

Supporting Information

Engineering 3D structure Mn/YTiO_x nanotube catalyst with an efficient H₂O and SO₂ tolerance for low temperature selective catalytic reduction of NO with NH₃

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26 **Experimental section**

27 **Catalysts characterization**

28 The crystal structure of samples were analyzed by the powder X-ray diffraction
29 (XRD) patterns in a 2θ range of $10\text{--}60^\circ$ at a scanning speed of $0.02^\circ\cdot\text{s}^{-1}$ using an X-ray
30 diffractometer (Rigaku Smartlab-SE, Japan) employing Cu $K\alpha$ radiation ($\lambda=1.5404\text{ \AA}$).
31 Raman spectra were collected by LabRAM HR Evolution Raman spectrometer
32 (HORIBA Jobin Yvon SAS, France) with a 532 nm laser. The Brunauer-Emmett-Teller
33 (BET) surface areas and pore structure characteristics were obtained through N_2
34 adsorption-desorption experiment using a physisorption analyzer (Micromeritics ASAP
35 2020, USA) at liquid nitrogen temperature ($-196\text{ }^\circ\text{C}$) using N_2 as the probe molecule.
36 H_2 -temperature programmed reduction (H_2 -TPR) and NH_3 -temperature programmed
37 desorption (NH_3 -TPD) experiments were determined on a multifunctional automatic
38 chemical adsorption apparatus (Xianquan TP-5080, China), equipped with thermal
39 conductivity detector (TCD). For H_2 -TPR experiment, 50 mg sample was firstly
40 pretreated at $300\text{ }^\circ\text{C}$ in a flow of Ar for 1 h, then cooled down to $30\text{ }^\circ\text{C}$. Subsequently,
41 the samples were heated from $30\text{ }^\circ\text{C}$ to $700\text{ }^\circ\text{C}$ at a rate of $10\text{ }^\circ\text{C min}^{-1}$ in a mixture of
42 5% H_2/N_2 (100 mL min^{-1}) and the corresponding TPD curve was collected. For NH_3 -
43 TPD experiment, the samples were also preheated at $300\text{ }^\circ\text{C}$ in a flow of Ar for 1 h prior
44 to the measurement, then cooled down to $100\text{ }^\circ\text{C}$. Subsequently, the samples were
45 exposed to a mixture of 5% NH_3/N_2 for 30 min at $100\text{ }^\circ\text{C}$, then purged with N_2 to
46 remove surface physisorbed NH_3 . Finally, the samples were heated from $100\text{ }^\circ\text{C}$ to 700
47 $^\circ\text{C}$ at a rate of $10\text{ }^\circ\text{C min}^{-1}$, and the corresponding TPD profile was recorded. The

48 morphology and structure of the samples was observed by transmission electron
49 microscopy (TEM, JEOL JEM-2010). The X-ray photoelectron spectroscopy (XPS)
50 measurement were recorded by a VG ESCALAB 210 Spectrometer using an Al K α
51 source ($h\nu=1486.6$ eV) radiation. The binding energy of C 1s at 284.6 eV was used as
52 the standard for calibration of the spectrum of O, Mn, Ti and Y.

53 In situ diffuse reflectance infrared Fourier transform (DRIFT) spectroscopy was
54 used to investigate the surface species involved in NO_x selectivity reduction over
55 Mn/3%YTiO_x catalysts using a Fourier transform infrared spectrometer (VERTEX 70)
56 equipped with a high temperature reaction chamber (HVC, harrick) and liquid nitrogen-
57 cooled HgCdTe (MCT) detector. The spectra were measured by the parameter of 64
58 scans at a resolution of 4 cm⁻¹. The catalyst was firstly pretreated at 300 °C for 30 min
59 using flowing 30 mL/min N₂. When the catalyst was cooled to 50 °C, the background
60 spectrum was recorded in the flow of N₂ and was automatically subtracted from
61 spectrum collected in subsequent tests. The adsorption experiments of NH₃ or NO+O₂
62 were performed by exposing the catalyst to 1 vol% NH₃ or 1 vol% NO+O₂ at 50 °C for
63 30 min and followed by purging with N₂. Afterwards, the desorption spectra of catalyst
64 was collected with ramping temperatures. In the case of the transient reactions, the
65 catalyst was exposed to the reaction gases (1 vol% NH₃ or 1 vol% NO+O₂) at 180 °C
66 for 30 min, another reaction gas (1 vol% NO+O₂ or 1 vol% NH₃) was then switched
67 onto the catalyst surface accordingly, and meanwhile the spectra were recorded with
68 different reaction times.

70 Catalytic performance evaluation

71 The catalytic performance of all catalysts for NH₃-SCR reaction was performed
72 on a fix-bed reactor with a stainless steel tubular reactor of 1.2 cm inner diameter under
73 atmospheric pressure. 0.4 g catalyst (40-60 mesh) was mixed with 0.6 g silica sand and
74 placed in the reactor between two quartz wool plugs. The reactor temperature was
75 controlled using an electric tubular furnace regulated by a temperature controller. The
76 total flow of the simulated gas, which consisted of 500 ppm NO, 500 ppm NH₃, 5 vol%
77 O₂, 5 vol% H₂O (when used), and 100 ppm SO₂ (when used) balanced with N₂, was
78 kept as 200 mL·min⁻¹, and the corresponding gas hourly space velocity (GHSV) was
79 calculated to be 30,000 h⁻¹. The flue gas analyzer (Kane, KM9106) was used to detect
80 the inlet and outlet concentration of NO_x. All data were obtained when the SCR reaction
81 reached a steady state at each temperature. The NO conversion and N₂ selectivity were
82 calculated using Eqs. (1) and (2).

$$83 \text{ NO}_x \text{ conversion (\%)} = \frac{[\text{NO}_x]_{\text{in}} - [\text{NO}_x]_{\text{out}}}{[\text{NO}_x]_{\text{in}}} \times 100\% \quad (1)$$

$$84 \text{ N}_2 \text{ selectivity (\%)} = 1 - \frac{2[\text{N}_2\text{O}]_{\text{out}} + [\text{NO}_2]_{\text{out}}}{[\text{NH}_3]_{\text{in}} + [\text{NO}_x]_{\text{in}} - [\text{NH}_3]_{\text{out}} - [\text{NO}_x]_{\text{out}}} \times 100\% \quad (2)$$

85 Where NO_x represents the total concentration of NO and NO₂. [NO_x]_{out}, [NO_x]_{out},
86 [NH₃]_{in}, [NH₃]_{out}, [N₂O]_{out} and [NO₂]_{out} represent the corresponding concentrations of
87 the inlet and outlet gases, respectively.

88 Kinetics studies were performed to investigate the intrinsic catalytic activity, we
89 calculated the reaction rate and apparent activation energy of Mn/TiO₂-NT,
90 Mn/1%YTiO_x, Mn/3%YTiO_x and Mn/5%YTiO_x, where the NO conversion was kept

91 below 40% (in order to ensure that all of the catalytic active sites were at operational
 92 states). The specific reaction rates based on the catalyst's mass (R_m) and specific surface
 93 area (R_s) can be calculated according to the following equations, as shown in Eqs.(3-4):

$$94 \quad R_m (\text{mol} \cdot \text{g}^{-1} \cdot \text{s}^{-1}) = \text{GHSV} (\text{mL} \cdot \text{h}^{-1} \cdot \text{g}^{-1}) \times \frac{1}{3600} (\text{h} \cdot \text{s}^{-1}) \times \frac{1}{1000} (\text{L} \cdot \text{mL}^{-1}) \times$$

$$C_{\text{NO}} \times X_{\text{NO}} \times \frac{1}{22.4} (\text{mol} \cdot \text{L}^{-1}) \quad (3)$$

$$95 \quad R_s (\text{mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}) = R_m (\text{mol} \cdot \text{g}^{-1} \cdot \text{s}^{-1}) \times \frac{1}{S_{\text{BET}}} (\text{g} \cdot \text{m}^{-2}) \quad (4)$$

96 Where, GHSV is the air velocity, C_{NO} is the concentration of NO and X_{NO} is the
 97 conversion of NO.

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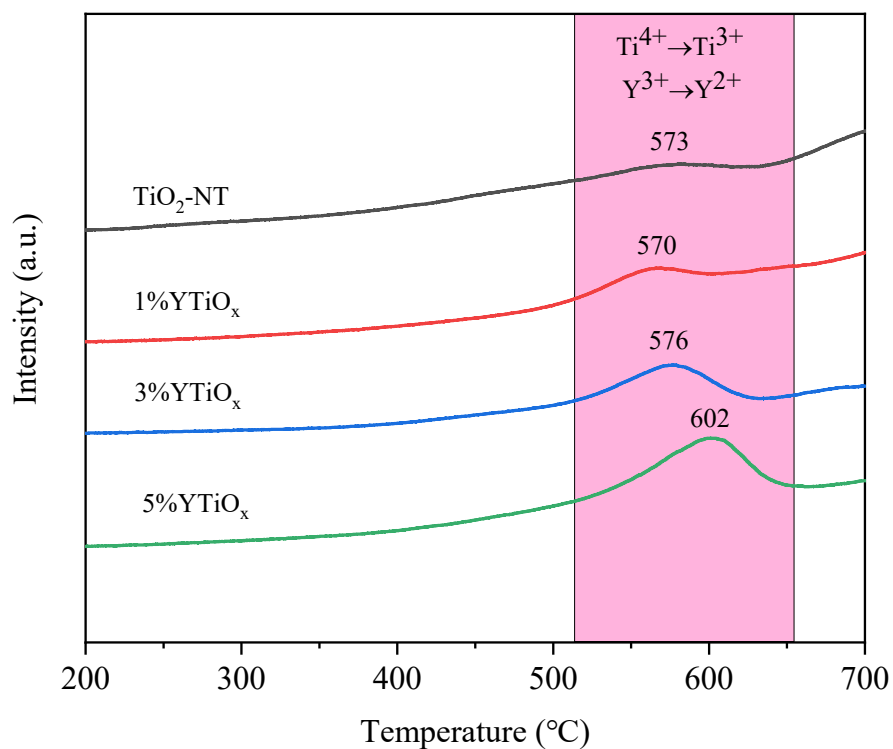
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116 Results and discussion

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119 Fig. S1. H₂-TPR profiles of TiO₂-NT and Y-doped TiO₂.

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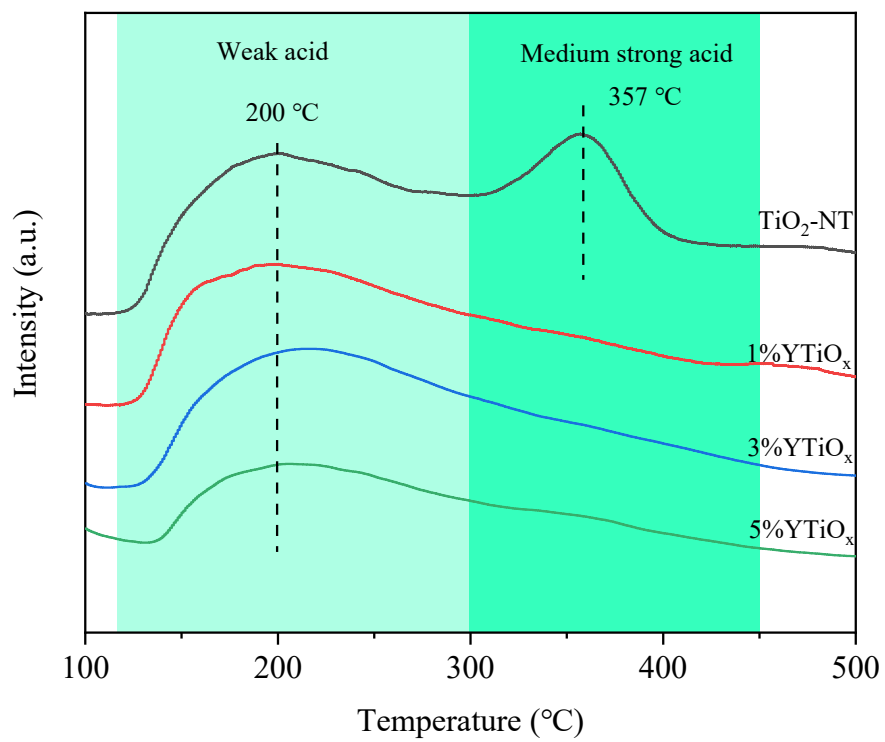
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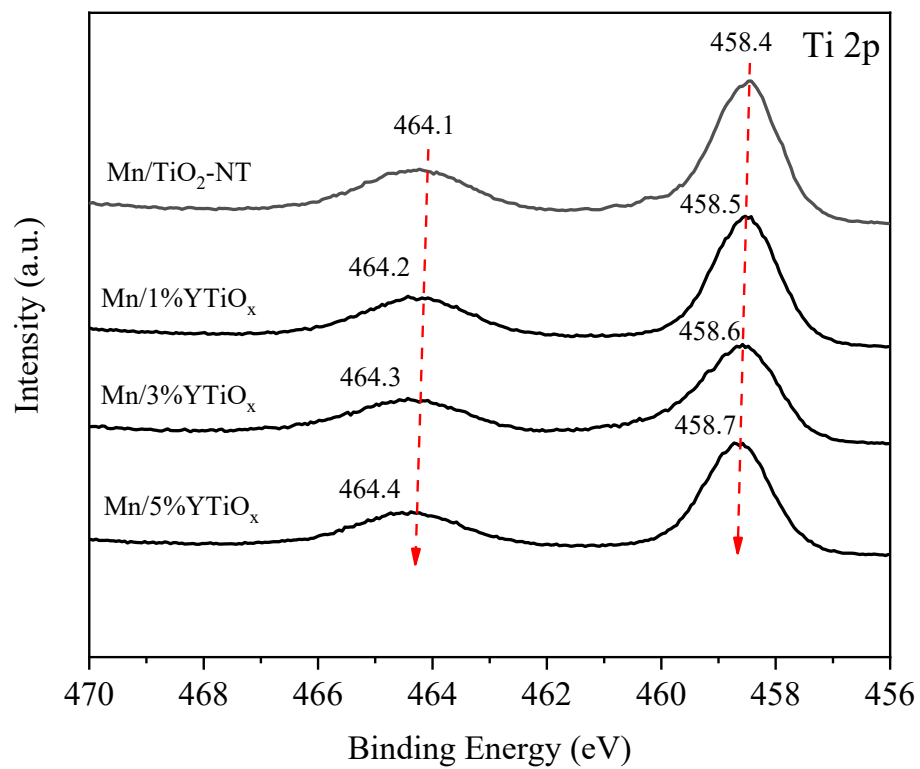
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Fig. S2. NH_3 -TPD profiles of TiO_2 -NT and Y-doped TiO_2 .

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138 Fig. S3. Ti 2p XPS spectra of Mn/TiO₂-NT and Y-doped TiO₂ supported MnO_x

139 catalysts.

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Table S1 Composition and proportion of surface elements of Mn/TiO₂-NT and Y-doped TiO₂ supported MnO_x catalysts.

Catalysts	Atom concentration (%)				Atom ratio		Mn 2p (eV)			Y 3d (eV)		O 1s (eV)	
	Mn	Y	Ti	O	Mn/Ti	Y/Ti	Mn ⁴⁺	Mn ³⁺	Mn ²⁺	Y ³⁺	Y ²⁺	O _α	O _β
Mn/TiO ₂ -NT	3.5	-	27.5	69.0	0.13	-	643.0	641.6	640.7	157.7	156.9	531.0	529.9
Mn/1%YTiO _x	3.7	0.3	28.0	68.0	0.13	0.01	643.0	641.6	640.7	157.7	156.9	531.0	529.9
Mn/3%YTiO _x	3.5	0.9	26.4	69.0	0.13	0.03	643.0	641.6	640.7	157.7	156.9	531.0	529.9
Mn/5%YTiO _x	3.9	1.5	26.9	67.6	0.14	0.05	643.0	641.6	640.7	157.7	156.9	531.0	530.0