *T*, *ZT*, *T*<sub>c</sub>, *T*<sub>h</sub> are the temperature difference, Kelvin temperature, Figure of merit, cold side temperature and hot side temperature, respectively.

### **References:**

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