

## Supporting Information

### Spectroscopic and Theoretical Studies on Hydrogen Bonding Clusters, Triplet Species and Relaxation Mechanism of Light ( $^1\pi\pi^*$ ) State of 4-Methyl-1, 2, 4-Triazole-3-Thione

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Bin-Bin Xie<sup>+\*</sup>,

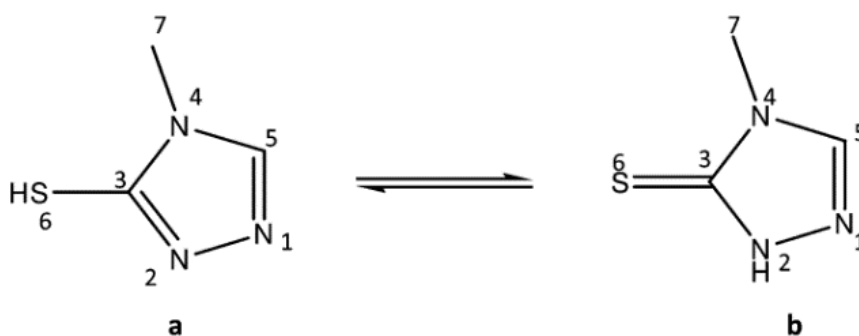
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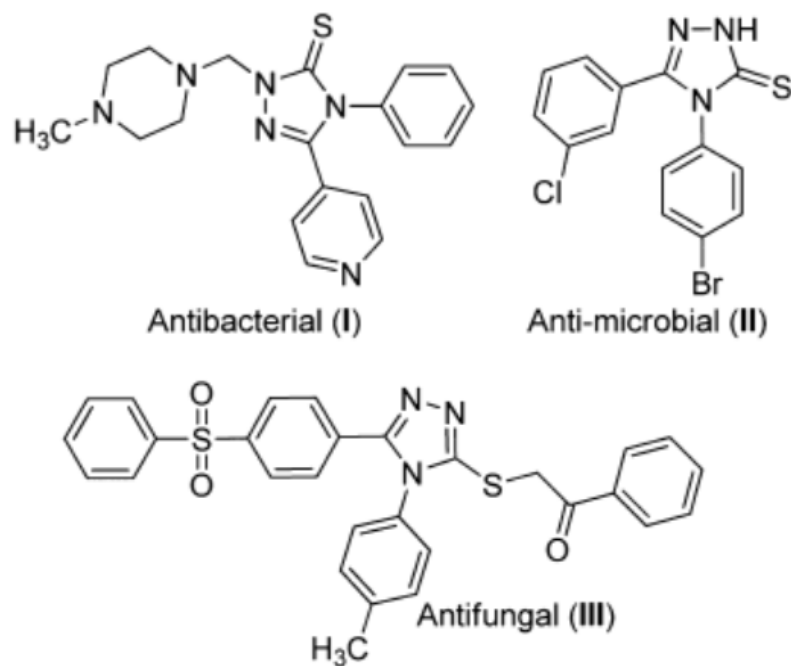
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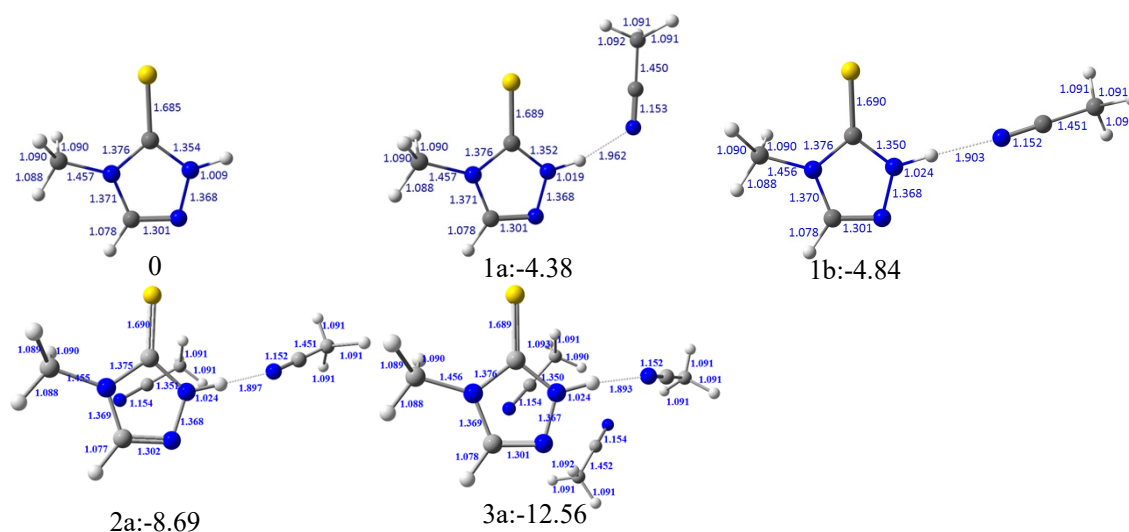
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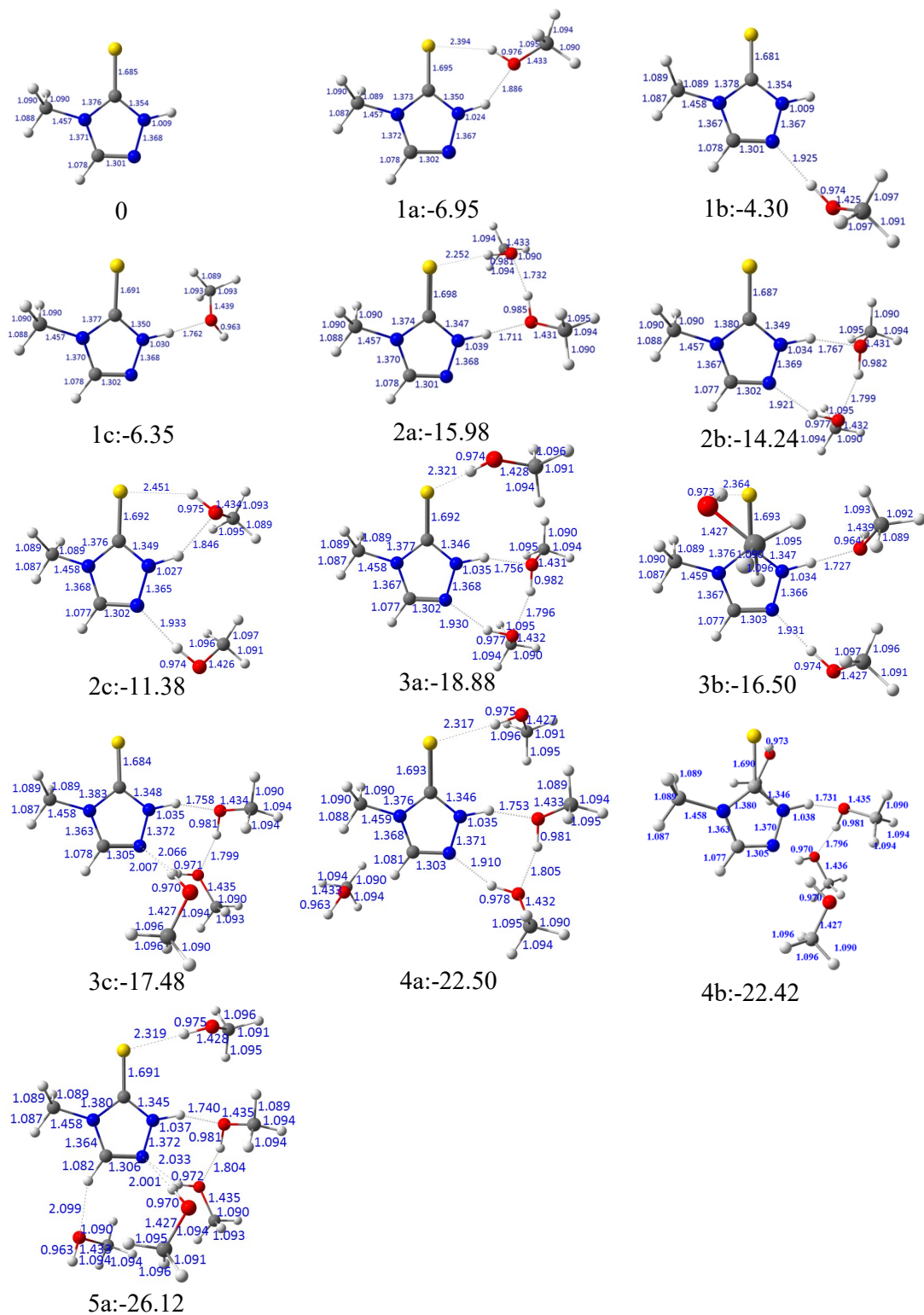
**Scheme S1.** 4-MTT in (a) thiol and (b) thione forms.



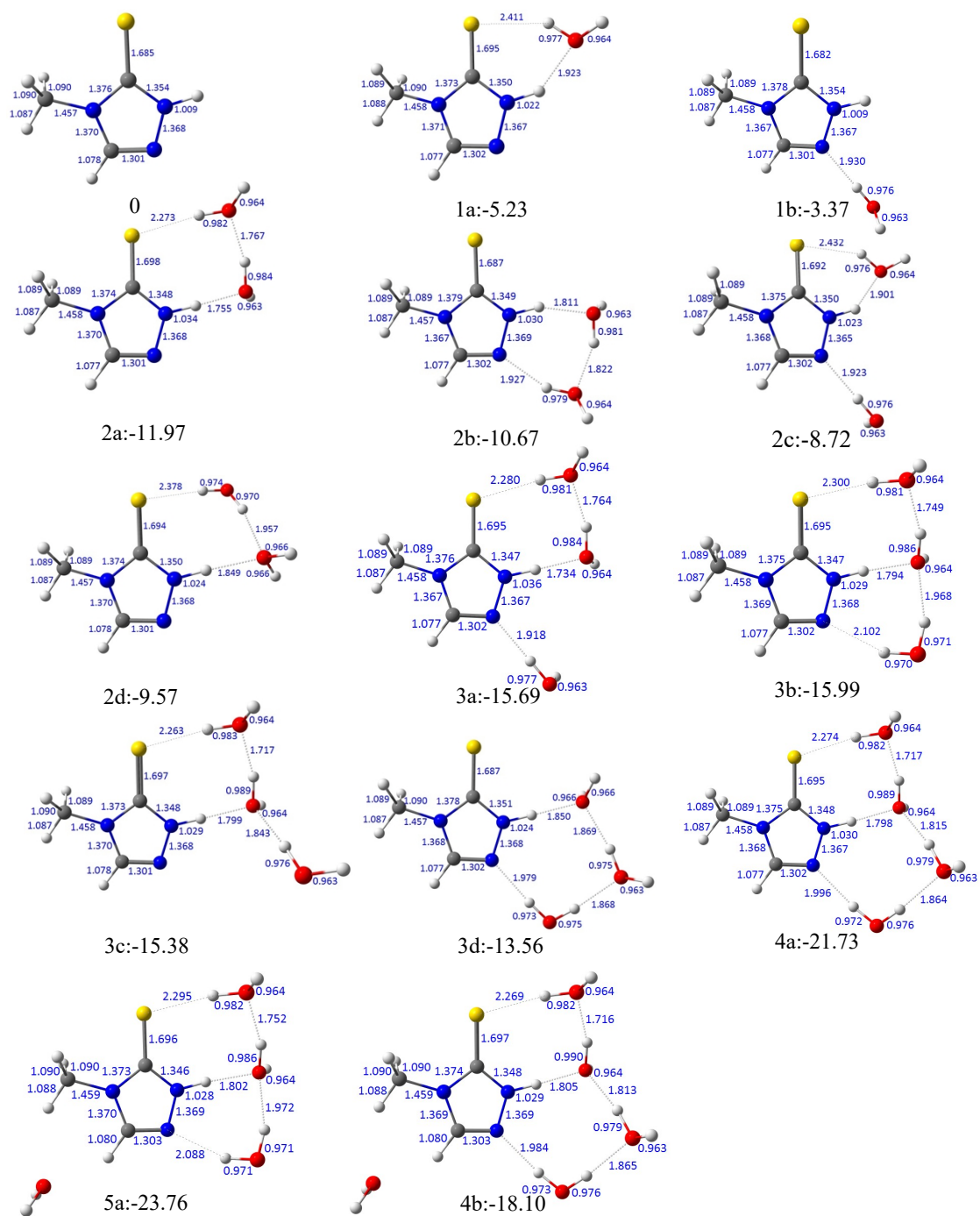
**Scheme S2.** Some biologically active 1,2,4-triazole-3-thione derivatives.



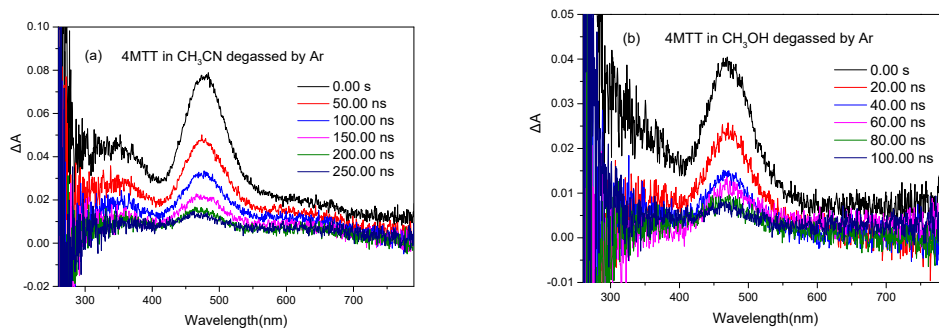
**Figure S1.** Optimized bond lengths (in Å) and relative energies ( $\Delta E$ , in kcal/mol) of 4MTT and 4MTT(CH<sub>3</sub>CN)<sub>n</sub> (n=1~3) clusters at B3LYP-D3(BJ)/6-311++G(d, p) level with PCM solvent model.



**Figure S2.** Optimized bond lengths (in Å) and relative energies ( $\Delta E$ , in kcal/mol) of 4MTT and 4MTT(CH<sub>3</sub>OH)<sub>n</sub> (n=1~5) clusters at B3LYP-D3(BJ)/6-311++G(d,p) level with PCM solvent model.



**Figure S3.** Optimized bond lengths (in Å) and relative energies ( $\Delta E$ , in kcal/mol) of 4MTT and 4MTT(H<sub>2</sub>O)<sub>n</sub> (n=1~5) clusters at B3LYP-D3(BJ)/6-311++G(d, p) level with PCM solvent model.



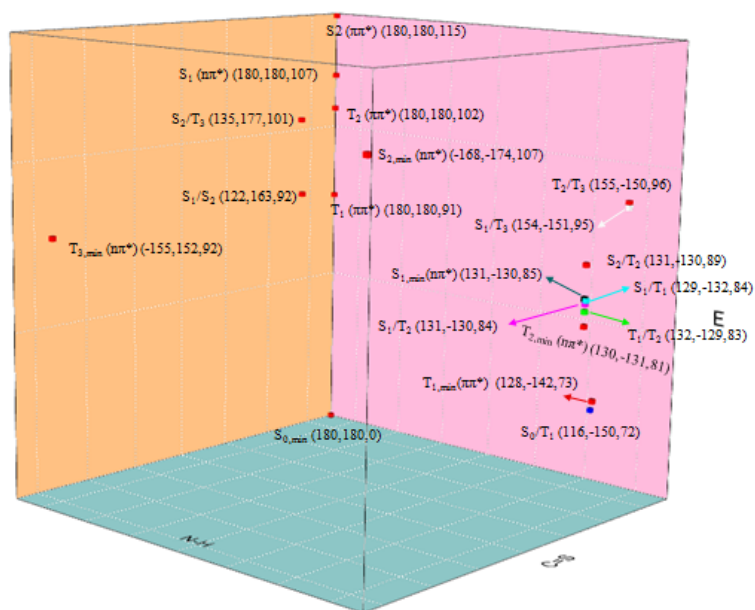
**Figure S4.** Nanosecond transient absorption spectra ( $\lambda_{\text{ex}}=266$  nm) in (a)  $\text{CH}_3\text{CN}$  and (b)  $\text{CH}_3\text{OH}$  in degassed by Ar.

**Figure S5.** Calculated potential decay energy profile of the excited singlet and triplet electronic states from vertical excited  $S_2(\pi\pi^*)$  state at (TD)B3LYP-D3(BJ)/6-311G(d, p) level with PCM Water model. The red dotted line indicated one most possible decay path direct to the triplet state observed experimentally.

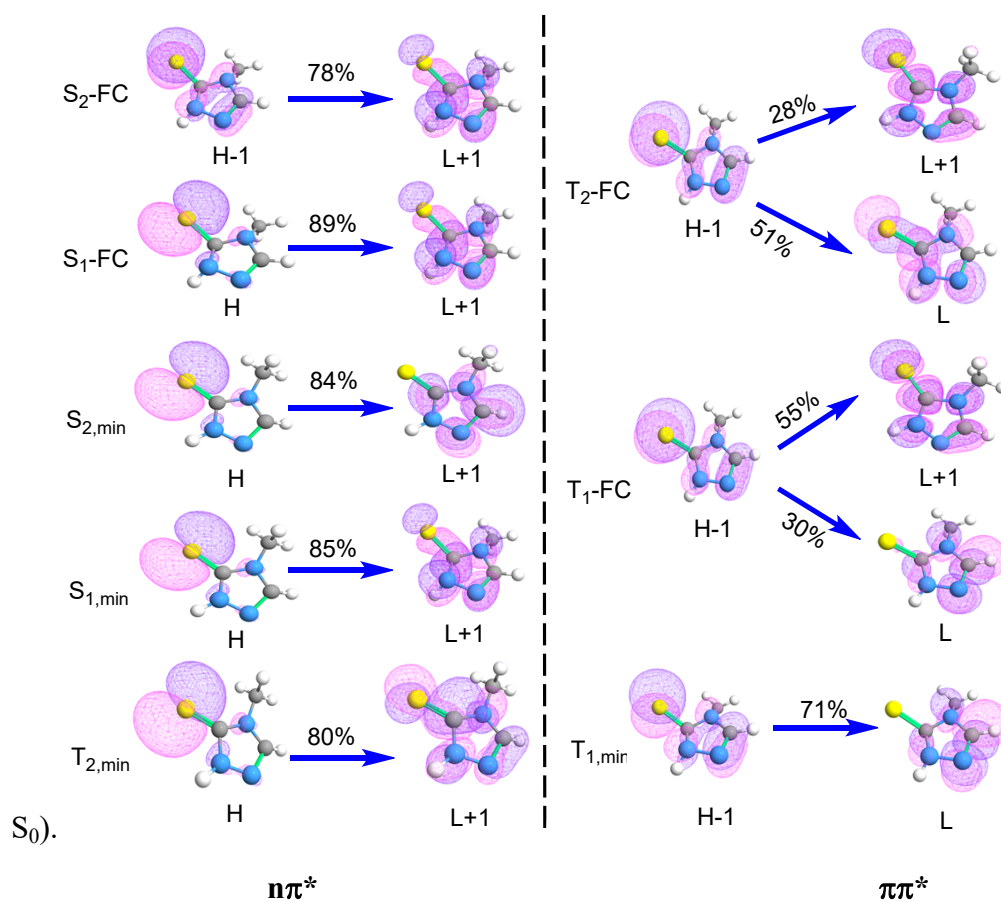
The ground planar 4MTT was stimulated to the  $S_2$  state in the Frank-Condon district ( $S_2$ -FC) with  $\sim 120$  kcal/mol<sup>-1</sup> using 266 nm laser, which was corresponding to the first observed band at  $\sim 250$  nm. Two relaxation pathways that connect the  $S_2$ -FC point were shown in Figure 9. One directs to the pyramidal minimum structure  $S_{2min}(\pi\pi^*)$  with  $\sim 95$  kcal/mol, the other along with the relaxation of  $S_1(n\pi^*)$  state with  $\sim 107$  kcal/mol via a very fast internal conversion(IC) point. And then along ( $^1n\pi^*$ ) state to the intersystem crossing points ( $S_1/T_1$ ) was seamlessly reached to the ( $^3\pi\pi^*$ ) state. However, excited state intramolecular proton transfer (ESIPT) from  $S_1/T_1$  point could pass a barrier of  $\sim 16$  kcal/mol<sup>-1</sup> to tautomeric triplet. Furthermore, the photophysical pathways were calculated either direct to  $S_{1min}$  or to normal triplet species via conical intersection point  $S_0/T_1$ . Thus four possible decay pathways were proposed. According to our experiments, one of the most possible relaxation pathways direct to the triplet state species was observed. The mechanism was proposed as  $S_2(\pi\pi^*) \rightarrow S_1(n\pi^*) \rightarrow S_1(n\pi^*)/T_1(\pi\pi^*) \rightarrow S_0/T_1(\pi\pi^*) \rightarrow ^3(\pi\pi^*)_{min}$  or nonradiative to ground state from  $T_1(\pi\pi^*)$  via the  $S_0/T_1(\pi\pi^*)$ .



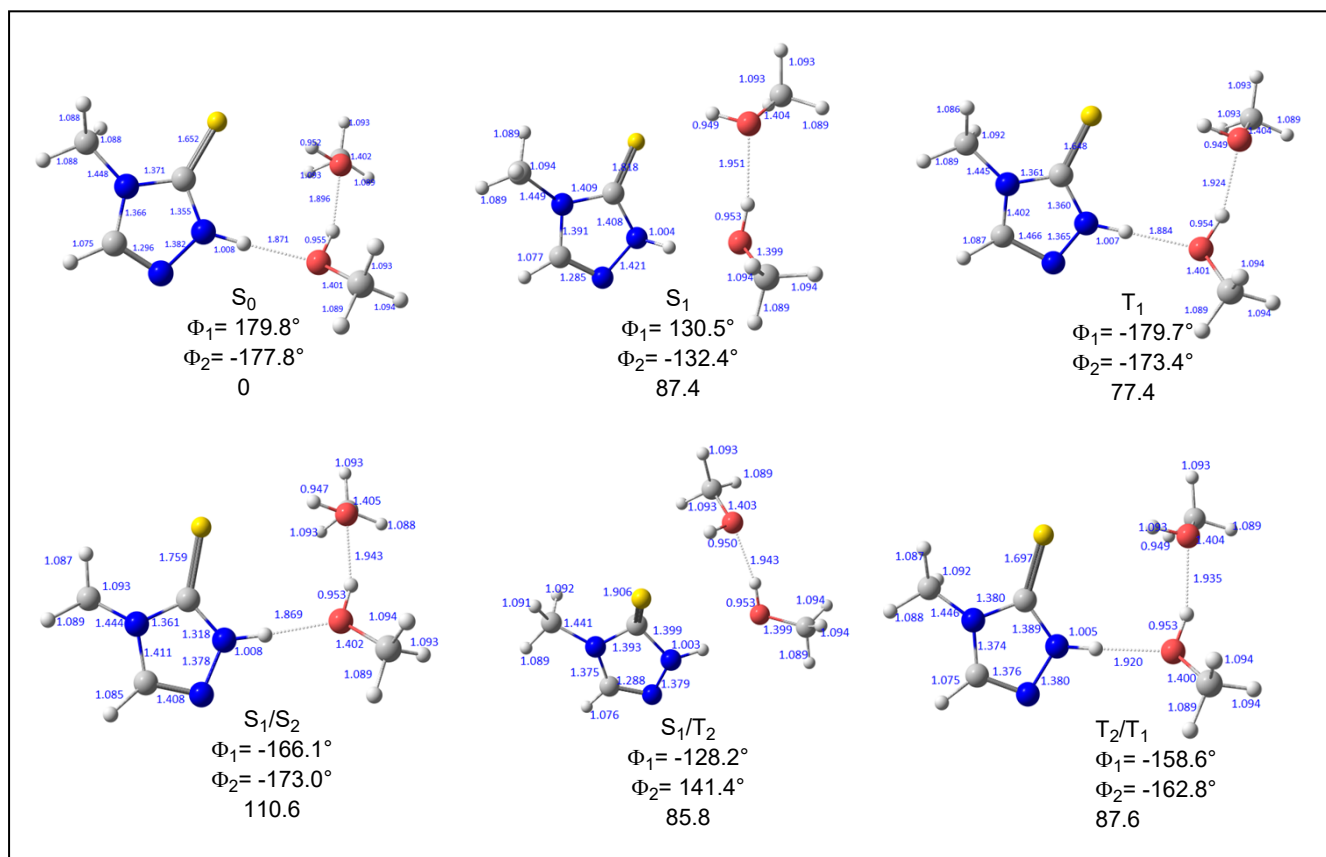
**Figure S6.** Calculated potential decay energy profile of the excited singlet and triplet electronic states from vertical excited  $S_2(\pi\pi^*)$  state at (TD)B3LYP-D3(BJ) /6-311G(d,p) level with PCM acetonitrile model. The red dotted line indicated one most possible decay path direct to the triplet state observed experimentally.



**Figure S7.** The Optimized all the minima at CASSCF(12e,9o)/cc-pVDZ level (the data in parentheses are indicated ( $\Phi_1=D_{N4-C1-C5-S7}$ ,  $\Phi_2=D_{C1-N5-N4-H9}$ , energy relative to



**Figure S8.** Frontier molecular orbitals of 4MTT in excited states calculated at CASSCF(12e,9o)/cc-pVDZ level.



**Figure S9.** Optimized bond lengths and angles for different minimum structures ( $S_{2min}$ ,  $S_{1min}$ , and  $T_{1min}$ ), and CI points ( $S_2/S_1$ ,  $S_2/T_2$ ,  $S_1/T_2$ , and  $T_1/T_2$ ) at CASSCF(12e/9o)/cc-pVDZ level (the arrow in dotted points to the plane and the solid points out of the plane,  $\Phi_1 = D_{N4-C1-C5-S7}$ ,  $\Phi_2 = D_{C1-N5-N4-H9}$ ).



**Table S1.** Experimental and calculated vibrational frequencies at B3LYP-D3/6-311++G(d, p) level and assignments of 4MTTdimer.

Mode ( $C_s$ )	Calc. (Raman activity/ IR intensity)	Exp.		Descriptions (PED%)
		FT- Raman	FT-IR	
v <sub>1</sub>	3263.3(0.001/1959.6)			N <sub>2</sub> H <sub>6</sub> +N <sub>14</sub> H <sub>18</sub> stretch
v <sub>2</sub>	3260.4(333.6/0.04)			N <sub>2</sub> H <sub>6</sub> +N <sub>14</sub> H <sub>18</sub> +C <sub>5</sub> H <sub>9</sub> +C <sub>17</sub> H <sub>21</sub> stretch
v <sub>3</sub>	3258.5(0.005/1172.5)		3120	C <sub>5</sub> H <sub>9</sub> +C <sub>17</sub> H <sub>21</sub> stretch
v <sub>4</sub>	3214.1(1389.7/0.007)	3128		N <sub>2</sub> H <sub>6</sub> +N <sub>14</sub> H <sub>18</sub> +C <sub>5</sub> H <sub>9</sub> +C <sub>17</sub> H <sub>21</sub> stretch
v <sub>5</sub>	3142.1(88.7/3.6)			C <sub>8</sub> H <sub>11</sub> +C <sub>20</sub> H <sub>23</sub> stretch
v <sub>6</sub>	3142.1(21.3/14.8)			C <sub>8</sub> H <sub>11</sub> +C <sub>20</sub> H <sub>23</sub> stretch
v <sub>7</sub>	3119.7(19.4/9.7)			C <sub>8</sub> H <sub>10</sub> +C <sub>8</sub> H <sub>12</sub> +C <sub>20</sub> H <sub>22</sub> +C <sub>20</sub> H <sub>24</sub> stretch
v <sub>8</sub>	3119.7(72.5/2.6)	3085		C <sub>8</sub> H <sub>10</sub> +C <sub>8</sub> H <sub>12</sub> +C <sub>20</sub> H <sub>22</sub> +C <sub>20</sub> H <sub>24</sub> stretch
v <sub>9</sub>	3050.6(349.3/0.003)	2943		C <sub>8</sub> H <sub>10</sub> +C <sub>8</sub> H <sub>11</sub> +C <sub>8</sub> H <sub>12</sub> +C <sub>20</sub> H <sub>22</sub> +C <sub>20</sub> H <sub>23</sub> +C <sub>20</sub> H <sub>24</sub> stretch
v <sub>10</sub>	3050.5(0.02/56.7)		2943	C <sub>8</sub> H <sub>10</sub> +C <sub>8</sub> H <sub>11</sub> +C <sub>8</sub> H <sub>12</sub> +C <sub>20</sub> H <sub>22</sub> +C <sub>20</sub> H <sub>23</sub> +C <sub>20</sub> H <sub>24</sub> stretch
v <sub>11</sub>	1604.1(28.5/0.0004)	1552		N <sub>1</sub> C <sub>5</sub> stretch+N <sub>13</sub> C <sub>17</sub> stretch+H <sub>18</sub> N <sub>14</sub> N <sub>13</sub> bend+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> bend
v <sub>12</sub>	1599.3(0.0001/132.2)		1552	N <sub>1</sub> C <sub>5</sub> stretch+N <sub>13</sub> C <sub>17</sub> stretch+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> bend
v <sub>13</sub>	1540.5(0.0004/297.6)		1489	N <sub>2</sub> C <sub>3</sub> stretch+N <sub>14</sub> C <sub>15</sub> stretch+H <sub>18</sub> N <sub>14</sub> N <sub>13</sub> bend+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
v <sub>14</sub>	1532.3(44.5/0.002)	1493		N <sub>2</sub> C <sub>3</sub> stretch+N <sub>14</sub> C <sub>15</sub> stretch+H <sub>18</sub> N <sub>14</sub> N <sub>13</sub> bend+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
v <sub>15</sub>	1508.3(0.002/24.6)	<b>1423/ 1431</b>		H <sub>10</sub> C <sub>8</sub> H <sub>12</sub> bend+H <sub>22</sub> C <sub>20</sub> H <sub>24</sub> bend+H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> tors+H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> tors+H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors+H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
v <sub>16</sub>	1507.6(20.9/0.003)		<b>1425</b>	H <sub>10</sub> C <sub>8</sub> H <sub>12</sub> bend+H <sub>22</sub> C <sub>20</sub> H <sub>24</sub> bend+H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> tors+H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> tors+H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors+H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors

V <sub>17</sub>	1473.9(10.8/11.2)		<b>1425</b>	H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> +H <sub>23</sub> C <sub>20</sub> H <sub>22</sub> bend
V <sub>18</sub>	1473.9(6.9/17.5)	<b>1394</b>		H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> +H <sub>23</sub> C <sub>20</sub> H <sub>22</sub> bend
V <sub>19</sub>	1469.0(0.001/16.5)	<b>1394</b>		H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> bend+H <sub>12</sub> C <sub>8</sub> H <sub>11</sub> bend+H <sub>23</sub> C <sub>20</sub> H <sub>22</sub> bend+H <sub>24</sub> C <sub>20</sub> H <sub>23</sub> bend+H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> tors+ H <sub>23</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>20</sub>	1468.4(15.1/0.001)		<b>1390</b>	H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> bend+H <sub>12</sub> C <sub>8</sub> H <sub>11</sub> bend+H <sub>23</sub> C <sub>20</sub> H <sub>22</sub> bend+H <sub>24</sub> C <sub>20</sub> H <sub>23</sub> bend+H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> tors+ H <sub>23</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>21</sub>	1411.0(53.9/0.0)	1361		N <sub>1</sub> C <sub>5</sub> stretch+N <sub>13</sub> C <sub>17</sub> stretch+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend
V <sub>22</sub>	1405.5(0.0/61.6)		<b>1361</b>	N <sub>1</sub> C <sub>5</sub> stretch+N <sub>13</sub> C <sub>17</sub> stretch+N <sub>4</sub> C <sub>8</sub> stretch+N <sub>16</sub> C <sub>20</sub> stretch+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend
V <sub>23</sub>	1357.6(0.005/261.0)		1323	N <sub>16</sub> C <sub>17</sub> stretch+N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> bend+N <sub>16</sub> C <sub>17</sub> N <sub>13</sub> bend+H <sub>18</sub> N <sub>14</sub> N <sub>13</sub> bend+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> bend
V <sub>24</sub>	1353.9(37.5/0.03)	1325		N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> bend+N <sub>16</sub> C <sub>17</sub> N <sub>13</sub> bend+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>25</sub>	1293.1(32.6/0.008)	<b>1275</b>		N <sub>2</sub> C <sub>3</sub> stretch+N <sub>14</sub> C <sub>15</sub> stretch+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>26</sub>	1287.6(0.004/82.5)		<b>1267</b>	N <sub>2</sub> C <sub>3</sub> stretch+N <sub>14</sub> C <sub>15</sub> stretch+C <sub>3</sub> N <sub>2</sub> H <sub>6</sub> bend
V <sub>27</sub>	1251.1(0.0001/42.2)		<b>1219</b>	H <sub>9</sub> C <sub>5</sub> N <sub>1</sub> +H <sub>21</sub> C <sub>17</sub> N <sub>13</sub> bend
V <sub>28</sub>	1250.4(18.1/0.0002)	<b>1216</b>		H <sub>9</sub> C <sub>5</sub> N <sub>1</sub> +H <sub>21</sub> C <sub>17</sub> N <sub>13</sub> bend
V <sub>29</sub>	1179.2(0.0001/30.1)		1151	C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> bend
V <sub>30</sub>	1167.4(32.3/0.0001)	1149		C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> bend
V <sub>31</sub>	1150.6(0.1/0.1)			H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>23</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>32</sub>	1150.6(1.6/0.004)			H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>23</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>33</sub>	1106.5(6.2/0.0008)	1082		N <sub>1</sub> N <sub>2</sub> +N <sub>14</sub> N <sub>13</sub> stretch
V <sub>34</sub>	1105.2(0.0005/8.5)		1078	N <sub>1</sub> N <sub>2</sub> +N <sub>14</sub> N <sub>13</sub> stretch
V <sub>35</sub>	1062.0(9.2/0.0009)	1043		N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> bend+N <sub>16</sub> C <sub>17</sub> N <sub>13</sub>

			bend+H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>36</sub>	1061.3(0.0001/63.5)	1041	N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> bend+N <sub>16</sub> C <sub>17</sub> N <sub>13</sub>
V <sub>37</sub>	957.6(0.0001/72.6)	950	bend+H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>38</sub>	952.2(29.5/0.0002)	941	N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> +N <sub>16</sub> C <sub>17</sub> N <sub>13</sub> +C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> +N <sub>14</sub> N <sub>13</sub> C <sub>17</sub> bend
V <sub>39</sub>	832.6(0.0/86.4)	881	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> +H <sub>9</sub> C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> +H <sub>21</sub> C <sub>17</sub> N <sub>13</sub> N <sub>14</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>40</sub>	827.7(0.4/0.002)		N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> +H <sub>9</sub> C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> +H <sub>21</sub> C <sub>17</sub> N <sub>13</sub> N <sub>14</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>41</sub>	810.9(0.0/13.5)	852	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> +H <sub>18</sub> N <sub>14</sub> N <sub>13</sub> C <sub>17</sub> +C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> +H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>42</sub>	793.6(5.3/0.0)	852	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> +H <sub>18</sub> N <sub>14</sub> N <sub>13</sub> C <sub>17</sub> +C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> +H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>43</sub>	705.0(0.0/8.4)	690	N <sub>4</sub> C <sub>8</sub> stretch+N <sub>16</sub> C <sub>20</sub> stretch+N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> bend+N <sub>16</sub> C <sub>17</sub> N <sub>13</sub> bend
V <sub>44</sub>	701.8(31.4/0.0)	698	N <sub>4</sub> C <sub>8</sub> stretch+N <sub>16</sub> C <sub>20</sub> stretch+N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> bend+N <sub>16</sub> C <sub>17</sub> N <sub>13</sub> bend
V <sub>45</sub>	674.3(3.5/0.0)		N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> C <sub>17</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors+S <sub>7</sub> N <sub>2</sub> N <sub>4</sub> C <sub>3</sub> out+ S <sub>19</sub> N <sub>14</sub> N <sub>16</sub> C <sub>15</sub> out
V <sub>46</sub>	673.2(0.0/8.6)	673	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> C <sub>17</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors+S <sub>7</sub> N <sub>2</sub> N <sub>4</sub> C <sub>3</sub> out+ S <sub>19</sub> N <sub>14</sub> N <sub>16</sub> C <sub>15</sub> out
V <sub>47</sub>	638.8(0.6/0.0)		N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> +N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> +N <sub>16</sub> C <sub>17</sub> N <sub>13</sub> N <sub>14</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>48</sub>	638.7(0.0/5.8)		N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> +N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> +N <sub>16</sub> C <sub>17</sub> N <sub>13</sub> N <sub>14</sub> +N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>49</sub>	542.0(0.0001/28.8)	542	S <sub>7</sub> C <sub>3</sub> stretch+S <sub>19</sub> C <sub>15</sub> stretch+C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> bend
V <sub>50</sub>	539.6(17.4/0.0001)	544	S <sub>7</sub> C <sub>3</sub> stretch+S <sub>19</sub> C <sub>15</sub> stretch+C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> bend
V <sub>51</sub>	431.1(0.0/1.2)		S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> bend+C <sub>8</sub> N <sub>4</sub> C <sub>5</sub> bend+C <sub>20</sub> N <sub>16</sub> C <sub>17</sub> bend+S <sub>19</sub> C <sub>15</sub> N <sub>16</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+ N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>52</sub>	418.1(2.2/0.0)	422	S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> bend+C <sub>8</sub> N <sub>4</sub> C <sub>5</sub> bend+S <sub>19</sub> C <sub>15</sub> N <sub>16</sub> bend+C <sub>20</sub> N <sub>16</sub> C <sub>17</sub> bend
V <sub>53</sub>	262.2(0.0/26.7)		S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> bend+C <sub>8</sub> N <sub>4</sub> C <sub>5</sub> bend+C <sub>20</sub> N <sub>16</sub> C <sub>17</sub> bend+S <sub>19</sub> C <sub>15</sub> N <sub>16</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors
V <sub>54</sub>	248.7(6.3/0.0)	251	S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> bend+C <sub>8</sub> N <sub>4</sub> C <sub>5</sub> bend+C <sub>20</sub> N <sub>16</sub> C <sub>17</sub> bend+S <sub>19</sub> C <sub>15</sub> N <sub>16</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors
V <sub>55</sub>	231.5(0.2/0.0)		N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> C <sub>17</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub>

V <sub>56</sub>	230.4(0.0/0.03)	tors+S <sub>7</sub> N <sub>2</sub> N <sub>4</sub> C <sub>3</sub> out+ S <sub>19</sub> N <sub>14</sub> N <sub>16</sub> C <sub>15</sub> out C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> tors+C <sub>15</sub> N <sub>14</sub> N <sub>13</sub> C <sub>17</sub> tors+S <sub>7</sub> N <sub>2</sub> N <sub>4</sub> C <sub>3</sub> out+ S <sub>19</sub> N <sub>14</sub> N <sub>16</sub> C <sub>15</sub> out
V <sub>57</sub>	199.3(1.1/0.0)	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors+C <sub>20</sub> C <sub>15</sub> C <sub>17</sub> N <sub>16</sub> out+ C <sub>8</sub> C <sub>3</sub> C <sub>5</sub> N <sub>4</sub> out
V <sub>58</sub>	198.2(0.0/1.2)	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors+C <sub>20</sub> C <sub>15</sub> C <sub>17</sub> N <sub>16</sub> out+ C <sub>8</sub> C <sub>3</sub> C <sub>5</sub> N <sub>4</sub> out
V <sub>59</sub>	113.3(0.9/0.0)	H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>23</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>60</sub>	104.7(0.0002/0.1)	H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> +H <sub>22</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>23</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> +H <sub>24</sub> C <sub>20</sub> N <sub>16</sub> C <sub>15</sub> tors
V <sub>61</sub>	104.3(0.9/0.0)	S <sub>19</sub> H <sub>6</sub> stretch+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> bend+H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>62</sub>	83.2(0.0/12.0)	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> bend+H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>63</sub>	78.3(1.7/0.0)	S <sub>19</sub> H <sub>6</sub> stretch+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> bend+H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>64</sub>	45.9(2.6/0.0)	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> bend+N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> N <sub>14</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> tors+ N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>65</sub>	34.5(0.0/4.2)	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> tors+ N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors
V <sub>66</sub>	7.8(0.0/6.2)	N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> tors+H <sub>6</sub> S <sub>19</sub> C <sub>15</sub> N <sub>14</sub> tors+C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> tors+H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> N <sub>4</sub> tors+ N <sub>1</sub> N <sub>2</sub> H <sub>6</sub> S <sub>19</sub> tors

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PED=potential energy distribution, only contributions larger than 10% were given.

**Table S2.** The assignments of 488 nm Raman in different solvents and calculated spectra at B3LYP-D3(BJ)/6-311++G(d, p)level for 4MTT(H<sub>2</sub>O)<sub>2</sub>.

Mode	Exp.			Cal.	Descriptions (PED%)
	In CH <sub>3</sub> CN	In CH <sub>3</sub> OH	In H <sub>2</sub> O	(Raman activity/IR intensity)	
v <sub>1</sub>				3274(220.9/1.0)	C <sub>5</sub> H <sub>9</sub> (99)stretch
v <sub>2</sub>				3172(424.9/1534.0)	N <sub>2</sub> H <sub>6</sub> (93)stretch
v <sub>3</sub>				3165(122.4/10.3)	C <sub>8</sub> H <sub>10</sub> (11)+C <sub>8</sub> H <sub>11</sub> (79)+C <sub>8</sub> H <sub>12</sub> (11)stretch
v <sub>4</sub>				3137(97.5/11.1)	C <sub>8</sub> H <sub>10</sub> (50)+C <sub>8</sub> H <sub>12</sub> (50)stretch
v <sub>5</sub>				3066(342.1/29.0)	C <sub>8</sub> H <sub>10</sub> (39)+C <sub>8</sub> H <sub>11</sub> (21)+C <sub>8</sub> H <sub>12</sub> (39)stretch
v <sub>6</sub>	1556(m)	1559(w)	1561(w)	1544(125.6/267.9)	N <sub>1</sub> C <sub>5</sub> (14)stretch+N <sub>2</sub> C <sub>3</sub> (17)stretch+N <sub>4</sub> C <sub>5</sub> (12)stretch+ H <sub>6</sub> N <sub>2</sub> N <sub>1</sub> (16)bend
v <sub>7</sub>	1480(w)	1498(m)	1500(vs)	1503(21.4/35.6)	H <sub>10</sub> C <sub>8</sub> H <sub>12</sub> (52)bend+H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> (12)bend+H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (11)tors+ H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (10)tors
v <sub>8</sub>				1470(17.6/21.0)	H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> (47)bend+H <sub>12</sub> C <sub>8</sub> H <sub>11</sub> (27)bend+H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (18)tors
v <sub>9</sub>	1427(vw)	1425(w)	1428(s)	1466(41.5/18.4)	N <sub>1</sub> C <sub>5</sub> (20)stretch+H <sub>10</sub> C <sub>8</sub> H <sub>12</sub> (14)bend+H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> (14)bend+ H <sub>12</sub> C <sub>8</sub> H <sub>11</sub> (40)bend
v <sub>10</sub>	1362(m)	1365(m)	1365(m)	1411(38.4/24.2)	N <sub>1</sub> C <sub>5</sub> (26)+N <sub>4</sub> C <sub>5</sub> (21)+N <sub>4</sub> C <sub>8</sub> (15)stretch
v <sub>11</sub>	1326(w)	1334(s)	1339(vs)	1362(156.9/276.5)	N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> (14)+C <sub>3</sub> N <sub>2</sub> N <sub>1</sub> (14)bend
v <sub>12</sub>	1255(w)	1274(m)	1284(m)	1301(51.7/36.5)	N <sub>2</sub> C <sub>3</sub> (49)+N <sub>4</sub> C <sub>5</sub> (15)stretch
v <sub>13</sub>	1224(vw)	1225(vw)	1227 (vw)	1254(14.8/56.9)	N <sub>4</sub> C <sub>8</sub> (12)stretch+H <sub>9</sub> C <sub>5</sub> N <sub>1</sub> (67)bend
v <sub>14</sub>	1154(vw)	1154(w)	1157(w)	1176(25.7/71.7)	N <sub>4</sub> C <sub>8</sub> (11)stretch+S <sub>7</sub> C <sub>3</sub> (17)stretch+C <sub>3</sub> N <sub>2</sub> N <sub>1</sub> (39)bend
v <sub>15</sub>				1150(1.4/0.1)	H <sub>11</sub> C <sub>8</sub> H <sub>10</sub> (18)bend+H <sub>12</sub> C <sub>8</sub> H <sub>11</sub> (16)bend+H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (17)tors H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (31)tors+H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (17)tors
v <sub>16</sub>	1071(vvw)	1074(vw)	1078(vvw)	1107(7.4/15.7)	N <sub>2</sub> N <sub>1</sub> (65)stretch
v <sub>17</sub>	1036(vw)	1049(vvw)	1047(vvw)	1067(14.1/87.1)	N <sub>4</sub> C <sub>5</sub> (17)stretch+N <sub>2</sub> N <sub>1</sub> (14)stretch+N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> (15)bend+H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (1

v <sub>18</sub>	935(s)	935(s)	946(s)	961(27.7/55.7)	2)tors+H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (12)tors N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> (13)+N <sub>2</sub> N <sub>1</sub> C <sub>5</sub> (61)bend
v <sub>19</sub>				854(2.1/13.8)	H <sub>9</sub> C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> (80)tors
v <sub>20</sub>	689(vvs)	689(vvs)	688(vvs)	701(32.2/5.2)	N <sub>4</sub> C <sub>8</sub> (46)stretch+N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> (22)bend
v <sub>21</sub>				682(3.6/9.7)	C <sub>3</sub> N <sub>2</sub> N <sub>1</sub> C <sub>5</sub> (38)tors+S <sub>7</sub> N <sub>2</sub> N <sub>4</sub> C <sub>3</sub> (46)out
v <sub>22</sub>				646(1.0/5.7)	H <sub>9</sub> C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> (12)+N <sub>4</sub> C <sub>5</sub> N <sub>1</sub> N <sub>2</sub> (75)tors
v <sub>23</sub>	535(vs)	535(vs)	530(m)	535(13.7/29.1)	S <sub>7</sub> C <sub>3</sub> (55)stretch+C <sub>3</sub> N <sub>2</sub> N <sub>1</sub> (14)bend+C <sub>8</sub> N <sub>4</sub> C <sub>5</sub> (11)bend
v <sub>24</sub>	402(m)	402(w)	404(w)	420(4.1/8.7)	S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> (21)+C <sub>8</sub> N <sub>4</sub> C <sub>5</sub> (41)bend
v <sub>25</sub>	238(s)	240(m)	243(m)	207(2.2/4.4)	H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (10)tors+C <sub>3</sub> N <sub>2</sub> N <sub>1</sub> C <sub>5</sub> (30)tors+ C <sub>8</sub> C <sub>3</sub> C <sub>5</sub> N <sub>4</sub> (35)out+S <sub>7</sub> N <sub>2</sub> N <sub>4</sub> C <sub>3</sub> (10)out
v <sub>26</sub>				105(0.8/0.2)	H <sub>10</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (25)tors+H <sub>11</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (27)tors+H <sub>12</sub> C <sub>8</sub> N <sub>4</sub> C <sub>3</sub> (25)tors+C <sub>8</sub> C <sub>3</sub> C <sub>5</sub> N <sub>4</sub> (20)out
v <sub>1</sub> '				3858(114.2/99.6)	O <sub>13</sub> H <sub>15</sub> (99)stretch
v <sub>2</sub> '				3849(95.0/132.5)	O <sub>16</sub> H <sub>17</sub> (98)stretch
v <sub>3</sub> '				3477(512.9/1326.0)	O <sub>13</sub> H <sub>14</sub> (28)+O <sub>16</sub> H <sub>18</sub> (71)stretch
v <sub>4</sub> '				3418(359.0/1095.1)	O <sub>13</sub> H <sub>14</sub> (66)+O <sub>16</sub> H <sub>18</sub> (27)stretch
v <sub>5</sub> '				1640(2.7/17.6)	H <sub>15</sub> O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> (38)+H <sub>14</sub> O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> (13)tors
v <sub>6</sub> '				1610(8.7/108.4)	H <sub>17</sub> O <sub>16</sub> H <sub>18</sub> (38)bend+H <sub>6</sub> N <sub>2</sub> N <sub>1</sub> (15)bend+H <sub>15</sub> O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> (10)tors
v <sub>7</sub> '				1606(17.4/156.5)	H <sub>17</sub> O <sub>16</sub> H <sub>18</sub> (47)bend+H <sub>15</sub> O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> (19)tors
v <sub>8</sub> '				910(1.2/161.7)	O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> (31)bend+H <sub>15</sub> O <sub>13</sub> H <sub>6</sub> (19)bend+H <sub>6</sub> N <sub>2</sub> N <sub>1</sub> C <sub>5</sub> (29)tors
v <sub>9</sub> '				860(1.7/218.0)	O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (32)bend+H <sub>17</sub> O <sub>16</sub> H <sub>18</sub> S <sub>7</sub> (10)tors+ H <sub>18</sub> O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (12)tors+O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> N <sub>2</sub> (12)tors
v <sub>10</sub> '				644(6.7/201.7)	H <sub>18</sub> O <sub>16</sub> H <sub>14</sub> (38)bend+O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (20)bend+ H <sub>17</sub> O <sub>16</sub> H <sub>18</sub> S <sub>7</sub> (11)tors+H <sub>18</sub> O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (10)tors
v <sub>11</sub> '				462(1.8/99.6)	H <sub>15</sub> O <sub>13</sub> H <sub>6</sub> (14)bend+O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (11)bend+ H <sub>18</sub> O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (21)tors+ O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> N <sub>2</sub> (18)tors
v <sub>12</sub> '				348(1.9/40.4)	H <sub>17</sub> O <sub>16</sub> H <sub>18</sub> S <sub>7</sub> (28)+H <sub>18</sub> O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (13)+O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> N <sub>2</sub> (22)tors
v <sub>13</sub> '				296(0.4/174.7)	H <sub>15</sub> O <sub>13</sub> H <sub>6</sub> (40)bend+H <sub>17</sub> O <sub>16</sub> H <sub>18</sub> S <sub>7</sub> (15)tors

v <sub>14</sub> '	255(2.6/30.2)	O <sub>16</sub> H <sub>14</sub> (16)stretch+S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> (22)bend+C <sub>8</sub> N <sub>4</sub> C <sub>5</sub> (12)bend
v <sub>15</sub> '	250(1.3/117.1)	S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> (11)bend+H <sub>17</sub> O <sub>16</sub> H <sub>18</sub> S <sub>7</sub> (16)tors+H <sub>18</sub> O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> (17)tors+O <sub>16</sub> H <sub>14</sub> O <sub>13</sub> N <sub>2</sub> (15)tors
v <sub>16</sub> '	245(0.9/57.5)	O <sub>16</sub> H <sub>14</sub> (42)stretch+C <sub>8</sub> C <sub>3</sub> C <sub>5</sub> N <sub>4</sub> (10)out
v <sub>17</sub> '	244(0.1/70.3)	O <sub>16</sub> H <sub>14</sub> (16)stretch+C <sub>8</sub> C <sub>3</sub> C <sub>5</sub> N <sub>4</sub> (15)out+S <sub>7</sub> N <sub>2</sub> N <sub>4</sub> C <sub>3</sub> (24)out
v <sub>18</sub> '	185(0.4/23.5)	O <sub>13</sub> H <sub>6</sub> (84)stretch
v <sub>19</sub> '	147(0.7/17.2)	S <sub>7</sub> C <sub>3</sub> N <sub>4</sub> (11)bend+H <sub>14</sub> O <sub>13</sub> H <sub>6</sub> (36)bend+O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> (11)tors
v <sub>20</sub> '	87(2.5/0.8)	H <sub>14</sub> O <sub>13</sub> H <sub>6</sub> (20)bend+H <sub>6</sub> N <sub>2</sub> N <sub>1</sub> (27)bend+O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> C <sub>3</sub> (15)tors
v <sub>21</sub> '	60(1.4/8.1)	O <sub>13</sub> H <sub>6</sub> N <sub>2</sub> (25)bend+H <sub>6</sub> N <sub>2</sub> N <sub>1</sub> C <sub>5</sub> (33)tors+C <sub>8</sub> C <sub>3</sub> C <sub>5</sub> N <sub>4</sub> (11)out

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□m=middle, s= strong, vs= very strong, w=weak, vw=very weak; PED=potential energy distribution, only contributions larger than 10% were given.

**Table S3.** Calculated and experimental electronic transition energy ( $\Delta E$ , in kcal/mol) and oscillator intensity (f) for 4MMT(CH<sub>3</sub>CN), 4MMT(CH<sub>3</sub>OH)<sub>2</sub> and 4MMT(H<sub>2</sub>O)<sub>2</sub> clusters in singlet states at TD-B3LYP-D3(BJ)/6-311++G(d,p), PCM level.

	Orbitals(coefficients)	Electronic transition	Transition Energy(nm)		Oscillator strength(f)	
			Calc.(a)	Expt.	Calc.	Expt.
<b>In CH<sub>3</sub>CN</b>						
S <sub>1</sub>	40→42(0.66302)	n→π*	268.3(269 <sup>a</sup> )		0.0004	
S <sub>2</sub>	<b>41→42(0.68625)</b>	<b>π→π*</b>	245.6(263 <sup>a</sup> )	<b>255</b>	<b>0.1964</b>	<b>0.1324</b>
S <sub>3</sub>	41→43(0.58499)	π→Ryd <sub>1</sub>	239.8(232 <sup>a</sup> )		0.0559	
S <sub>4</sub>	41→44(0.68646)	π→π*	237.4(216 <sup>a</sup> )	222	0.1383	
<b>In CH<sub>3</sub>OH</b>						
S <sub>1</sub>	47→49(0.67053)	n→π*	253.9		0.0021	
S <sub>2</sub>	<b>48→49(0.68233)</b>	<b>π→π*</b>	<b>240.0</b>	<b>251</b>	<b>0.2319</b>	<b>0.1431</b>
S <sub>3</sub>	48→51(0.65948)	π→Ryd <sub>1</sub>	236.0		0.0546	
S <sub>4</sub>	48→50(0.66678)	π→π*	233.1		0.1078	
<b>In H<sub>2</sub>O</b>						
S <sub>1</sub>	39→41(0.66857)	n→π*	253.2(242 <sup>a</sup> )		0.0012	
S <sub>2</sub>	40→42(0.51193)	π→Ryd <sub>1</sub>	241.5(253 <sup>a</sup> )		0.1068	
S <sub>3</sub>	<b>40→41(0.50007)</b>	<b>π→π*</b>	<b>238.4(218<sup>a</sup>)</b>	<b>245</b>	<b>0.1843</b>	<b>0.1032</b>
S <sub>4</sub>	40→43(0.69426)	π→π*	232.5(144 <sup>a</sup> )		0.1162	

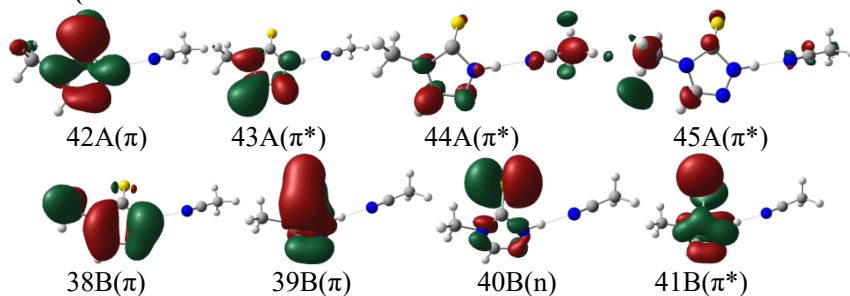
**Table S4.** Calculated and experimental electronic transition energy ( $\Delta E$ , in kcal/mol) and oscillator intensity (f) for 4MMT(CH<sub>3</sub>CN), 4MMT(CH<sub>3</sub>OH)<sub>2</sub> and 4MMT(H<sub>2</sub>O)<sub>2</sub> clusters in triplet states at TD- B3LYP -D3(BJ)/6-311++G(d, p), PCM level.

	Orbitals(coefficients)	Electronic transition	Transition Energy(nm)		Oscillator strength(f)	
			Calc.(a)	Expt.	Calc.	Expt.
<b>In CH<sub>3</sub>CN</b>						
T <sub>2</sub>	42A→43A(0.66264)	π→π*	496.6		0.0559	
	39B→41B(0.74234)	π→π*				
T <sub>3</sub>	<b>42A→43A(0.60196)</b>	<b>π→π*</b>	<b>457.7</b>	<b>470</b>	<b>0.0482</b>	
	<b>39B→41B(0.63109)</b>	<b>π→π*</b>				
T <sub>4</sub>	38B→41B(0.93748)	π→π*	384.1		0.0266	
T <sub>5</sub>	<b>42A→44A(0.72983)</b>	<b>π→π*</b>	<b>368.0</b>	<b>350</b>	<b>0.0266</b>	



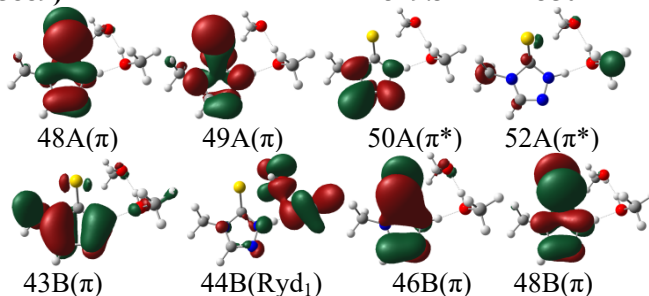
42A → 45A(0.60226

$\pi \rightarrow \pi^*$



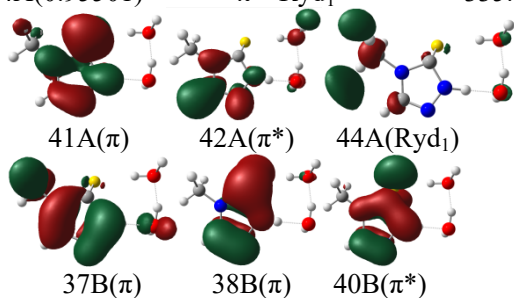
**In CH<sub>3</sub>OH**

T <sub>2</sub>	49A → 50A(0.51168)	$\pi \rightarrow \pi^*$	501.19	0.0653
	46B → 48B(0.81893)	$\pi \rightarrow \pi^*$		
T <sub>3</sub>	49A → 50A(0.73861)	$\pi \rightarrow \pi^*$	459.5	470
	46B → 48B(0.65542)	$\pi \rightarrow \pi^*$		0.0314
T <sub>6</sub>	43B → 48B(0.65542)	$\pi \rightarrow \pi^*$	389.34	0.0130
	44B → 48B(0.65542)	Ryd <sub>1</sub> → $\pi^*$		
T <sub>9</sub>	49A → 52A(0.65889)		329.3	350



**In H<sub>2</sub>O**

T <sub>2</sub>	41A → 42A(0.60086)	$\pi \rightarrow \pi^*$	500.4	0.0703
	38B → 40B(0.82498)	$\pi \rightarrow \pi^*$		
T <sub>3</sub>	38B → 40B(0.51149)	$\pi \rightarrow \pi^*$	457.9	0.0337
T <sub>4</sub>	37B → 40B(0.91099)	$\pi \rightarrow \pi^*$	397.8	0.0221
T <sub>7</sub>	41A → 44A(0.95501)	$\pi \rightarrow$ Ryd <sub>1</sub>	335.0	0.0206



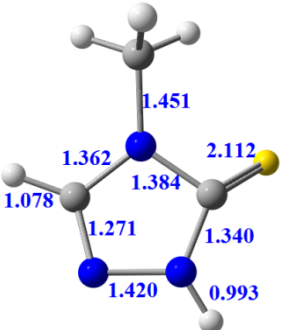
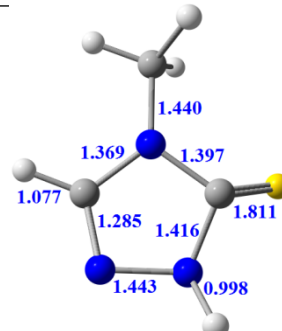
**Table S5.** Optimized bond lengths and angles for different minimum structures ( $S_{2\min}$ ,  $S_{1\min}$ , and  $T_{2\min}$ ), and ISC points( $S_1/T_1$  and  $S_0/T_1$ ) (TD-B3LYP-D3(BJ)/6-311G(d, p) levels with PCM (solvent=acetonitrile) model. (Atom number referred to Figure S1)

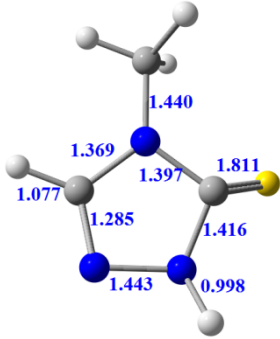
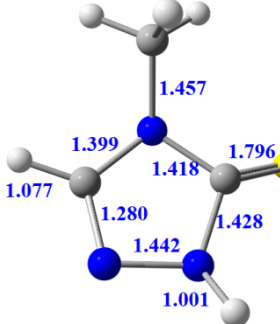
	$d(S_7-C_3-N_2-N_1)$	$C_3=S_7$	$N_1-N_2$	$N_2-H_6$	$N_2-C_3$	$C_3-N_4$	$N_4-C_5$	$N_4-H_8$	$N_1-C_5$	$C_5-H_9$
$S_0$	180.0	1.688	1.367	1.008	1.353	1.374	1.371	1.457	1.300	1.077
$S_{2\min}$	125.0	1.875	1.370	1.007	1.400	1.411	1.358	1.449	1.306	1.078
$S_{1\min}$	125.0	1.874	1.370	1.007	1.400	1.411	1.358	1.449	1.306	1.078
$T_{1\min}$	119.4	1.759	1.357	1.010	1.443	1.446	1.340	1.449	1.319	1.079
$S_1/T_1$	105.8	1.844	1.438	1.028	1.473	1.421	1.412	1.465	1.280	1.081
$S_0/T_1$	165.1	1.648	1.365	1.013	1.404	1.373	1.429	1.456	1.468	1.101

**Table S6.** Optimized Cartesian coordinates and Hartree-Fock energies (a.u.) at CASSCF(12e/9o)/cc-pVDZ level.

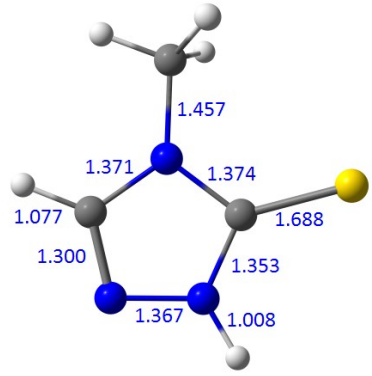
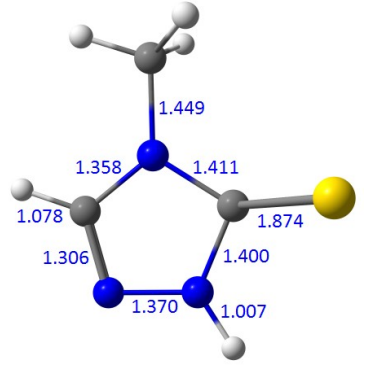
State	HF energy	Structure	Cartesian coordinates			
S <sub>0</sub> , min	-678.46027		C	0.45490073	1.31869935	0.03582096
			C	-0.2345193	-0.7924653	0.0042314
			C	-2.0227182	0.98389392	-0.0094002
			N	-0.6544216	0.50878365	0.0088384
			N	1.47793492	0.42052945	0.04563403
			N	1.05745911	-0.897038	0.02625257
			S	0.53120189	2.96874506	0.05217782
			H	-0.9062152	-1.6311936	-0.0157399
			H	2.44719002	0.63772897	0.06625092
			H	-2.2208185	1.58480666	0.87527623
S <sub>1</sub> , min	-678.33025		C	0.43662423	1.36550339	0.06934993
			C	-0.2218552	-0.7469508	-0.104321
			C	-2.0128661	0.94391418	0.10582193
			N	-0.6673314	0.55645472	-0.2721521
			N	1.5409475	0.47783534	0.02479787
			N	1.04390338	-0.8608563	0.085128
			S	0.66315487	2.91920734	-0.8246342
			H	-0.885243	-1.5916753	-0.1819305
			H	2.26130915	0.61374561	0.70325371
			H	-2.1285983	1.03430148	1.18938889
H	-2.2628298	1.89848109	-0.3538083			
H	-2.714508	0.19994029	-0.2681463			

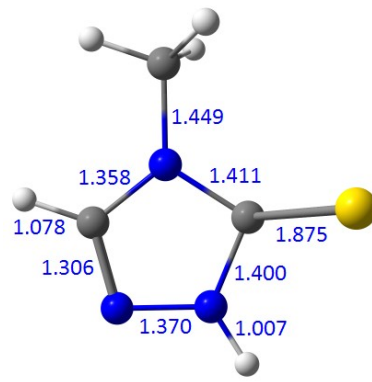
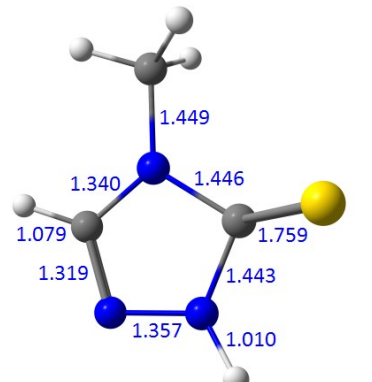
$S_{2, \min}$	-678.30277		<table border="1"> <tbody> <tr><td>C</td><td>0.44911543</td><td>1.26841398</td><td>0.10381955</td></tr> <tr><td>C</td><td>-0.2763262</td><td>-0.7965428</td><td>-0.2710408</td></tr> <tr><td>C</td><td>-2.0261407</td><td>0.97934322</td><td>-0.0409605</td></tr> <tr><td>N</td><td>-0.6728872</td><td>0.50234122</td><td>0.12072973</td></tr> <tr><td>N</td><td>1.4709932</td><td>0.43614435</td><td>-0.0207996</td></tr> <tr><td>N</td><td>1.11959661</td><td>-0.8906101</td><td>-0.1297813</td></tr> <tr><td>S</td><td>0.57730982</td><td>2.97129558</td><td>0.52177361</td></tr> <tr><td>H</td><td>-0.8890154</td><td>-1.6242801</td><td>0.06602354</td></tr> <tr><td>H</td><td>2.43336676</td><td>0.68363335</td><td>0.04458994</td></tr> <tr><td>H</td><td>-2.1455796</td><td>1.93487329</td><td>0.46391402</td></tr> <tr><td>H</td><td>-2.2844743</td><td>1.08867498</td><td>-1.0966267</td></tr> <tr><td>H</td><td>-2.703251</td><td>0.25661413</td><td>0.41110651</td></tr> </tbody> </table>	C	0.44911543	1.26841398	0.10381955	C	-0.2763262	-0.7965428	-0.2710408	C	-2.0261407	0.97934322	-0.0409605	N	-0.6728872	0.50234122	0.12072973	N	1.4709932	0.43614435	-0.0207996	N	1.11959661	-0.8906101	-0.1297813	S	0.57730982	2.97129558	0.52177361	H	-0.8890154	-1.6242801	0.06602354	H	2.43336676	0.68363335	0.04458994	H	-2.1455796	1.93487329	0.46391402	H	-2.2844743	1.08867498	-1.0966267	H	-2.703251	0.25661413	0.41110651
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$T_{1, \min}$	-678.34883		<table border="1"> <tbody> <tr><td>C</td><td>0.43498552</td><td>1.36565477</td><td>0.17526186</td></tr> <tr><td>C</td><td>-0.2246557</td><td>-0.7506409</td><td>-0.0670139</td></tr> <tr><td>C</td><td>-2.0346869</td><td>0.95676349</td><td>0.0954269</td></tr> <tr><td>N</td><td>-0.6662595</td><td>0.54484496</td><td>-0.1199996</td></tr> <tr><td>N</td><td>1.51140897</td><td>0.46902312</td><td>0.0497773</td></tr> <tr><td>N</td><td>1.0575688</td><td>-0.8608862</td><td>0.04749891</td></tr> <tr><td>S</td><td>0.660073</td><td>2.87409471</td><td>-0.79876</td></tr> <tr><td>H</td><td>-0.884069</td><td>-1.5957789</td><td>-0.1647695</td></tr> <tr><td>H</td><td>2.36824395</td><td>0.61799224</td><td>0.53535443</td></tr> <tr><td>H</td><td>-2.2505443</td><td>1.09553107</td><td>1.15720857</td></tr> <tr><td>H</td><td>-2.2154949</td><td>1.893478</td><td>-0.4273543</td></tr> <tr><td>H</td><td>-2.7038626</td><td>0.19982455</td><td>-0.3098826</td></tr> </tbody> </table>	C	0.43498552	1.36565477	0.17526186	C	-0.2246557	-0.7506409	-0.0670139	C	-2.0346869	0.95676349	0.0954269	N	-0.6662595	0.54484496	-0.1199996	N	1.51140897	0.46902312	0.0497773	N	1.0575688	-0.8608862	0.04749891	S	0.660073	2.87409471	-0.79876	H	-0.884069	-1.5957789	-0.1647695	H	2.36824395	0.61799224	0.53535443	H	-2.2505443	1.09553107	1.15720857	H	-2.2154949	1.893478	-0.4273543	H	-2.7038626	0.19982455	-0.3098826
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H	-2.2154949	1.893478	-0.4273543																																																
H	-2.7038626	0.19982455	-0.3098826																																																
$T_{2, \min}$	-678.33552		<table border="1"> <tbody> <tr><td>C</td><td>0.44156691</td><td>1.36698283</td><td>0.07095964</td></tr> <tr><td>C</td><td>-0.2199391</td><td>-0.7476218</td><td>-0.1051957</td></tr> <tr><td>C</td><td>-2.0088144</td><td>0.94689677</td><td>0.10827326</td></tr> <tr><td>N</td><td>-0.6614051</td><td>0.55825329</td><td>-0.2648092</td></tr> <tr><td>N</td><td>1.54110024</td><td>0.47298294</td><td>0.03794874</td></tr> <tr><td>N</td><td>1.04414752</td><td>-0.8621262</td><td>0.09120168</td></tr> </tbody> </table>	C	0.44156691	1.36698283	0.07095964	C	-0.2199391	-0.7476218	-0.1051957	C	-2.0088144	0.94689677	0.10827326	N	-0.6614051	0.55825329	-0.2648092	N	1.54110024	0.47298294	0.03794874	N	1.04414752	-0.8621262	0.09120168																								
C	0.44156691	1.36698283	0.07095964																																																
C	-0.2199391	-0.7476218	-0.1051957																																																
C	-2.0088144	0.94689677	0.10827326																																																
N	-0.6614051	0.55825329	-0.2648092																																																
N	1.54110024	0.47298294	0.03794874																																																
N	1.04414752	-0.8621262	0.09120168																																																

			S	0.62615232	2.91635315	-0.8558438
			H	-0.884069	-1.5957789	-0.1647695
			H	2.36824395	0.61799224	0.53535443
			H	-2.2505443	1.09553107	1.15720857
			H	-2.2154949	1.893478	-0.4273543
			H	-2.7038626	0.19982455	-0.3098826
S <sub>1</sub> /S <sub>2</sub>	-678.31869		C	0.45168082	1.3292891	0.32321865
	-678.32170		C	-0.2030692	-0.7449139	-0.1141762
			C	-2.0301862	0.95525847	0.09706694
			N	-0.6431788	0.53700411	0.02478555
			N	1.44496342	0.43464966	0.42001008
			N	1.04568202	-0.8835734	0.0756995
			S	0.59224607	2.92033234	-1.0588398
			H	-0.861399	-1.5614708	-0.3608926
			H	2.41696307	0.63481342	0.44300777
			H	-2.3909901	0.94538573	1.1262346
			H	-2.1308944	1.96130019	-0.2998493
			H	-2.6391104	0.28182609	-0.5035173
S <sub>2</sub> /T <sub>2</sub>	-678.32362		C	0.43722014	1.34810603	0.30676611
	-678.3299		C	-0.1958307	-0.7411021	-0.1348184
			C	-2.0369535	0.95662896	0.10717846
			N	-0.669823	0.50814568	0.1627594
			N	1.54171128	0.52526558	-0.0219544
			N	1.08408887	-0.8301099	-0.213114
			S	0.61357386	2.88020536	-0.643013
			H	-0.8515648	-1.5857819	-0.2653749
			H	2.3243388	0.54875855	0.59711229
			H	-2.3159988	1.46078795	1.03285272
			H	-2.1876151	1.64248139	-0.730317

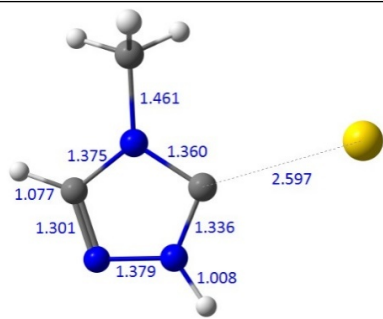
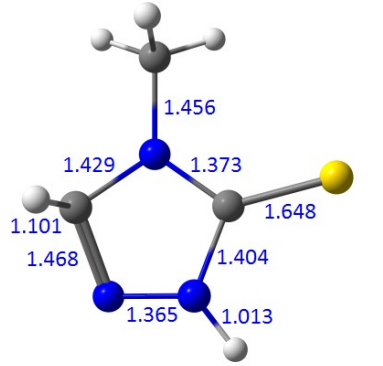
			H	-2.6904397	0.09651539	-0.0253294
S <sub>1</sub> /T <sub>2</sub>	-678.3299		C	0.43722014	1.34810603	0.30676611
	-678.32209		C	-0.1958307	-0.7411021	-0.1348184
T <sub>1</sub> /T <sub>2</sub>	-678.33409		C	-2.0369535	0.95662896	0.10717846
			N	-0.669823	0.50814568	0.1627594
			N	1.54171128	0.52526558	-0.0219544
			N	1.08408887	-0.8301099	-0.213114
			S	0.61357386	2.88020536	-0.643013
			H	-0.8515648	-1.5857819	-0.2653749
			H	2.3243388	0.54875855	0.59711229
			H	-2.3159988	1.46078795	1.03285272
			H	-2.1876151	1.64248139	-0.730317
			H	-2.6904397	0.09651539	-0.0253294
	-678.33473		C	0.43777585	1.38569347	-0.0329063
			C	-0.2184649	-0.7313767	-0.1715402
			C	-1.9858701	0.93346052	0.14918433
			N	-0.6746504	0.57545964	-0.3758382
			N	1.54996351	0.49754473	0.08132909
			N	1.02603108	-0.8458376	0.10392862
			S	0.69117747	2.8691731	-1.0135847
			H	-0.8751793	-1.5782408	-0.281495
			H	2.10561209	0.62543782	0.90367172
			H	-2.0041938	0.96523266	1.24227163
			H	-2.2832535	1.90850943	-0.2320972
			H	-2.7162408	0.20484464	-0.2001759

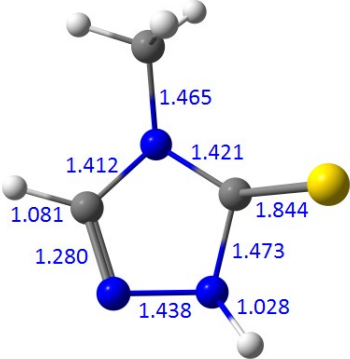
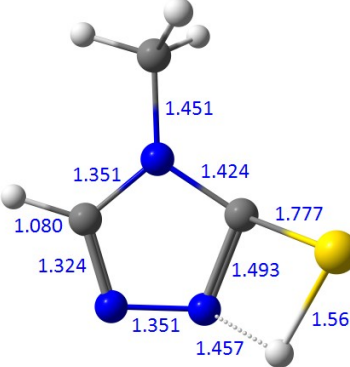
**Table S7.** Optimized Cartesian coordinates and Hartree-Fock energies (a.u.) at (TD-)B3LYP-(D3)BJ/6-311G(d, p) level with PCM acetonitrile model.

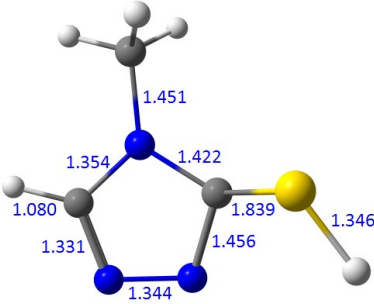
State	H-F energy	Structure	Cartesian coordinates
S <sub>0</sub>	-679.89932840	 <p>d(S-C-N-N): 180.0</p>	N -1.77609500 -1.15252300 0.00000400 N -0.43844100 -1.43621800 0.00001300 C 0.35302500 -0.33916000 -0.00000200 N -0.55435900 0.69313500 -0.00002800 C -1.81204000 0.14707500 -0.00004400 H -0.11801800 -2.39236900 0.00004100 S 2.03857200 -0.24692200 0.00003200 C -0.21071600 2.10863200 -0.00001400 H -2.71271700 0.73817400 -0.00006700 H 0.37379200 2.34491500 -0.88861000 H -1.13277700 2.68493000 -0.00036400 H 0.37321500 2.34506700 0.88892500
S <sub>1min</sub>	-679.76005806	 <p>d(S-C-N-N): 125.0</p>	N 1.38008500 -1.46201600 -0.23532500 N 0.13128300 -1.44340300 0.32745600 C -0.35113800 -0.15927600 0.60767900 N 0.70904400 0.62582900 0.10736000 C 1.68857500 -0.19805900 -0.34696100 H -0.30141500 -2.30942300 0.60322300 S -2.01254900 0.03012800 -0.23869100 C 0.70336200 2.07448200 0.11308000 H 2.62112300 0.16006700 -0.75291000

			H	0.70082400	2.45047300	1.13765800
			H	1.58590600	2.43895000	-0.40827600
			H	-0.19332400	2.43212600	-0.39987100
S <sub>2min</sub>	-679.74743943	 <p>d(S-C-N-N): 125.0</p>	N	1.37925000	-1.46257700	-0.23545800
			N	0.13054400	-1.44342200	0.32774400
			C	-0.35095900	-0.15898200	0.60808200
			N	0.70949400	0.62564000	0.10750300
			C	1.68828300	-0.19878500	-0.34745800
			H	-0.30202000	-2.30920100	0.60449100
			S	-2.01254700	0.03077900	-0.23887400
			C	0.70434700	2.07431900	0.11319500
			H	2.62088300	0.15884600	-0.75374700
			H	0.70180100	2.45029300	1.13776800
			H	1.58711700	2.43846700	-0.40800900
			H	-0.19206500	2.43232700	-0.39995100
T <sub>1min</sub>	-679.78442281	 <p>d(S-C-N-N): 119.4</p>	N	1.37554600	-1.46018400	-0.22836400
			N	0.17296500	-1.47869000	0.40064800
			C	-0.41800800	-0.17041800	0.55020900
			N	0.68694000	0.63366000	0.07885300
			C	1.66166100	-0.17863800	-0.35341700
			H	-0.37547800	-2.32598200	0.35958700
			S	-1.97813800	0.03477200	-0.23687800
			C	0.70310000	2.08112000	0.13654900
			H	2.58737100	0.17949500	-0.77639500
			H	0.72363300	2.41339200	1.17681000

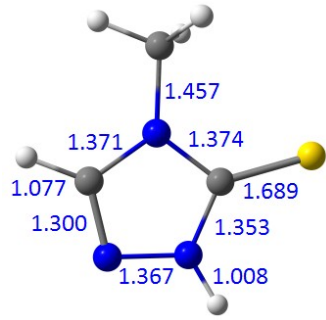
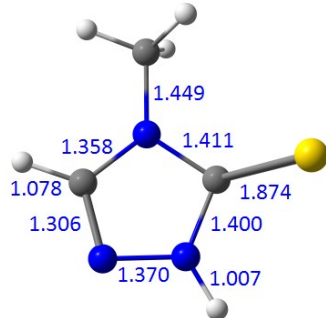


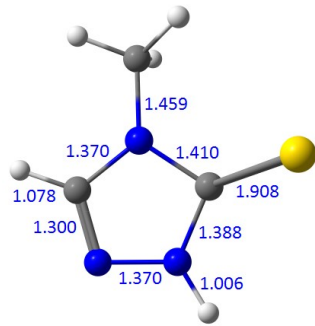
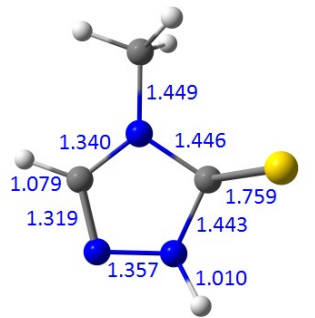
			H 1.58303000 2.45115100 -0.38555500
			H -0.19700800 2.46970900 -0.34241400
T <sub>2min</sub>	-679.7828686	 <p>d(S-C-N-N): 137.1</p>	N 2.00967700 -1.08547300 -0.23717000 N 0.75883900 -1.42224100 0.23563600 C -0.05638200 -0.38831700 0.46279600 N 0.71882100 0.67240000 0.11091500 C 1.94666600 0.21201200 -0.30386500 H 0.54130800 -2.39577600 0.38210500 S -2.57484500 -0.26016100 -0.15778300 C 0.27536800 2.06409400 0.11579900 H 2.74877600 0.85212600 -0.63163400 H -0.30121900 2.25029500 1.01897900 H 1.14671900 2.71574200 0.10124200 H -0.34334600 2.26065900 -0.76021900
S <sub>0</sub> /T <sub>1</sub>	-679.76186289	 <p>d(S-C-N-N): 165.1</p>	N -1.81202200 -1.16914000 -0.33201100 N -0.54312100 -1.42461400 0.10054500 C 0.27219100 -0.29600100 -0.08177600 N -0.60106100 0.74082200 -0.30029300 C -1.88752000 0.24095700 0.06919800 H -0.16014900 -2.35356300 -0.02999400 S 1.91916600 -0.28378700 -0.01935400 C -0.23202500 2.14153100 -0.15440000 H -2.15247800 0.41982100 1.12318100 H 0.74561100 2.30027300 -0.60418700 H -0.97230100 2.74804600 -0.67234000

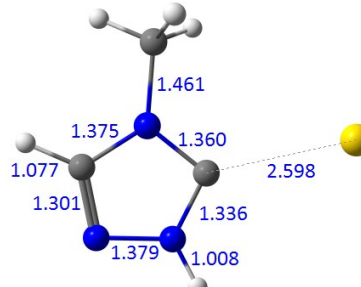
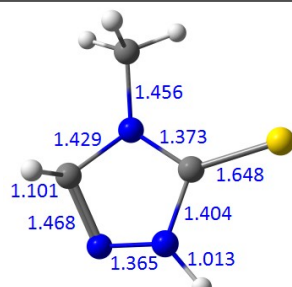
			H	-0.19528900	2.42948000	0.90131800
S <sub>1</sub> /T <sub>1</sub>	-679.74785189	 <p>d(S-C-N-N): 105.8</p>	N	1.24163900	-1.41817300	-0.38780200
			N	0.21441100	-1.55081400	0.61034900
			C	-0.19558800	-0.14243900	0.74667500
			N	0.95708400	0.65832100	0.52658600
			C	1.62722400	-0.19816100	-0.37441600
			H	-0.53535100	-2.12747400	0.20821400
			S	-1.82799200	0.00082300	-0.09878900
			C	0.71715000	2.04822500	0.13038000
			H	2.47405800	0.16300600	-0.94164500
			H	0.40772900	2.62935900	0.99859000
			H	1.64472000	2.46861700	-0.25589600
H	-0.06364400	2.10993300	-0.64564000			
T <sub>1</sub> -TS	-679.72096069	 <p>d(S-C-N-N): 117.4</p>	N	0.47224200	-1.83557800	-0.20322000
			N	-0.55804400	-1.32448800	0.50625100
			C	-0.33908800	0.14759000	0.62969900
			N	0.97968200	0.32423700	0.12185400
			C	1.35786400	-0.86852600	-0.38695600
			S	-1.78860000	0.67634700	-0.25134200
			C	1.69128600	1.58718000	0.06632400
			H	2.29788800	-1.01082500	-0.90005100
			H	1.72754000	2.03010800	1.06267100
			H	2.70501600	1.40882300	-0.28737300
			H	1.18910900	2.27837300	-0.61497100
H	-1.81948200	-0.87469700	-0.06740600			

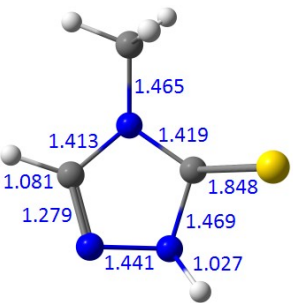
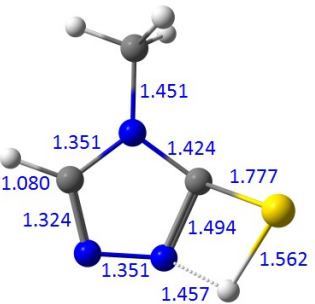
T <sub>1min</sub> '	-679.74663123	 <p data-bbox="761 542 985 574">d(S-C-N-N): 113.5</p>	N	1.19105300	-1.59144900	-0.25326500
			N	0.05887700	-1.57368500	0.47143000
			C	-0.32438400	-0.17689500	0.61536800
			N	0.80087500	0.56694600	0.16631500
			C	1.61719200	-0.34109100	-0.41822800
			S	-1.89391000	0.18844400	-0.27146600
			C	0.89917900	2.01432200	0.13089600
			H	2.51826300	-0.07092000	-0.94827600
			H	0.67681200	2.41853400	1.11871600
			H	1.91215200	2.29455100	-0.15213400
			H	0.19743800	2.43664900	-0.59442300
			H	-2.50965300	-0.88462200	0.25999500

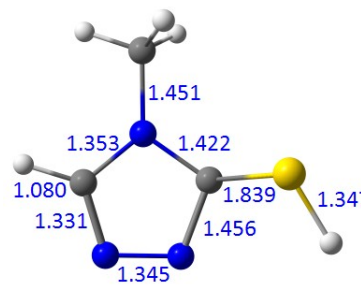
**Table S8.** Optimized Cartesian coordinates and Hartree-Fock energies (a.u.) at (TD-)B3LYP-(D3)BJ/6-311G(d, p) level with PCM  
(solvent=water)model.

State	H-F energy	Structure	Cartesian coordinates			
S <sub>0</sub>	-679.8997099	 <p>d(S-C-N-N): 180.0</p>	N	-1.77570100	-1.15293300	0.00000600
			N	-0.43805400	-1.43632300	0.00001400
			C	0.35270900	-0.33907600	-0.00000300
			N	-0.55457300	0.69299900	-0.00002800
			C	-1.81209900	0.14668700	-0.00004600
			H	-0.11743200	-2.39244600	0.00004300
			S	2.03886400	-0.24652000	0.00003100
			C	-0.21140800	2.10869500	-0.00001300
			H	-2.71287500	0.73757800	-0.00007000
			H	0.37286100	2.34515000	-0.88871200
			H	-1.13357600	2.68471300	-0.00036100
			H	0.37228800	2.34530000	0.88902600
S <sub>1min</sub>	-679.760175520	 <p>d(S-C-N-N): 125.0</p>	N	1.38050200	-1.46161900	-0.23543900
			N	0.13198200	-1.44389500	0.32798400
			C	-0.35130800	-0.15967400	0.60718200
			N	0.70872800	0.62598800	0.10725500
			C	1.68839600	-0.19746000	-0.34749300
			H	-0.30003200	-2.31006400	0.60445000
			S	-2.01259800	0.02987500	-0.23878800
			C	0.70296300	2.07469300	0.11359100
			H	2.62059900	0.16111400	-0.75382500

			H	0.70044300	2.45019700	1.13833500
			H	1.58550000	2.43943400	-0.40753000
			H	-0.19373500	2.43263600	-0.39911400
S <sub>2min</sub>	-679.75441601	 <p>d(S-C-N-N): 121.1</p>	N	1.67728900	-1.19508300	-0.21745100
			N	0.46127900	-1.44338000	0.36285800
			C	-0.30728300	-0.30855300	0.57997800
			N	0.51997500	0.68644000	0.02001500
			C	1.67574400	0.08994700	-0.41126500
			H	0.21818800	-2.38600500	0.61638100
			S	-2.02617700	-0.21656900	-0.24238500
			C	0.33554300	2.12252500	0.20296300
			H	2.48993800	0.63832100	-0.85643100
			H	0.54412700	2.40151400	1.23853800
			H	1.01796600	2.64937700	-0.46125700
			H	-0.68522000	2.40254900	-0.04707600
T <sub>1min</sub>	-679.7846827	 <p>d(S-C-N-N): 119.4</p>	N	1.37501600	-1.46054500	-0.22842900
			N	0.17264900	-1.47893400	0.40081100
			C	-0.41812800	-0.17036000	0.55003300
			N	0.68709100	0.63349500	0.07875300
			C	1.66150100	-0.17886800	-0.35349400
			H	-0.37596800	-2.32614800	0.35962800
			S	-1.97810500	0.03527600	-0.23686600
			C	0.70377700	2.08102800	0.13667200
			H	2.58729000	0.17907900	-0.77643200
			H	0.72385300	2.41296100	1.17702400

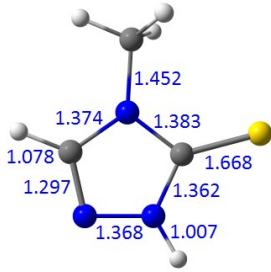
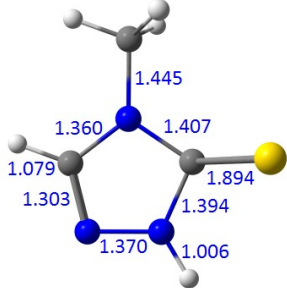
			H	1.58417900	2.45072500	-0.38477500
			H	-0.19585300	2.47005600	-0.34280200
T <sub>2min</sub>	-679.7831993	 <p>d(S-C-N-N): 136.8</p>	N	2.00686300	-1.08762700	-0.23893400
			N	0.75729200	-1.42222700	0.23835500
			C	-0.05598000	-0.38704500	0.46668300
			N	0.71943300	0.67233400	0.11077500
			C	1.94525800	0.21001300	-0.30709500
			H	0.53905000	-2.39530200	0.38706400
			S	-2.57443500	-0.25919600	-0.15908300
			C	0.27840000	2.06481800	0.11720100
			H	2.74705400	0.84873900	-0.63829400
			H	-0.27532900	2.25917800	1.03293800
			H	1.15035900	2.71438800	0.07623500
			H	-0.36134200	2.25605500	-0.74471700
S <sub>0</sub> /T <sub>1</sub>	-679.762029508	 <p>d(S-C-N-N): 165.2</p>	N	-1.81047700	-1.16991800	-0.33511600
			N	-0.54409900	-1.42427300	0.10520800
			C	0.27225000	-0.29626500	-0.07559600
			N	-0.59929700	0.74003200	-0.30247600
			C	-1.88790000	0.24134600	0.06183800
			H	-0.16055400	-2.35382100	-0.01949500
			S	1.91901100	-0.28413500	-0.00321800
			C	-0.23087100	2.14114400	-0.15798400
			H	-2.15793700	0.42297500	1.11396800
			H	0.74836700	2.29915800	-0.60450700
			H	-0.96927300	2.74642200	-0.67997900

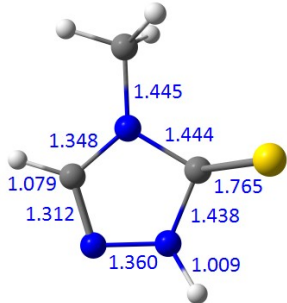
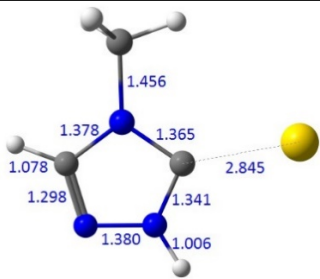
			H	-0.19821700	2.43115900	0.89724400
S <sub>1</sub> /T <sub>1</sub>	-679.749000534	 <p>d(S-C-N-N): 106.4</p>	N	1.24433900	-1.42038000	-0.38624300
			N	0.20955800	-1.54758100	0.60796300
			C	-0.19472800	-0.14225400	0.74992300
			N	0.95527500	0.65689400	0.52349600
			C	1.63028500	-0.20139500	-0.37312200
			H	-0.53938700	-2.12316100	0.20394700
			S	-1.83377300	0.00821000	-0.08935700
			C	0.71772500	2.04699300	0.12757900
			H	2.48027700	0.15925200	-0.93601900
			H	0.40891900	2.62876600	0.99566600
H	1.64580400	2.46616000	-0.25868400			
H	-0.06285300	2.10972000	-0.64854200			
T <sub>1</sub> -TS	-679.7212113	 <p>d(S-C-N-N): 117.3</p>	N	0.47180200	-1.83570000	-0.20310200
			N	-0.55828000	-1.32446400	0.50678700
			C	-0.33892200	0.14794700	0.62965800
			N	0.97958300	0.32405600	0.12130100
			C	1.35744400	-0.86862300	-0.38742500
			S	-1.78865700	0.67672400	-0.25145100
			C	1.69223200	1.58662400	0.06672100
			H	2.29721800	-1.01094700	-0.90093600
			H	1.73057300	2.02773800	1.06377100
			H	2.70509400	1.40794400	-0.28916400
H	1.18925500	2.27918100	-0.61251700			
H	-1.81987900	-0.87442400	-0.06656900			

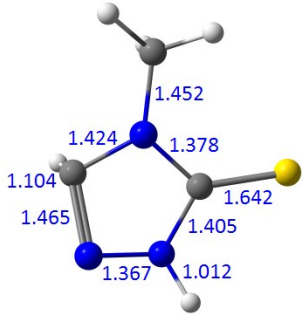
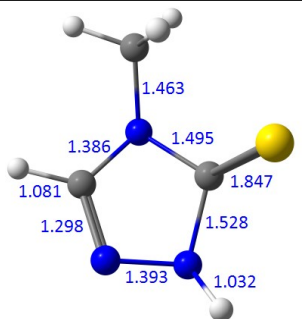
$T_{1min}$	-679.7469643	 <p>d(S-C-N-N): 113.5</p>	N 1.19128700 -1.59143300 -0.25326800 N 0.05889900 -1.57377200 0.47161900 C -0.32453900 -0.17701800 0.61513600 N 0.80063800 0.56683800 0.16578500 C 1.61718800 -0.34090700 -0.41819800 S -1.89389300 0.18840400 -0.27159600 C 0.89934300 2.01433600 0.13123600 H 2.51840200 -0.07056900 -0.94790100 H 0.67794100 2.41787300 1.11952900 H 1.91212900 2.29428800 -0.15259100 H 0.19703900 2.43705200 -0.59322900 H -2.51094800 -0.88299700 0.26172800
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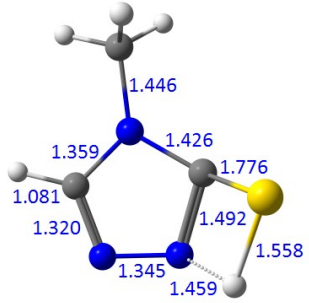
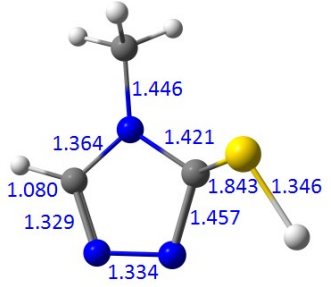


**Table S9.** Optimized Cartesian coordinates and Hartree-Fock energies (a.u.) at (TD-)B3LYP-(D3)BJ/6-311G(d, p) level in vacuum.

State	H-F energy	Structure	Cartesian coordinates			
S <sub>0</sub>	-679.8850049	 <p>d(S-C-N-N): 180.0</p>	N	-1.79733600	-1.12646000	-0.00005100
			N	-0.46296700	-1.42952500	0.00000200
			C	0.35907600	-0.34391000	0.00001700
			N	-0.54516700	0.70313100	-0.00003500
			C	-1.81140700	0.17094600	-0.00002200
			H	-0.15326600	-2.38725300	0.00001800
			S	2.02524100	-0.27276100	0.00005900
			C	-0.16477300	2.10468800	-0.00003200
			H	-2.70714200	0.77039800	-0.00004500
			H	0.43367900	2.32467000	-0.88477900
			H	-1.06935000	2.71115300	-0.00037000
			H	0.43313200	2.32484300	0.88504400
S <sub>1min</sub>	-679.753590536	 <p>d(S-C-N-N): 125.5</p>	N	1.33693000	-1.49133900	-0.23963700
			N	0.08843500	-1.42618000	0.32021900
			C	-0.34161100	-0.13750900	0.63284200
			N	0.73392300	0.61373700	0.12400700
			C	1.68459100	-0.24008300	-0.34291300
			H	-0.36999600	-2.27762600	0.59638600
			S	-2.01053900	0.05960100	-0.24047300
			C	0.74853300	2.05879600	0.09572600
			H	2.63022000	0.08692500	-0.74555700
			H	0.71874000	2.45973300	1.11111500
			H	1.65259600	2.40205700	-0.40537700

			H	-0.12702100	2.41454100	-0.45505000
T <sub>1min</sub>	-679.7745007	 <p>d(S-C-N-N): 119.8</p>	N	1.40462800	-1.43841100	-0.22591200
			N	0.19564800	-1.46986500	0.39520700
			C	-0.41228500	-0.17601400	0.55483900
			N	0.67834000	0.64370400	0.08230900
			C	1.67044100	-0.15945600	-0.34946600
			H	-0.34392200	-2.32096500	0.34866400
			S	-1.97897500	0.00550900	-0.23669300
			C	0.66075500	2.08760900	0.13190900
			H	2.59168100	0.21046200	-0.77279400
			H	0.70333800	2.43329300	1.16848200
H	1.51371400	2.47999500	-0.42111800			
H	-0.26499600	2.44822700	-0.32106500			
T <sub>2min</sub>	-679.75777507	 <p>d(S-C-N-N): 117.7</p>	N	1.97853500	-1.06722400	-0.37662900
			N	0.86276900	-1.39493200	0.36648900
			C	0.06946600	-0.37158000	0.71347000
			N	0.73372800	0.68005100	0.15077900
			C	1.86237200	0.22022800	-0.49327400
			H	0.70725000	-2.36316800	0.59252100
			S	-2.61700700	-0.29041600	-0.22068200
			C	0.26203700	2.05735300	0.17835200
			H	2.56129600	0.85120800	-1.01755900
			H	1.08337900	2.73182400	0.42377600
H	-0.16248900	2.33543300	-0.78822200			

			H	-0.50580700	2.13009900	0.94463800
S <sub>0</sub> /T <sub>1</sub>	-679.755321997	 <p>d(S-C-N-N): 164.3</p>	N	-1.82574000	-1.14201500	0.31946900
			N	-0.55800200	-1.41645900	-0.11094200
			C	0.28083900	-0.30640300	0.08106900
			N	-0.58487300	0.74606100	0.28654200
			C	-1.87931000	0.27029600	-0.06709600
			H	-0.18946300	-2.34759000	0.03720600
			S	1.92233600	-0.32208600	0.04413400
			C	-0.19050700	2.13689100	0.15230200
			H	-2.16488000	0.46917300	-1.11471400
			H	-0.19480800	2.44919800	-0.89870000
H	-0.88921400	2.75290100	0.71645600			
H	0.81334200	2.25995500	0.55408000			
S <sub>1</sub> /T <sub>1</sub>	-679.71160035	 <p>d(S-C-N-N): 93.2</p>	N	1.18414600	-1.40464400	-0.35945700
			N	0.26389400	-1.61959400	0.66390100
			C	-0.20446600	-0.16708900	0.73152000
			N	1.03052200	0.66458300	0.59294000
			C	1.60582800	-0.17677400	-0.34567200
			H	-0.50439300	-2.15949400	0.23531900
			S	-1.68596600	0.23891900	-0.29401200
			C	0.71449800	2.02380400	0.15511600
			H	2.41353100	0.14864800	-0.98659800
			H	0.44847100	2.64270400	1.01116900
H	1.57006000	2.45946900	-0.36296800			

			H	-0.17468300	1.99069200	-0.52465200
T <sub>1</sub> -TS	-679.7116299	 <p>d(S-C-N-N): 117.1</p>	N	0.46930800	-1.83291600	-0.20680300
			N	-0.55610000	-1.32300500	0.49885600
			C	-0.33895100	0.14651500	0.63728600
			N	0.98605000	0.32381700	0.14157700
			C	1.35736300	-0.87328500	-0.38464600
			S	-1.78251100	0.67427400	-0.25301000
			C	1.67825100	1.59009000	0.05675700
			H	2.29363100	-1.01880100	-0.90438200
			H	1.64521700	2.08945600	1.02702200
			H	2.71861000	1.41536600	-0.21818600
			H	1.21553500	2.24152100	-0.69140800
			H	-1.82760300	-0.87112200	-0.05667500
T <sub>1min</sub> '	-679.7343833	 <p>d(S-C-N-N): 113.7</p>	N	1.18589500	-1.58832700	-0.25500000
			N	0.06018000	-1.57120200	0.46110200
			C	-0.31927800	-0.17373800	0.62439100
			N	0.81030900	0.57286400	0.19265600
			C	1.61882700	-0.34181500	-0.41684000
			S	-1.89185200	0.18533400	-0.26656900
			C	0.88259600	2.01494400	0.11494100
			H	2.51590100	-0.07610500	-0.95619900
			H	0.57929000	2.44644800	1.06989600
			H	1.90932300	2.31396300	-0.09672800
			H	0.22999600	2.40932900	-0.67285600

			H	-2.45244500	-0.94867400	0.19473400
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