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| 1 | Supplementary files |
|----|---|
| 2 | Insight into the potential application of CuO_x/CeO_2 catalyst for NO removal by CO: |
| 3 | perspective from the morphology & crystal-plane of CeO_2 |
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1 **1 Experimental section**

1.1 Details of catalytic performance evaluation 2

S_{BET} normalized reaction rates (rs, mol m⁻² s⁻¹) was calculated by the 3

following formula: 4

rs (mol m - 2 s - 1) =
$$\frac{\text{Cin} \times \text{F}}{\text{mcat} \times \text{SBET}} \times \ln(1 - \text{X})$$

Where C_{in} refers to the NO concentration (ppm) in the inlet gas, F (mol s⁻ 6 $^{1})$ is the flow rate, $m_{cat}\left(g\right)$ is the mass of catalyst, $S_{BET}\left(m^{2}\,g^{\text{-1}}\right)$ is the specific 7 surface area calculated via BET method, X is the NO conversion.

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1.2 Calculation of turnover frequency (TOF) 10

TOF value, representing the turnover conversion of single active sites per 11 12 second, was calculated as following equation:

$$TOF = \frac{v \times a}{Vm \times n Cu - surf}$$

Where v is the flow rate of NO (m³ s⁻¹), V_m is the gas molar constant (m³ 14 mol⁻¹), a is the NO conversion at certain temperature (%), $n_{Cu-surf}$ is the 15 ¹⁶ mole number of active Cu atoms on the catalytic surface (mol). Notedly, the NO conversion was controlled below 20% within the whole 17 temperature range to avoid the heat transfer effect (The corresponding data 18 were displayed in Fig. S6 and Table S3). n_{Cu-surf} was calculated as following 19 20 equation:

$$n \operatorname{Cu} - \operatorname{surf} = \frac{\operatorname{NCu} - \operatorname{surf}}{\operatorname{NA}}$$

1 Where $N_{Cu-surf}$ is mole number of active Cu atoms on the catalytic surface 2 and N_A is the Avogadro constant (6.02×10²³ mol⁻¹). Then $N_{Cu-surf}$ was 3 calculated as following equation:

4
$$m_{catal} \times S_{surf} = S_{Cu-surf} + S_{Ce-surf} + S_{O-surf}$$

5 =
$$N_{Cu-surf} \times S_{Cu-single} + N_{Ce-surf} \times S_{Ce-single} + N_{O-surf} \times S_{O-single}$$

- 6 where $m_{catal}(g)$ is the mass of catalyst, $S_{surf}(m^2 g^{-1})$ is the surface area of 7 catalysts by BET method, $S_{Cu-single}(m^2)$, $S_{Ce-single}(m^2)$, and $S_{O-single}(m^2)$ are 8 surface area of single atoms, r (m) is the value of atomic radii.
- 9 The atomic radii employed for Cu, Ce and O are shown as follows:

10
$$r_{Cu} = 1.28 \times 10^{-10} \text{ m}, r_{Ce} = 1.83 \times 10^{-10} \text{ m}, r_{O} = 6.6 \times 10^{-10} \text{ m}$$

11 The relationship between N_{Cu-surf}, N_{Ce-surf}, N_{O-surf} was calculated based on
12 XPS and relevant values were listed in Table S3.

13 **1.3 normalized reaction rate**

NO+CO reaction on the catalyst is recognized as a firstorder reaction with
respect to NO. Assuming the diffusion to be limitation-free, the reaction
rate (r) can be calculated using NO conversion below 20% as

$$r = -\frac{F \times \alpha}{SMn - surf}$$

18 where F is the flow of gaseous molecules (mol s⁻¹), α is the fractional 19 conversion, and S_{Mn-surf} is the surface area of Mn atoms on the surfaces of 20 catalysts (m²). N_{Mn-surf} and S_{Mn-surf} were estimated from the BET and XPS 21 data as reported before¹.

1 1.4 Calculation of apparent activation energy (Ea)

2 The Arrhenius formula (k=A exp (Ea/RT)) was applied to calculate the
3 apparent activation energies (Ea) from the slope of the linear plot of ln(R)
4 versus 1000/T, and use it to analyze the difference in catalytic activity of
5 CuO_x/CeO₂-X catalysts. Ea and k were calculated by the following
6 equation:

$$k = -\frac{V}{w} \times \ln (1 - x)$$

$$k = -\frac{Ea}{RT} + \ln A$$
8

9 k is the reaction rate constant (mol $g^{-1} s^{-1}$), V is the total gas flow (mol 10 s^{-1}), w is the mass of catalyst (g), x is the NO conversion (%), Ea is the 11 apparent activation energy of catalyst (kJ mol⁻¹), R is the gas constant 12 (8.314 J mol⁻¹ K⁻¹), T is the reaction temperature (K) and A is the pre-13 exponential factor (mol $g^{-1} s^{-1}$).

1 2 Figure captions

- 2 Fig. S1 The N₂ selectivity (%) of (a) CuO_x/CeO_2 -H, (b) CuO_x/CeO_2 -T, (c)
- $3 \text{ CuO}_{x}/\text{CeO}_{2}\text{-C}$, (d) CuO_x/CeO₂-F at different GHSV.
- 4 Fig. S2 Resistance tests to $O_2 + H_2O + SO_2$ over CuO_x/CeO_2 -H catalysts at
- 5 270 °C.
- 6 **Fig. S3** XRD patterns of CeO_2 -X.
- 7 Fig. S4 SEM images of CuO_x/CeO₂-H(a), CuO_x/CeO₂-T(b), CuO_x/CeO₂-
- 8 C(c) and CuO_x/CeO₂-F(d).
- 9 Fig. S5 Raman spectra of CeO_2 -X.
- 10 Fig. S6 N₂ adsorption/desorption isotherms (a) and pore size distribution
- 11 (b) of CuO_x/CeO_2 -X catalysts.
- 12 Fig. S7 S_{BET} normalized reaction rates of CuO_x/CeO₂-X catalysts for
- 13 NO+CO reaction.
- 14 Fig. S8 In situ FTIR spectra of NO adsorption on sulfurized CuO_x/CeO₂-
- 15 X at 150 °C.
- 16 Fig. S9 NO conversion in NO+CO reaction over the catalysts. Reaction
- 17 conditions: [NO] = 350 ppm, [CO] = 700 ppm, GHSV=450,000 h⁻¹.
- 18

1 3 Table captions

- 2 Table S1 Catalytic performance of transition metal oxide Reported in the
- 3 Literature.
- 4 Table S2 The surface areas, pore diameter, pore volume and lattice.
- 5 Table S3 TOF parameter information of CuO_x/CeO₂-H, CuO_x/CeO₂-T,
- 6 CuO_x/CeO_2 -C(c) and CuO_x/CeO₂-F catalysts.
- 7

1 Figure:

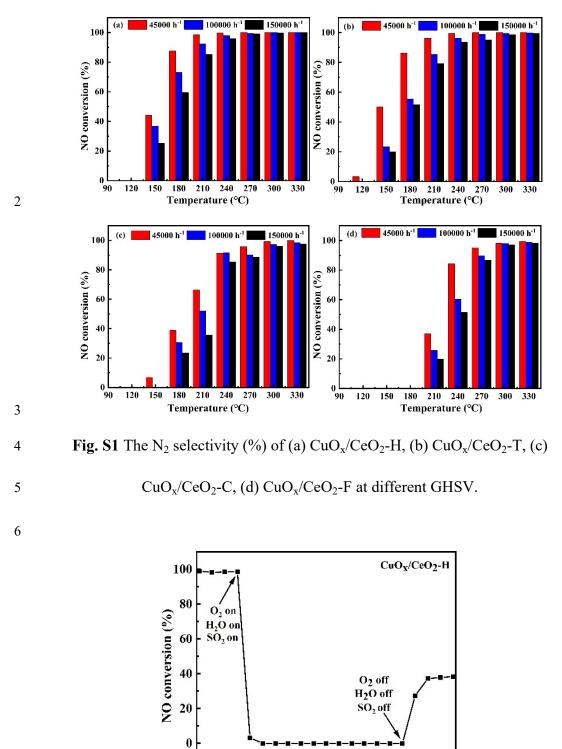


Fig. S2 Resistance tests to $O_2 + H_2O + SO_2$ over CuO_x/CeO_2 -H catalysts at 270 °C.

 Time (h)

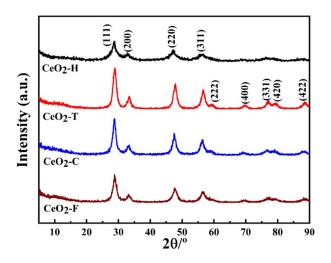


Fig S3 XRD patterns of CeO₂-X supports.

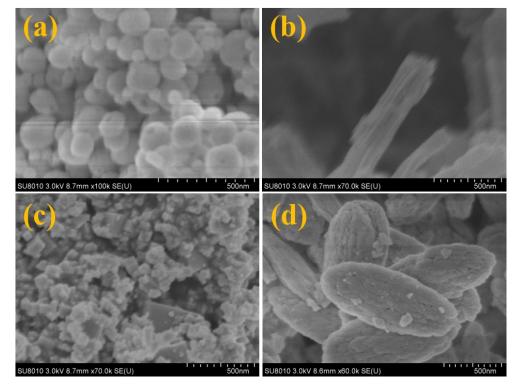
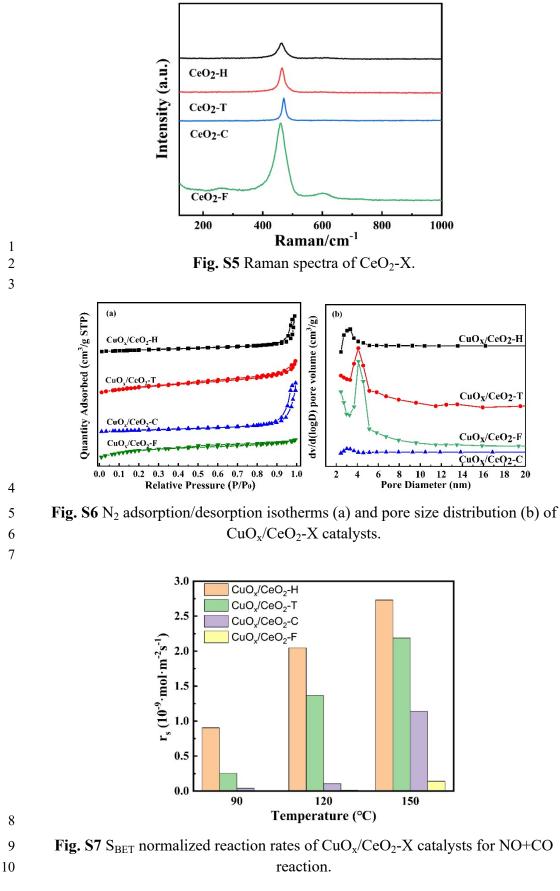


Fig. S4 SEM images of CuO_x/CeO_2 -H(a), CuO_x/CeO_2 -T(b), CuO_x/CeO_2 -C(c), and CuO_x/CeO_2 -F(d).



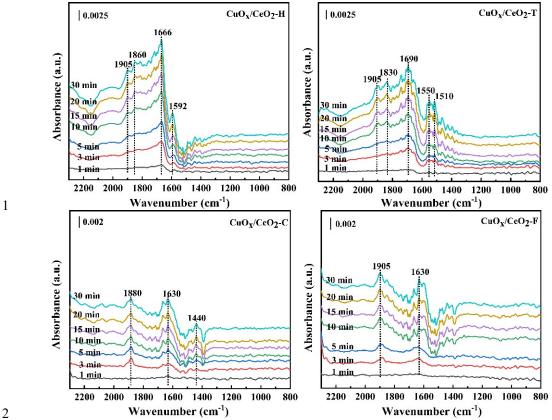
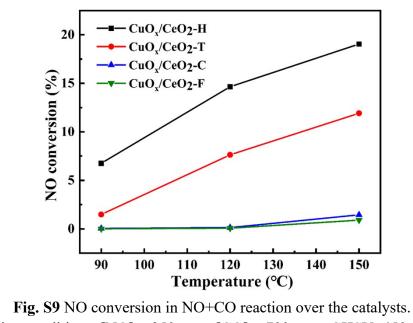


Fig. S8 In situ FTIR spectra of NO adsorption on sulfurized CuO_x/CeO₂-X at 150 °C. 3

As shown in Fig. S8, the peaks located at 1860, 1905 cm⁻¹ 4 (CuO_x/CeO_2-H) , 1830, 1905 cm⁻¹ (CuO_x/CeO₂-T), 1880 cm⁻¹ (CuO_x/CeO₂-5 C) and 1905 cm⁻¹ (CuO_x/CeO₂-F) are attributed to the gaseous NO/ weak 6 adsorption of NO on Cu⁺ or Cu²⁺. The bands located at 1666 cm⁻¹ 7 (CuO_x/CeO₂-H) and 1690 cm⁻¹ (CuO_x/CeO₂-T) correspond to bridged 8 nitrate. The peaks located at 1630 cm⁻¹ (CuO_x/CeO₂-C, CuO_x/CeO₂-F) can 9 be attributed to vibration modes of bridging bidentate nitrates ²⁻⁷. The bands 10 at 1592 cm⁻¹ (CuO_x/CeO₂-H) and 1550 cm⁻¹ (CuO_x/CeO₂-T) are coincided 11 with the chelating bidentate nitrates. While two bands at 1510 cm⁻¹ 12 (CuO_x/CeO_2-T) and 1440 cm⁻¹ (CuO_x/CeO_2-C) correspond to monodentate 13 14 nitrates and linear monodentate nitrites, respectively. From Fig. S6, it is

discovered that the peak strength of CuO_x/CeO₂-H and CuO_x/CeO₂-T is
slightly higher than that of CuO_x/CeO₂-C and CuO_x/CeO₂-F. The results
indicate that CuO_x/CeO₂-H and CuO_x/CeO₂-T can effectively alleviate the
competitive adsorption between NO and SO₂.





8 Reaction conditions: [NO] = 350 ppm, [CO] = 700 ppm, GHSV=450,000 h⁻¹.

9

6

1 Table:

| | Reaction conditions | | | | | | |
|---|---------------------------|---|-------------|-------------|-----------------|------------------|---------|
| Catalyst | Temperature range (°C) | GHSV or WHSV | NO (ppm) | CO (ppm) | T ₅₀ | T _{max} | Ref. |
| MnO _x /TiO ₂ | 200 | 50,000h-1 | 400 | 400 | \ | 200 | 8 |
| Cu-Ce/CNT | 140-260 | 12,600 h ⁻¹ | 250 | 5000 | 170 | 240 | 9 |
| NiO-CeO ₂ | 100-300 | 9000 ml g^{-1} h^{-1} | 2.5% | 5% | 135 | 175 | 10 |
| Fe/TiO ₂ | 150-500 | 75,000 h ⁻¹ | 5000 | 5000 | 470 | 500 | 11 |
| CuO/ZrO ₂ | 100-450 | 12,000 h ⁻¹ | 5% | 10% | 250 | 450 | 12 |
| Cu/TiO ₂ - CeO ₂ | 150-400 | 24,000 ml g ⁻¹ h ⁻¹ | 5% | 10% | 220 | 310 | 13 |
| CuO/CeO ₂ | 100-200 | 12,000 h ⁻¹ | 5% | 10% | \ | 200 | 14 |
| Cu/CeO ₂ | 100-325 | 15,000 ml g ⁻¹ h ⁻¹ | 5% | 10% | 135 | 300 | 15 |
| CuO/CeO ₂ | 100-330 | 24,000 ml g ⁻¹ h ⁻¹ | 5% | 10% | 175 | 300 | 16 |
| CuO/CeO ₂ | 100-400 | 12,000 ml g ⁻¹ h ⁻¹ | 5% | 10% | 150 | 400 | 17 |
| Cu/CeO ₂ | 150-400 | 32,000 h ⁻¹ | 5000 | 5000 | ١ | 300 | 18 |
| CuO/CeO ₂ | 50-300 | 36,000 ml g ⁻¹ h ⁻¹ | 1 vol% | 1 vol% | 105 | 200 | 19 |
| CuO _x /CeO ₂ -H | 90-330 | 45,000 h ⁻¹ | 350 | 700 | 102 | 270 | This wo |

2 Table S1 Catalytic performance of transition metal oxide Reported in the Literature.

3 GHSV means gaseous hourly space velocity (h⁻¹)

4 WHSV means weight hourly space velocity (ml g⁻¹ h⁻¹)

 T_{50} represents the temperature when the efficiency is 50%

- T_{max} represents the temperature when the efficiency is maximum

| 3 | supports. | | | | | | |
|---|---------------------|-----------------|----------------------------|--------------------------|---------------|--|--|
| | Catalyata | $S_{BET}{}^{a}$ | Pore diameter ^b | Pore volume ^c | Lattice | | |
| | Catalysts | (m^{2}/g) | (nm) | (cm^{3}/g) | parameter (Å) | | |
| | CeO ₂ -H | 29 | 11 | 0.1 | 5.46 | | |
| | CeO ₂ -T | 85 | 7 | 0.1 | 5.37 | | |
| | CeO ₂ -C | 20 | 26 | 0.1 | 5.38 | | |
| | CeO ₂ -F | 125 | 4 | 0.1 | 5.41 | | |

Table S2 The surface areas, pore diameter, pore volume and lattice parameter of

4 ^a Calculated by BET method ^{b,c} Calculated by BJH formula

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Table S3 TOF parameter information of CuOx/CeO2-X catalysts.

| C + 1 + | Mass (g) | $S_{BET} (m^2 \cdot g^{-1})$ – | Normalized ratio of each element | | | |
|---------------------------------------|----------|--------------------------------|----------------------------------|------|-------|--|
| Catalysts | | | Cu | Ce | Ο | |
| CuO _x /CeO ₂ -H | 0.04 | 112 | 1.00 | 2.84 | 10.27 | |
| CuO _x /CeO ₂ -T | 0.04 | 84 | 1.00 | 3.50 | 11.37 | |
| CuO _x /CeO ₂ -C | 0.04 | 19 | 1.00 | 1.74 | 6.49 | |
| CuO _x /CeO ₂ -F | 0.04 | 92 | 1.00 | 2.66 | 10.65 | |

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