

## Supporting Information

### Photoluminescence and energy transfer mechanisms of $\text{Tm}^{3+}$ doped $\text{Y}_2\text{O}_3$ laser crystals: Experimental and theoretical insights

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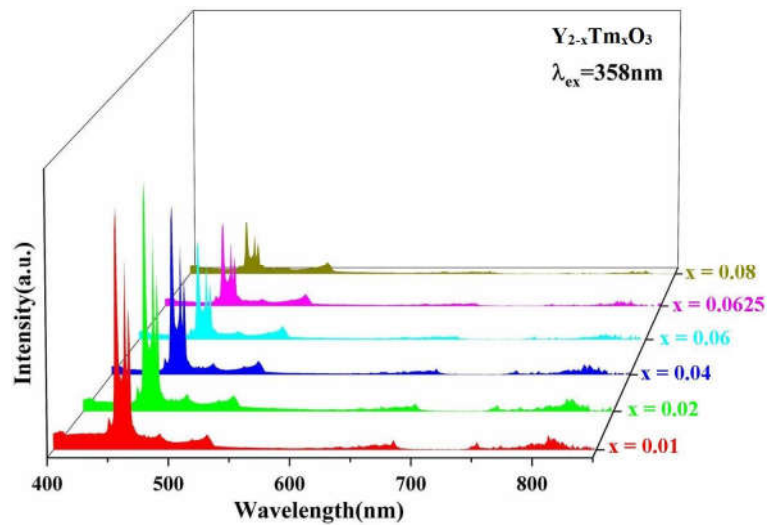
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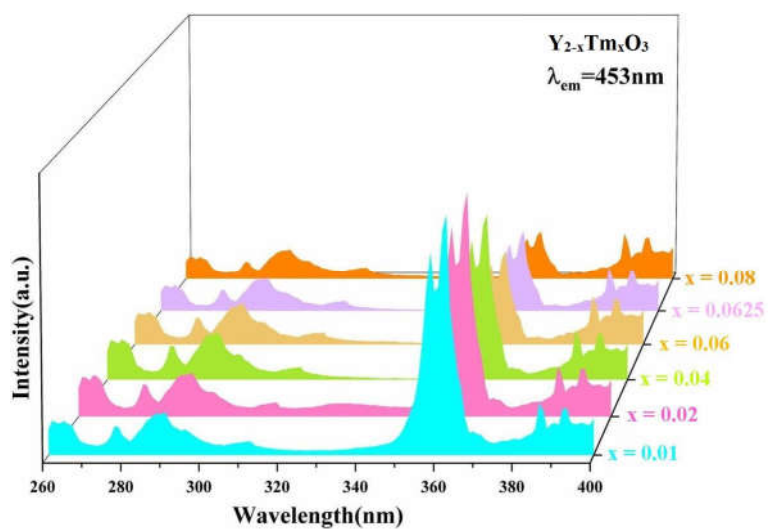
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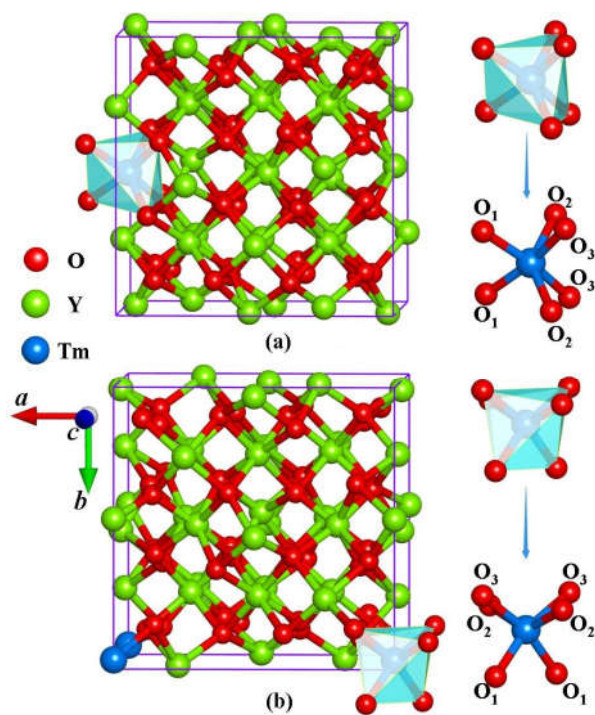
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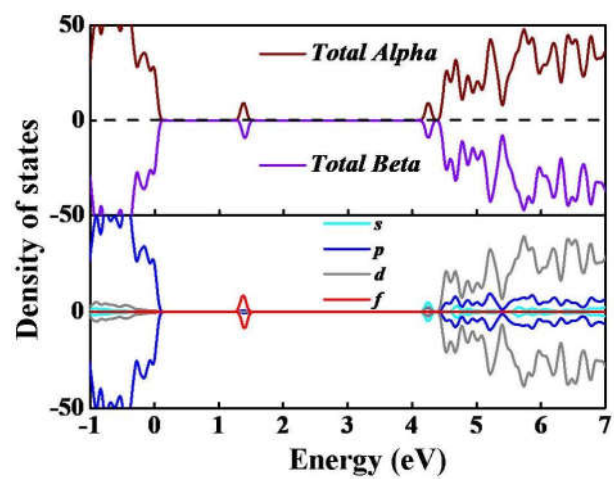
**Figure S1.** Dependence of photoluminescence emission intensities of  $Y_{2-x}Tm_xO_3$  at  $\lambda_{ex} = 358\text{ nm}$  at different  $Tm^{3+}$  concentrations.



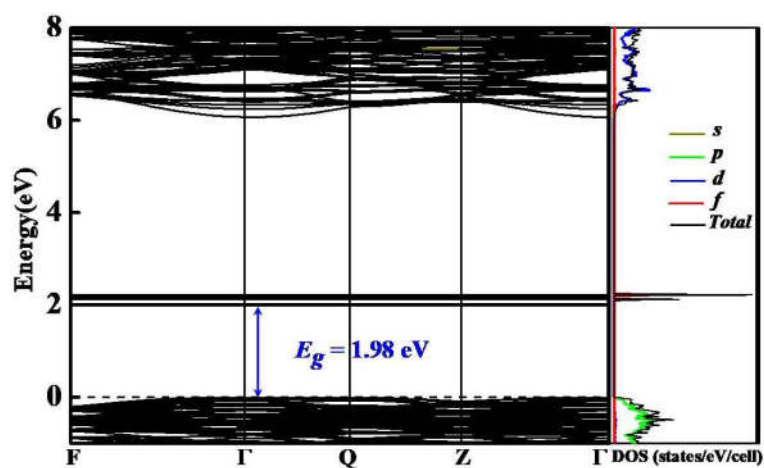
**Figure S2.** Dependence of photoluminescence excitation intensities of  $Y_{2-x}Tm_xO_3$  at  $\lambda_{em} = 453\text{ nm}$  at different  $Tm^{3+}$  concentrations.



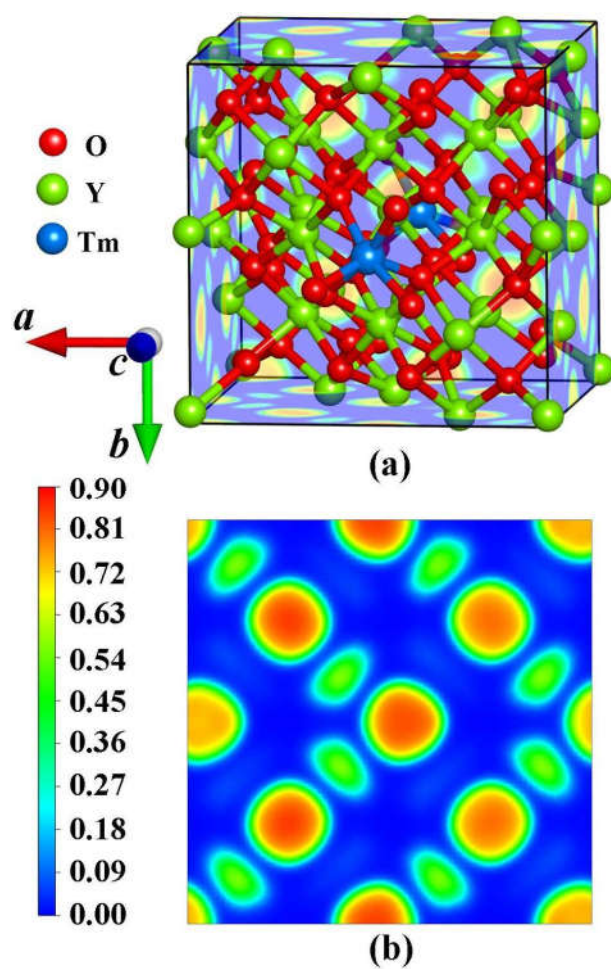
**Figure S3.** The metastable structures (a) and (b) for  $\text{Y}_2\text{O}_3:\text{Tm}^{3+}$ .



**Figure S4.** The calculated total and partial density of states (DOS) of Y<sub>2</sub>O<sub>3</sub>:Tm<sup>3+</sup>.



**Figure S5.** The calculated band structure and partial density of states (DOS) of  $\text{Y}_2\text{O}_3:\text{Tm}^{3+}$  using the modified Becke and Johnson (BJ) method as implemented in the reliable Wien2k program.



**Figure S6.** (a) Electron localization function (ELF) of Y<sub>2</sub>O<sub>3</sub>:Tm crystal. (b) The ELF of <001> plane for Y<sub>2</sub>O<sub>3</sub>:Tm<sup>3+</sup>.

**Table S1.** Coordinates of all atoms for the ground state  $\text{Y}_2\text{O}_3:\text{Tm}^{3+}$ .

Atom	$x$	$y$	$z$	Wyckoff site symmetry
Tm	0.50000	0.53271	0.00000	1c
Y1	0.00021	0.25008	0.24996	2e
Y2	0.00011	0.74992	0.75007	2e
Y3	0.50052	0.74915	0.24916	2e
Y4	0.49929	0.25113	0.75091	2e
Y9	0.71746	-0.00002	0.24997	2e
Y11	-0.21806	0.49995	0.24946	2e
Y13	0.00000	0.96742	0.00000	1a
Y14	0.00000	0.03263	0.50000	1b
Y15	0.50000	0.46753	0.50000	1d
Y16	-0.25080	0.25101	0.96759	2e
Y17	-0.25005	0.74994	0.53285	2e
Y20	-0.21773	0.00012	0.75024	2e
Y21	0.28374	0.50046	0.24879	2e
Y24	0.50000	0.03267	0.00000	2e
Y25	0.00000	0.53242	0.50000	1b
Y26	0.00000	0.46732	0.00000	1a
Y27	0.50000	0.96727	0.50000	1d
Y28	-0.25076	0.74916	0.03229	2e
Y29	0.25014	0.25006	0.53229	2e
O1	0.14107	0.15168	0.37963	2e
O2	0.63790	0.65052	0.88192	2e
O3	-0.14159	0.84782	0.87970	2e
O4	0.35908	0.34850	0.37863	2e
O9	0.13050	0.39128	0.15146	2e
O10	0.62949	0.89073	0.65222	2e
O11	0.62948	0.11024	0.84834	2e
O12	0.13012	0.60894	0.34791	2e
O17	-0.09839	0.37978	0.39089	2e
O18	0.40155	0.87961	0.89106	2e
O21	0.40191	0.12052	0.60933	2e
O22	-0.09867	0.62018	0.10888	2e
O25	0.35889	0.84796	0.62032	2e
O26	-0.14078	0.34816	0.12034	2e
O27	0.64119	0.15153	0.12008	2e
O28	0.14134	0.65150	0.62041	2e



O33	0.37211	0.60606	0.85121	2e
O34	-0.12976	0.10908	0.34832	2e
O35	-0.12974	0.89074	0.15163	2e
O36	0.37005	0.39117	0.65103	2e
O41	0.59808	0.62023	0.60948	2e
O42	0.09882	0.12034	0.10864	2e
O45	0.09832	0.87977	0.39088	2e
O46	0.59545	0.38271	0.89394	2e

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**Table S2.** Lattice constants  $a$ ,  $b$  and  $c$ , unit-cell volume, relative energies for the ground state and metastable  $\text{Y}_2\text{O}_3:\text{Tm}^{3+}$  crystals.

	Space group	$a$ (Å)	$b$ (Å)	$c$ (Å)	$V$ (Å <sup>3</sup> )	$\Delta E$ (meV)
$\text{Y}_2\text{O}_3:\text{Tm}^{3+}$	$P2$	10.6765	10.6749	10.6758	1216.73	0
Isomer (a)	$P1$	10.6748	10.6758	10.6762	1216.68	0.358
Isomer (b)	$P2$	10.6754	10.6745	10.6752	1216.49	0.401

**Table S3.** Comparison between the calculated and experimental energy levels of  $\text{Tm}^{3+}$  in  $\text{Y}_2\text{O}_3$  (in units of  $\text{cm}^{-1}$ ).

$^{2s+1}\text{L}_J$	$E_{\text{expt}}^{[1]}$	This work		Other	
		$E_{\text{calc}}$	$\Delta E$	$\Delta E^{[1]}$	$\Delta E$
$^3\text{H}_6$	0	-51.0	51.0	73.8	-73.8
$^3\text{F}_4$	5644.3	5690.6	-46.3	5636.7	7.6
$^3\text{H}_5$	8091.6	8135.6	-44.0	8231.3	-139.7
$^3\text{H}_4$	12500.3	12520.7	-20.4	12535.4	-35.1
$^3\text{F}_3$	14349.1	14330.2	18.9	14143.8	205.3
$^3\text{F}_2$	14854.9	14837.3	17.6	14724.7	130.2
$^1\text{G}_4$	21324.0	21296.9	27.1	21319.1	4.9
$^1\text{D}_2$	27522.9	27515.8	7.1	27555.7	-32.8
$^1\text{I}_6$	—	34388.4	—	33899.0	2.3
$^3\text{P}_0$	34955.2	34958.6	-3.4	35095.8	140.6
$^3\text{P}_1$	35791.0	35781.5	9.6	35822.8	-31.8
$^3\text{P}_2$	37638.3	37655.6	-17.3	37673.3	-35.0
$^1\text{S}_0$	—	76562.5	—	77506.1	—

**Table S4.** Calculated wavelengths ( $\lambda$ ), ED ( $A_{ED}$ ) and MD ( $A_{MD}$ ) radiative decay rates, branching ratios ( $\beta$ ) and radiative lifetimes ( $\tau$ ) for spontaneous emission transitions between the first 9 excited states of  $\text{Tm}^{3+}$  in  $\text{Y}_2\text{O}_3$ . Available theoretical and experimental results are also listed for comparison.

Transition	$\lambda$ (nm)		$A_{ED}$ ( $\text{s}^{-1}$ )		$A_{MD}$ ( $\text{s}^{-1}$ )		$\beta$		$\tau$ ( $\mu\text{s}$ )	
	Present	Other	Present	Other	Present	Other	Present	Other	Present	Other
$^3\text{F}_4 \rightarrow ^3\text{H}_6$	1742	1698 <sup>[3]</sup> , 1632 <sup>[5]</sup>	353.6	305.5 <sup>[3]</sup> , 277 <sup>[6]</sup>	0	0 <sup>[3]</sup> , 0 <sup>[6]</sup>	1.00	1.00 <sup>[3]</sup>	2828	3270 <sup>[3]</sup> , 3500 <sup>[4]</sup> , 3610 <sup>[6]</sup>
$^3\text{H}_5 \rightarrow ^3\text{H}_6$	1221	1199 <sup>[3]</sup>	284.5	234.7 <sup>[3]</sup> , 237 <sup>[6]</sup>	101.1	85.7 <sup>[3]</sup> , 84.1 <sup>[6]</sup>	0.98	0.99 <sup>[3]</sup>	2543	3090 <sup>[3]</sup> , 3310 <sup>[6]</sup>
$^3\text{H}_5 \rightarrow ^3\text{F}_4$	4090	4080 <sup>[3]</sup>	7.4	3.1 <sup>[3]</sup>	0.2	0.2 <sup>[3]</sup>	0.02	0.01 <sup>[3]</sup>		
$^3\text{H}_4 \rightarrow ^3\text{H}_6$	795	788 <sup>[3]</sup> , 766 <sup>[4]</sup>	1568.4	1197.1 <sup>[3]</sup> , 1534 <sup>[6]</sup>	0	0 <sup>[3]</sup>	0.88	0.88 <sup>[3]</sup>	560	734 <sup>[3]</sup> , 310 <sup>[4]</sup> , 639 <sup>[6]</sup>
$^3\text{H}_4 \rightarrow ^3\text{F}_4$	1464	1470 <sup>[3]</sup> , 1550 <sup>[4]</sup>	145.1	110.4 <sup>[3]</sup>	26.0	19.8 <sup>[3]</sup> , 31.2 <sup>[6]</sup>	0.10	0.09 <sup>[3]</sup>		
$^3\text{H}_4 \rightarrow ^3\text{H}_5$	2280	2300 <sup>[3]</sup>	35.0	26.3 <sup>[3]</sup>	11.6	9.2 <sup>[3]</sup>	0.02	0.03 <sup>[3]</sup>		
$^3\text{F}_3 \rightarrow ^3\text{H}_6$	695	690 <sup>[3]</sup>	2029.1	1620.2 <sup>[3]</sup> , 2467 <sup>[6]</sup>	0	0 <sup>[3]</sup>	0.76	0.77 <sup>[3]</sup>	375	473 <sup>[3]</sup> , 394 <sup>[6]</sup>
$^3\text{F}_3 \rightarrow ^3\text{F}_4$	1157	1162 <sup>[3]</sup>	52.3	40.0 <sup>[3]</sup>	74.5	61.0 <sup>[3]</sup> , 67.8 <sup>[6]</sup>	0.05	0.05 <sup>[3]</sup>		
$^3\text{F}_3 \rightarrow ^3\text{H}_5$	1614	1625 <sup>[3]</sup>	509.8	389.8 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.19	0.18 <sup>[3]</sup>		
$^3\text{F}_3 \rightarrow ^3\text{H}_4$	5526		4.3		0.3		0			

${}^3F_2$	${}^3H_6$	672	658 <sup>[3]</sup> , 680 <sup>[5]</sup>	502.6	424.1 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.28	0.03 <sup>[3]</sup>	566	705 <sup>[3]</sup>
	${}^3F_4$	1093	1074 <sup>[3]</sup>	1016.7	781.1 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.58	0.55 <sup>[3]</sup>		
	${}^3H_5$	1492	1458 <sup>[3]</sup>	230.0	193.3 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.13	0.14 <sup>[3]</sup>		
	${}^3H_4$	4317	3988 <sup>[3]</sup>	18.4	19.0 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.01	0.01 <sup>[3]</sup>		
	${}^3F_3$	19720		0.02		0.02		0			
${}^1G_4$	${}^3H_6$	468	465 <sup>[3]</sup> , 464 <sup>[4]</sup> , 476 <sup>[5]</sup>	1646.4	1236.5 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.51	0.50 <sup>[3]</sup>	312	408 <sup>[3]</sup> , 170 <sup>[4]</sup> , 286 <sup>[6]</sup>
	${}^3F_4$	641	640 <sup>[3]</sup>	184.5	134.9 <sup>[3]</sup>	14.0	11.7 <sup>[3]</sup>	0.06	0.06 <sup>[3]</sup>		
	${}^3H_5$	760	760 <sup>[3]</sup>	762.3	591.4 <sup>[3]</sup>	160.7	131.2 <sup>[3]</sup>	0.29	0.29 <sup>[3]</sup>		
	${}^3H_4$	1139	1134 <sup>[3]</sup>	310.1	247.4 <sup>[3]</sup>	41.6	33.3 <sup>[3]</sup>	0.11	0.11 <sup>[3]</sup>		
	${}^3F_3$	1435	1426 <sup>[3]</sup>	57.9	46.9 <sup>[3]</sup>	4.8	3.7 <sup>[3]</sup>	0.02	0.02 <sup>[3]</sup>		
	${}^3F_2$	1548		20.0		0		0.01			
${}^1D_2$	${}^3H_6$	363	360 <sup>[3]</sup> , 363 <sup>[4]</sup>	10720.2	8436.6 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.26	0.25 <sup>[3]</sup>	24	30 <sup>[3]</sup> , 8.5 <sup>[4]</sup> , 17 <sup>[6]</sup>
	${}^3F_4$	458	457 <sup>[3]</sup> , 450 <sup>[5]</sup>	24981.6	20121.3 <sup>[3]</sup> 3]	0	0 <sup>[3]</sup>	0.60	0.61 <sup>[3]</sup>		
	${}^3H_5$	516		94.5		0		0			
	${}^3H_4$	667	663 <sup>[3]</sup> , 654 <sup>[5]</sup>	2341.3	1648.0 <sup>[3]</sup>	0	0 <sup>[3]</sup>	0.05	0.05 <sup>[3]</sup>		
	${}^3F_3$	758	753 <sup>[3]</sup>	1749.1	1381.1 <sup>[3]</sup>	112.9	88.2 <sup>[3]</sup>	0.04	0.04 <sup>[3]</sup>		
	${}^3F_2$	789	795 <sup>[3]</sup>	1420.9	1083.1 <sup>[3]</sup>	69.9	52.2 <sup>[3]</sup>	0.04	0.03 <sup>[3]</sup>		

	$^1G_4$	1608		235.9	0	0.01		
$^1I_6$	$^3H_6$	290	290 <sup>[4]</sup>	1687.4	78.6	0.09	53	25 <sup>[4]</sup> , 34 <sup>[6]</sup>
	$^3F_4$	348	360 <sup>[4]</sup>	10374.6	0	0.55		
	$^3H_5$	381		70.6	25.1	0.01		
	$^3H_4$	457		2945.3	0	0.16		
	$^3F_3$	498		26.4	0	0		
	$^3F_2$	511		781.0	0	0.04		
	$^1G_4$	764		2683.1	0	0.14		
	$^1D_2$	1455		70.0	0	0.01		

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**Table S5.** The calculated spontaneous emission rates and MD oscillator strengths for transitions  $\psi(SLJ\Gamma_i) \rightarrow \psi(S'L'J'\Gamma'_i)$  between different levels of  $\text{Tm}^{3+}$  in  $\text{Y}_2\text{O}_3$ .

$^{2S+1}L_J$ (Sta.) <sup>a</sup>	$S'L'J'$ (Sta.)	$\lambda$ (nm)	$A'_{MD}$ ( $\text{s}^{-1}$ )	$P_{MD} \times 10^8$
$^3\text{H}_5$ (23)	$^3\text{H}_6$ (1)	1210	36.00	79.09
	$^3\text{H}_6$ (2)	1215	21.98	48.70
	$^3\text{H}_6$ (3)	1223	18.31	41.11
$^3\text{H}_5$ (24)	$^3\text{H}_6$ (1)	1203	16.00	34.72
	$^3\text{H}_6$ (2)	1208	36.74	80.44
	$^3\text{H}_6$ (4)	1235	12.18	27.89
	$^3\text{H}_6$ (5)	1236	14.00	32.09
$^3\text{H}_5$ (25)	$^3\text{H}_6$ (1)	1200	11.26	24.29
	$^3\text{H}_6$ (3)	1212	31.73	69.96
	$^3\text{H}_6$ (4)	1231	16.59	37.71
	$^3\text{H}_6$ (5)	1232	18.96	43.16
	$^3\text{H}_6$ (8)	1264	3.01	7.21
$^3\text{H}_5$ (26)	$^3\text{H}_6$ (3)	1193	8.28	17.66
	$^3\text{H}_6$ (4)	1211	32.12	70.62
	$^3\text{H}_6$ (6)	1233	6.75	15.38
	$^3\text{H}_6$ (7)	1236	15.85	36.32
	$^3\text{H}_6$ (8)	1243	7.14	16.54
	$^3\text{H}_6$ (9)	1252	18.61	43.71
$^3\text{H}_5$ (27)	$^3\text{H}_6$ (2)	1184	5.79	12.17
	$^3\text{H}_6$ (3)	1192	2.36	5.03
	$^3\text{H}_6$ (5)	1211	27.67	60.83
	$^3\text{H}_6$ (6)	1232	5.05	11.49
	$^3\text{H}_6$ (7)	1235	8.25	18.89
	$^3\text{H}_6$ (8)	1242	28.43	65.79
	$^3\text{H}_6$ (9)	1251	16.99	39.86
	$^3\text{H}_6$ (9)	1251	16.99	39.86
$^3\text{H}_5$ (28)	$^3\text{H}_6$ (3)	1184	7.54	15.86
	$^3\text{H}_6$ (5)	1203	5.44	11.80
	$^3\text{H}_6$ (6)	1223	29.71	66.68
	$^3\text{H}_6$ (7)	1227	33.75	76.17
	$^3\text{H}_6$ (8)	1234	5.18	11.83
	$^3\text{H}_6$ (9)	1242	11.30	26.15
	$^3\text{H}_6$ (11)	1274	3.66	8.90
$^3\text{H}_5$ (29)	$^3\text{H}_6$ (4)	1200	5.80	12.53
	$^3\text{H}_6$ (6)	1221	29.60	66.16
	$^3\text{H}_6$ (7)	1225	20.69	46.52
	$^3\text{H}_6$ (8)	1231	16.02	36.40
	$^3\text{H}_6$ (9)	1240	18.24	42.04

${}^3\text{H}_5$ (30)	${}^3\text{H}_6$ (4)	1172	5.67	11.68
	${}^3\text{H}_6$ (6)	1192	2.19	4.66
	${}^3\text{H}_6$ (7)	1195	3.79	8.13
	${}^3\text{H}_6$ (8)	1202	19.02	41.17
	${}^3\text{H}_6$ (10)	1236	20.41	46.75
	${}^3\text{H}_6$ (11)	1240	39.82	91.82
	${}^3\text{H}_6$ (13)	1258	10.52	24.95
${}^3\text{H}_5$ (31)	${}^3\text{H}_6$ (5)	1172	6.25	12.88
	${}^3\text{H}_6$ (9)	1210	19.58	42.97
	${}^3\text{H}_6$ (10)	1236	42.71	97.82
	${}^3\text{H}_6$ (11)	1240	22.66	52.24
	${}^3\text{H}_6$ (12)	1257	7.81	18.50
${}^3\text{H}_5$ (32)	${}^3\text{H}_6$ (8)	1181	3.87	8.10
	${}^3\text{H}_6$ (10)	1214	20.78	45.94
	${}^3\text{H}_6$ (12)	1234	44.65	102.00
	${}^3\text{H}_6$ (13)	1235	35.96	82.24
${}^3\text{H}_5$ (33)	${}^3\text{H}_6$ (9)	1189	4.07	8.62
	${}^3\text{H}_6$ (11)	1218	22.18	49.31
	${}^3\text{H}_6$ (12)	1234	36.26	82.76
	${}^3\text{H}_6$ (13)	1235	44.43	101.54
${}^3\text{H}_4$ (34)	${}^3\text{F}_4$ (14)	1446	8.63	27.07
	${}^3\text{F}_4$ (15)	1461	10.23	32.72
	${}^3\text{F}_4$ (18)	1535	3.45	12.18
	${}^3\text{H}_5$ (23)	2340	3.20	26.30
${}^3\text{H}_4$ (35)	${}^3\text{F}_4$ (16)	1456	13.13	41.75
	${}^3\text{F}_4$ (20)	1529	6.76	23.68
	${}^3\text{H}_5$ (24)	2309	3.41	27.23
${}^3\text{H}_4$ (36)	${}^3\text{F}_4$ (14)	1418	8.99	27.08
	${}^3\text{F}_4$ (16)	1449	9.90	31.14
	${}^3\text{F}_4$ (19)	1519	3.96	13.68
${}^3\text{H}_4$ (37)	${}^3\text{F}_4$ (14)	1392	3.04	8.83
	${}^3\text{F}_4$ (18)	1474	9.68	31.56
	${}^3\text{F}_4$ (22)	1517	6.02	20.76
	${}^3\text{H}_5$ (28)	2342	3.86	31.71
	${}^3\text{H}_5$ (29)	2351	3.64	30.18
${}^3\text{H}_4$ (38)	${}^3\text{F}_4$ (15)	1396	9.50	27.77
	${}^3\text{F}_4$ (17)	1459	8.58	27.41
	${}^3\text{F}_4$ (20)	1481	3.05	10.04
	${}^3\text{H}_5$ (28)	2316	3.23	25.95



${}^3\text{H}_4$ (39)	${}^3\text{F}_4$ (15)	1390	4.09	11.86
	${}^3\text{F}_4$ (17)	1453	7.21	22.83
	${}^3\text{F}_4$ (18)	1457	4.21	13.42
	${}^3\text{F}_4$ (22)	1499	4.52	15.21
	${}^3\text{H}_5$ (31)	2420	4.35	38.19
${}^3\text{H}_4$ (40)	${}^3\text{F}_4$ (14)	1369	3.19	8.95
	${}^3\text{F}_4$ (19)	1464	8.95	28.77
	${}^3\text{F}_4$ (20)	1465	3.47	11.15
	${}^3\text{F}_4$ (21)	1471	6.72	21.79
	${}^3\text{H}_5$ (30)	2396	5.19	44.68
${}^3\text{H}_4$ (41)	${}^3\text{F}_4$ (17)	1416	7.73	23.22
	${}^3\text{F}_4$ (18)	1420	4.67	14.11
	${}^3\text{F}_4$ (22)	1460	7.65	24.44
	${}^3\text{H}_5$ (32)	2399	4.75	40.97
	${}^3\text{H}_5$ (33)	2401	4.92	42.54
${}^3\text{H}_4$ (42)	${}^3\text{F}_4$ (19)	1432	9.24	28.41
	${}^3\text{F}_4$ (20)	1434	4.23	13.04
	${}^3\text{F}_4$ (21)	1439	8.88	27.56
	${}^3\text{H}_5$ (32)	2393	4.61	39.53
	${}^3\text{H}_5$ (33)	2395	4.14	35.60
${}^3\text{F}_3$ (43)	${}^3\text{F}_4$ (14)	1117	14.46	27.07
	${}^3\text{F}_4$ (15)	1126	8.25	15.67
	${}^3\text{F}_4$ (17)	1167	15.46	31.55
	${}^3\text{F}_4$ (18)	1170	7.55	15.48
	${}^3\text{F}_4$ (20)	1180	6.50	13.57
	${}^3\text{F}_4$ (21)	1184	15.75	33.10
	${}^3\text{F}_4$ (22)	1196	5.28	11.32
${}^3\text{F}_3$ (43)	${}^3\text{F}_4$ (14)	1114	21.13	39.32
	${}^3\text{F}_4$ (15)	1123	25.87	48.88
	${}^3\text{F}_4$ (16)	1133	18.65	35.91
	${}^3\text{F}_4$ (19)	1176	4.43	9.19
	${}^3\text{F}_4$ (22)	1193	3.07	6.54
${}^3\text{F}_3$ (45)	${}^3\text{F}_4$ (14)	1109	9.66	17.82
	${}^3\text{F}_4$ (16)	1128	5.20	9.93
	${}^3\text{F}_4$ (17)	1158	11.44	22.99
	${}^3\text{F}_4$ (18)	1161	10.84	21.90
	${}^3\text{F}_4$ (19)	1170	22.46	46.13
	${}^3\text{F}_4$ (21)	1175	3.85	7.96
	${}^3\text{F}_4$ (22)	1187	8.13	17.17
${}^3\text{F}_3$ (46)	${}^3\text{F}_4$ (15)	1117	6.72	12.58
	${}^3\text{F}_4$ (16)	1127	5.39	10.27
	${}^3\text{F}_4$ (17)	1157	19.66	39.45

	$^3F_4$ (19)	1170	12.94	26.53
	$^3F_4$ (20)	1170	12.49	25.65
	$^3F_4$ (21)	1174	9.02	18.64
$^3F_3$ (47)	$^3F_4$ (14)	1107	3.59	6.60
	$^3F_4$ (16)	1126	13.66	25.96
	$^3F_4$ (18)	1158	13.38	26.92
	$^3F_4$ (19)	1168	11.92	24.39
	$^3F_4$ (20)	1169	7.31	14.98
	$^3F_4$ (21)	1172	7.95	16.39
	$^3F_4$ (22)	1184	13.24	27.84
$^3F_3$ (48)	$^3F_4$ (15)	1112	7.54	13.98
	$^3F_4$ (18)	1154	10.43	20.85
	$^3F_4$ (20)	1165	19.42	39.49
	$^3F_4$ (21)	1168	16.36	33.48
	$^3F_4$ (22)	1180	16.45	34.35
$^3F_3$ (49)	$^3F_4$ (16)	1119	5.69	10.67
	$^3F_4$ (17)	1148	6.91	13.64
	$^3F_4$ (18)	1151	10.42	20.68
	$^3F_4$ (19)	1160	5.25	10.59
	$^3F_4$ (20)	1161	13.84	27.96
	$^3F_4$ (21)	1164	8.25	16.78
	$^3F_4$ (22)	1176	16.11	33.43
$^1G_4$ (55)	$^3F_4$ (15)	657	7.28	4.71
	$^3F_4$ (16)	661	5.77	3.78
	$^3F_4$ (17)	671	5.95	4.02
	$^3H_5$ (23)	791	6.89	6.46
	$^3H_5$ (24)	794	34.83	32.89
	$^3H_5$ (25)	795	3.88	3.68
	$^3H_5$ (26)	804	39.27	38.07
	$^3H_5$ (27)	804	27.65	26.83
	$^3H_5$ (28)	808	14.37	14.07
	$^3H_5$ (29)	809	23.09	22.67
	$^3H_4$ (34)	1194	7.72	16.51
	$^3H_4$ (36)	1215	9.00	19.91
$^1G_4$ (56)	$^3F_4$ (14)	650	4.41	2.79
	$^3F_4$ (19)	670	3.84	2.59
	$^3H_5$ (23)	784	16.54	15.24
	$^3H_5$ (25)	789	42.25	39.39
	$^3H_5$ (26)	797	26.58	25.33
	$^3H_5$ (27)	798	38.36	36.58
	$^3H_5$ (28)	801	7.07	6.80
	$^3H_5$ (29)	802	11.17	10.77
	$^3H_4$ (34)	1179	10.89	22.69
	$^3H_4$ (38)	1225	11.94	26.86

	$^3\text{H}_4$ (39)	1230	3.39	7.69
$^1\text{G}_4$ (57)	$^3\text{F}_4$ (18)	665	6.07	4.03
	$^3\text{H}_5$ (23)	782	57.15	52.37
	$^3\text{H}_5$ (24)	785	39.66	36.62
	$^3\text{H}_5$ (25)	786	31.79	29.47
	$^3\text{H}_5$ (26)	795	3.85	3.65
	$^3\text{H}_5$ (29)	800	4.48	4.29
	$^3\text{H}_4$ (35)	1189	15.88	33.65
	$^3\text{H}_4$ (36)	1194	12.46	26.62
	$^3\text{H}_4$ (38)	1219	3.33	7.42
$^1\text{G}_4$ (58)	$^3\text{F}_4$ (20)	653	3.63	2.32
	$^3\text{H}_5$ (23)	760	23.69	20.51
	$^3\text{H}_5$ (24)	763	27.70	24.16
	$^3\text{H}_5$ (26)	772	19.25	17.22
	$^3\text{H}_5$ (27)	773	4.87	4.36
	$^3\text{H}_5$ (28)	776	41.35	37.34
	$^3\text{H}_5$ (29)	777	19.65	17.78
	$^3\text{H}_5$ (32)	798	4.07	3.89
	$^3\text{H}_4$ (34)	1126	7.19	13.66
	$^3\text{H}_4$ (37)	1161	21.20	42.82
	$^3\text{H}_4$ (40)	1177	3.67	7.63
	$^1\text{G}_4$ (59)	$^3\text{F}_4$ (19)	651	3.66
$^3\text{H}_5$ (25)		763	10.66	9.30
$^3\text{H}_5$ (26)		771	15.13	13.48
$^3\text{H}_5$ (28)		775	42.13	37.89
$^3\text{H}_5$ (29)		775	40.67	36.67
$^3\text{H}_5$ (30)		788	21.70	20.18
$^3\text{H}_5$ (31)		788	4.10	3.81
$^3\text{H}_5$ (33)		797	11.66	11.10
$^3\text{H}_4$ (34)		1122	3.92	7.41
$^3\text{H}_4$ (38)		1164	16.71	33.92
$^3\text{H}_4$ (39)		1168	8.20	16.77
$^3\text{H}_4$ (41)		1193	4.21	8.99
$^1\text{G}_4$ (60)	$^3\text{F}_4$ (21)	650	3.07	1.94
	$^3\text{H}_5$ (24)	758	8.56	7.37
	$^3\text{H}_5$ (25)	760	10.27	8.88
	$^3\text{H}_5$ (27)	768	48.82	43.15
	$^3\text{H}_5$ (28)	771	12.03	10.72
	$^3\text{H}_5$ (29)	772	6.12	5.47
	$^3\text{H}_5$ (30)	784	32.86	30.30
	$^3\text{H}_5$ (31)	784	29.18	26.91
	$^3\text{H}_5$ (33)	793	4.74	4.47
	$^3\text{H}_4$ (35)	1128	11.33	21.62
	$^3\text{H}_4$ (36)	1133	6.68	12.86
	$^3\text{H}_4$ (39)	1160	5.15	10.39

	$^3\text{H}_4$ (41)	1185	8.04	16.93
	$^3\text{H}_4$ (42)	1187	3.31	6.99
$^1\text{G}_4$ (61)	$^3\text{F}_4$ (17)	641	3.37	2.08
	$^3\text{H}_5$ (25)	754	8.84	7.54
	$^3\text{H}_5$ (26)	762	17.47	15.21
	$^3\text{H}_5$ (29)	767	14.35	12.65
	$^3\text{H}_5$ (30)	779	35.09	31.89
	$^3\text{H}_5$ (31)	779	53.74	48.86
	$^3\text{H}_5$ (32)	788	12.71	11.82
	$^3\text{H}_4$ (36)	1121	6.15	11.59
	$^3\text{H}_4$ (37)	1138	4.49	8.71
	$^3\text{H}_4$ (40)	1154	14.08	28.10
	$^3\text{H}_4$ (42)	1174	13.08	27.02
	$^3\text{F}_3$ (45)	1438	3.41	10.55
$^1\text{G}_4$ (62)	$^3\text{F}_4$ (22)	647	5.37	3.37
	$^3\text{H}_5$ (23)	746	4.26	3.56
	$^3\text{H}_5$ (25)	750	4.74	4.00
	$^3\text{H}_5$ (30)	774	34.26	30.79
	$^3\text{H}_5$ (32)	783	44.41	40.82
	$^3\text{H}_5$ (33)	783	61.75	56.79
	$^3\text{H}_4$ (40)	1144	12.65	24.81
	$^3\text{H}_4$ (42)	1164	16.92	34.37
$^1\text{G}_4$ (63)	$^3\text{F}_4$ (21)	640	4.13	2.54
	$^3\text{H}_5$ (28)	757	3.42	2.93
	$^3\text{H}_5$ (29)	757	3.74	3.21
	$^3\text{H}_5$ (31)	769	33.99	30.15
	$^3\text{H}_5$ (32)	778	60.71	55.05
	$^3\text{H}_5$ (33)	778	46.40	42.10
	$^3\text{H}_4$ (37)	1118	4.25	7.96
	$^3\text{H}_4$ (39)	1128	10.78	20.54
	$^3\text{H}_4$ (41)	1151	20.30	40.32
$^1\text{D}_2$ (64)	$^3\text{F}_3$ (43)	763	40.34	35.19
	$^3\text{F}_3$ (44)	764	32.09	28.10
	$^3\text{F}_3$ (45)	767	3.26	2.88
	$^3\text{F}_3$ (46)	767	27.46	24.22
	$^3\text{F}_2$ (50)	793	47.53	44.79
	$^3\text{F}_2$ (51)	801	10.23	9.84
	$^3\text{F}_2$ (52)	804	4.86	4.71
	$^3\text{F}_2$ (53)	811	5.39	5.31
$^1\text{D}_2$ (65)	$^3\text{F}_3$ (43)	761	30.31	26.32
	$^3\text{F}_3$ (44)	763	19.80	17.26
	$^3\text{F}_3$ (45)	765	7.19	6.30
	$^3\text{F}_3$ (47)	766	26.92	23.67
	$^3\text{F}_3$ (49)	769	21.67	19.23

	$^3F_2$ (51)	799	25.08	24.00
	$^3F_2$ (52)	802	17.64	17.03
	$^3F_2$ (53)	809	8.43	8.26
$^1D_2$ (66)	$^3F_3$ (44)	757	13.93	11.97
	$^3F_3$ (45)	760	45.85	39.66
	$^3F_3$ (46)	760	35.18	30.45
	$^3F_3$ (47)	761	24.42	21.18
	$^3F_2$ (50)	785	39.00	36.05
	$^3F_2$ (51)	793	5.56	5.24
	$^3F_2$ (52)	797	15.18	14.45
	$^3F_2$ (54)	807	8.20	8.02
$^1D_2$ (67)	$^3F_3$ (44)	751	17.55	14.86
	$^3F_3$ (45)	754	15.34	13.06
	$^3F_3$ (47)	755	22.60	19.30
	$^3F_3$ (48)	756	35.14	30.15
	$^3F_3$ (49)	758	22.91	19.74
	$^3F_2$ (51)	787	37.43	34.74
	$^3F_2$ (52)	790	14.26	13.35
	$^3F_2$ (53)	796	19.62	18.64
$^1D_2$ (68)	$^3F_3$ (45)	752	4.56	3.87
	$^3F_3$ (46)	753	14.20	12.06
	$^3F_3$ (48)	755	36.86	31.50
	$^3F_3$ (49)	757	30.38	26.07
	$^3F_2$ (51)	785	6.50	6.00
	$^3F_2$ (52)	789	11.48	10.70
	$^3F_2$ (53)	795	9.69	9.17
	$^3F_2$ (54)	799	36.08	34.55
$^1I_6$ (69)	$^3H_6$ (11)	301	5.43	0.74
	$^3F_4$ (17)	359	3.26	0.63
	$^3H_5$ (28)	394	8.25	1.92
	$^3H_5$ (29)	395	4.95	1.16
$^1I_6$ (70)	$^3F_4$ (14)	354	3.24	0.61
	$^3H_5$ (28)	394	7.14	1.67
	$^3H_5$ (29)	395	5.97	1.39
$^1I_6$ (71)	$^3H_5$ (31)	392	8.68	1.99
	$^3H_5$ (32)	394	4.04	0.94
	$^1G_4$ (58)	777	3.22	2.91
$^1I_6$ (72)	$^3F_4$ (15)	349	3.03	0.55
	$^3H_5$ (30)	391	7.93	1.81
	$^3H_5$ (33)	393	4.27	0.99
$^1I_6$ (73)	$^3H_5$ (27)	386	5.16	1.16

	$^3\text{H}_5$ (30)	390	6.04	1.38
	$^3\text{H}_5$ (33)	393	5.16	1.19
$^1\text{I}_6$ (74)	$^3\text{H}_5$ (26)	386	3.46	0.77
	$^3\text{H}_5$ (31)	390	4.93	1.12
	$^3\text{H}_5$ (32)	392	7.37	1.70
	$^3\text{H}_5$ (33)	392	3.07	0.71
$^1\text{I}_6$ (75)	$^3\text{F}_4$ (19)	352	4.49	0.83
	$^3\text{H}_5$ (23)	381	4.19	0.91
	$^3\text{H}_5$ (25)	382	6.58	1.44
	$^1\text{G}_4$ (61)	773	3.95	3.54
$^1\text{I}_6$ (76)	$^3\text{H}_5$ (23)	379	10.96	2.36
	$^3\text{H}_5$ (24)	379	7.50	1.62
$^1\text{I}_6$ (77)	$^3\text{H}_5$ (23)	378	7.76	1.66
	$^3\text{H}_5$ (24)	378	10.84	2.33
$^1\text{I}_6$ (78)	$^3\text{H}_5$ (25)	376	4.78	1.01
	$^3\text{H}_5$ (26)	378	4.87	1.04
	$^3\text{H}_5$ (29)	379	3.13	0.68
	$^3\text{H}_5$ (30)	382	4.66	1.02
$^1\text{I}_6$ (79)	$^3\text{H}_5$ (25)	376	6.01	1.27
	$^3\text{H}_5$ (31)	382	3.66	0.80
$^3\text{P}_0$ (80)	$^3\text{F}_4$ (17)	343	3.01	0.53
	$^3\text{F}_4$ (19)	344	6.38	1.13
	$^3\text{F}_4$ (20)	344	5.86	1.04
	$^3\text{F}_4$ (21)	344	5.45	0.97
$^1\text{I}_6$ (81)	$^3\text{H}_5$ (26)	373	3.05	0.64
	$^3\text{H}_5$ (27)	373	3.49	0.73
	$^3\text{H}_5$ (28)	374	3.26	0.68
	$^3\text{H}_5$ (29)	374	3.71	0.78
	$^3\text{H}_5$ (32)	379	4.93	1.06
$^1\text{I}_6$ (82)	$^3\text{H}_5$ (27)	373	4.00	0.83
	$^3\text{H}_5$ (28)	374	3.12	0.66
	$^3\text{H}_5$ (29)	374	3.64	0.76
	$^3\text{H}_5$ (33)	379	4.32	0.93
$^3\text{P}_1$ (83)	$^3\text{H}_5$ (28)	365	4.50	0.90
	$^3\text{F}_2$ (51)	482	5.86	2.04
	$^3\text{F}_2$ (53)	485	6.97	2.46
	$^3\text{F}_2$ (54)	487	9.53	3.39
	$^3\text{P}_2$ (66)	1227	12.92	29.16
	$^3\text{P}_2$ (67)	1242	13.96	32.30

	$^1D_2$ (68)	1246	11.57	26.95
$^3P_1$ (84)	$^3H_4$ (42)	433	3.27	0.92
	$^3F_3$ (47)	465	3.06	0.99
	$^3F_2$ (50)	474	5.02	1.69
	$^3F_2$ (51)	477	9.77	3.34
	$^3F_2$ (52)	479	10.83	3.72
	$^3F_2$ (54)	482	6.19	2.16
	$^3P_2$ (64)	1182	11.20	23.44
	$^3P_2$ (65)	1186	9.77	20.60
	$^3P_2$ (67)	1213	4.34	9.59
	$^1D_2$ (68)	1217	8.99	19.98
$^3P_1$ (85)	$^3F_3$ (49)	465	3.27	1.06
	$^3F_2$ (50)	473	12.79	4.29
	$^3F_2$ (51)	476	3.09	1.05
	$^3F_2$ (52)	477	4.54	1.55
	$^3F_2$ (53)	479	9.29	3.20
	$^3P_2$ (64)	1172	10.61	21.84
	$^3P_2$ (65)	1176	11.01	22.82
	$^3P_2$ (66)	1189	8.50	17.99
	$^3P_2$ (67)	1203	3.07	6.67
	$^3P_2$ (86)	$^3F_3$ (43)	435	46.35
$^3F_3$ (44)		435	10.01	2.84
$^3F_3$ (45)		436	40.70	11.60
$^3F_3$ (47)		436	38.68	11.04
$^3F_2$ (53)		450	3.88	1.18
$^3P_2$ (64)		1011	51.55	79.05
$^3P_2$ (66)		1024	38.93	61.19
$^3P_2$ (87)		$^3F_3$ (43)	432	28.70
	$^3F_3$ (44)	432	16.49	4.61
	$^3F_3$ (46)	433	31.93	8.97
	$^3F_3$ (47)	433	4.92	1.39
	$^3F_3$ (48)	434	24.43	6.89
	$^3F_3$ (49)	434	24.70	6.98
	$^3F_2$ (54)	448	4.35	1.31
	$^3P_2$ (64)	994	7.08	10.49
	$^3P_2$ (65)	997	43.92	65.44
	$^3P_2$ (66)	1006	8.62	13.07
	$^3P_2$ (67)	1016	25.32	39.21
	$^1D_2$ (68)	1019	6.64	10.34
	$^3P_2$ (88)	$^3F_3$ (43)	430	18.65
$^3F_3$ (44)		430	15.57	4.32
$^3F_3$ (45)		431	9.69	2.70
$^3F_3$ (46)		431	34.16	9.51
$^3F_3$ (47)		431	7.00	1.95

	<sup>3</sup> F <sub>3</sub> (48)	432	29.99	8.38
	<sup>3</sup> F <sub>3</sub> (49)	432	14.93	4.18
	<sup>3</sup> F <sub>2</sub> (54)	446	3.29	0.98
	<sup>3</sup> P <sub>2</sub> (64)	984	7.32	10.62
	<sup>3</sup> P <sub>2</sub> (65)	987	21.12	30.83
	<sup>3</sup> P <sub>2</sub> (66)	996	25.18	37.42
	<sup>3</sup> P <sub>2</sub> (67)	1006	28.66	43.47
	<sup>1</sup> D <sub>2</sub> (68)	1009	5.21	7.95
<sup>3</sup> P <sub>2</sub> (89)	<sup>3</sup> F <sub>3</sub> (44)	425	17.79	4.82
	<sup>3</sup> F <sub>3</sub> (45)	426	34.37	9.35
	<sup>3</sup> F <sub>3</sub> (46)	426	23.15	6.30
	<sup>3</sup> F <sub>3</sub> (47)	426	37.51	10.22
	<sup>3</sup> F <sub>3</sub> (49)	427	5.79	1.59
	<sup>3</sup> P <sub>2</sub> (64)	959	12.33	17.00
	<sup>3</sup> P <sub>2</sub> (65)	962	8.23	11.41
	<sup>3</sup> P <sub>2</sub> (67)	980	36.83	53.00
	<sup>1</sup> D <sub>2</sub> (68)	982	13.37	19.35
<sup>3</sup> P <sub>2</sub> (90)	<sup>3</sup> F <sub>3</sub> (44)	424	12.53	3.37
	<sup>3</sup> F <sub>3</sub> (45)	424	6.57	1.77
	<sup>3</sup> F <sub>3</sub> (47)	425	9.29	2.51
	<sup>3</sup> F <sub>3</sub> (48)	425	42.38	11.49
	<sup>3</sup> F <sub>3</sub> (49)	426	44.02	11.96
	<sup>3</sup> P <sub>2</sub> (64)	950	6.55	8.86
	<sup>3</sup> P <sub>2</sub> (66)	961	23.42	32.46
	<sup>1</sup> D <sub>2</sub> (68)	973	40.82	57.98

<sup>a</sup>Only transitions between 300-2500 nm with emission rates  $A_{MD} > 3 \text{ s}^{-1}$  are listed.



## Appendix – Method and equations for the calculations of energy levels and transition intensities

The model Hamiltonian for  $Tm^{3+}$  is defined as<sup>[7]-[8]</sup>

$$\begin{aligned}
 H_f = E_{AVE} + \sum_{k=2,4,6} F^k f_k + \zeta_{4f} \times \sum_i \vec{l}_i \cdot \vec{s}_i + \alpha L(L+1) + \beta G(G_2) + \gamma G(R_7) \\
 + \sum_{j=0,2,4} M^j m_j + \sum_{k=2,4,6} P^k p_k
 \end{aligned} \tag{A1}$$

where  $E_{AVE}$  represents the barycenter energy of the  $4f^3$  configuration. The next seven terms represent the Coulomb repulsion, spin-orbit, two-body, three-body, spin-other-orbit and electrostatically correlated spin-orbit interactions. Moreover,  $F^k$  and  $\zeta_{4f}$  are the radial parts of the electrostatic and spin-orbit coupling constant. Two-body parameters are represented by  $\alpha$ ,  $\beta$ , and  $\gamma$ .  $G(G_2)$  and  $G(R_7)$  represent the eigenvalues of the Casimir's operators for the Lie groups  $G_2$  and  $R_7$ . The remaining parameters,  $M^j$  and  $P^k$ , are used to represent the Marvin integrals and spin-orbit perturbations.

The crystal field interaction  $H_{CF}$  for  $Tm^{3+}$  in  $Y_2O_3$ , in the form of Wybourne normalization, can be expressed as<sup>[9]</sup>

$$\begin{aligned}
 H_{CF} = B_2^0 C_2^0 + ReB_2^2 (C_2^2 + C_2^{-2}) + B_4^0 C_4^0 \\
 + ReB_4^2 (C_4^2 + C_4^{-2}) + iImB_4^2 (C_4^2 - C_4^{-2}) \\
 + ReB_4^4 (C_4^4 + C_4^{-4}) + iImB_4^4 (C_4^4 - C_4^{-4}) + B_6^0 C_6^0 \\
 + ReB_6^2 (C_6^2 + C_6^{-2}) + iImB_6^2 (C_6^2 - C_6^{-2}) \\
 + ReB_6^4 (C_6^4 + C_6^{-4}) + iImB_6^4 (C_6^4 - C_6^{-4}) \\
 + ReB_6^6 (C_6^6 + C_6^{-6}) + iImB_6^6 (C_6^6 - C_6^{-6})
 \end{aligned} \tag{A2}$$

where  $C_q^k$  are the normalized spherical-tensor operators and  $B_q^k$  are the crystal field parameters (CFPs). The values of these CFPs can be determined by the least-squares fit to the observed energy levels.<sup>[9]</sup>

The ED ( $A_{ED}$ ) radiative decay rates can be written as<sup>[10]-[11]</sup>

$$A_{ED(SLJ \rightarrow S'L'J')} = \frac{16\pi^3 e^2}{3\varepsilon_0 h c^3} \frac{\nu^3}{(2J+1)} \chi_{ED} \sum_{\lambda=2,4,6} \Omega_{(\lambda)} \left| \left\langle l^N SLJ \parallel U^{(\lambda)} \parallel l^N S'L'J' \right\rangle \right|^2 \quad (\text{A3})$$

where  $\nu$  is the transition frequency,  $n$  is the refractive index and  $\chi_{ED}$  is the local-field correction for ED induced transitions with the form of  $(n^2+1)^2/(9n)$  and  $n(n^2+1)^2/9$  for absorption and emission transition, respectively. The Judd-Ofelt intensity parameters  $\Omega_{(\lambda)}$  should be summed over  $\lambda=2,4,6$  for a product with the even-rank reduced matrix elements of the  $U^{(\lambda)}$  tensor operator.

The MD ( $A_{MD}$ ) radiative decay rates can be written as<sup>[10]-[11]</sup>

$$A_{MD} = \frac{\pi h e^2}{3\varepsilon_0 c^5 m_e^2} \frac{\nu^3}{g} \chi_{MD} \left| \left\langle l^N \psi \parallel L + g_e S \parallel l^N \psi' \right\rangle \right|^2 \quad (\text{A4})$$

where  $g_e = 2.00232$  is the gyromagnetic ratio of the electron and  $g$  is the degeneracy of the initial level.  $\chi_{MD}$  is the local-field correction for MD induced transitions with the form of  $n$  and  $n^3$  for the absorption and emission transition, respectively.  $\psi$  and  $\psi'$  are the statevectors for the initial and terminating levels for the  $\psi \rightarrow \psi'$  transition, respectively. For transitions between J-multiplets, the statevector takes the form of  $\psi(SLJ)$  with  $g = (2J+1)$  while for transitions between crystal field levels, it takes the form of  $\psi(SLJ_i)$ .

The radiative lifetime can be written as<sup>[10]-[11]</sup>

$$\tau_{SLJ} = \frac{1}{\sum_{S'L'J'} (A_{ED(SLJ \rightarrow S'L'J')} + A_{MD(SLJ \rightarrow S'L'J')})} \quad (\text{A5})$$

The branching ratio can be written as<sup>[10]-[11]</sup>

$$\beta_{(SLJ \rightarrow SL'J')} = \tau_{SLJ} \times [A_{ED(SLJ \rightarrow SL'J')} + A_{MD(SLJ \rightarrow SL'J')}] \quad (\text{A6})$$

The MD absorption oscillator strengths can be written as<sup>[10]-[11]</sup>

$$P_{MD} = \frac{h\nu}{6m_e c^2} \frac{n}{(2J+1)} \left| \langle l^N SLJ \| L + g_e S \| l^N SLJ' \rangle \right|^2 \quad (\text{A7})$$

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