## Supporting Information Effects of strain and thickness on the mechanical, electronic, and optical properties of Cu<sub>2</sub>Te

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Phase	Direction	Carrier	m*/m0	E1(eV)	$C_{2D}(J^*m^{-2})$	$\mu(10^3 \text{cm}^2 \text{V}^{-1} \text{S}^{-1})$
ζ-Cu <sub>2</sub> Te	Х	h	0.18	4.27±0.02	80.04	1.32-1.34
ζ-Cu <sub>2</sub> Te	У	h	0.15	5.35±0.01	83.85	1.06-1.07
		e	0.37	3.97±0.02	71.9	2.65-2.67
$\lambda$ -Cu <sub>2</sub> Te		h	0.38	5.35±0.02	82.9	1.64-1.66

Table S1 The Calculated Effective Mass (m\*), Elastic Modulus (C2D), Deformation Potential Constant El, and Carrier Mobility ( $\mu$ ) of monolayer  $\lambda$ -Cu<sub>2</sub>Te and  $\zeta$ -Cu<sub>2</sub>Te

Table S2 Theoretical Young's modulus Y (in N/m) and Poisson's ratio v of monolayer

ζ-Cu <sub>2</sub> Te	Y(N/m)	V	$\lambda$ -Cu <sub>2</sub> Te	Y(N/m)	V
$\varepsilon_{bia} = -4\%$	96.56–121.17	0.38-0.48	$\varepsilon_{bia} = -4\%$	111.41	0.41
$\varepsilon_{bia} = -2\%$	98.06–110.63	0.38–0.44	$\epsilon_{bia} = -2\%$	102.04	0.42
$\epsilon_{bia}\!=\!0\%$	72.08-89.43	0.40–0.51	$\epsilon_{bia} = 0\%$	90.11	0.43
$\epsilon_{bia} = 2\%$	63.52-83.26	0.40–0.54	$\epsilon_{bia} = 2\%$	81.99	0.45
$\epsilon_{bia} = 4\%$	51.15-68.86	0.42–0.58	$\epsilon_{bia} = 4\%$	61.22	0.51
$\epsilon_x = -4\%$	93.36–102.23	0.39–0.43	$\epsilon_x = -4\%$	71.75–106.75	0.32-0.54
$\epsilon_x \!=\! -2\%$	95.14–101.67	0.38–0.42	$\epsilon_x = -2\%$	67.21–110.29	0.34-0.51
$\epsilon_x \!=\! 0\%$	82.63–99.22	0.37–0.47	$\epsilon_x = 0\%$	90.11	0.43
$\epsilon_x = 2\%$	70.061–97.32	0.36–0.54	$\epsilon_x = 2\%$	60.76–110.78	0.32-0.60
$\epsilon_x = 4\%$	62.48–95.401	0.38–0.59	$\epsilon_x = 4\%$	60.66–108.78	0.31-0.64
$\epsilon_y \!=\! -4\%$	82.96–114.56	0.34–0.51			
$\epsilon_y = -2\%$	82.72–107.22	0.35–0.49			
$\epsilon_y \!= 0\%$	81.758–98.91	0.37–0.47			
$\epsilon_y = 2\%$	78.528–91.16	0.39–0.47			
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 $\lambda\text{-}Cu_2Te$  and  $\zeta$  -Cu\_2Te under various strain.

 $\epsilon_y = 4\%$  68.292-84.91 0.41-0.52



Fig. S1 Orientation-dependent Young's modulus and Poisson's ratio v of monolayer  $\zeta$ -Cu<sub>2</sub>Te calculated under various values of strain ( $\epsilon = -2\%$ , 0%, 2%).



Fig. S2 Orientation-dependent in-plane Young's modulus and Poisson's ratio for 2D monolayer  $\lambda$ -Cu<sub>2</sub>Te (a, d) and  $\zeta$ -Cu<sub>2</sub>Te (b, c) under various biaxial compressive and tensile strains.



Fig. S3 Orientation-dependent in-plane Young's modulus and Poisson's ratio for 2D monolayer  $\lambda$ -Cu<sub>2</sub>Te under x-directional strains (a, d) and  $\zeta$ -Cu<sub>2</sub>Te under various compressive and tensile strains along the x- (b, e) and y-directions (c, f).



Fig. S4 Projection energy band structures of  $\zeta$ -Cu<sub>2</sub>Te corresponding to various biaxial strain values (a)  $\mathcal{E} = -3\%$ , (b) 0% and (c) 5% through HSE06 calculations.



Fig. S5 Calculated (a) biaxial compressive strain– and (b) biaxial tensile strain– dependent electronic band structures of monolayer  $\zeta$ -Cu<sub>2</sub>Te obtained through HSE06 calculations.



Fig. S6 Calculated (a) biaxial compressive strain– and (b) biaxial tensile strain– dependent electronic band structures of monolayer  $\lambda$ -Cu<sub>2</sub>Te obtained through HSE06 calculations.



Fig. S7 Calculated (a) uniaxial compressive strain– and (b) uniaxial tensile strain– dependent electronic band structures of monolayer  $\lambda$ -Cu<sub>2</sub>Te obtained through HSE06 calculations.



Fig. S8 Calculated (a) uniaxial compressive strain– and (b) uniaxial tensile strain– dependent electronic band structures of monolayer  $\zeta$ -Cu<sub>2</sub>Te obtained through HSE06 calculations.



Fig. S9 Calculated (a) uniaxial compressive strain– and (b) uniaxial tensile strain– dependent electronic band structures of monolayer  $\zeta$ -Cu<sub>2</sub>Te obtained through HSE06 calculations.



Fig. S10 Projection energy band structures of  $\lambda$ -Cu<sub>2</sub>Te corresponding to various biaxial strain values (a)  $\mathcal{E} = -2\%$ , (b) 0% (c) 2%, through HSE06 calculations.



Fig. S11 Band-edge alignment of monolayer (a)  $\lambda$ -Cu<sub>2</sub>Te and (b)  $\zeta$ -Cu<sub>2</sub>Te under various biaxial strain through HSE06 calculations with respect to the vacuum level. The gray dashed lines denote the water potential of water.



Fig. S12 Band-edge alignment of monolayer (a)  $\lambda$ -Cu<sub>2</sub>Te and (b, c)  $\zeta$ -Cu<sub>2</sub>Te under various uniaxial strain through HSE06 calculations with respect to the vacuum level. The gray dashed lines denote the redox potential of water.



Fig. S13 Calculated formation energies of 2L (a)  $\lambda$ -Cu<sub>2</sub>Te and (b)  $\zeta$ -Cu<sub>2</sub>Te. Side views of the structures of  $\lambda$ -Cu<sub>2</sub>Te and  $\zeta$ -Cu<sub>2</sub>Te are also shown.

	Y (N/m)	V
ζ-Cu <sub>2</sub> Te		
2-Layers	171.20–196.18	0.40-0.47
3-Layers	246.54–288.27	0.39–0.47
$\lambda$ -Cu <sub>2</sub> Te		
2-Layers	184.12	0.47
3-Layers	286.54	0.43

Table S3 Theoretical Young's modulus Y (in N/m) and Poisson's ratio v of few-layered  $\lambda$ -Cu<sub>2</sub>Te and  $\zeta$ -Cu<sub>2</sub>Te.



Fig. S14 Young's modulus and Poisson's ratio of (a, b)  $\zeta$ -Cu<sub>2</sub>Te and (c, d)  $\lambda$ -Cu<sub>2</sub>Te. Both are functions of the in-plane angle  $\theta$ .



Fig. S15 Band structure of (a)  $\lambda$ -Cu<sub>2</sub>Te and (b)  $\zeta$ -Cu<sub>2</sub>Te with the number of layers ranging from 1 to 3, through HSE06 calculations.



Fig. S16 Thickness-dependent projection energy band structures in few-layer (a)  $\zeta$ -Cu<sub>2</sub>Te and (b)  $\lambda$ -Cu<sub>2</sub>Te obtained through HSE06 calculations.