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# **Supplementary Information**

## Surface Functionalized Poly(vinyl alcohol)-Hydrous Zirconium Oxide Composite

### Beads for Efficient and Selective Sequestration of Phosphate from Wastewater

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#### Data analysis and modeling

#### **Determination of batch adsorption performance**

The equilibrium uptake amount  $(q_e, mg/g)$  and the uptake amount  $(q_t, mg/g)$  at time t of the adsorbent beads were determined by eqs. (S1) and (S2).

$$q_{\rm e} = \frac{(C_o - C_{\rm e}) \times V}{m} \tag{S1}$$

$$q_t = \frac{(C_o - C_t) \times V}{m}$$
(S2)

where  $C_o(\text{mg/L})$ ,  $C_e(\text{mg/L})$  and  $C_t(\text{mg/L})$  are phosphate concentrations in the aqueous solutions at the initial time, equilibrium time, and time t (min); V is the volume of the aqueous solution (L); and m is the mass of the beads (g).

The desorption efficiency (DE) was determined from eq. (S3).

$$DE = \frac{C \times V}{(q \times m)} \times 100\%$$
(S3)

where *C* is phosphate concentration in the desorption solution (mg/L); *V* is the volume of the desorption solution (L); *q* is the amount of phosphate adsorbed on the adsorbent beads before desorption (mg/g); and *m* is the mass of adsorbent beads (g).

#### Modeling of adsorption kinetics and isotherms

The adsorption kinetics data were fitted with the non-linear pseudo-first-order model (eq. (S4)), non-linear pseudo-second-order model (eq. (S5)), non-linear Elovich model (eq. (S6)), and intraparticle diffusion model (eq. (S7)), and the equations were presented as follows.<sup>1</sup>

Non-linear pseudo-first-order:

$$q_{t} = q_{e}(1 - e^{-k_{1}t})$$
 (S4)

#### Non-linear pseudo-second-order:

$$q_{t} = \frac{k_{2}q_{e}^{2}t}{1 + k_{2}q_{e}t}$$
(S5)

where  $q_e$  (mg-P/g) and  $q_t$  (mg-P/g) are the amount of phosphate adsorbed onto the adsorbent at an equilibrium concentration ( $C_e$ , mg/L) and a predetermined time (t, min), respectively.  $k_1$  (1/min) and  $k_2$  (g/mg/min) are the rate constants for the pseudo-first-order model and pseudo-second-order model, respectively.

#### Non-linear Elovich equation:

$$q_t = \left(\frac{1}{\beta}\right) \ln(1 + \alpha\beta t) \tag{S6}$$

where  $\alpha$  is regarded as the initial rate (mg g<sup>-1</sup> min<sup>-1</sup>), and the  $\beta$  is adsorption constant (g mg<sup>-1</sup>).

Intra-particle diffusion model:

$$q_{\rm t} = k_{id} t^{0.5} \tag{S7}$$

where  $k_{id}$  (mg/g/min<sup>0.5</sup>) is the intra-particle diffusion rate constant.

The adsorption isotherms data were fitted by the nonlinear Langmuir model (eq. (S8)) and Freundlich model (eq. (S9)) as follows.<sup>1,2</sup>

$$q_{\rm e} = \frac{q_{\rm m} k_L C_{\rm e}}{1 + k_L C_{\rm e}}$$
(S8)  
$$q_{\rm e} = k_F C_e^{1/n}$$
(S9)

where  $q_e \pmod{P/g}$  and  $q_m \pmod{P/g}$  denote the adsorption capacity at equilibrium and predicted maximum adsorption capacity.  $C_e \pmod{L}$  is the equilibrium phosphate concentration;  $k_L (L/mg)$  is the Langmuir adsorption constant;  $k_F ((mg/g)(L/mg)^{1/n})$  and *n* represent the Freundlich adsorption constant and heterogeneity factor, respectively. The calculation of distribution coefficient  $K_d$  (L/g) was defined as the ratio of adsorbed phosphate to the dissolved phosphate remaining in the solution, which was calculated as follows.<sup>3</sup>

$$K_d = \frac{V \times (C_0 - C_e)}{m \times C_e}$$
(S10)

where  $C_o (\text{mg/L})$  and  $C_e (\text{mg/L})$  are phosphate concentrations in the aqueous solutions at the initial time and equilibrium time; V is the volume of the aqueous solution (L); and m is the mass of the beads (g).

#### **Determination of column adsorption performance**

The total amount of phosphorus (P) adsorbed onto the adsorbent beads ( $q_{total}$ , mg) and the equilibrium adsorption capacity ( $q_e$ , mg P/g) were calculated by the following eqs. (S11) and (S12).<sup>4</sup>

$$q_{total} = \frac{Q}{1000} \int_{t=0}^{t=T_{total}} (C_o - C_t) dt$$
 (S11)

$$q_e = \frac{q_{total}}{m} \tag{S12}$$

where Q (mL/min) is the feed flow rate;  $C_o$  (mg/L) and  $C_t$  (mg/L) represent the influent and effluent P concentration at the initial stage and t time caused by adsorption.  $T_{total}$ (min) is the total time when the column achieves the exhaustion point ( $C_t/C_0=90\%$ ); m(g) is the mass of adsorbent beads packed in the column.

#### Modeling of column adsorption for breakthrough curves

The fixed-bed column adsorption data were fitted by the Thomas model (eq. (S13)) to predict the breakthrough curves.<sup>1, 2, 4</sup>

$$\ln(\frac{C_o}{C_t} - 1) = k_{Th}q_o \frac{m}{Q} - k_{Th}C_o t$$
 (S13)

where Q (mL/min) is the feed flow rate;  $C_o$  (mg/L) is the influent phosphate concentration;  $C_t$  (mg/L) is the effluent phosphate concentration at time t (min);  $k_{Th}$  (mL/min/mg) is the Thomas rate constant;  $q_o$  (mg P/g) is the equilibrium absorption capacity; m (g) is the mass of adsorbent in the column.

### Determination of the value of pH at point of zero charge ( $pH_{pzc}$ )

The pH at point of zero charge (pH<sub>pzc</sub>) for HZO-PVA and TETA@HZO-PVA was determined by the pH drift method.<sup>5</sup> Specifically, 20 mg of HZO-PVA or TETA@HZO-PVA was added into 80 mL of 0.1 M NaCl solution at desired pH values (2-12). The initial pH (pH<sub>i</sub>) of the aqueous solution was adjusted by HCl or NaOH solution (1 M). The final pH (pH<sub>f</sub>) was recorded after continuous stirring at 35 °C for 24 h. Then the pH<sub>PZC</sub> is the point where the curve of  $\Delta pH$  (= pH<sub>f</sub> - pH<sub>i</sub>) versus pH<sub>i</sub> crosses the line equal to zero.

Туре	Parameter	HZO-PVA	TETA@HZO-PVA	
	$q_e ({ m mg/g})$	8.80	23.47	
Pseudo-first-order model	$k_1 (\min^{-1})$	0.006	0.009	
	$R^2$	0.962	0.958	
	$q_e (\mathrm{mg/g})$	9.74	25.54	
Pseudo-second-order model	$k_2$ (g/mg/min)	8.185×10-4	4.867×10-4	
	$R^2$	0.993	0.992	
	$\alpha (mg g^{-1} min^{-1})$	0.176	0.963	
Elovich model	$\beta (g m g^{-1})$	0.550	0.236	
	R <sup>2</sup>	0.979	0.958	
	$q_{\rm m}$ (mg/g)	31.23	39.87	
Langmuir model	$k_{\rm L}$ (L/mg)	0.058	0.430	
	$R^2$	0.987	0.956	
	$k_F ((mg/g)(L/mg)^{1/n})$	3.645	16.595	
Freundlich model	n	2.047	4.167	
	$R^2$	0.989	0.980	

 Table S1. Kinetic and isotherm parameters for phosphate sequestration.

Step	Parameter	HZO-PVA	TETA@HZO-PVA	
Step 1	$k_{1d}$ (mg/g/min <sup>0.5</sup> )	0.448	1.501	
	$R^2$	0.977	0.986	
Step 2	$k_{2d} ({ m mg/g/min^{0.5}})$	0.113	0.258	
	$R^2$	0.957	0.948	

 Table S2. Intraparticle diffusion model parameters for phosphate sequestration.

Somulas	Spacing	Binding	FWHM	Aera	Percentage
Samples	Species	energy (eV)	(eV)	(cps eV)	(%)
	C-0	532.53	1.68	50145.79	54.0
	-OH	530.26	1.68	19422.96	20.9
HZO-PVA	O <sup>2-</sup>	531.39	1.68	23220.87	25.0
	Zr 3d5/2	182.39	1.32	24033.73	60.0
	Zr 3d3/2	184.77	1.32	16026.68	40.0
	C-0	532.60	1.60	51540.27	52.9
D loaded UZO	-OH	530.39	1.60	17218.51	17.7
	O <sup>2-</sup>	531.48	1.60	28660.01	29.4
ΓVΑ	Zr 3d5/2	182.60	1.31	22530.13	59.8
	Zr 3d3/2	184.98	1.31	15175.82	40.2

**Table S3** Fitting parameters for O 1s and Zr 3d spectra of virgin and P-loaded HZO-PVA.

		Binding	Binding FWHM		Percentage	
Samples	Species	energy (eV)	(eV)	(cps eV)	(%)	
	-NH <sub>2</sub> , -NH-	399.47	1.64	7932.54	65.9	
	-NH <sub>3</sub> <sup>+</sup> , -NH <sub>2</sub> <sup>+</sup>	401.94	1.64 4102.30		34.1	
	C-O	532.45	1.70	53250.56	67.7	
TETA@HZO-PVA	O <sup>2-</sup>	531.38	31.38 1.70		17.0	
	-OH	530.20	1.70	11985.58	15.2	
	Zr 3d5/2	182.27	1.36	16426.44	60.5	
	Zr 3d3/2	184.65	1.36	10718.57	39.5	
	-NH <sub>2</sub> , -NH-	399.52	1.58	5445.04	46.3	
	-NH <sub>3</sub> <sup>+</sup> , -NH <sub>2</sub> <sup>+</sup>	401.97	1.58 6308		53.7	
P-loaded	C-O	532.60	1.70	69128.38	65.9	
TETA@HZO-PVA at	O <sup>2-</sup>	531.97	1.70	26626.75	25.4	
pH 2	-OH	530.60	1.70	9153.73	8.7	
	Zr 3d5/2	182.67	1.42	10470.41	58.2	
	Zr 3d3/2	185.05	1.42	7525.38	41.8	
	-NH <sub>2</sub> , -NH-	399.58	1.72	5144.14	60.6	
P-loaded TETA@HZO-PVA at	-NH <sub>3</sub> <sup>+</sup> , -NH <sub>2</sub> <sup>+</sup>	401.92	1.72	3344.58	39.4	
	C-O	532.59	1.66	76511.38	69.3	
	O <sup>2-</sup>	531.58	1.66	21977.44	19.9	
pH 8	-OH	530.42	1.66	11907.13	10.8	
	Zr 3d5/2	182.41	1.41	11460.15	59.7	
	Zr 3d3/2	184.79	1.41	7734.13	40.3	

**Table S4** Fitting parameters for O 1s, N 1s and Zr 3d spectra of TETA@HZO-PVAbefore and after phosphate adsorption at different pH conditions.

Sample	pH (g)	m	Q (mL/min)	<i>C</i> <sub>o</sub> (mg/L)	q <sub>total</sub> (mg P)	$q_e \pmod{(\mathrm{mg P/g})}$	Thomas model		
		(g)					$k_{Th}$ (mL/(min·mg))	$q_o$ ) (mg P/g)	<i>R</i> <sup>2</sup>
Synthetic solution	5.8	3	5	3.08	83.67	27.89	0.185	28.13	0.984
Real wastewater	7.7	3	5	3.08	60.93	20.13	0.189	20.15	0.961

Table S5. Column tests conditions and results.



Fig. S1 Photographs of the freeze-dried HZO-PVA and TETA@HZO-PVA composite beads.



Fig. S2 XRD patterns of HZO-PVA and TETA@HZO-PVA.



Fig. S3 TGA curves of neat PVA, HZO-PVA and TETA@HZO-PVA.



Fig. S4 Distribution of phosphate species as a function of pH.



Fig. S5 The pH at point of zero charge ( $pH_{pzc}$ ) for HZO-PVA and TETA@HZO-PVA.



Fig. S6 Phosphate adsorption kinetics onto HZO-PVA and TETA@HZO-PVA with Elovich model fitting.



**Fig. S7** XPS analysis of HZO-PVA before and after phosphate adsorption: (a) widescan spectrum; (b) O1s before adsorption; (c) Zr 3d before adsorption; (d) P 2p; (e) O 1s after adsorption; (f) Zr 3d after adsorption.



Fig. S8 P 2p XPS spectra of TETA@HZO-PVA after phosphate adsorption at pH 2 and

8.



Fig. S9. Plots of linear regressions on Thomas model.

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