

SUPPLEMENTAL INFORMATION

Super- soft, firm, and strong elastomers toward replication of tissue viscoelastic response

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S1 Materials and Synthesis

S1.1 Materials. Tetrahydrofuran (THF), toluene, acetone, hexane, acetonitrile, and p-xylene were purchased from Fisher Scientific and used as received. Styrene and n-butyl acrylate (BA) were purchased from Fisher Scientific and were passed twice through basic alumina column to remove inhibitor. 2,2'-Azobis(2-methylpropionitrile) (AIBN, 98%), Methyl 2-(dodecylthiocarbonothioylthio)-2-methylpropionate (CTA, 97%), α -bromoisobutyryl bromide (BiBB, 98%), 2-Hydroxyethyl 2-bromoisobutyrate (HEBIB, 95%), methacryloyl chloride (MACl, 97%), triethylamine (TEA), copper(I) bromide (CuBr, 99.999%), *tris*[2-(dimethylamino)ethyl]amine (Me₆TREN), N,N,N',N'',N''-Pentamethyldiethylenetriamine (PMDETA), dibutyltin dilaurate (DBTDL, 95%), 2-isocyanatoethyl methacrylate (IEM, 98%), tetrabutylammonium bromide (TBAB, 98%), 33 wt. % hydrobromic acid solution in acetic acid (HBr), aluminum oxide (activated, basic, Brockmann I), silica gel (230-400 mesh) were purchased from Sigma Aldrich and used as received. Poly(ethylene glycol) methacrylate (PEGMA, $M_n = 500$ g/mol) was obtained from Sigma Aldrich and purified by passing (twice) through basic alumina column to remove inhibitor. Monomethacryloxypropyl terminated polydimethylsiloxane (PDMSMA, MCR-M11, $M_n = 1000$ g/mol) and potassium methacrylate (KOMA, 95-100%) were obtained from Gelest. The former was purified using a basic alumina column to remove inhibitor and the latter was used as received. RB HR-PIB-1000 was obtained from RB Products and used as received. Methyl methacrylate (MMA, 99%) and styrene (Sty, 99%) was obtained from Fisher Scientific and purified using a basic alumina column to remove inhibitor. Teflon petri dishes were purchased from Welch Fluorocarbon.

CRP OF poly[MMA-g-(PDMS/PMMA)] AND poly[nBA-ran-MMA-g-(PDMS/PMMA)]

S1.2 Functionalization of PEGMA-OH. PEGMA (40g, 40mmol), TEA (4.04g, 40mmol), THF (40mL) and a stir bar were added to a round bottom flask and left to stir at 0°C for 30 minutes. BiBB (9.16g, 4.92mL, 40mmol) was added dropwise over 15 minutes to the reaction mixture. The solution was brought to room temperature and left to stir for an additional 2 hours. The mixture was centrifuged and the organic layer decanted and concentrated under vacuum. The reaction mixture was then passed through a silica column and dried overnight resulting in a functionalized PEGMA-Br ATRP initiator as a functional site for future polymerization.

S1.3 Grafting Through RAFT copolymerization. For a graft copolymer macroinitiator with architectural parameters of $n_g = 8$, $n_{sc} = 14$, $n_x = 100$, PDMSMA (20g, 20mmol), BA (17.9g, 0.14mol), PEGMA-Br (1.04g, 1.6mmol), CTA (21.8 μ L, 57.6 μ mol), AIBN (2.3mg, 14.4 μ mol), toluene (20mL), and a stir bar were added to a Schlenk flask. The solution was bubbled with dry nitrogen for 1 hour, then submerged into an oil bath at 70°C, and left to polymerize overnight. The polymerization was quenched by opening the flask, the reaction mixture dried, and the conversion determined by ¹H-NMR to be 88% of a random PDMSMA, PEGMA-Br and PBA copolymer with $n_{bb} = 1935$ (Fig. S5). The polymer mixture was precipitated from methanol 2-3 times to remove residual PDMSMA and dried under vacuum until a constant mass was reached (Fig. S6).

S1.4 Grafting From to synthesize poly[MMA-g-(PDMS/PMMA)] via ATRP. The resulting polymer brushes polymerized by RAFT were then used as macroinitiators for ATRP growth of linear MMA. For a typical graft copolymer elastomer, graft copolymer initiator (2g), excess MMA (2g), M₆TREN (5 μ L, 18.7 μ mol), toluene (50mL) and a stir bar were added to a Schlenk flask. The solution was bubbled with dry nitrogen for 1 hr then Cu(I)Br (2.8 mg, 18.7 μ mol) was quickly added to the reaction mixture under nitrogen atmosphere. The flask was sealed, purged for an additional 15 minutes, and then immersed in an oil bath at 45°C. The polymerization was visually monitored to avoid gelation of the growing chains. The polymerization was quenched at various times to afford a series of graft copolymers with increasing PMMA ratio. Note, reaction times were relatively short (0.5-1.5hr) using 20mL of toluene before observed gelation similarly documented in the literature,¹ however excess toluene (>80mL) allowed for larger growth time (2hr) of PMMA chains before gelation. All resulting graft copolymer elastomers were swelled and washed two-three times with acetone to remove PMMA homopolymer, and then swelled and washed two-three times with hexanes to remove unreacted brushes. These impurities typically represent <10% of the total yield.² Finally, the n_A and ϕ_A of the PMMA side chains were measured by ¹H-NMR (Fig. S8-S12) as summarized in Table 1, PEG appendage excluded. Samples were then dissolved in THF (75 wt% solvent) and poured into Teflon petri-dishes and left to dry overnight to yield films for further mechanical testing. Note that the grafting from approached exhibited synthetic limitations where ϕ_A did not exceed 0.07 due to insolubility between the growing A-g-B brush strand in residual monomer/solvent solution. Another factor may be the polarity/functionality of the RAFT end groups during ATRP. Further experimentation is needed to greater understand the interplay between attainable ϕ_A and χ of monomers and synthesized

yielding 98% functionalized polymer (determined by $^1\text{H-NMR}$, Fig. S15). No residual olefin residue was present suggesting higher conversion.

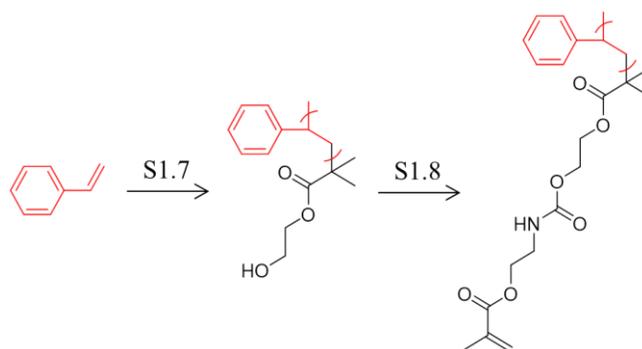
S1.6 Synthesis of PIB macromonomer, $n_{sc} = 18$. The functionalized oligomer (45g, 0.042mol) was dissolved in THF (350mL) and transferred to an oven dried 500mL round bottom flask equipped with a stir bar. The solution was charged with 26.0g KOMA (0.21mol) and 67.6g TBAB (0.25mol) and stirred for 36 hrs at 45°C. The solution was centrifuged to remove residual salt and unreacted reagent. Subsequently, the solution was condensed by bubbling with air and washed with H_2O /hexane twice. The organic layer was separated, dried with anhydrous MgSO_4 , and ran through a SiO_2 column twice yielding PIB ($n_{sc} = 18$) macromonomer product (99% conversion, ~90% yield). Again, no residual peaks were present from the α -hydrogens suggesting higher yield. $^1\text{H-NMR}$ of the synthetic progression is shown in Fig. S15.



Scheme 2. PIB macromonomer synthesis.

S1.7 Synthesis of PS oligomers. ATRP of polystyrene homopolymer was performed with a target $n_A = 60$ at 34% conversion to avoid large viscosities at higher conversion. Styrene (100g, 0.96mol), HEBIB (1.16g, 5.5mmol), PMDETA (0.095g, 0.114mL, 0.55mmol), and a stir bar were added to a Schlenk flask. The solution was bubbled with dry nitrogen for 1 hour then Cu(I)Br (0.079g, 0.55mmol) was quickly added to the reaction mixture under nitrogen atmosphere. The flask was sealed, purged for an additional 15 minutes, and then immersed in an oil bath at 90°C. The reaction mixture was left to polymerize for 14 hrs to receive a 34% conversion ($n_{sc} = 60$) and the reaction was quenched by exposing the mixture to oxygen (Fig. S14). The mixture was centrifuged and gravity filtered to remove residual Cu-ligand complex. Residual styrene monomer was evaporated and the remaining PS oligomer was dissolved in minimal THF and crashed in excess methanol (1:10, THF:Methanol by volume) 3 times. The washed PS oligomer was dried overnight at room temperature under reduced pressure to remove any residual solvent.

S1.8 Synthesis of PS (DP = 60) macromonomer. The PS oligomer (30 g, 4.8mmol, DP = 60) was transferred to a round bottom flask sealed by rubber septum and parafilm and dissolved in 60 ml of THF. Once the PS was fully dissolved, 0.05 g (47 μ L, 80 μ mol) dibutyltin dilaurate was added to the solution, it was subsequently purged of oxygen by bubbling the solution with nitrogen for 10 minutes. IEM (0.82g, 0.75mL, 5.3mmol) was added dropwise to the round bottom flask under constant stirring. Nitrogen was removed from the flask, and the solution was set to stir for 18hr. The subsequent solution was further diluted with THF (5-10x) and passed through silica column twice. The purified mixture was dried under reduced pressure and characterized by $^1\text{H-NMR}$ (Fig. S14). $^1\text{H-NMR}$ reveals 80% conversion so subsequent calculations for ϕ_A for performed considering an 80% ratio of macromonomers.

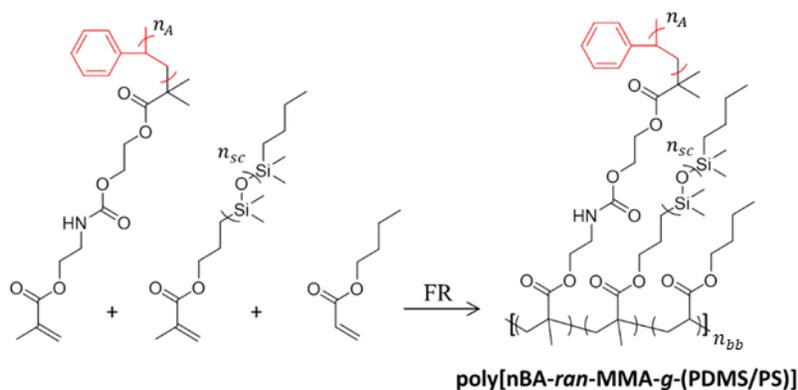


Scheme 3. PS macromonomer synthesis.

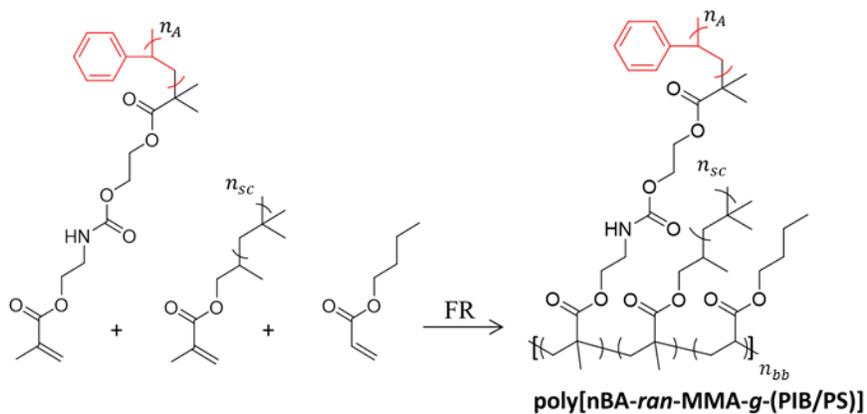
S1.9 FR polymerization of A-g-B brush copolymers by grafting through. A Schlenk flask was charged with appropriate molar quantities of side-chain macromonomer (PDMS, PIB), spacer (n-BA), A-block macromonomer (PS), 1:1 volume of p-xylene, and 0.15 mol% initiator (BAPO). The flask was shielded from light and purged with nitrogen for 30 minutes. Subsequently, the solution was removed from nitrogen and allowed to polymerize under UV-light for 18hr. The solution exhibits a light-yellow color upon introduction to the UV-light but returns to transparent after polymerization. The unwashed polymer solution was casted in a Teflon mold at 60°C and dried overnight. The resultant polymer was washed according to chemistry. poly[nBA-*ran*-MMA-g-(PIB/PS)]: the unwashed polymer was dissolved in THF and crashed with acetonitrile (1:1.2, THF:acetonitrile) 3 times (Fig. S1). The washed polymer was dissolved in p-xylene once more and casted into a Teflon petri-dishes (Welch Fluorocarbon) at 60°C and dried overnight to be characterized by $^1\text{H-NMR}$ where no macromonomer peaks remained (Fig. S16). poly[nBA-*ran*-MMA-g-(PDMS/PS)]: the unwashed polymer was dissolved in acetone and crashed out in acetonitrile (2:1, acetone:acetonitrile). This wash was repeated three times. The washed polymer

was dissolved in p-xylene once more and cast into a Teflon petri-dishes and dried overnight to be characterized by $^1\text{H-NMR}$ where no macromonomer peaks remained. Note that unreacted reagents act as diluent and decrease the modulus of the network. Comparing washed and unwashed A-g-B network stress-strain curves exhibit this behavior (Fig. S24). The number average molecular weight (M_n) of the A-g-B brush polymer stand was determined by light scattering detection during gel-permeation chromatography (Fig. S18, S20)

Ex. synthetic calculations. poly[nBA-*ran*-MMA-*g*-(PIB/PS)]. Sample: 030722_1. 2.00g n-butyl acrylate (15.6mmol), 2.41g PIB macromonomer (2.23mmol), 0.27g PS macromonomer (43 μmol , 80% conversion PS mixture, total mass 0.34g), 7mg BAPO (17 μmol , 0.15w/w%), and 4.5mL of p-xylene.



Scheme 4. Polymerization of poly[nBA-*ran*-MMA-*g*-(PDMS/PS)] brush graft copolymers.



Scheme 5. Polymerization of poly[nBA-*ran*-MMA-*g*-(PIB/PS)] brush graft copolymers.

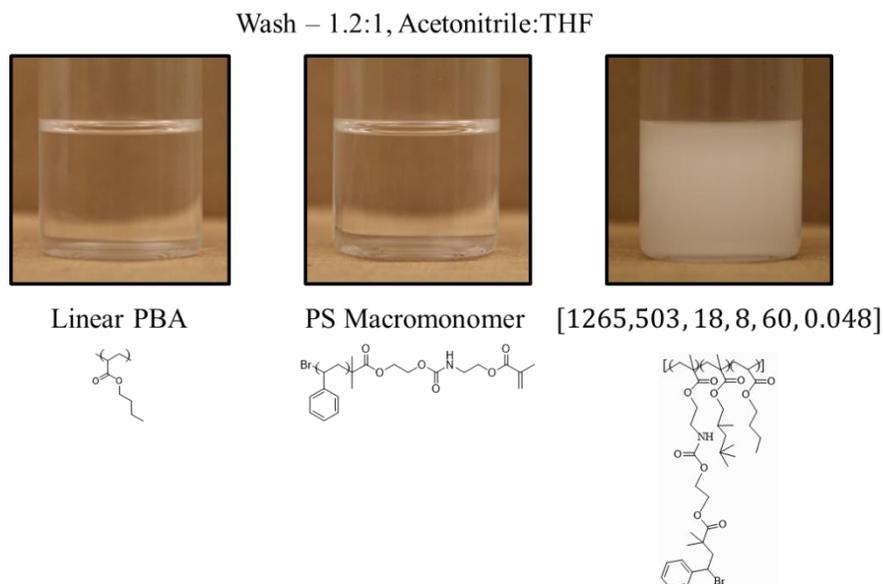


Fig. S1. Example purification of A-g-B brush copolymers, poly[nBA-*ran*-MMA-g-(PIB/PS)].

S2 Materials Characterization

S2.1 Atomic force microscopy. Monolayers of A-g-B brush copolymers were prepared by Langmuir-Blodgett using a KSV 5000 onto a muscovite sheet (Fig. 2a,b). The monolayer was formed by diluting the polymer in dichloromethane to 0.3 mg/mL and dispersing 75 μ L onto the water reservoir. The muscovite sheet was removed from the water reservoir at a 5mm/min once the surface tension had reached 0.5 mN/m, forming a polymer monolayer on the muscovite sheet. Obtaining an image with clustered domains was achieved by forming a less dense layer of polymers on the surface of the water with a surface tension \sim 0.4 mN/m. Imaging was performed in PeakForce QNM mode using a multimode AFM (Brüker) with a nanoscope V controller and silicon nitride (Scanasyt-Air by Brüker, resonance frequency of 50-90 HZ and spring constant of 0.4 N/m). Inter-brush distance was calculated by the mean of 50 individual measurements between brush peaks on the AFM height micrograph on the Nanoscope Analysis software (Brüker).

S2.2 Small angle X-ray scattering (SAXS). SAXS measurements were performed on the ID02 and BM26 beamlines of the ESRF (grenoble, France). The experiments at ID02 were conducted in transmittance geometry with a photon energy of 12.46 KeV. The total phototon flux on the sample is estimated to 9.1¹¹ photons persecond with the monochromatic incident X-ray beam collimated to a footprint of 100 x 200 μ m² (V x H) allowing an acquisition time of less than 100 ms per frame. The q values ($q = 4\pi \sin(\theta) / \lambda$) range from 7.5x10⁻³ nm⁻¹ to 3 nm⁻¹ at a sample

detector distance of 2 m. Optimization of the signal-noise ratio through a Rayonix MX-170HS in a 35 m long vacuum flight tube was achieved through the binning of 2x2 pixel leading to an effective pixel size of 89 μm in both directions.

SAXS images at BM26 were collected using a Pilatus 1M detector (169 mm x 179 mm active area). The experiments were performed in transmission geometry using a photon energy of 12.99 keV and sample-to-detector distance of 2.8 m. Mechanical stretching of the samples was carried out using tensile cell from Linkam (LINKAM TST 350). The data correction, calibration, and integration was performed using the fast azimuthal integration Python library. (reference to insert : G. Ashiotis, A. Deschildre, Z. Nawaz, J. P. Wright, D. Karkoulis, F. E. Picca and J. Kieffer Journal of Applied Crystallography, 2015, 48, 510-519). To compute form factor parameters 1D SAXS curves were fit to a scattering for a polydisperse population of spheres with uniform scattering length density. The distribution of radii is a Gaussian distribution. The data modelling and analysis were performed using the SANS & USANS data reduction and analysis package provided by NIST⁵ for Igor Pro 6.7.3.2 environment from WaveMetrics Ltd.

S2.3 Uniaxial tensile stress strain measurements. Dog bone shaped samples with bridge dimensions of 12 mm \times 2 mm \times 1 mm were loaded into an RSA-G2 DMA (TA Instruments) and subjected to uniaxial extension at 20°C and constant strain rate of 0.005 s⁻¹ for PDMS samples and 0.001 s⁻¹ for PIB samples. Samples were stretched until rupture, revealing the entire mechanical profile. In each case, mechanical tests were conducted in triplicate to ensure accuracy of the data. The elongation ratio λ for uniaxial network deformation is defined as the ratio of the sample's instantaneous size L to its initial size L_0 , $\lambda = L/L_0$. At small and intermediate deformation range, all stress-deformation curves, $\sigma_{true}(\lambda)$, follow non-linear equation of network elasticity⁶ and switch to a linear scaling, $\sigma_{true}(\lambda) \sim \lambda$, at large deformations (see Fig. S2).^{1,7} Network elastic parameters (E, E_0, β) obtained from the fitting of stress-deformation curves were averaged over sample triplicates, while reported λ_{max} and σ_{max} are given for the largest of each triplicate.

Fitting structural modulus (E) and strain stiffening (β). In the elastic deformation regime, raw stress strain curves for uniaxial deformation were fitted to the following non-linear equation⁶

$$\sigma_{true}(\lambda) = \frac{E}{9}(\lambda^2 - \lambda^{-1}) \left(1 + 2 \left(1 - \frac{\beta(\lambda^2 + 2\lambda^{-1})}{3} \right)^{-2} \right). \quad (\text{S1})$$

with E and β being fitting parameters as illustrated in Fig. S2. The corresponding Young's modulus, E_0 , at small deformations, $\lambda \rightarrow 1$, is given by

$$E_0 = \frac{E}{3}(1 + 2(1 - \beta)^{-2}). \quad (\text{S2})$$

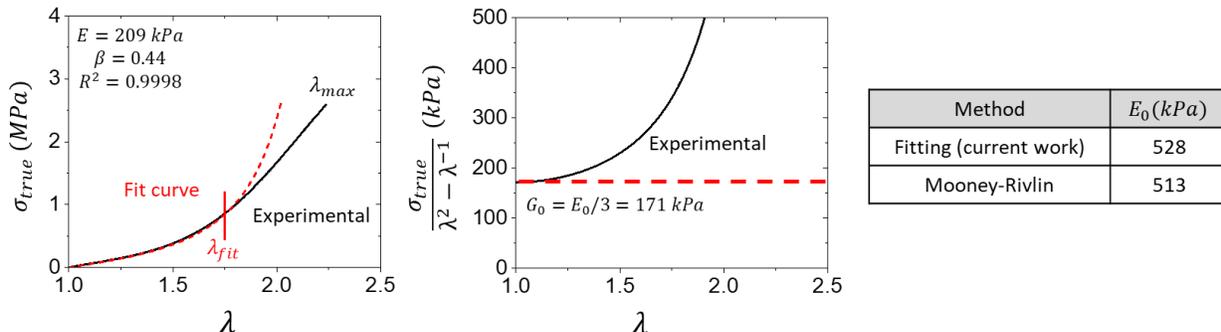


Fig. S2. Comparing fitting vs. Mooney-Rivlin method for determination of E_0 . The fitting method shows good agreement with the Mooney-Rivlin method within 3 percent variation. $[(528\text{kPa} - 513\text{kPa})/(513\text{kPa})] * 100 = 2.9\%$. $\dot{\epsilon} = 0.005$, $T = 22^\circ\text{C}$.

S2.4 Rheology. Frequency and temperature sweeps were performed on the ARES-G2 Rheometer (TA instruments) with 8mm compression plate geometries. Samples were prepared by cutting 8mm diameter disks with approximate height of 1mm (exact height was specified in the rheometer for each sample). The frequency sweep was performed from 0.01 to 100 Hz (within the viscoelastic PSA range) at 22°C at with $\epsilon = 0.05$ to ensure adequate contact area between the compression plate and sample. The temperature sweep was performed from 20°C to 200°C with $\epsilon = 0.05$ oscillating at 1 Hz. Noisy data in melt state at high temperatures as a consequence to the infacial contact area between the compression plate and sample decreasing were removed.

S2.5 Fused-filament fabrication 3D printing. Fused-filament fabrication 3D printing was performed with poly[nBA-ran-MMA-g-(PIB/PS)] sample 030722_2 using a Cellink BioX 3D printer where shape stl. files were created with Tinkercad (for dogbones) and Photoshop (for UNC logo) (Fig. 4c). The polymer reservoir was heated to 150°C to ensure adequate flow and extruded at a pressure of 120 kPa. Multiple dog-bone shape samples were printed with one left raw and the other annealed at 100°C for 5 minutes (Fig. S31).

S2.6 Modified probe tack testing. The W_{adh} was measured using a modified version of the probe tack test using a G2-RSA DMA.⁸ The top arm contained a 2 mm diameter probe and the bottom

arm was a 25 mm plate both with roughness of 0.5 microns (TA instruments). Segments of sample were placed on the bottom compression plate and allowed to wet the surface over time. In addition, a rubber roller was used to apply light pressure ensuring the adhesive bond between the elastomer and bottom plate (acting as carrier) remained intact during measurement.

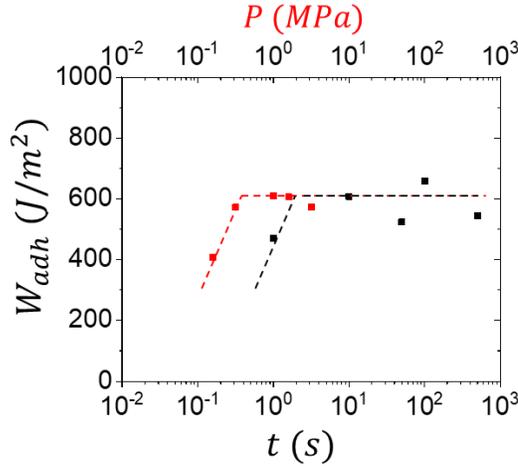


Fig. S3. Optimization of contact pressure and dwelling time. The modified probe tack test was performed using a control PSA elastomer independently changing the contact pressure (P) and contact time (t) in effort to maximize the contact area of the PSA bond. The degree of contact area coverage and subsequent W_{adh} , calculated as

$$W_{adh} = h_0 \int_0^{\varepsilon_{max}} \sigma_{eng}(\varepsilon) d\varepsilon, \quad (S3)$$

where h_0 is the initial thickness of the adhesive film and ε_{max} is the maximum strain before catastrophic failure of the bond, plateaued $\sim 600 \text{ J/m}^2$. Parameters of 1 MPa contact pressure and 100s contact time were used for further experimentation.

Each run consisted of compression at 0.01 mm/s until a contact pressure, $P = 1 \text{ MPa}$, was attained. The probe was held at a dwell time, $t = 100 \text{ s}$ and removed at 1mm/s for debonding.

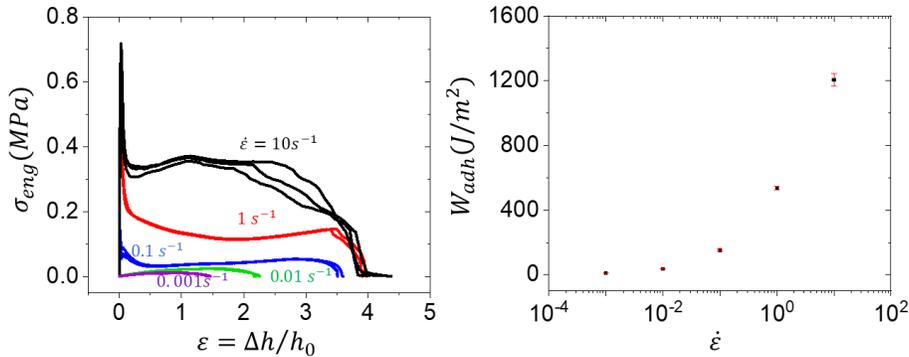


Fig. S4. Repeatability of modified probe tack test experiment. The modified probe tack was performed 3 times at the various debonding rates on a control brush PSA. The experimental procedure yields less than 4 percent deviation in W_{adh} between tests at the same strain rate. $h_0 \sim 1 \text{ mm}$, $T = 22^\circ \text{C}$.

S2.7. Gel-permeation chromatography (GPC). The molecular weight of the A-g-B brush copolymers synthesized by grafting through free-radical polymerization was determined by GPC using a Tosoh EcoSEC *Elite* GPC system equipped with a TSKgel Super HM-M (17392) column maintained at 40°C with an RI detector and Tosoh LENSTM 3 multiangle light scattering detector. Tetrahydrofuran was used as the mobile phase at a flow rate of 0.5 mL/min. Molecular weight and dispersity is reported based on polystyrene standards. Note that molecular weight readings are not very reliable from the RI detection,⁹ so molecular weights were reported from light scattering detection.

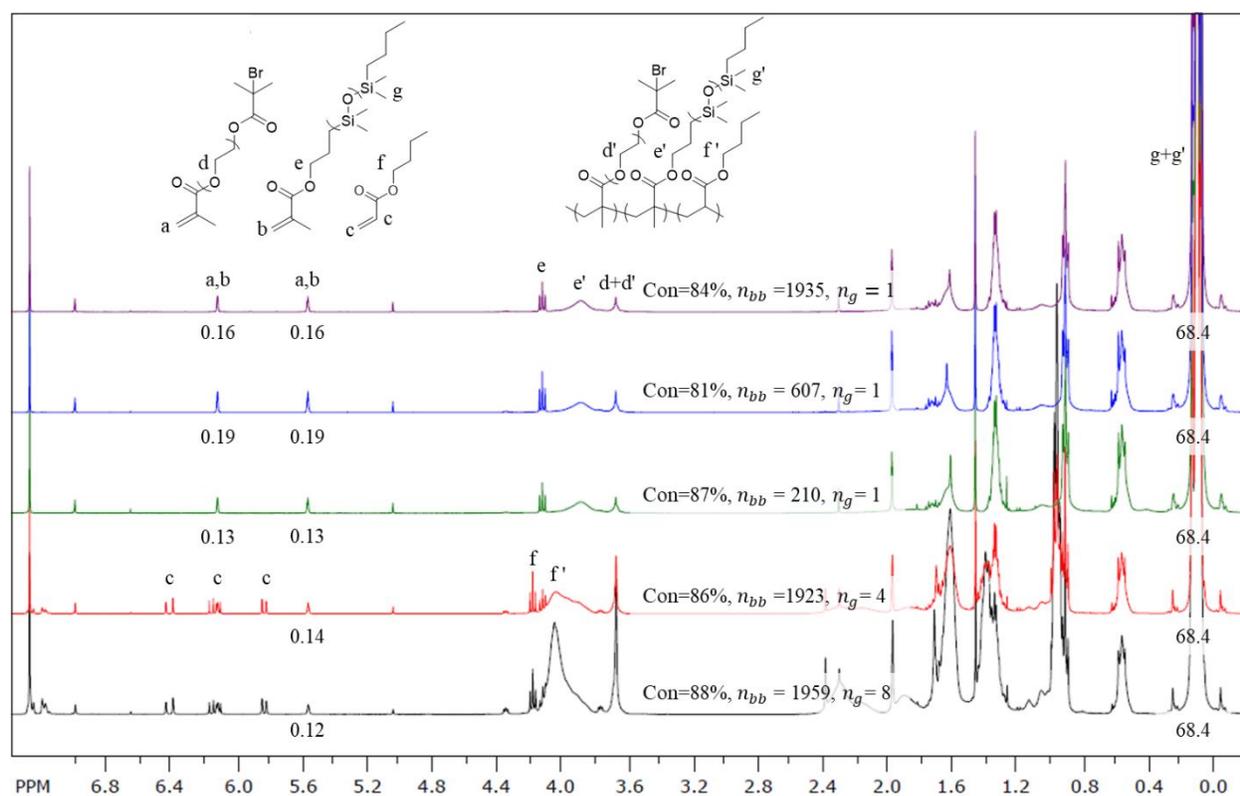


Fig. S5. ¹H-NMR of graft copolymer macroinitiators synthesized by CRP after termination (400 MHz, CDCl₃): 6.42, 6.14, 5.84 (CH₂=CH-C-, Residual BA monomer, d, 1H; m, 1H; d, 1H), 6.12, 5.56 (CH₂=C(CH₃)-C-, PDMS macromonomer, s, 1H), 4.18 ((C=O)-O-CH₂-, Residual BA monomer, t, 2H), 4.13 ((C=O)-O-CH₂-, PDMS macromonomer, t, 2H), 4.05 ((C=O)-O-CH₂-, PBA brush, m, 2H), 3.89 ((C=O)-O-CH₂-, PDMS brush, m, 2H), 3.67 (-O-CH₂-CH₂-, PEG side chain, m, 4H), 0.09 (-Si(CH₃)₂-O)_n-, PDMS macromonomer and brush mixture, s, 68.4H). Conv. = [area(g+g')/68.4-area(a,b)/1]/[area(g+g')/68.4], n_{bb} = Conv.*([PDMS]+[BA]+[PEGMA])/[I].

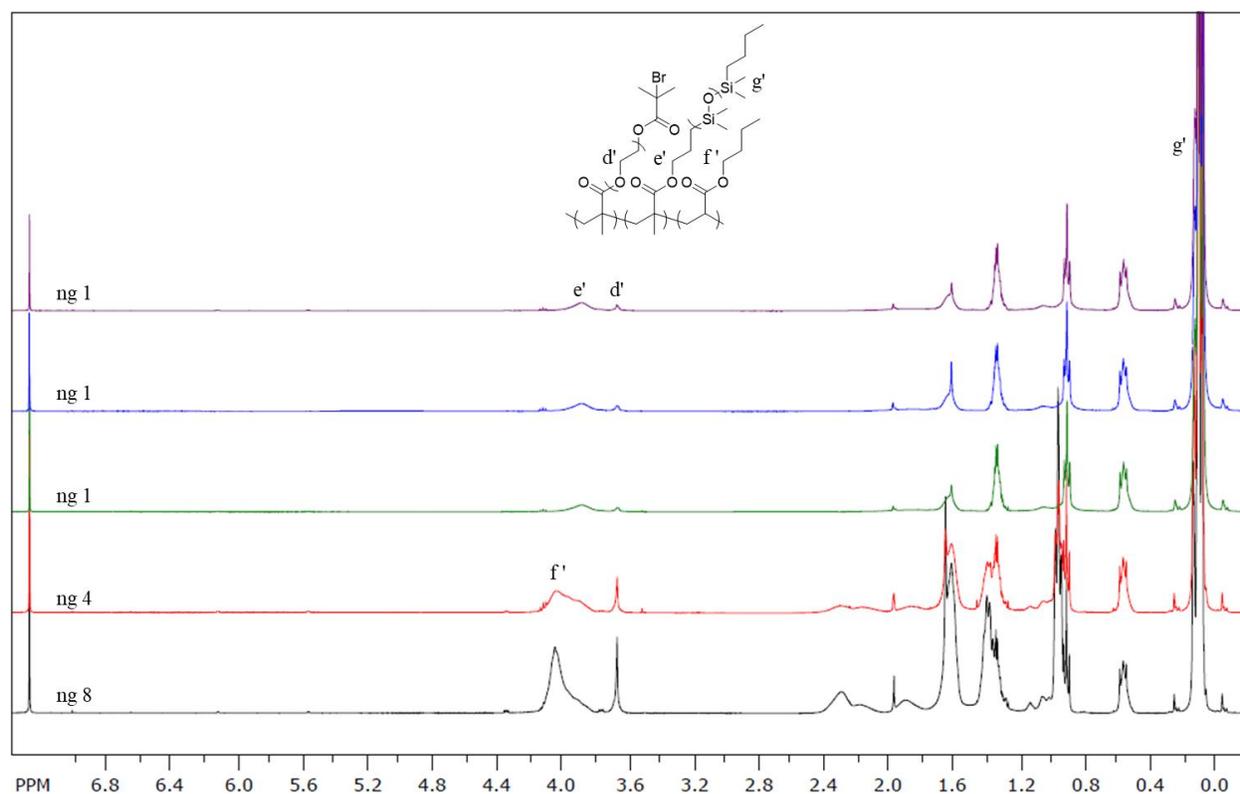


Fig. S6. $^1\text{H-NMR}$ of purified graft copolymer macroinitiators synthesized by CRP (400 MHz, CDCl_3): 4.05 ((C=O)-O-CH₂-, PBA brush, m, 2H), 3.89 ((C=O)-O-CH₂-, PDMS brush, m, 2H), 3.67 (-O-CH₂-CH₂-, PEG side chain, m, 4H), 0.09 (-Si(CH₃)₂-O)_n-, PDMS macromonomer and brush mixture, s, 68.4H). $d'=0.295$ for $n_g = 1$ backbones. $d'=0.905$ for $n_g = 4$ backbones. $d'=1.951$ for $n_g = 8$ backbones.

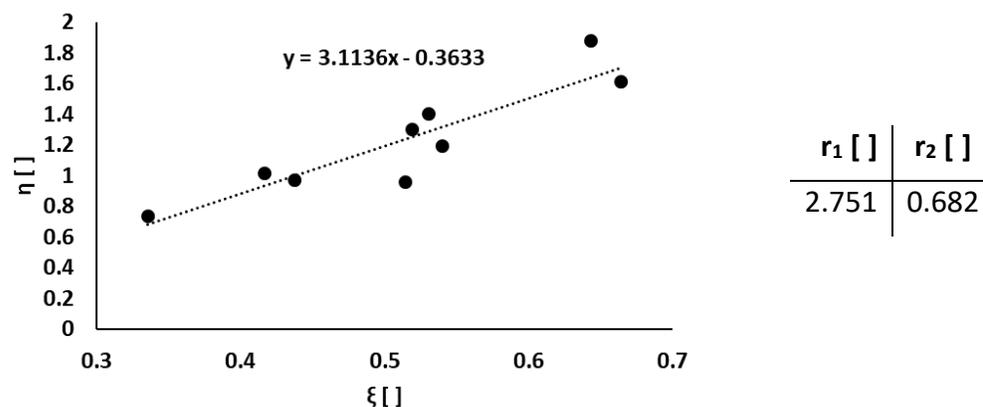


Fig. S7. Kelen-Tüdös plot for PDMS and PEGOH macromonomers during ATRP at 45°C. Reactivity ratios determined using the Kelen-Tüdös method¹⁰ reveal gradient distribution of PDMSMA (r_1) and PEGMA (r_2) into a brush backbone. From this CRP method, we expect gradient distribution for RAFT used in this study as well due to differences in size and chemistry.

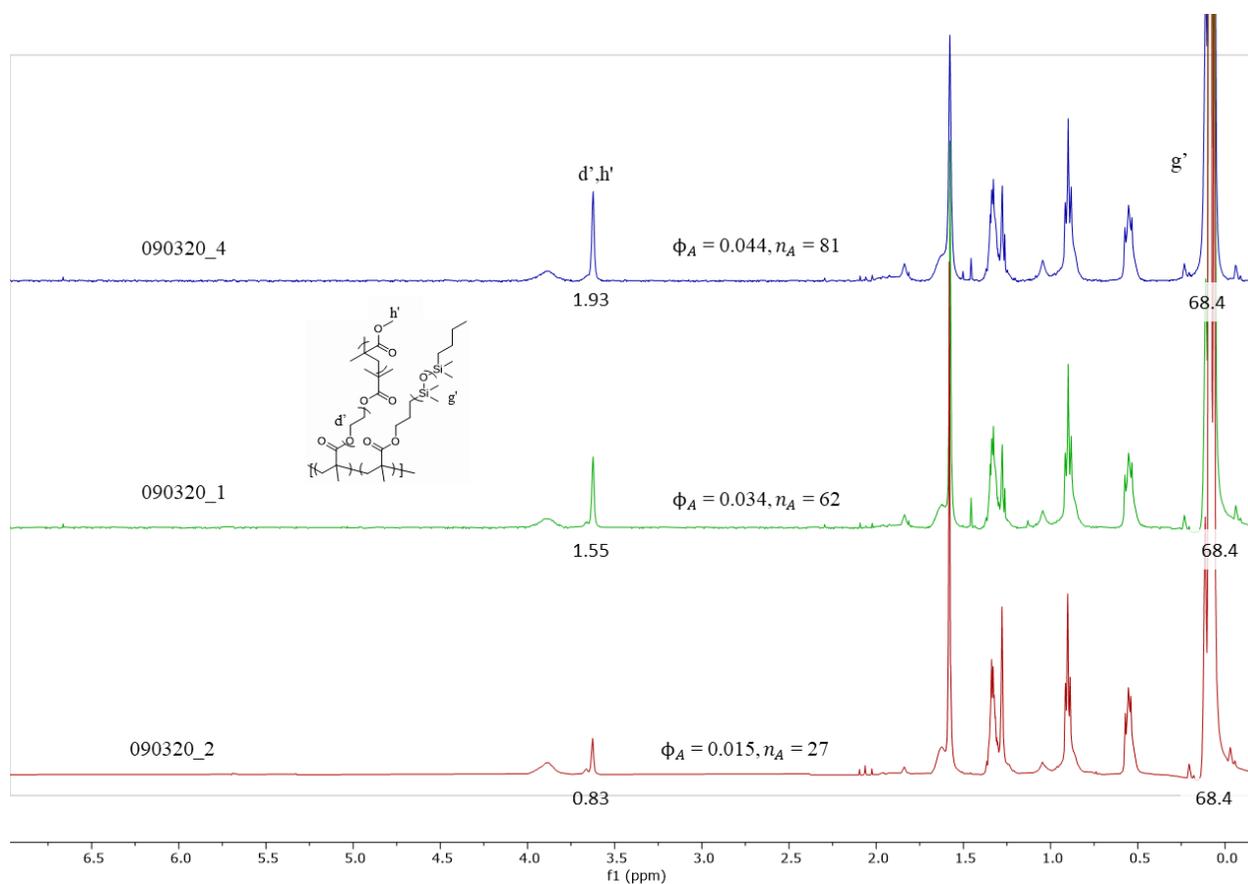


Fig. S8. $^1\text{H-NMR}$ of purified poly[MMA-*g*-(PDMS/PMMA)] brush copolymer series $n_{bb}=1935$, $n_g=1$ synthesized by CRP (400 MHz, CDCl_3): 3.89 ((C=O)-O-CH₂-, PDMS brush, m, 2H), 3.62 ((C=O)-O-CH₃- and -O-CH₂-CH₂-, PMMA and PEG respectively, m, 7H), 0.09 (-Si(CH₃)₂-O)_n, PDMS macromonomer and brush mixture, s, 68.4H).

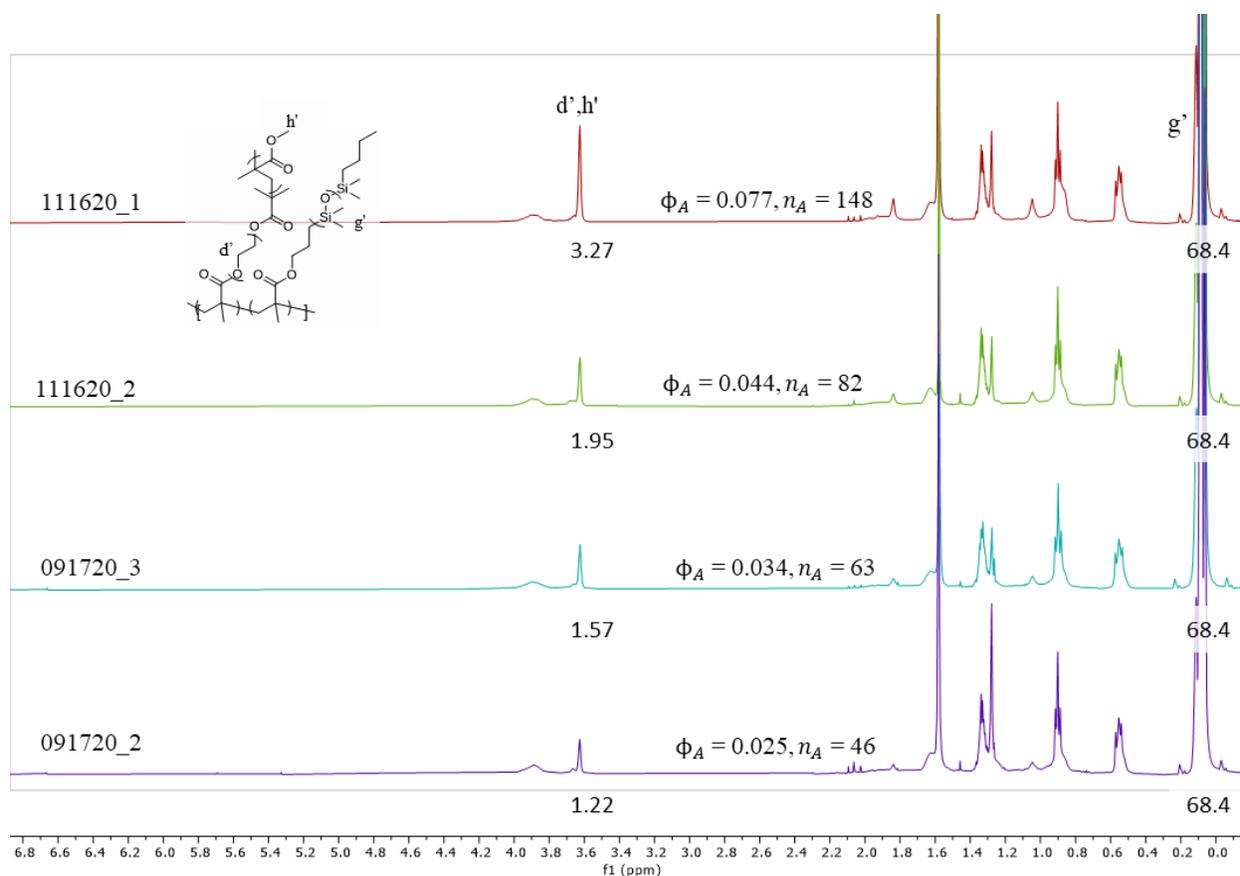


Fig. S9. $^1\text{H-NMR}$ of purified poly[MMA-*g*-(PDMS/PMMA)] brush copolymer series $n_{bb}=607$, $n_g=1$ synthesized by CRP (400 MHz, CDCl_3): 3.89 ((C=O)-O-CH₂-, PDMS brush, m, 2H), 3.62 ((C=O)-O-CH₃- and -O-CH₂-CH₂-, PMMA and PEG respectively, m, 7H), 0.09 (-Si(CH₃)₂-O)_n-, PDMS macromonomer and brush mixture, s, 68.4H).

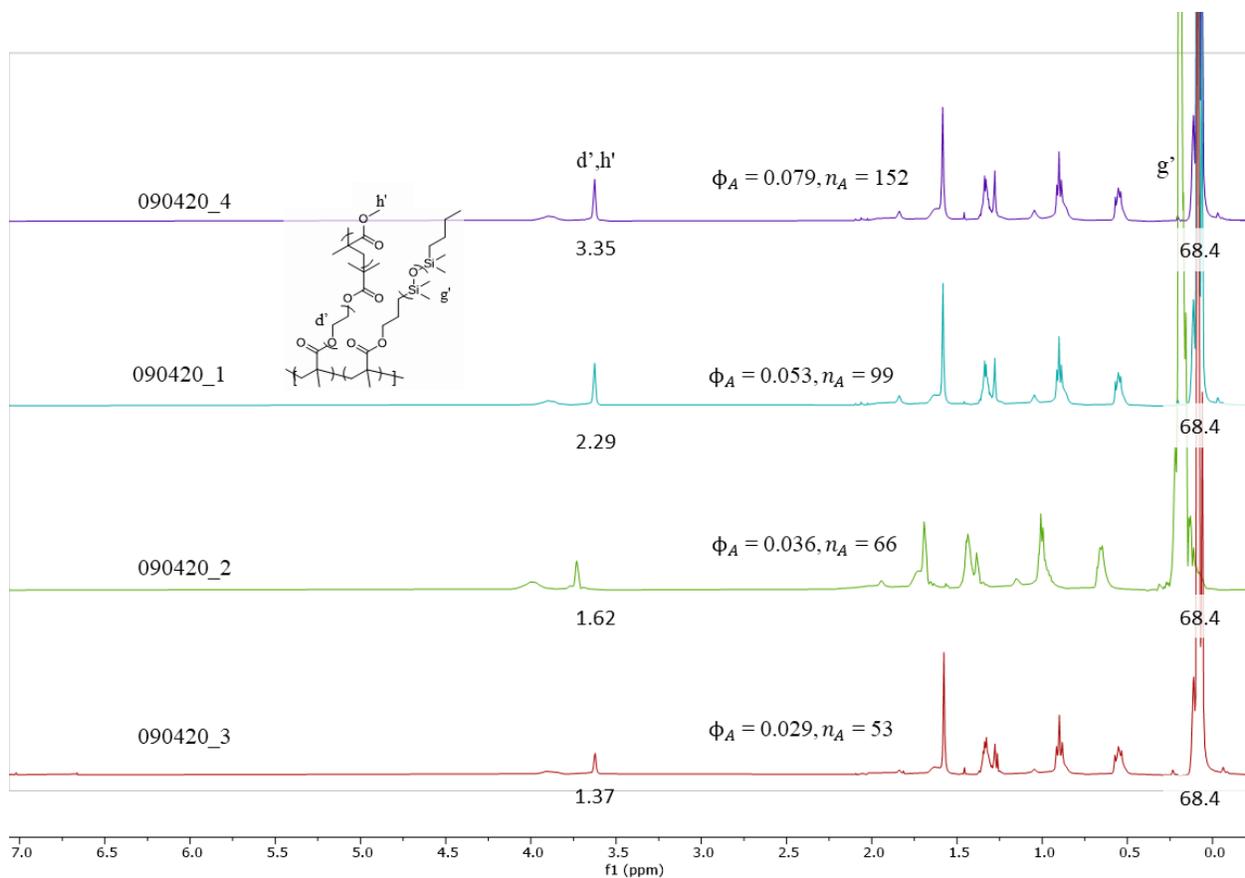


Fig. S10. $^1\text{H-NMR}$ of purified poly[MMA-*g*-(PDMS/PMMA)] brush copolymer series $n_{bb}=210$, $n_g=1$ synthesized by CRP (400 MHz, CDCl_3): 3.89 ((C=O)-O-CH₂-, PDMS brush, m, 2H), 3.62 ((C=O)-O-CH₃- and -O-CH₂-CH₂-, PMMA and PEG respectively, m, 7H), 0.09 (-(Si(CH₃)₂-O)_n-, PDMS macromonomer and brush mixture, s, 68.4H).

Ex. calculation for densely grafted A-*g*-B networks. Sample 090320_4:

$$n_A = n_x \left(\frac{d',h' - d'}{3H} \right) = 149 \left(\frac{1.93 - 0.295}{3} \right) = 45$$

$$\phi_A = \frac{n_A \left(\frac{M_{PMMA}}{\rho_{PEG,PMMA}} \right)}{n_A \left(\frac{M_{PMMA}}{\rho_{PMMA}} \right) + (n_x - 1) \left(\frac{M_{PDMS}}{\rho_{PDMS}} \right)} = \frac{45 \left(\frac{100g}{1.15 \frac{g}{mL}} \right)}{45 \left(\frac{100g}{1.15 \frac{g}{mL}} \right) + (149 - 1) \left(\frac{1000g}{0.96 \frac{g}{mL}} \right)} = 0.043$$

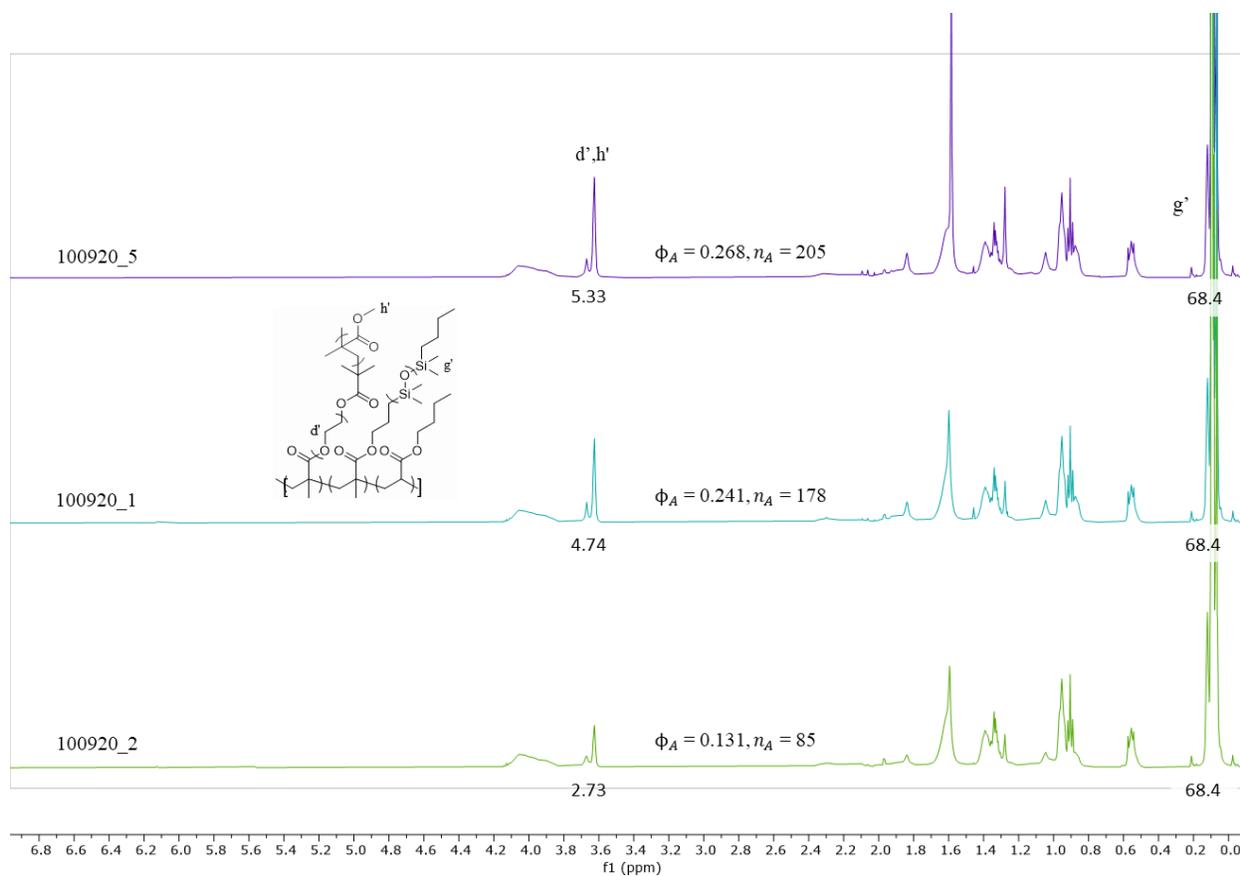


Fig. S11. $^1\text{H-NMR}$ of purified poly[nBA-ran-MMA-g-(PDMS/PMMA)] brush copolymer series $n_{bb}=1923, n_g=4$ synthesized by CRP (400 MHz, CDCl_3): 3.89 ((C=O)-O-CH₂-, PDMS brush, m, 2H), 3.62 ((C=O)-O-CH₃- and -O-CH₂-CH₂-, PMMA and PEG respectively, m, 7H), 0.09 (-Si(CH₃)₂-O)_n-, PDMS macromonomer and brush mixture, s, 68.4H).

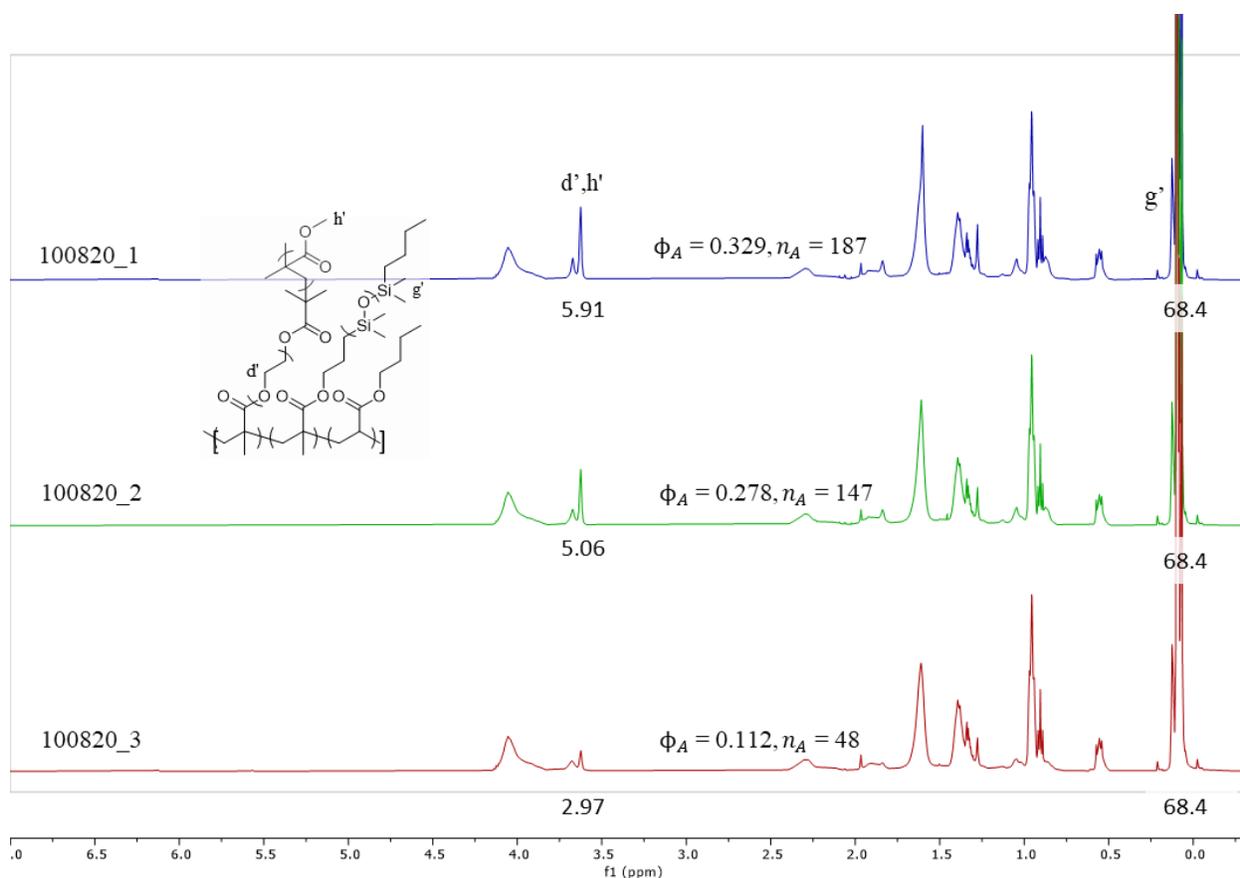


Fig. S12. $^1\text{H-NMR}$ of purified poly[nBA-*ran*-MMA-*g*-(PDMS/PMMA)] brush copolymer series $n_{bb}=1959$, $n_g=8$ synthesized by CRP (400 MHz, CDCl_3): 3.89 ((C=O)-O- CH_2 -, PDMS brush, m, 2H), 3.62 ((C=O)-O- CH_3 - and -O- CH_2 - CH_2 -, PMMA and PEG respectively, m, 7H), 0.09 (- $(\text{Si}(\text{CH}_3)_2\text{-O})_n$ -, PDMS macromonomer and brush mixture, s, 68.4H).

Ex. calculation for comb-like grafted A-*g*-B networks. Sample 100920_5:

$$n_A = n_x \left(\frac{d'H' - d'}{3H} \right) = 139 \left(\frac{5.33 - 0.905}{3} \right) = 205$$

$$\phi_A = \frac{n_A \left(\frac{M_{\text{PMMA}}}{\rho_{\text{PMMA}}} \right)}{n_A \left(\frac{M_{\text{PMMA}}}{\rho_{\text{PMMA}}} \right) + \left(\frac{n_x}{n_g} \right) \left(\frac{M_{\text{PDMS}}}{\rho_{\text{PDMS}}} \right) + \left(n_x - \frac{n_x}{n_g} \right) \left(\frac{M_{\text{PBA}}}{\rho_{\text{PBA}}} \right)} = \frac{105 \left(\frac{100g}{1.15 \frac{g}{\text{mL}}} \right)}{105 \left(\frac{100g}{1.15 \frac{g}{\text{mL}}} \right) + \left(\frac{139}{4} \right) \left(\frac{1000g}{0.96 \frac{g}{\text{mL}}} \right) + \left(139 - \frac{139}{4} \right) \left(\frac{128g}{1.08 \frac{g}{\text{mL}}} \right)} = 0.268$$

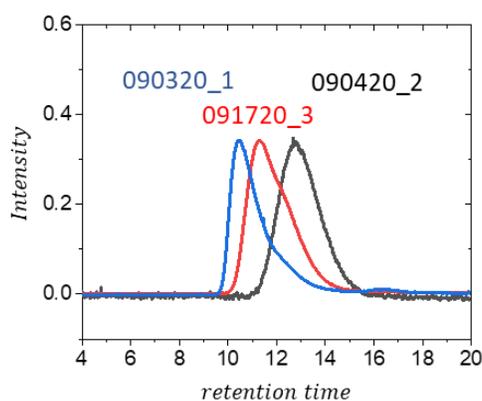


Fig. S13. Different n_{bb} verification by gel permeation chromatography for poly[MMA-*g*-(PDMS/PMMA)].

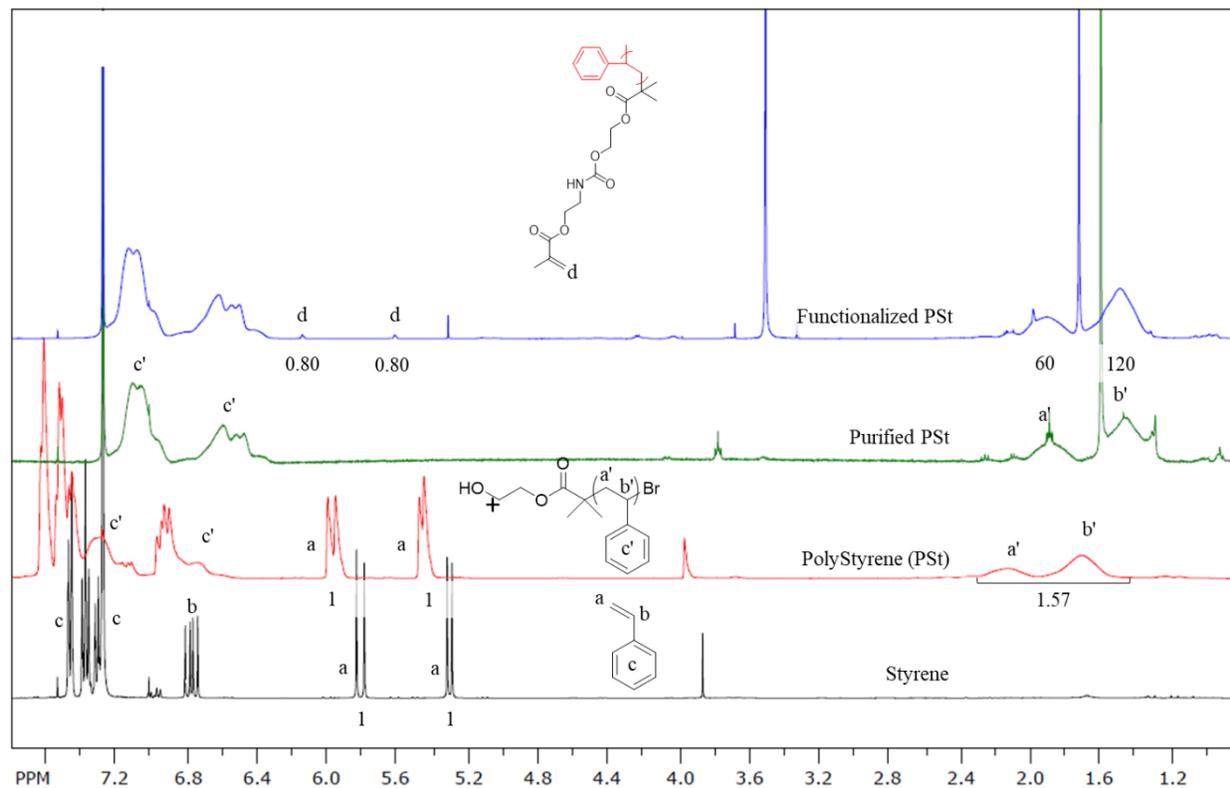


Fig. S14. $^1\text{H-NMR}$ of functionalized polystyrene (PS) macromonomers used in FR polymerization at different stages (400 MHz, CDCl_3): 7.66-6.31 (C_6H_6 -, residual styrene and PS, m, 6H), 6.15, 5.61 ($\text{CH}_2=\text{C}(\text{CH}_3)\text{-C-}$, functionalized PS, s, 1H), 5.70, 5.46 ($\text{CH}_2=\text{CH-}$, residual styrene, s, 1H), 2.16-1.27 ($-\text{CH}_2\text{-CH-}$, PS, m, 3H). 3.50, 1.71 (residual methanol), 1.58 (residual water). $n_A = [\text{styrene}]/[\text{I}] \cdot (a'+b')/3 / [a/1 + a'+b')/3] = 175 \cdot 1.57/3 / [1+1.57/3] = 175 \cdot 0.34 = 60.1$.

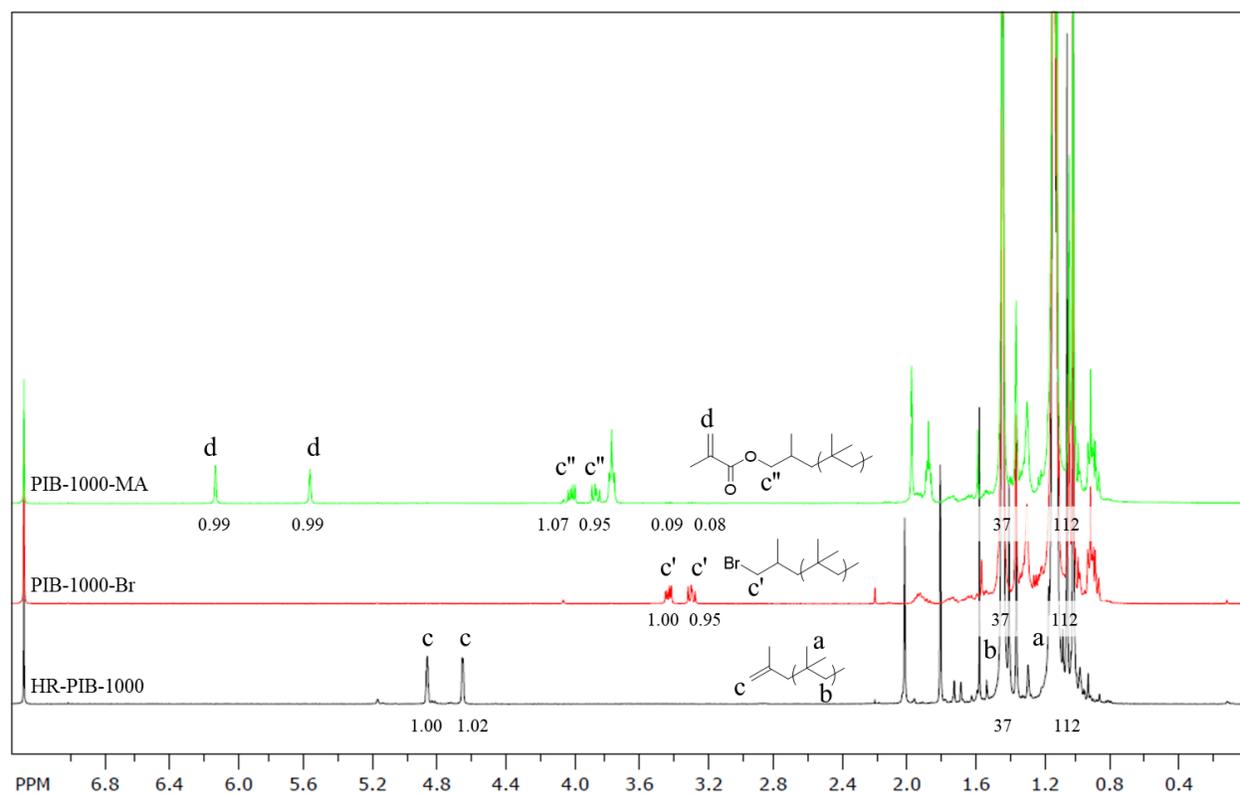


Fig. S15. $^1\text{H-NMR}$ of PIB macromonomer synthesis (400 MHz, CDCl_3): 6.14, 5.58 ($\text{CH}_2\text{-C}(\text{CH}_3)\text{-C-}$, PIB-1000-MA (PIB macromonomer), s, 1H), 4.89, 4.67 ($\text{CH}_2\text{=C}(\text{CH}_3)\text{-}$, HR-PIB-1000, s, 1H), 4.00, 3.87 ($\text{-C}(\text{=O})\text{-O-CH}_2\text{-}$, PIB-1000-MA, s, 1H), 3.43, 3.29 ($\text{Br-CH}_2\text{-C}(\text{CH}_3)\text{-}$, PIB-1000-Br, s, 1H), 1.47 ($\text{CH}_2\text{-C}(\text{CH}_3)_2\text{-}$, PIB polymer, m, 37H), 1.16 ($\text{-CH}_2\text{-C}(\text{CH}_3)_2\text{-}$, PIB polymer, m, 112H).

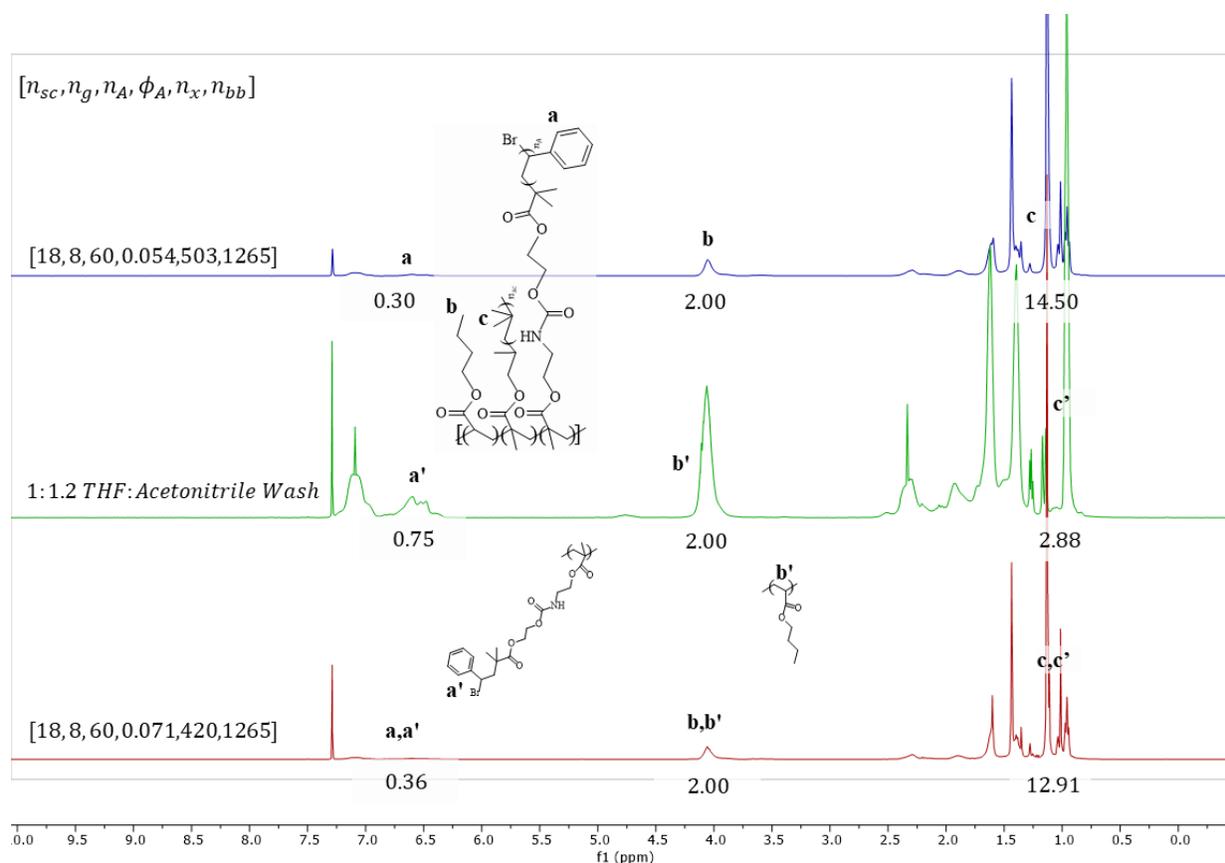


Fig. S16. Example wash of poly[nBA-ran-MMA-g-(PIB/PS)]. From bottom to top: unwashed network, wash supernatant, pure network. Bottom: (400 MHz, CDCl_3): 6.56 (CH-CH=CH-C-, PS side-chain and unreacted PS oligomer, d, 120H), 4.10 ((C=O)-O-CH₂-, PBA spacer and unreacted homopolymer, t, 2H), 1.15 (CH₂-C-(CH₃)₂-, PIB side chain and unreacted homopolymer, s, 112H). Middle: (400 MHz, CDCl_3): 6.56 (CH-CH=CH-C-, unreacted PS oligomer, d, 120H), 4.10 ((C=O)-O-CH₂-, unreacted PBA homopolymer, t, 2H), 1.15 (CH₂-C-(CH₃)₂-, unreacted PIB homopolymer, s, 112H). Top: (400 MHz, CDCl_3): 6.56 (CH-CH=CH-C-, PS side-chain, d, 120H), 4.10 ((C=O)-O-CH₂-, PBA spacer, t, 2H), 1.15 (CH₂-C-(CH₃)₂-, PIB side chain, s, 112H).

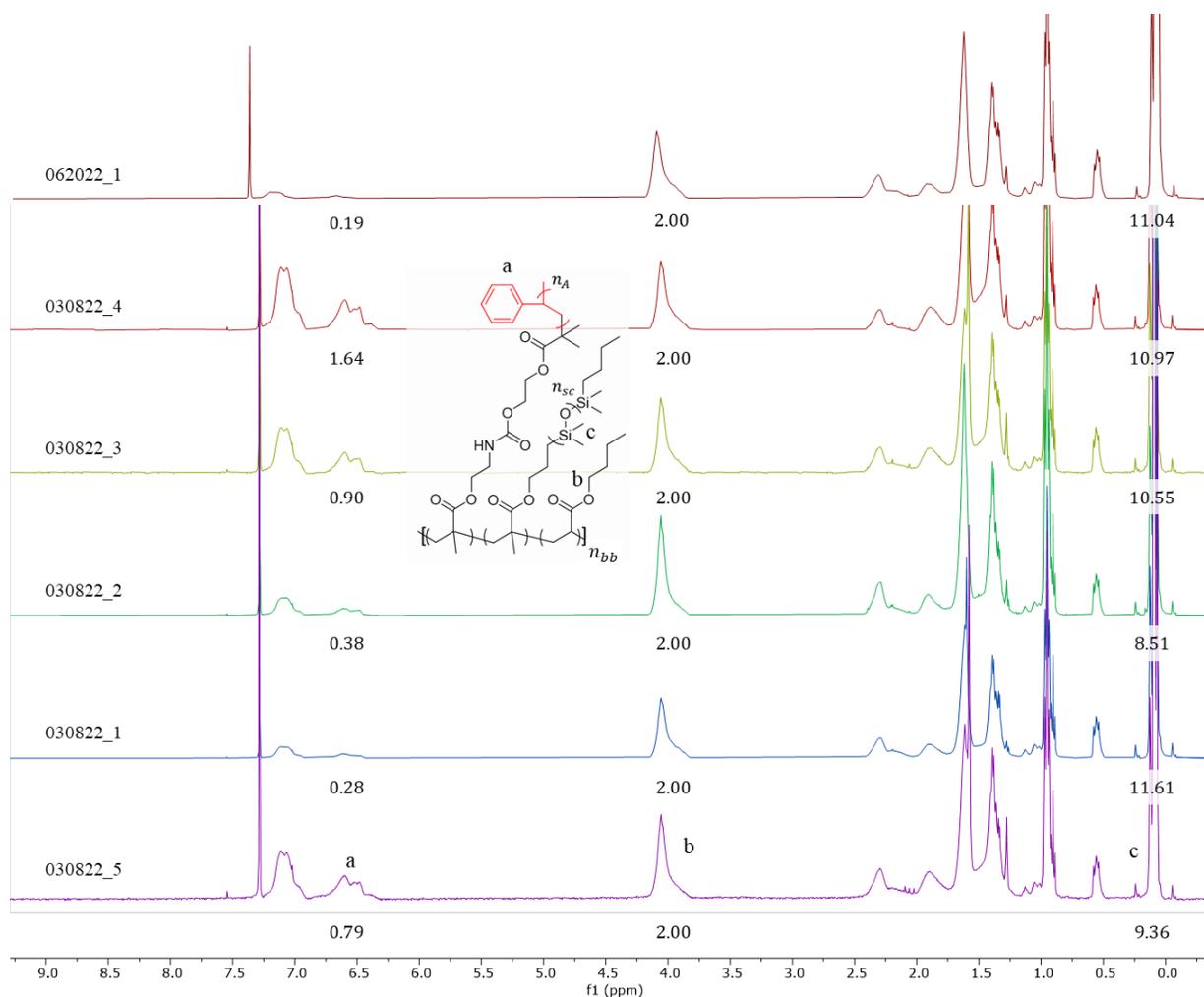


Fig. S17. $^1\text{H-NMR}$ of purified poly[nBA-ran-MMA-g-(PDMS/PS)]. (400 MHz, CDCl_3): 6.56 (CH-CH=CH-C-, PS side-chain, d, 120H), 4.07 ((C=O)-O-CH₂-, PBA spacer, d, 2H), 0.09 (- (Si(CH₃)₂-O)_n-, PDMS macromonomer and brush mixture, s, 68.4H).

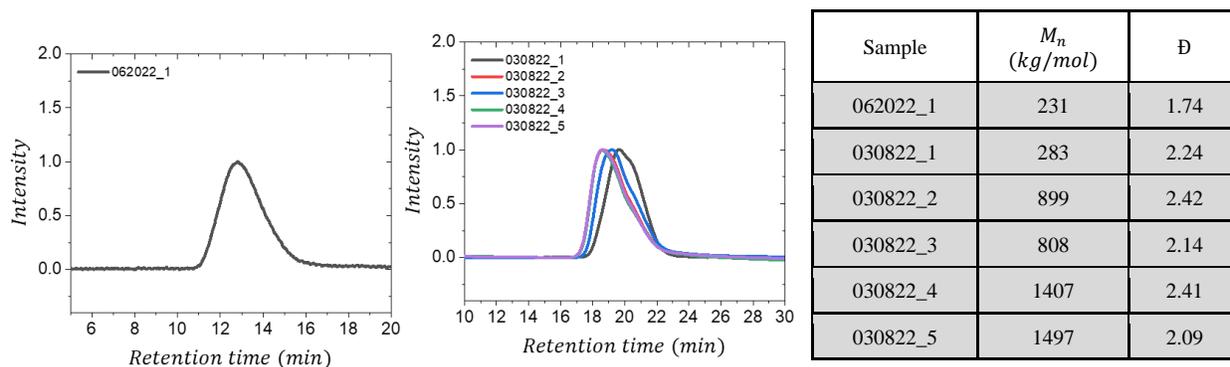


Fig. S18. GPC of poly[nBA-ran-MMA-g-(PDMS/PS)]. 1mg/mL, HALS. Note: sample 062022_1 was run on a 30-minute run cycle while the others were run on a 60-minute run cycle.

Ex. calculation:

$$n_x = \frac{2H * n_A}{a} + [(\frac{2H * n_A}{a}) / (\frac{112H}{c})] + 1 = \frac{2 * 60}{0.90} + [(\frac{2 * 60}{0.90}) / (\frac{68.4}{10.55})] + 1 = 155$$

$$z = \frac{M_n}{M_{n_{PBA}}(\frac{2H * n_A}{a}) + M_{n_{PDMS}}[(\frac{2H * n_A}{a}) / (\frac{68.4H}{c})] + M_{n_{PS}}(1)} = \frac{808000 \text{ g/mol}}{128(\frac{2 * 60}{0.90}) + 1000[(\frac{2 * 60}{0.90}) / (\frac{68.4}{10.55})] + 6240(1)} = 18.4$$

$$n_{bb} = n_x * z = 155 * 18.4 = 2854$$

$$\phi_A = \frac{\frac{M_{n,PS}}{\rho_{PS}}}{\frac{M_{PBA}}{\rho_{PBA}}(\frac{2H * n_A}{a}) + \frac{M_{n,PDMS}}{\rho_{PDMS}}[(\frac{2H * n_A}{a}) / (\frac{68.4H}{c})] + \frac{M_{n,PS}}{\rho_{PS}}} = \frac{(\frac{6240g}{1.02 \frac{g}{mL}})}{(\frac{128g}{1.08 \frac{g}{mL}})(\frac{2 * 60}{0.90}) + (\frac{1000g}{0.96 \frac{g}{mL}})[(\frac{2 * 60}{0.90}) / (\frac{68.4}{10.55})] + (\frac{6240g}{1.02 \frac{g}{mL}})} = 0.151$$

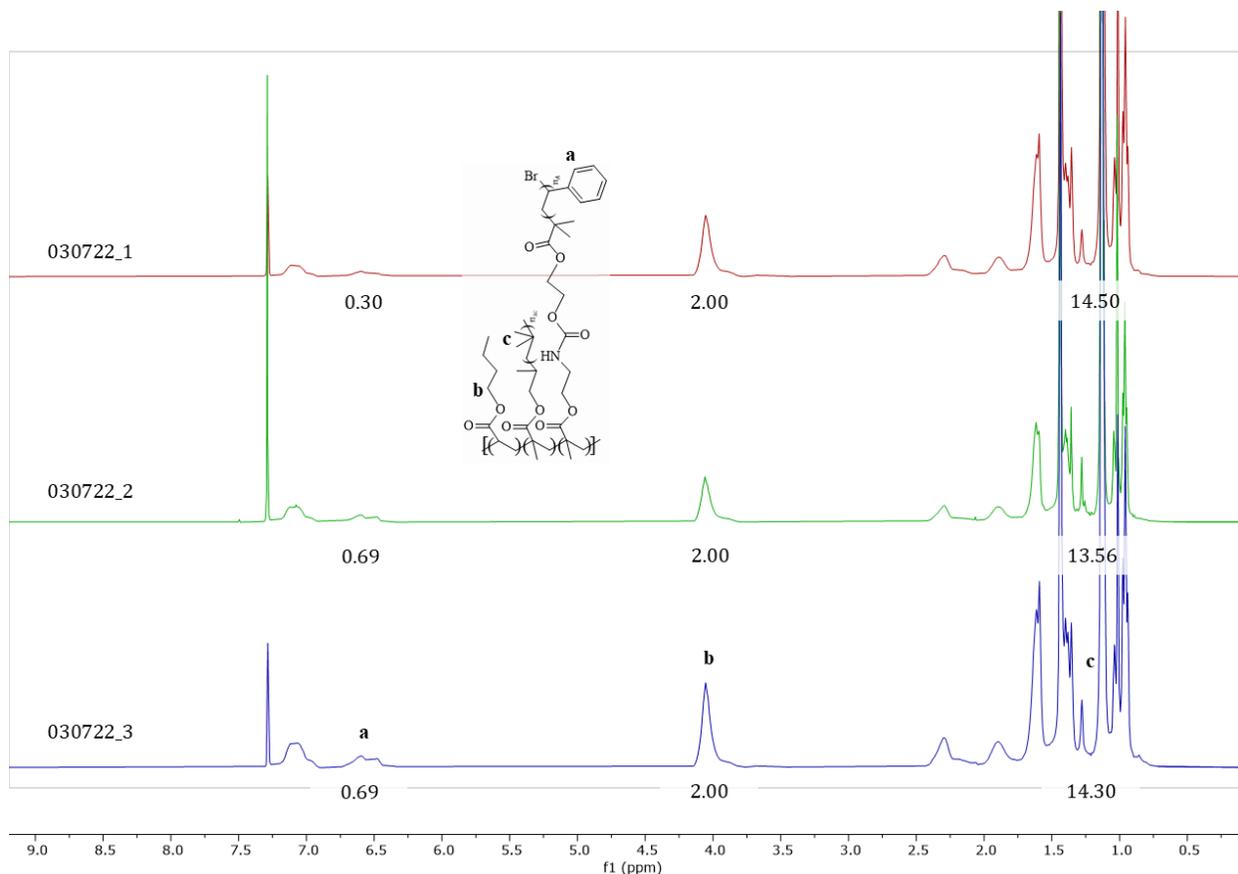
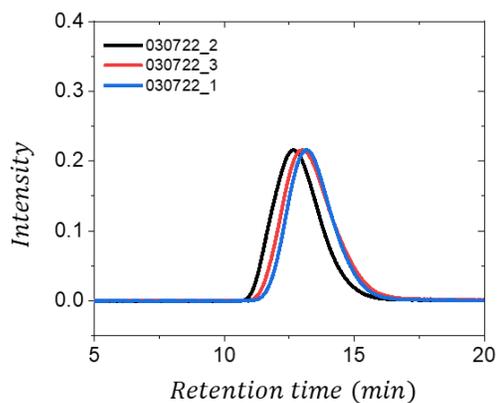


Fig. S19. $^1\text{H-NMR}$ of purified poly[nBA-ran-MMA-g-(PIB/PS)]. [. (400 MHz, CDCl_3): 6.56 (CH=CH-C-, PS side chain, d, 120H), 4.10 ((C=O)-O-CH₂-, PBA spacer, t, 2H), 1.15 (CH₂-C-(CH₃)₂-, PIB side chain, s, 112H).



Sample	M_n (kg/mol)	\bar{D}
030722_1	204	1.70
030722_2	327	1.78
030722_3	218	1.98

Fig. S20. GPC of poly[nBA-ran-MMA-g-(PIB/PS)]. 1mg/mL, HALS. Note: the samples were run on a 30-minute run cycle.

Ex. calculation:

$$n_x = \frac{2H * n_A}{a} + \left[\left(\frac{2H * n_A}{a} \right) / \left(\frac{112H}{c} \right) \right] + 1 = \frac{2 * 60}{0.69} + \left[\left(\frac{2 * 60}{0.69} \right) / \left(\frac{112}{13.56} \right) \right] + 1 = 216$$

$$z = \frac{M_n}{M_{n,PBA} \left(\frac{2H * n_A}{a} \right) + M_{n,PIB} \left[\left(\frac{2H * n_A}{a} \right) / \left(\frac{112H}{c} \right) \right] + M_{n,PS}(1)} = \frac{204000}{128 \left(\frac{2 * 60}{0.69} \right) + 1000 \left[\left(\frac{2 * 60}{0.69} \right) / \left(\frac{112}{13.56} \right) \right] + 6240(1)} = 6.60$$

$$n_{bb} = n_x * z = 216 * 6.60 = 1425$$

$$\phi_A = \frac{\left(\frac{M_{n,PS}}{V_{PS}} \right)}{\frac{M_{PBA}}{\rho_{PBA}} \left(\frac{2H * n_A}{a} \right) + \frac{M_{n,PIB}}{\rho_{PIB}} \left[\left(\frac{2H * n_A}{a} \right) / \left(\frac{112H}{c} \right) \right] + \frac{M_{n,PS}}{\rho_{PS}}} = \frac{\left(\frac{6240g}{1.02 \frac{g}{mL}} \right)}{\left(\frac{128g}{1.08 \frac{g}{mL}} \right) \left(\frac{2 * 60}{0.69} \right) + \left(\frac{1000g}{0.96 \frac{g}{mL}} \right) \left[\left(\frac{2 * 60}{0.69} \right) / \left(\frac{112}{13.56} \right) \right] + \left(\frac{6240g}{1.02 \frac{g}{mL}} \right)} = 0.108$$

S3. SAXS analysis

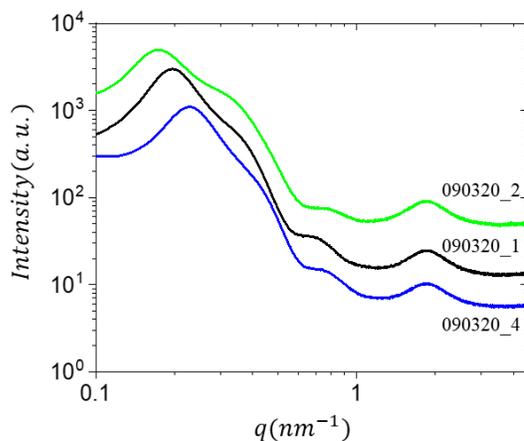


Fig. S21. SAXS curves of poly[MMA-g-(PDMS/PMMA)] samples with variable ϕ_A . Analysis reported in main text Table 1.

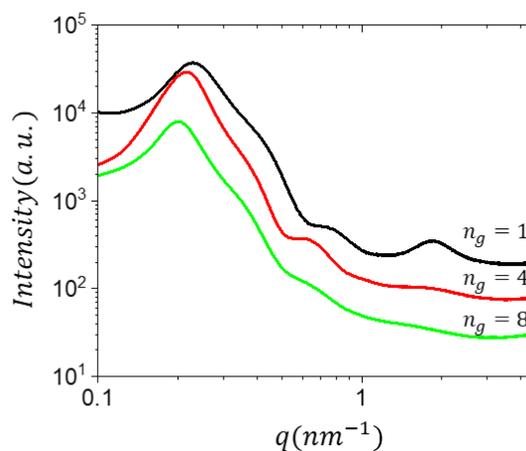


Fig. S22. SAXS curves of poly[nBA-ran-MMA-g-(PDMS/PMMA)] samples with variable n_g and ϕ_A (cf. Table 1).

S4. Atomic force microscopy.



Fig. S23. LB-monolayer of poly[MMA-g-(PDMS/PMMA)], sample 090320_4.

S5. Mechanical Properties

Table S1. Structural and mechanical parameters of soft biological tissue.

Sample	E^6 (MPa)	β^6	E_0^7 (kPa)	σ_{max}^9 (MPa)	Reference
Human abdominal skin	1.20	0.93	164	13	11
Porcine brain tissue	1.00	0.72	8.90	2.4	12
Artery adventitia A	0.35	0.91	28.8	2.5	13
Pig belly	5.46	0.45	13.8	1.2	14
Porcine aorta	19.8	0.67	128	2.0	15,16
Bovine nuchal ligament	0.15	0.93	20.0	5.0	1,16*
Vena cava	3.40	0.75	37.4	4.5	1,17*
Carotid artery	0.35	0.91	28.8	2.8	1,17*
Skeletal muscle tissue	2.02	0.54	7.00	2.8	1,18*
Human aorta: superior	21.0	0.72	185	6.7	19
Human aorta: high	105	0.55	380	4.6	19
Human aorta: Sinotubular junction	50.1	0.45	381	7.1	20
Ligament	Frequency Sweep from Fig. 4d				21

Bovine Paracardium	Frequency Sweep from Fig. 4d	22
Porcine Brain	Frequency Sweep from Fig. 4d	23

* E , β , and E_0 values correspond to class of tissue from ref. 1.

Table S2. Architectural parameters and mechanical properties of A-g-B brush copolymers.

Sample	$n_g^{1)}$	n_{sc}	$n_x^{2)}$	$n_A^{3)}$	$\phi_A^{4)}$	$n_{bb}^{5)}$	$E^{6)}$ (kPa)	$\beta^{6)}$	$E_0^{7)}$ (kPa)	$\lambda_{fit}^{8)}$	$\lambda_{max}^{9)}$	$\sigma_{max}^{10)}$ (kPa)
poly[MMA-g-(PDMS/PMMA)]												
090320_2	1	14	149	27	0.015	1935	5.65	0.31	9.8	2.10	2.81	104
090320_1	1	14	149	62	0.034	1935	14.4	0.40	31.4	1.90	2.92	605
090320_4	1	14	149	81	0.044	1935	20.5	0.46	53.1	1.70	2.98	898
091720_2	1	14	149	46	0.025	607	12.2	0.26	18.9	1.57	2.34	51.2
091720_3	1	14	149	63	0.034	607	10.5	0.45	26.6	1.65	2.07	94.3
111620_2	1	14	149	82	0.044	607	14.2	0.52	45.8	1.44	1.87	122
111620_1	1	14	149	148	0.077	607	15.1	0.52	48.6	1.64	1.84	144
090420_3	1	14	149	53	0.029	210	7.30	0.42	16.9	1.80	2.04	-
090420_2	1	14	149	66	0.036	210	4.38	0.51	13.6	1.45	1.52	10.6
090420_1	1	14	149	99	0.053	210	11.7	0.54	40.7	1.28	1.69	36.8
090420_4	1	14	149	152	0.079	210	13.6	0.57	53.5	1.54	1.63	84.4
poly[nBA-ran-MMA-g-(PDMS/PMMA)]												
100920_2	4	14	139	85	0.131	1923	36.3	0.18	47.9	2.50	3.40	606
100920_1	4	14	139	178	0.241	1923	61.6	0.29	103	2.20	2.83	1223
100920_5	4	14	139	205	0.268	1923	77.3	0.33	142	1.96	2.96	2572
100820_3	8	14	142	48	0.112	1959	15.8	0.09	18.0	3.32	4.95	558
100820_2	8	14	142	147	0.278	1959	50.4	0.13	60.9	3.25	5.21	2653
100820_1	8	14	142	187	0.329	1959	68.6	0.15	86.1	3.00	4.62	2674
poly[nBA-ran-MMA-g-(PDMS/PS)]												
062022_1*	8	14	844	60	0.03	1021	11.4	0.08	18.5	2.91	3.46	81.0
030822_1**	8	14	502	60	0.05	1061	47.4	0.18	78.1	2.37	2.78	256
030822_2	8	14	315	60	0.08	2807	77.1	0.22	110	2.13	2.71	610
030822_3	8	14	155	60	0.15	2854	209	0.44	528	1.64	2.23	2588
030822_4	8	14	86	60	0.24	4425	210	0.72	1853	1.24	2.09	5430

030822_5	10	14	178	60	0.15	5573	286	0.50	858	1.52	2.57	6000
poly[nBA- <i>ran</i> -MMA- <i>g</i> -(PIB/PS)]												
030722_1	8	18	503	60	0.048	940	46.8	0.16	59.9	2.49	3.85	740
030722_2	8	18	216	60	0.108	1425	170	0.20	232	2.32	4.67	3520
030722_3	8	18	218	60	0.106	938	133	0.23	193	2.35	3.46	2040

⁽¹⁾ Grafting density of side chains on the backbone with BA spacer. ⁽²⁾ Number average degree of polymerization of brush backbone between glassy block side chains that physically crosslink. ⁽³⁾ Number average degree of polymerization of each glassy block side chain as determined by ¹H-NMR. ⁽⁴⁾ Volume fraction glassy block, $\rho_{PMMA} = 1.15 \text{ g/mL}$, $\rho_{PIB} = 0.92 \text{ g/mL}$, $\rho_{PS} = 1.02 \text{ g/mL}$, $\rho_{PDMS} = 0.96 \text{ g/mL}$, $\rho_{PEG} = 0.94 \text{ g/mL}$, $\rho_{PBA} = 1.08 \text{ g/mL}$. ⁽⁵⁾ Number average degree of polymerization of the total brush strand. ⁽⁶⁾ Structural modulus $E \sim 1/(n_{bb}(n_{sc} + 1))$ and strain-stiffening parameter $\beta = \langle R_{in}^2 \rangle / R_{max}^2$ are fitting parameters in equation S1. ⁽⁷⁾ Apparent Young's modulus which can be determined either as tangent of a stress-strain curve at $\lambda \rightarrow 1$ or from the fitting equation S2. ⁽⁸⁾ Elongation range used for fitting equation S1 before deviation from the theory. ⁽⁹⁾ Maximum true stress and elongation at sample rupture. ⁽¹⁰⁾ Maximum stress-at-break (strength) of A-*g*-B brush copolymer samples. * $G_e = 1.9 \text{ kPa}$. ** $G_e = 5.1 \text{ kPa}$.

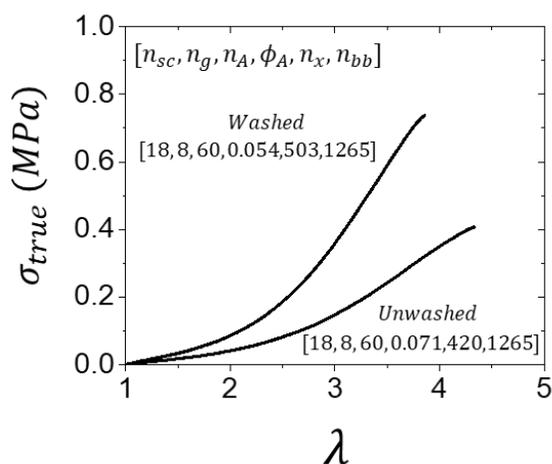


Fig. S24. Example Stress-elongation dependence on removing unreacted reagent, poly[nBA-*ran*-MMA-*g*-(PIB/PS)]. $\dot{\epsilon} = 0.001$, $T = 22^\circ\text{C}$.

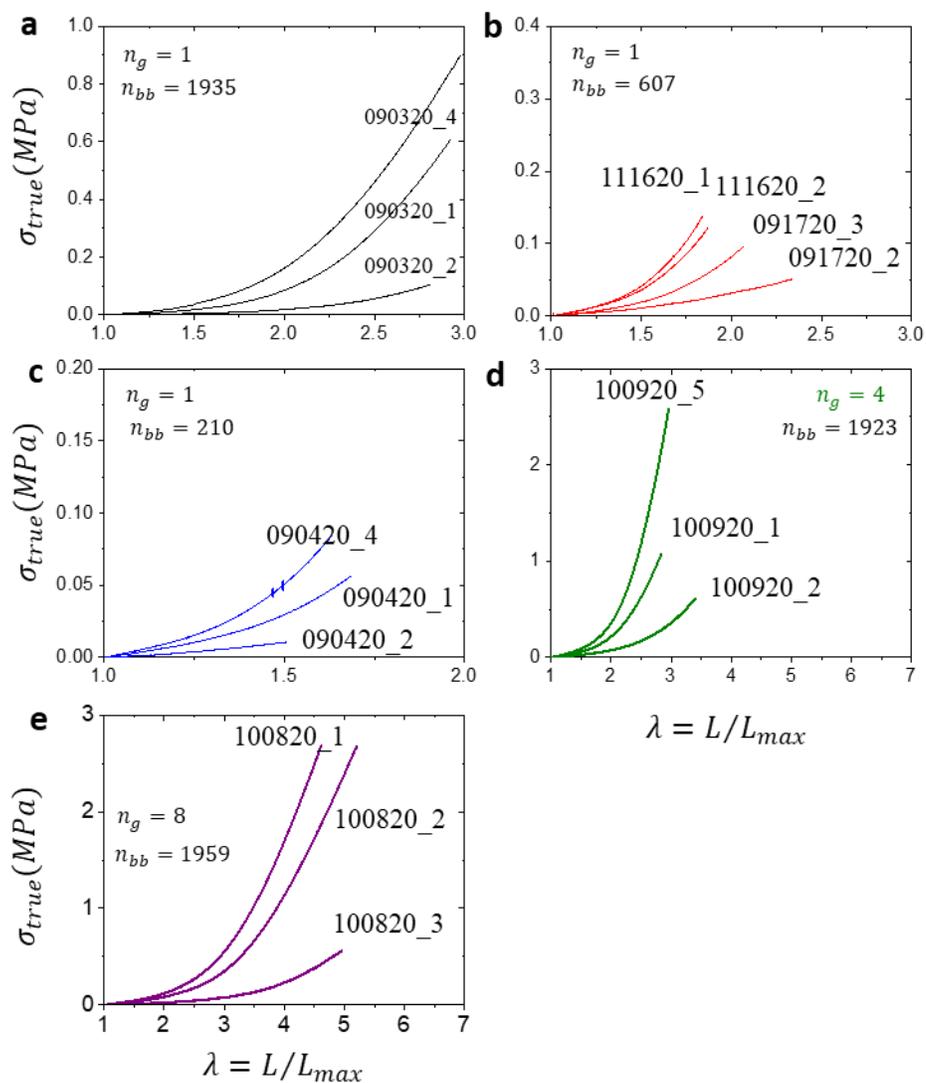


Fig. S25. True stress-elongation curve profiles of poly[MMA-*g*-(PDMS/PMMA)] and poly[nBA-*ran*-MMA-*g*-(PDMS/PMMA)] brush graft copolymers synthesized by CRP. a) Series $n_{bb} = 1935$, $n_g = 1$. b) Series $n_{bb} = 607$, $n_g = 1$. c) Series $n_{bb} = 210$, $n_g = 1$. d) Series $n_{bb} = 1923$, $n_g = 4$. e) Series $n_{bb} = 1959$, $n_g = 8$. $\dot{\epsilon} = 0.005$, $T = 22^\circ\text{C}$.

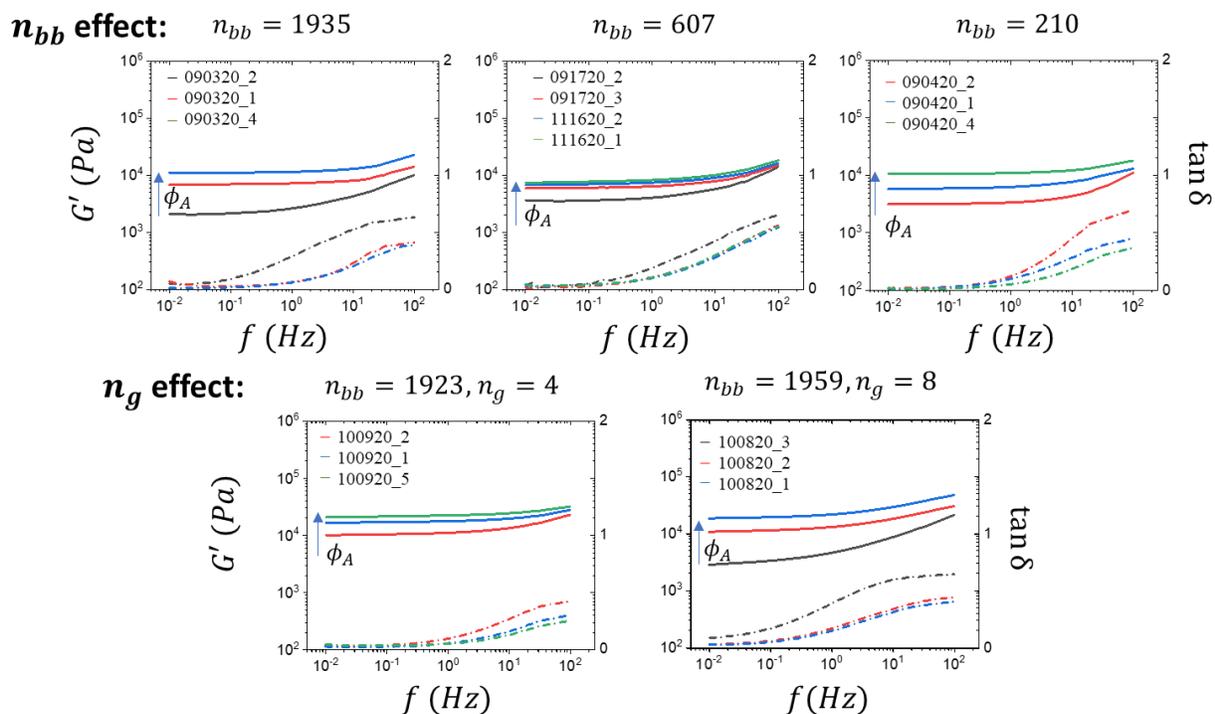


Fig. S26. Oscillatory frequency sweeps of poly[MMA-*g*-(PDMS/PMMA)] and poly[nBA-*ran*-MMA-*g*-(PDMS/PMMA)] brush graft copolymers synthesized by CRP. $\varepsilon=0.05$, $T=22^\circ\text{C}$.

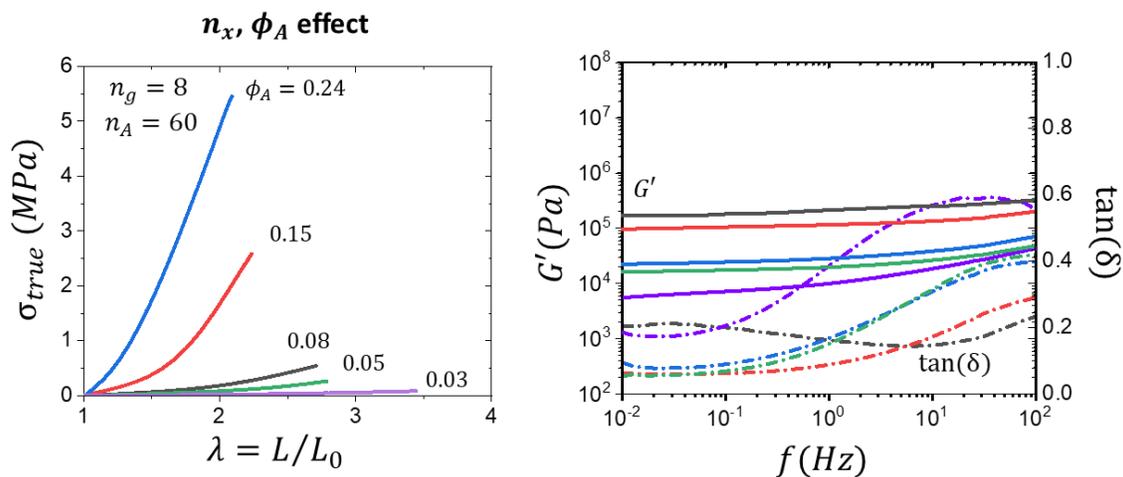


Fig. S27. Stress-elongation ($\dot{\varepsilon}=0.005$) and oscillatory frequency sweeps of poly[nBA-*ran*-MMA-*g*-(PDMS/PS)]. $\varepsilon=0.05$, $T=22^\circ\text{C}$.

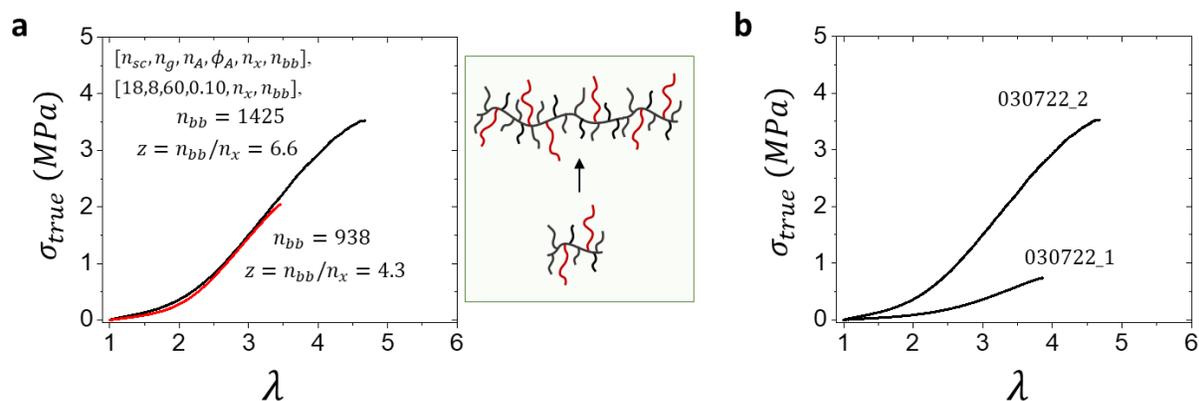


Fig. S28. Stress-elongation of poly[nBA-ran-MMA-g-(PIB/PS)]. a) n_{bb} effect on poly[nBA-ran-MMA-g-(PIB/PS)] through FR polymerization. Initiator concentration was varied to change n_{bb} . b) Changing ϕ_A and n_x control mechanical properties. $\dot{\epsilon} = 0.001$, $T = 22^\circ\text{C}$.

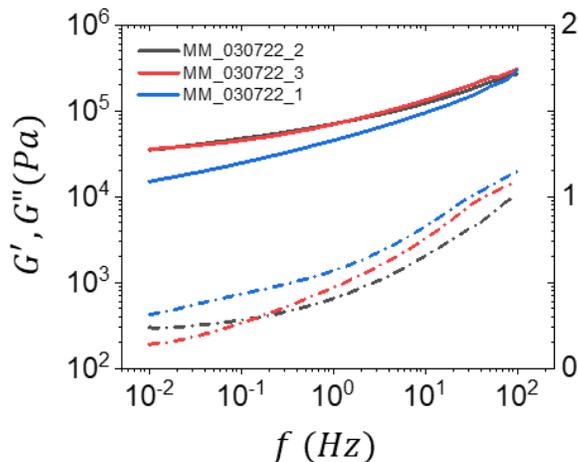


Fig. S29. Oscillatory frequency sweeps of poly[nBA-ran-MMA-g-(PIB/PS)]. $\epsilon = 0.05$, $T = 22^\circ\text{C}$.

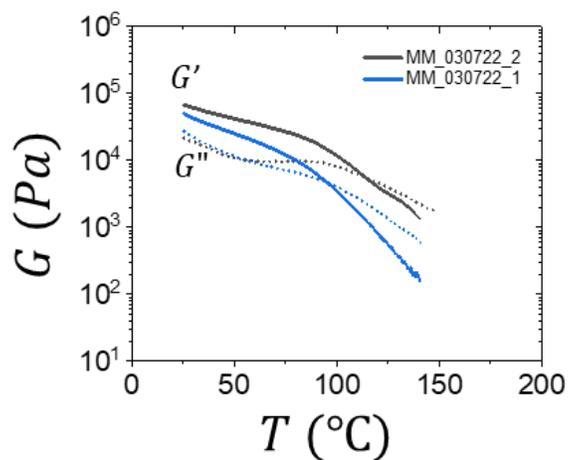


Fig. S30. Temperature evolution of poly[nBA-ran-MMA-g-(PIB/PS)]. $\epsilon = 0.05$, $f = 1$ Hz.

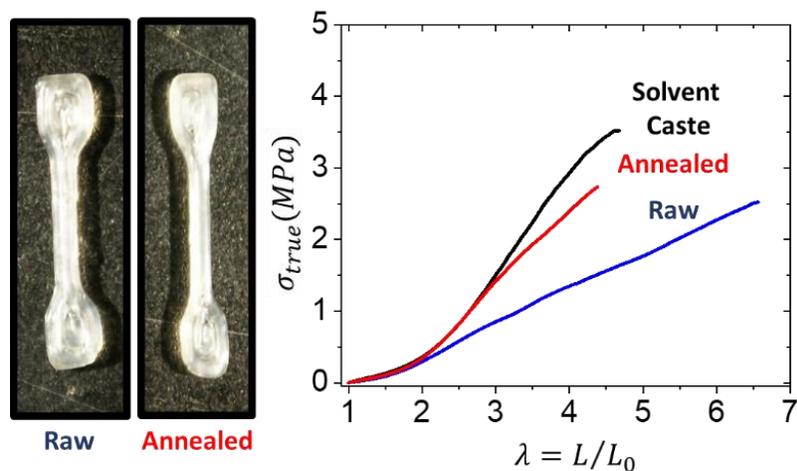


Fig. S31. 3D printed dog bones experience identical stress-elongation response after annealing to solvent caste preparation. Sample 030722_2. $\dot{\epsilon} = 0.001$, $T = 22^\circ\text{C}$.

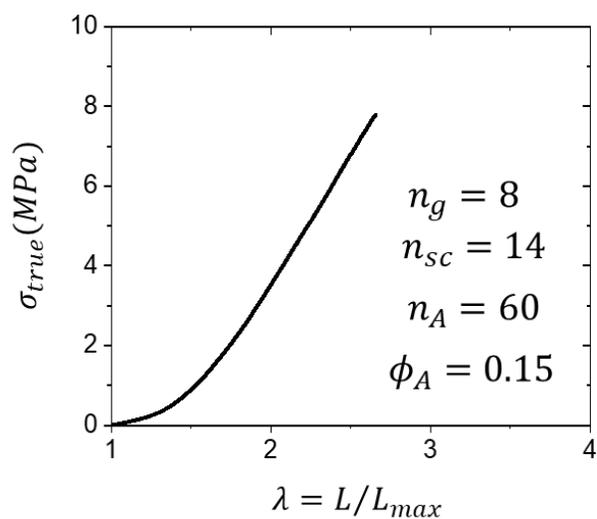


Fig. S32. PS-g-PDMS ($n_g=8$) series with additional covalent crosslinking. A-g-B polymers can be covalently crosslinked in addition to physical crosslinks. This was achieved by formulating PS-g-PDMS ($n_g=8$) and curing under nitrogen in a mold for an extended period of time ($>72\text{hr}$).

S6. Computer simulation of A-g-B graft copolymer networks

We have performed coarse-grained molecular dynamics simulations of self-assembled graft copolymers consisting of semiflexible thick backbone and grafted flexible side chains (Fig. S33). Each side chain with $n_A = 5$ monomers was separated by backbone block of $n_x = 20$ monomers. The copolymer chains were modelled as bead-spring chains with different bead sizes. This was done by implementing the modified, truncated, shifted Lennard-Jones (LJ) potential with an offset to the interaction range by Δ .

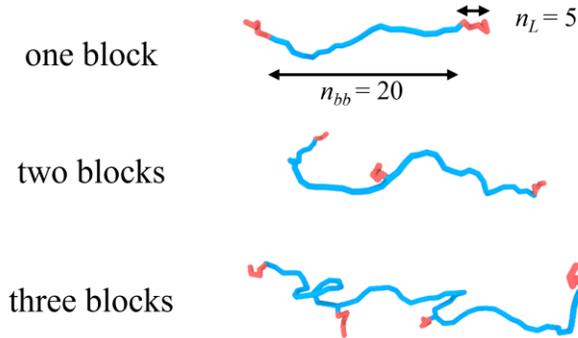


Fig. S33. Snapshots of block copolymers made by grafting flexible chains with n_A monomers (shown in red) to semiflexible backbone (shown in blue).

$$U_{LJ}(r) = \begin{cases} 4\varepsilon_{LJ} \left[\left(\frac{\sigma}{r-\Delta} \right)^{12} - \left(\frac{\sigma}{r-\Delta} \right)^6 - \left(\frac{\sigma}{r_{\text{cut}}} \right)^{12} + \left(\frac{\sigma}{r_{\text{cut}}} \right)^6 \right] & r \leq r_{\text{cut}} + \Delta \\ 0 & r > r_{\text{cut}} + \Delta \end{cases} \quad (\text{S4})$$

The connectivity of beads into chains was represented by the sum of the finite extensible nonlinear elastic (FENE) potential

$$U_{\text{FENE}}(r) = -0.5k_{\text{spring}}R_{\text{max}}^2 \ln(1 - (r - \Delta)^2/R_{\text{max}}^2) \quad (\text{S5})$$

with spring constant $k_{\text{spring}} = 30 k_B T / \sigma^2$ and the maximum bond length $R_{\text{max}} = 1.5\sigma$ and the pure repulsive modelled by the modified truncated-shifted LJ potential with $\varepsilon_{LJ} = 1.0k_B T$ and $r_{\text{cut}} = 2^{1/6}\sigma$ for backbone-backbone(B-B) pairs and linear-backbone (L-B) pair and $\varepsilon_{LJ} = 0.8k_B T$ and $r_{\text{cut}} = 2^{1/6}\sigma$ for linear-linear (L-L) pairs. In our simulation, the value of the parameter $\Delta = 0$ for the B-B pairs, $\Delta = -0.5\sigma$ for the L-L pairs, and $\Delta = -0.25\sigma$ for the L-B pairs. Based on these settings, the diameters of the identical backbone and linear side chain beads were equal to 1.0σ and 0.5σ , respectively.

The bending rigidity of the backbone was introduced by imposing the bending potential controlling mutual orientations between two neighboring along the backbone unit bond vectors \mathbf{n}_i and \mathbf{n}_{i+1} .

$$U_{i,i+1}^{bend} = k_B T K (1 - (\mathbf{n}_i \cdot \mathbf{n}_{i+1})) \quad (\text{S6})$$

where $K = 5.0$ and $k_B T$ is the thermal energy set to 1.0 in the energy units.

Simulations of copolymer systems were carried out in a constant volume with 3-D periodic boundary conditions at a constant temperature ensemble. The constant temperature was maintained by coupling the system to a Langevin thermostat implemented in LAMMPS.⁴ In this representation, the equation of motion of the i -th bead is given by

$$m \frac{d\mathbf{v}_i(t)}{dt} = \mathbf{F}_i(t) - \xi \mathbf{v}_i(t) + \mathbf{F}_i^R(t) \quad (\text{S7})$$

where m is the bead mass set to unity for all beads, $\mathbf{v}_i(t)$ is the i th bead velocity, $\mathbf{F}_i(t)$ is the net deterministic force acting on the i th bead, and $\mathbf{F}_i^R(t)$ is the stochastic force with a zero average and a δ -function correlation $\langle \mathbf{F}_i^R(t) \cdot \mathbf{F}_j^R(t') \rangle = 6k_B T \xi \delta_{ij} \delta(t - t')$. The friction coefficient was set to $\xi = 0.1m/\tau_{LJ}$, where $\tau_{LJ} = \sigma(m/k_B T)^{1/2}$ is the standard LJ-time. The velocity-Verlet algorithm with a time step $\Delta t = 0.005\tau_{LJ}$ was used for the integration of the equation of motion. All simulations were performed using LAMMPS.²⁴

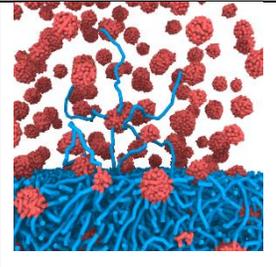
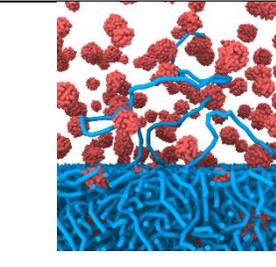
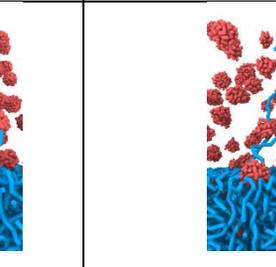
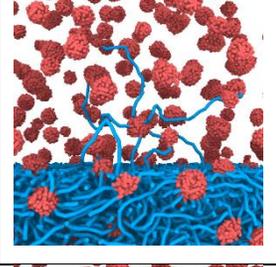
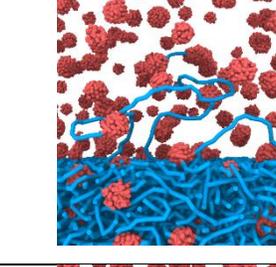
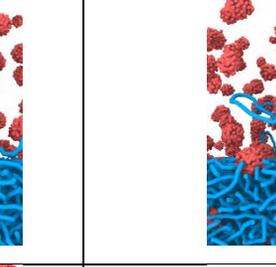
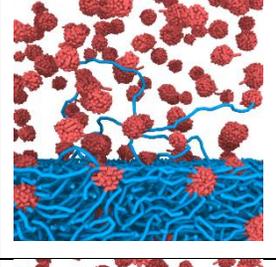
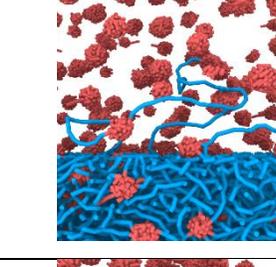
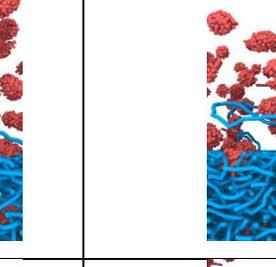
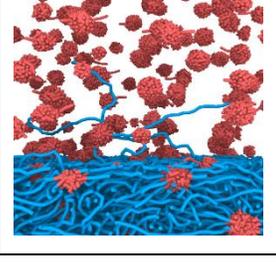
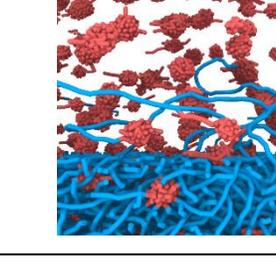
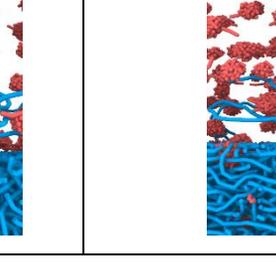
Table S3 Number of beads in studied systems

total number of beads	1 block	2 blocks	3 blocks
linear side chains	33200	27465	25280
backbones	73040	78733	80896

Systems were prepared by first randomly placing copolymer chains with number of beads summarized in **Table S3** in a cubic $50\sigma \times 50\sigma \times 50\sigma$ simulation box with a monomer density $\rho = 0.85\sigma^{-3}$. In the beginning, the non-bonded interaction potentials between all beads were set to be the same, with $\epsilon_{LJ} = 1.0k_B T$, $r_{cut} = 2^{1/6}\sigma$, and the conformations of chains were relaxed according to the method described in our previous work.^{25,26} To trigger the self-assembly, the interaction parameter between monomers belonging to the flexible side chains was gradually changed to an attractive truncated-shifted LJ potential with $r_{cut} = 2.5\sigma$ and ϵ_{LJ} from $0.1k_B T$ to $0.8k_B T$ with an increment of $0.1k_B T$ every $5 \times 10^3 \epsilon_{LJ}$. Then, a follow-up canonical NVT simulation run lasting 5

$\times 10^4 \varepsilon_{LJ}$ was performed to complete the equilibration of the self-assembled network. For this simulation, the interaction parameters (ε_{LJ} , r_{cut}) were set to $(1.0k_B T, 2^{1/6}\sigma)$ for B-B pairs, $(1.0k_B T, 2^{1/6}\sigma)$ for B-L pairs, and $(0.8k_B T, 2.5\sigma)$ for L-L pairs.

Table S4. Snapshots of deformation (horizontal plane) of self-assembled networks of graft copolymers

λ			
1.0			
1.25			
1.50			
1.75			

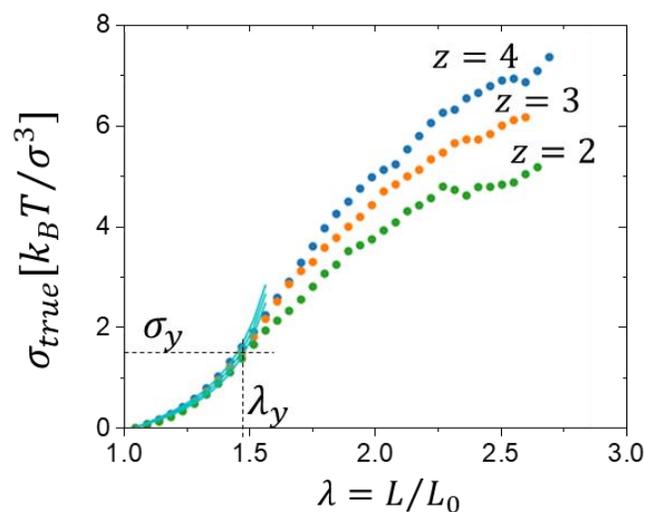
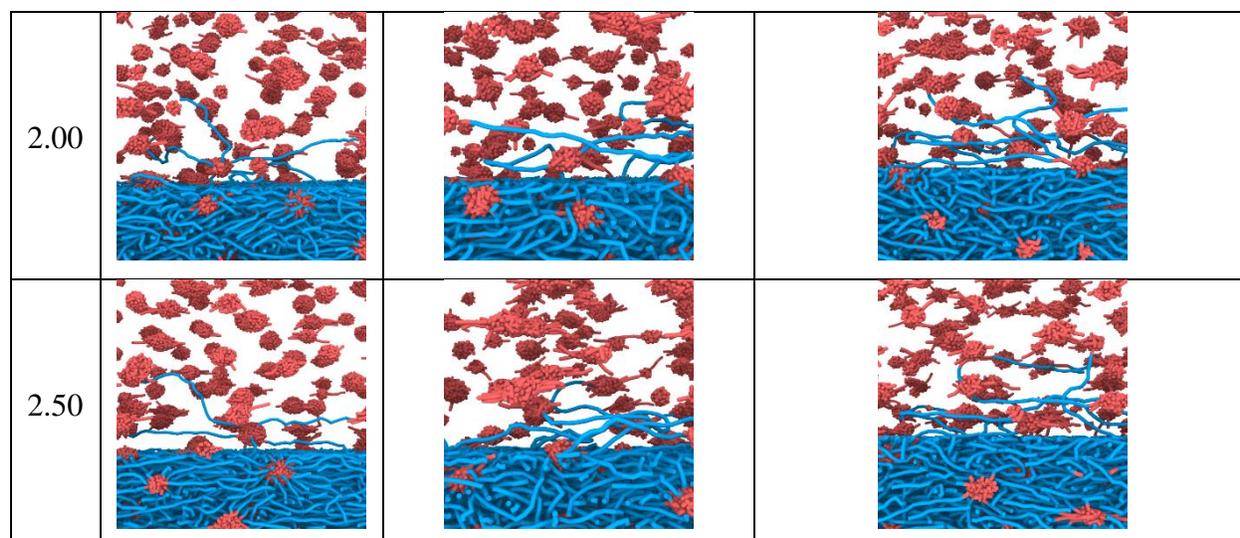


Fig. S34. Dependence of the tensile stress σ_{true} on the deformation ratio λ for self-assembled networks of copolymers consisting of one backbone block (green circles), two blocks (orange circles), and three blocks (blue circles).

To obtain the stress-strain curves shown in Fig. S34, the uniaxial deformation simulations were performed at a constant volume as described in previous work.²⁷ It follows from this figure that at small deformations and initial stages of the nonlinear deformation regime self-assembled network mechanical properties are almost identical and independent of the number of grafted flexible chains. This points out that in this deformation regime, network mechanical properties are determined by deformation of the backbone blocks connecting network nodes made by self-assembled chains. The departure from universal behavior begins when self-assembled domains

start to deform as illustrated in **Table S4** representing snapshots of networks at different deformation ratios. This first happens for networks of copolymers with the smallest number of backbone blocks. This trend is consistent with experimentally observed behavior in studied bottlebrush systems.

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