# Electronic Supplementary Information (ESI) 

# Facile Strategy to Incorporate Amidoxime Groups into Elastomers toward Self-Crosslinking and Self-Reinforcement 

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## Equilibrium swelling experiments.

Total crosslinking density was determined by equilibrium swelling experiments. The vulcanizates were immersed in toluene at room temperature for 72 h . Then, the samples were removed from the solvent, and immediately weighed after wiping off the surface residual toluene, and then dried in a vacuum oven at $60^{\circ} \mathrm{C}$ until a constant weight. The sol fraction is calculated according to $\left(\mathrm{m}_{0}-\mathrm{m}_{2}\right) / \mathrm{m}_{0}$, and the swelling ratio is defined as $\left(\mathrm{m}_{1}-\mathrm{m}_{2}\right) / \mathrm{m}_{2}$, where $\mathrm{m}_{0}$ is the weight of the sample before swelling, and $\mathrm{m}_{1}$ and $\mathrm{m}_{2}$ are the sample masses before and after drying, respectively. The crosslinking density was determined by the classical Flory-Rehner equation.

$$
V_{e}=-\frac{\ln \left(1-V_{r}\right)+V_{r}+\chi V_{r}^{2}}{\mathrm{~V}_{\mathrm{s}}\left(V_{r}^{\frac{1}{3}}-\frac{V_{r}}{2}\right)}
$$

$V_{r}$ is the volume fraction of rubber in the swollen gel, $V_{s}$ is the molar volume of the solvent ( $106.5 \mathrm{~cm}^{3} / \mathrm{mol}$ for toluene), and $\chi$ is the Flory-Huggins solvent-polymer interaction parameter and is calculated as below:
$\chi=0.487+0.228 * V_{r}$
$V_{r}$ was calculated according to the equation below:
$V_{r}=-\frac{\left(m_{2}-m_{0} \varphi\right) / \rho_{r}}{\frac{\left(m_{2}-m_{0} \varphi\right)}{\rho_{r}}+\frac{\left(m_{1}-m_{2}\right)}{\rho_{s}}}$
$\varphi$ is the weight fraction of the insoluble components (in this system it should be considered as 0 ), and ${ }^{\rho_{r}}$ and ${ }^{\rho_{s}}$ are the density of rubber and solvent, respectively.

Covalent crosslinking density was determined by equilibrium swelling experiments as well. The vulcanizates were immersed in dichloroacetic acid/toluene solution (volume ratio 1:4) at room temperature for 72 h (replace the solution every 24 hours). ${ }^{1}$ The subsequent processing and calculation methods are consistent with total crosslinking density.

Table S1. Mechanical properties of virgin NBR and AO-NBR

| Samples | Stress at <br> $100 \%(\mathrm{MPa})$ | Stress at $300 \%$ <br> $(\mathrm{MPa})$ | Tensile <br> Stress (MPa) | Elongation at <br> break (\%) |
| :---: | :---: | :---: | :---: | :---: |
| Virgin NBR | 0.5 | 0.4 | 0.5 | 1825 |
| AO-NBR-2 | 0.7 | 0.7 | 1.6 | 1818 |
| AO-NBR-5 | 0.9 | 1.0 | 2.5 | 1152 |
| AO-NBR-10 | 1.3 | 2.1 | 5.3 | 650 |
| AO-NBR-15 | 1.3 | 2.4 | 5.6 | 608 |



Fig S1. ${ }^{1} \mathrm{H}$ NMR spectrum of BAO.


Fig S2. ${ }^{1} \mathrm{H}$ NMR spectrum of BN


Fig S3. ${ }^{1} \mathrm{H}$ NMR spectrum of the mixture of BAO and BN at $160^{\circ} \mathrm{C}$ for 2 h .


Fig S4. ${ }^{13} \mathrm{C}$ NMR spectrum of BAO.


Fig S5. ${ }^{13} \mathrm{C}$ NMR spectrum of BN


Fig S6. ${ }^{13} \mathrm{C}$ NMR spectrum of the mixture of BAO and BN at $160{ }^{\circ} \mathrm{C}$ for 2 h .


Fig S7. ${ }^{1} \mathrm{H}$ NMR spectrum of BAO at $160{ }^{\circ} \mathrm{C}$ for 2 h .


Fig S8. ${ }^{13} \mathrm{C}$ NMR spectrum of BAO at $160{ }^{\circ} \mathrm{C}$ for 2 h .


Fig S9. mass spectrum of the mixture of BAO and BN at $160^{\circ} \mathrm{C}$ for 2 h


Scheme S1. Schematic illustration of the chemical reaction between BAO and BN.

Table S2. Mechanical properties of AO-NBR- $d$ with different amidoxime concentration and molding time

| Samples | Stress at 100\% <br> $(\mathrm{MPa})$ | Stress at 300\% <br> $(\mathrm{MPa})$ | Tensile Strength <br> $(\mathrm{MPa})$ | Elongation at <br> break (\%) |
| :---: | :---: | :---: | :---: | :---: |
| AO-NBR-5- $d-30$ <br> min | 1.9 | 5.4 | 5.9 | 326 |
| D-AO-NBR-10- <br> $d-30$ min | 6.6 | - | 20.7 | 259 |
| D-AO-NBR-15- <br> $d-30$ min | 14.4 | - | $16.8(\mathrm{Yield})$ | 133 |
| D-AO-NBR-10- <br> $d-20$ min | 5.2 | - | 16.6 | 270 |
| D-AO-NBR-10- <br> $d-40$ min | 8.7 | - | 16.4 | 173 |



Fig. S10. Calculated hysteresis energy through first tensile cycle with AO-NBR- $d$, (a) with different molding time, (b) with various amidoxime concentration.

Table S3. Mechanical properties of T-AO-NBR nanocomposites with different amidoxime degree and $\mathrm{Zn}(\mathrm{Ac})_{2}$ content

|  | Stress at <br> $100 \%$ <br> $(\mathrm{MPa})$ | Stress at <br> $300 \%$ <br> $(\mathrm{MPa})$ | Tensile <br> Sampless <br> $(\mathrm{MPa})$ | Elongation at <br> break <br> $(\%)$ |
| :---: | :---: | :---: | :---: | :---: |
| AO-NBR- $t-0.5 \mathrm{Zn}$ | 2.9 | 7.0 | 19.9 | 605 |
| AO-NBR- $t-1 \mathrm{Zn}$ | 3.1 | 8.6 | 25.2 | 579 |
| AO-NBR- $t-2 \mathrm{Zn}$ | 6.0 | 15.2 | 28.3 | 447 |
| AO-NBR-5-t-Zn | 3.2 | 8.8 | 12.4 | 408 |
| AO-NBR- $15-t-\mathrm{Zn}$ | - | - | Yield (33.1) | 70 |



Fig. S11. Calculated hysteresis energy through first tensile cycle with AO-NBR- $t-\mathrm{Zn}$ (a) with different Zn contents, (b) with various amidoxime concentration; (c) Hysteresis energy comparison between AO-NBR- $d$ and AO-NBR- $t-\mathrm{Zn}$.

1. J. Liu, S. Wang, Z. Tang, J. Huang, B. Guo and G. Huang, Macromolecules, 2016, 49, 8593-8604.
