Electronic Supplementary Material (ESI) for Energy & Environmental Science. This journal is © The Royal Society of Chemistry 2022

## **Supporting Information**

## Demonstration of 10+ Hour Energy Storage with $\phi$ 1" Laboratory Size Solid Oxide Iron-Air batteries

Qiming Tang<sup>1</sup>, Yongliang Zhang<sup>1</sup>, Nansheng Xu<sup>1</sup>, Xueling Lei<sup>2</sup>\* and Kevin Huang<sup>1</sup>\*

<sup>1</sup>Department of Mechanical Engineering, University of South Carolina, Columbia, SC 29201, USA

<sup>2</sup>Department of Physics, Jiangxi Normal University, Nanchang, Jiangxi 330022, China

\*Corresponding author: e-mail: huang46@cec.sc.edu; e-mail: xueling@mail.ustc.edu.cn

## Thermodynamic aspects of SOIAB

We here show how to calculate thermodynamic properties of Fe-O system. At 550 °C, the equilibrium between Fe and O<sub>2</sub> in SOIAB is given by <sup>[1]</sup>

$$3Fe(s) + 2O_2(g) \Leftrightarrow Fe_3O_4(s) \tag{S1}$$

The theoretical Nernst potential  $(^{E}N)$  related to this reaction is determined by:

$$E_N = E^o - \frac{RT}{nF} ln^{[n]} \left(\frac{1}{[pO_2]^2}\right)$$
 (S2)

where  $E^o = -\frac{\Delta G^0}{nF}$ , which refers to the EMF under the standard state;  $\Delta G^0$  is the standard Gibbs free energy change of Fe-Fe<sub>3</sub>O<sub>4</sub> at 550 °C; R is the universal gas constant, 8.314 J mol<sup>-1</sup> K<sup>-1</sup>; T is the temperature in kelvins; n is the number of electrons transferred in the reaction per mole metal, n = 8 for this case; and F is the Faraday constant, 96485 C mol<sup>-1</sup>;  $pO_2$  is the partial pressure of oxygen, 0.21 atm in air.

The theoretical specific energy (SE\*, based on the mass of iron element, Wh kg-1) can be

calculated by:

$$SE^* (Wh kg^{-1}) = \frac{Q^* \times E_N}{m_{Fe}(kg)} = \frac{nF \times E_N}{3600 \times M_{Fe} \times 0.001}$$
 (S3)

where  $Q^* = n \times F = I \times t(seconds)$ , which refers to the total theoretical charge per mole of Fe;  $M_{Fe}$  is the molar mass of Fe in g mol<sup>-1</sup>.

The theoretical specific charge capacity (Q\*, based on the mass of Fe, Ah kg<sup>-1</sup>) can be obtained by:

$$Q^* (Ah kg^{-1}) = \frac{SE^*}{E_N}$$
 (S4)

The practical specific energy (PSE, or denoted as DSE and CSE in the main text) is determined by the following:

$$PSE \left(Wh Kg^{-1}\right) = \frac{\int_{t_1}^{t_2} (I \times V) dt}{m_{Fe}(kg)}$$
(S5)

where,  $t_1$  and  $t_2$  refers to the duration of charging or discharging, respectively; I is the applied current; V is the actual measured potential. Thus, the round trip efficient (RTE, %) can be calculated by:

$$RTE = \frac{SE_d}{SE_c} = \frac{\int_{t_1}^{t_2} (I_d \times V_d) dt}{\int_{t_1}^{t_2} (I_c \times V_c) dt}$$
(S6)

The subscripts "c and "d" refer to "charge" and "discharge", respectively.

The C-rate, describing how fast a battery charges and discharges, can be expressed by the

applied current. For example, a 1C battery needs one hour to charge or discharge its full capacity ( $U_{Fe}$ =100%), while a 0.5C battery requires two hours:

$$I_{@1c} = \frac{nF}{3600 \ seconds} = \frac{nF}{7200 \ seconds}$$
 (S7)

Since the energy capacity of this system depends on the metal/metal oxide redox couple, utilization of metal ( $^{U}_{Fe}$ , %) is a crucial parameter for SOIAB. They are defined by:

$$t_{Fe}^* = \frac{Q_{Fe}^*}{I_a} \tag{S8}$$

$$U_{Fe} = \frac{Q_{Fe}}{Q_{Fe}^*} = \frac{t_{Fe}}{t_{Fe}^*}$$
 (S9)

where  $t_{Fe}^*$  is the theoretical full discharge or charge time;  $Q_{Fe}^*$  is the total theoretical charge capacity per mole Fe;  $Q_{Fe}$  and  $t_{Fe}$  are the measured charge capacity and actual discharge/charge time (seconds).

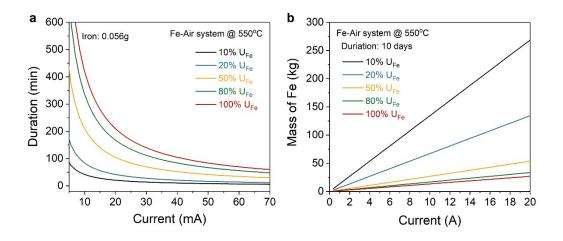


Figure S1. Current- $U_{Fe}$ -duration relationship. (a) Discharge/charge duration with 0.056 g Fe (used in this study)

vs. j and  $U_{Fe}$ ; (b) the mass of Fe for 10 days storage at different j and  $U_{Fe}$ .

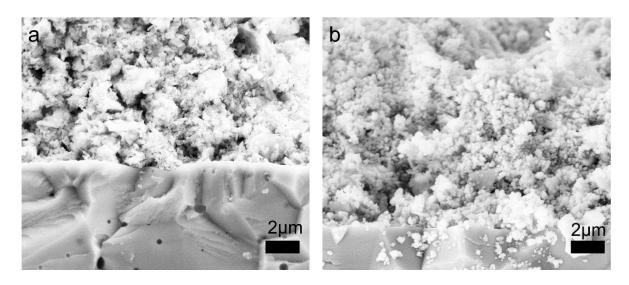


Figure S2 SEM images of LSM/BYC OE before (a) and after (b) 250h testing at 0.2C and 550°C.

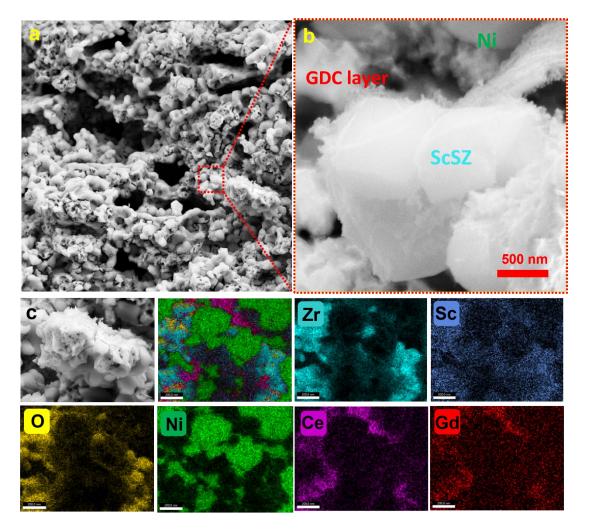


Figure S3. (a and b) SEM images of 4 wt% GDC infiltrated HE after reduction; (c) corresponded elemental mapping.

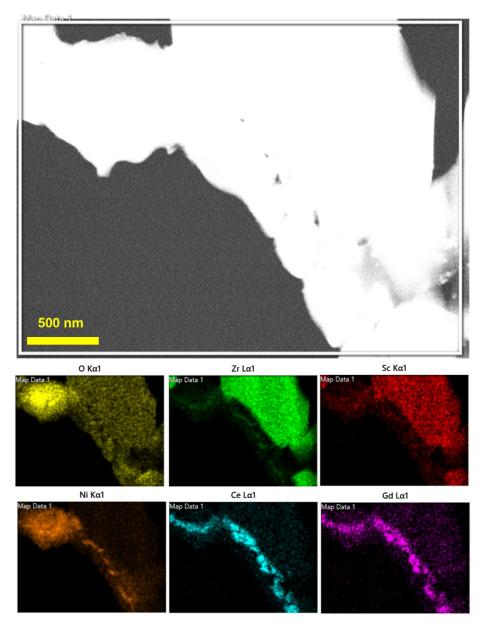
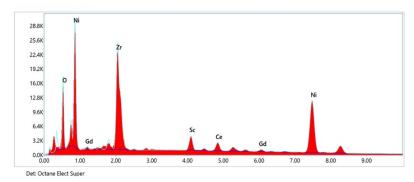
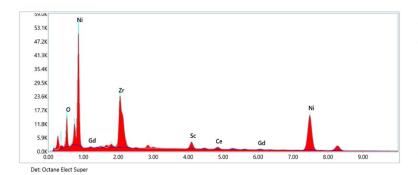


Figure S4. TEM image and the corresponding elemental mapping of 4 wt% GDC infiltrated HE after reduction.



Element	Weight %	Atomic %
ок	10.58	33.63
ScK	3.60	4.08
NiK	53.04	45.97
ZrL	23.25	12.96
CeL	7.25	2.63
GdL	2.28	0.74

Figure S5. EDS spectrum and corresponding elemental contents of 4 wt% GDC infiltrated HE.



Element	Weight %	Atomic %				
ок	8.65	27.93				
ScK	3.01	3.46				
NiK	62.35	54.87				
ZrL	21.38	12.10				
CeL	3.20	1.18				
GdL	1.41	0.46				

Figure S6. EDS spectrum and the corresponding elemental distributions of 2 wt% GDC infiltration HE.

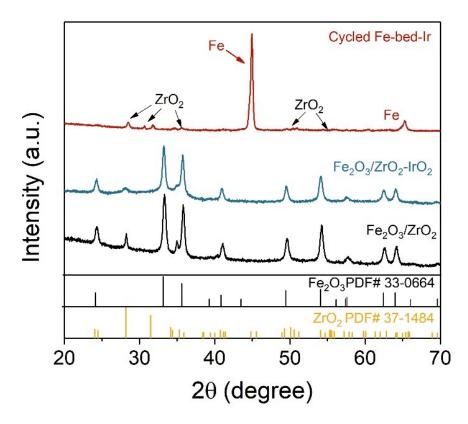


Figure S7. XRD pattern of as-prepared pristine  $Fe_2O_3/ZrO_2$  (bottom) and  $IrO_2$ -impregnated  $Fe_2O_3/ZrO_2$  (medium) and corresponding cycled Fe-bed-Ir (top) at  $U_{Fe}$ =50% and 0.2C.

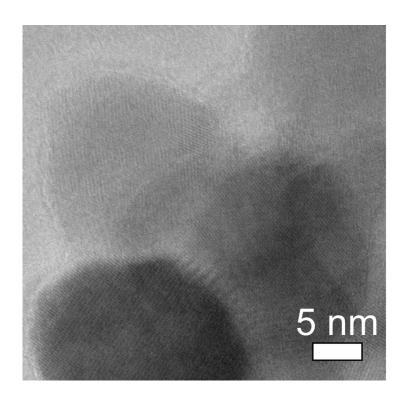
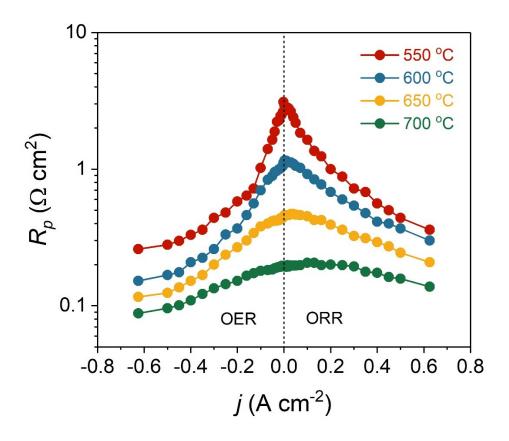


Figure S8. HRTEM image of a fresh Fe<sub>2</sub>O<sub>3</sub>/ZrO<sub>2</sub> sample.



**Figure S9.**  $R_p$  of LSM/BYC OE vs. j at different temperatures.

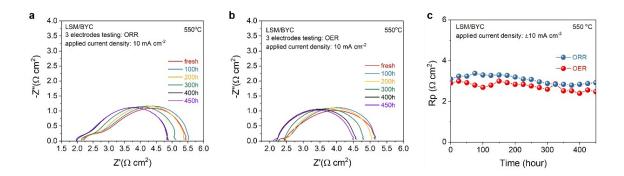
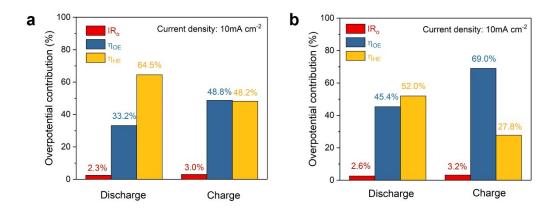
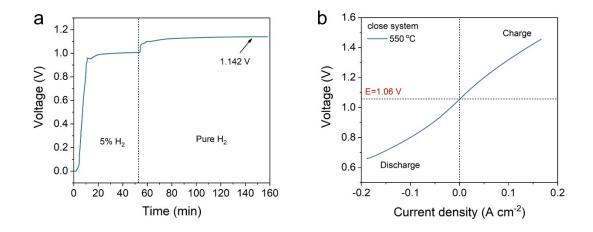


Figure S10. Stability of LSM/BYC OE evaluated by three-electrode symmetric cell under an applied j=10 mA cm<sup>-2</sup>: (a) EIS spectra vs. time during ORR process; (b) EIS spectra vs. time during OER process; (c)  $R_p$  of ORR and OER vs. time.

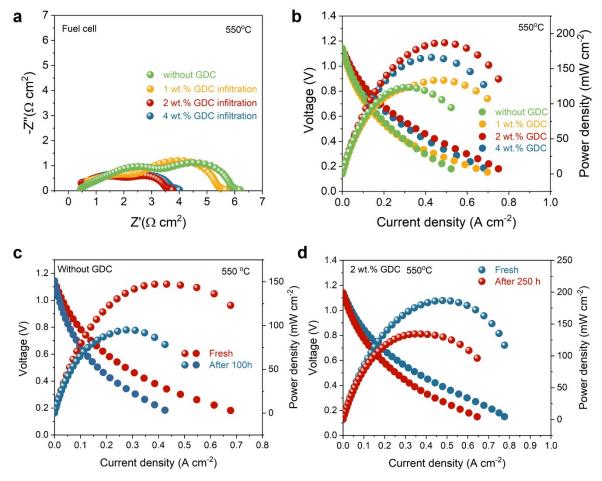


**Figure S11.** Overpotential contributions during charge and discharge process: (a) 1 wt% GDC infiltrated HE; (b) 4 wt% GDC infiltrated HE.



**Figure S12.** (a) OCV vs. time of RSOC in  $H_2$ -3% $H_2$ O for dip-coated cells in open system; (b) V-j curve of RSOC in the close system.

The performance of the SOIAB with improved RSOC and Fe<sub>3</sub>O<sub>4</sub>/ZrO<sub>2</sub>-Ir ESU material was tested at 550 °C. Figure S12a shows the variations of OCV of the cell vs. time in H<sub>2</sub>-3%H<sub>2</sub>O in open system. After full reduction, the cell exhibits a OCV of 1.144 V, which is close to the thermodynamic potential, suggesting a good gas tightness of the system. Then the performance of RSOC was tested in a closed system, where the H<sub>2</sub> inlet and outlet were closed. Figure S12b shows V-*j* curves in both fuel cell and electrolyzer modes in the close system, where the OCV of battery is seen to decrease to ~1.06 V, the thermodynamic equilibrium voltage for Fe-Fe<sub>3</sub>O<sub>4</sub> redox couple at 550°C.



**Figure S13.** Comparison of cell performance at different GDC loadings: (a) EIS; (b) V-I and P-I curves; (c) performance of 2 wt.% GDC infiltrated cell before and after testing; (d) performance of baseline cell before and after testing.

Figure S13a summarizes the ohmic resistance (R<sub>o</sub>) and electrode polarization resistance (R<sub>p</sub>) values. The R<sub>o</sub> remains a constant for different electrodes, while R<sub>p</sub> decreases gradually with the GDC loading, which is attributed to the additional catalytic activity of GDC. The performance was also evaluated in a single cell. The V-*j* curves (Figure S13b) indicates the maximum power density reaches to 200 mA cm<sup>-2</sup> at 550 °C for 2 wt% GDC infiltrated cell, which has a significant improvement compared to that of baseline HE cell. However, when the GDC loading increases to 4 wt%, the performance did not show further improvement. This behavior could be attributed to the thicker GDC layer covering more active Ni particles (see

Figure 2). Therefore, 2 wt% is the optimal GDC loading. In addition, after GDC infiltration, the stability of RSOC is also improved as shown in Figure S13c and S13d.

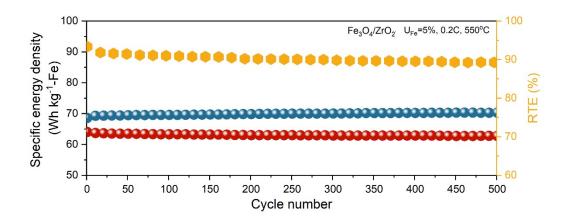


Figure S14. The corresponding SED and RTE of battery with  $Fe_3O_4/ZrO_2$  ESU materials at  $U_{Fe}=5\%$  and 0.2C.

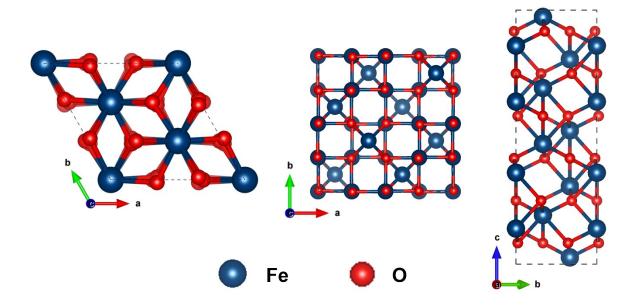


Figure S15. Illustrations of Fe<sub>3</sub>O<sub>4</sub> crystal structure in different views.

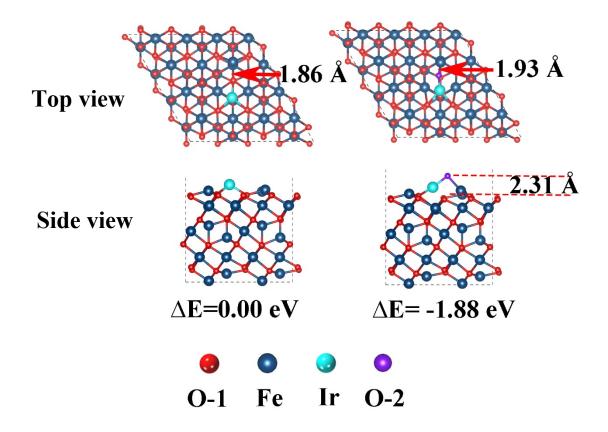


Figure S16. Top view and side view of two Fe<sub>3</sub>O<sub>4</sub>-Ir (111) surface structures along with the relative energy.

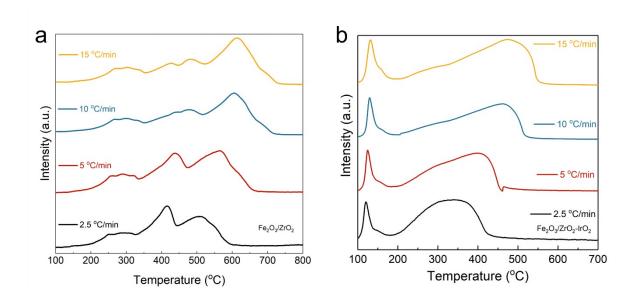


Figure S17. TPR profiles under different ramping rates of 2.5-15 °C/min for (a) fresh  $Fe_2O_3/ZrO_2$ ; (b) fresh  $Fe_2O_3/ZrO_2$ -IrO<sub>2</sub>.

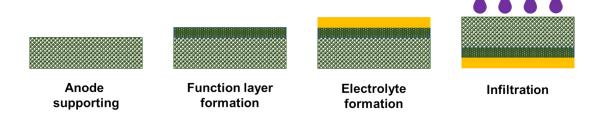


Figure S18. Schematic of HE-supported half-cell fabrication process including GDC infiltration.

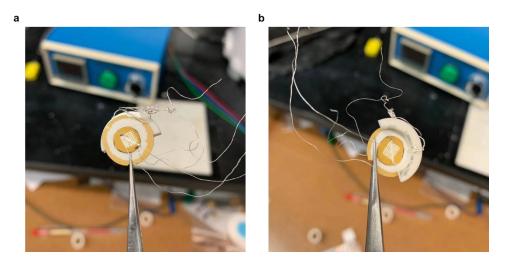


Figure S19. Picture of a three-electrode symmetric cell: (a) front; (b) back. Yellow: gold paste; center: Ag mesh;

white: ScSZ electrolyte.

Table S1. Electrochemical testing protocol for SOIAB with 0.001 mol Fe-loading as an example.

Protocol of Cell Testing														
1	Testing temperature													$\neg$
2	Glass powder melting													
3	OCV during reduction													
4	5% Hydrogen reduction													
5	Pure hydrogen reduction													
6	V-i curve for open system													
7	EIS for open system													
8	OCV between open and close													
9	V-i curve for close system													
10	EIS for close system													
11														
12	Rate performance at 10%	Rate	0.1C	0.2C	0.4C	0.5C	0.6C	0.8C	0.1C					
13		Current	0.007A	0.014A	0.028A	0.035A	0.042A	0.056A	0.007A					
14		Time	3600s	1800s	900s	720s	600s	450s	3600s					
15														
16	Utilization testing	$U_{Fe}$	5.00%	10%	20%	30%	40%	50%	60%	70%	80%	90%	100%	
17		Current	0.014A											
18		Time	900s	1800s	3600s	5400s	7200s	9000s	10800s	12600s	14400s	16200s	18000s	
19														
20	Cycling performance	U <sub>Fe</sub>	5.00%	20%	50%									
21		Current	0.014A	0.014A	0.028A									
22		Time	900s	3600s	4500s									
23		n	500	100	100				·		·	·		

## References

[1]. Zhang, C.; Ji, C.; Wang, W.; Schmidt, D.; Jin, X.; Lemmon, J. P.; Huang, K., *Energy Environ. Sci.* **2016**, *9* (12), 3746-3753.