

Supporting Information

**Electronic and structural properties of  $\text{Y}_6\text{Pt}_{13}\text{X}_4$ , the site occupancy variants of the  $\text{Ba}_6\text{Na}_{16}\text{N}$  subnitride ( $\text{X} = \text{Al, Ga}$ )**

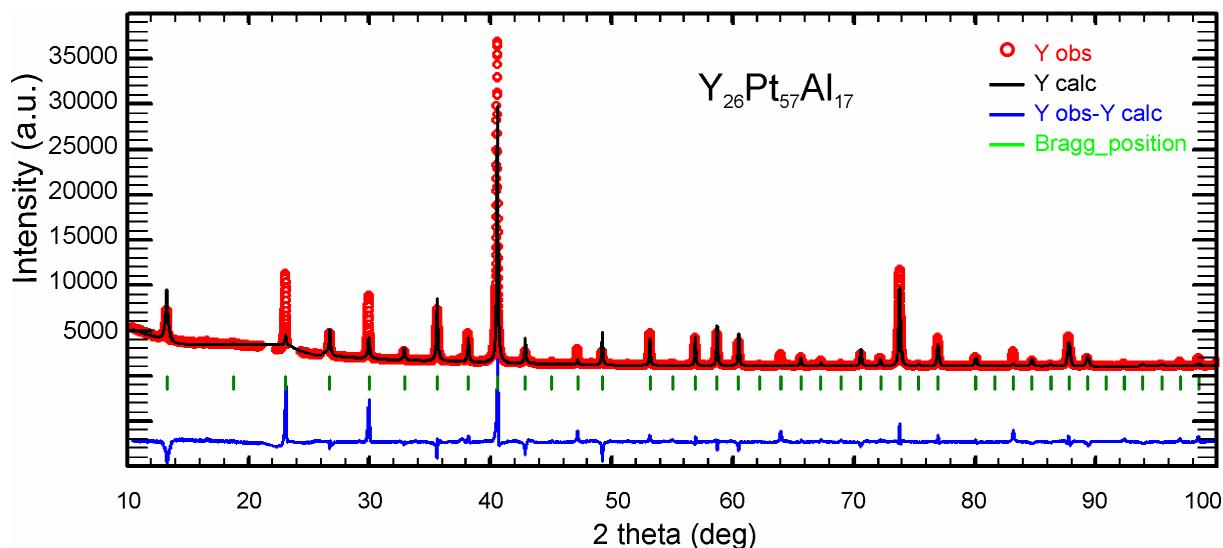
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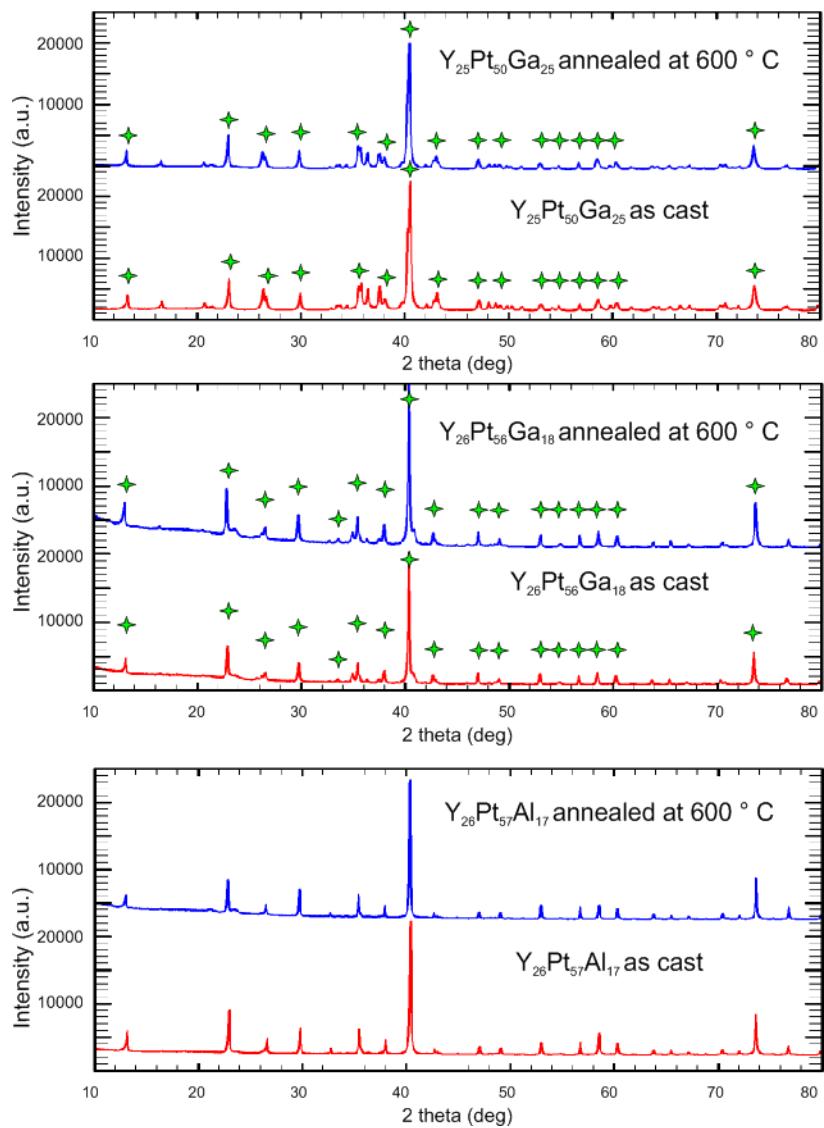
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**Figure S1.** Powder X-ray diffraction intensity data of  $\text{Y}_{26}\text{Pt}_{57}\text{Al}_{17}$  alloy refined on the basis of the  $\text{Ce}_3\text{Ni}_6\text{Si}_2$  structure model (space group  $Im-3m$ ,  $a=9.43052$  Å,  $R_F=0.190$ ,  $R_I=0.280$ ).



**Figure S2.** Powder X-ray diffraction intensity data of as cast and annealed multiphase Y-Pt-Ga alloys in comparison with single phase Y-Pt-Al alloy ( $\text{Y}_6\text{Pt}_{13}\text{Al}_4$  compound). Reflections marked with green stars correspond to  $\text{Y}_6\text{Pt}_{13}\text{Ga}_4$  phase.

# **Y<sub>6</sub>Pt<sub>13</sub>Al<sub>4</sub>: Crystallographic Information File**

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# Using CIFtbx version 2.6.2 16 Jun 1998

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# Dictionary vers : 2.2
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Refinement of F^2 against ALL reflections. The weighted R-factor wR and
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on F, with F set to zero for negative F^2. The threshold expression of
F^2 > 2sigma(F^2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F^2 are statistically about twice as large as those based on F, and R-
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;
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Pt1 Al1 Y1 60.182(4) 81 77 ?  
Pt1 Al1 Y1 119.818(4) 9 77 ?  
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# **Y<sub>6</sub>Pt<sub>13</sub>Ga<sub>4</sub>: Crystallographic Information File**

#\#CIF\_1.1

# CIF produced by WinGX routine CIF\_UPDATE  
# Created on 2023-01-28 at 14:56:34  
# Using CIFtbx version 2.6.2 16 Jun 1998

# Dictionary name : cif\_core.dic  
# Dictionary vers : 2.2  
# Request file : \wingx\files\archive.dat  
# CIF files read : yptga1\_5

data\_yptga1\_5

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\_audit\_creation\_method 'WinGX routine CIF\_UPDATE'  
\_audit\_conform\_dict\_name cif\_core.dic  
\_audit\_conform\_dict\_version 2.2  
\_audit\_conform\_dict\_location ftp://ftp.iucr.org/pub/cif\_core.dic  
\_publ\_requested\_category FI

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# CHEMICAL INFORMATION #  
#-----#

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;  
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#-----#  
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#-----#

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\_symmetry\_space\_group\_name\_Hall '-I 4 2 3'  
\_symmetry\_Int\_Tables\_number 229

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_cell_formula_units_Z	2
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_cell_measurement_wavelength	0.71073
_cell_measurement_reflns_used	6167

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_exptl_crystal_size_min        0.05
_exptl_crystal_density_diffrn   13.192
_exptl_crystal_density_method   'not measured'
_exptl_crystal_F_000           2744
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;
?
;

#-----#
#      ABSORPTION CORRECTION       #
#-----#


_exptl_absorpt_coefficient_mu    133.955
_exptl_absorpt_correction_type   none

#-----#
#      DATA COLLECTION            #
#-----#


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_diffrn_radiation_type          MoK\alpha
_diffrn_radiation_monochromator   graphite
_diffrn_measurement_device_type  'Bruker APEX II CCD area-detector'
_diffrn_reflns_av_R_equivalents   0.099
_diffrn_reflns_av_unetl/netl     0.0272
_diffrn_reflns_number            6167
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_diffrn_reflns_limit_k_min       -15
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_diffrn_reflns_limit_l_min       -15
_diffrn_reflns_limit_l_max       14
_diffrn_reflns_theta_min         3.05
_diffrn_reflns_theta_max         35.13
_diffrn_reflns_theta_full        35.13
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_reflns_number_total             220
_reflns_number_gt                192
_reflns_threshold_expression     >2sigma(I)

#-----#
#      COMPUTER PROGRAMS USED       #
#-----#


_computing_structure_refinement  'SHELXL-97 (Sheldrick, 1997)'

#-----#
#      REFINEMENT INFORMATION        #
#-----#


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;
Refinement of F^2 against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F^2, conventional R-factors R are based
on F, with F set to zero for negative F^2. The threshold expression of
F^2 > 2sigma(F^2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F^2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
;
_refine_ls_structure_factor_coef  Fsqd

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_refine_ls_matrix_type      full
_refine_ls_weighting_scheme calc
_refine_ls_weighting_details
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_atom_sites_solution_primary direct
_atom_sites_solution_secondary difmap
_atom_sites_solution_hydrogens 'none'
_refine_ls_hydrogen_treatment 'none'
_refine_ls_extinction_method SHELLXL
_refine_ls_extinction_expression
  Fc^*^=kFc[1+0.001xFc^2^|l^3^/sin(2\q)]^-1/4^
_refine_ls_extinction_coef   0.000042(12)
_refine_ls_number_reflns     220
_refine_ls_number_parameters 13
_refine_ls_number_restraints 0
_refine_ls_R_factor_all      0.0281
_refine_ls_R_factor_gt        0.0191
_refine_ls_wR_factor_ref      0.0353
_refine_ls_wR_factor_gt        0.0339
_refine_ls_goodness_of_fit_ref 1.052
_refine_ls_restrained_S_all    1.052
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_refine_ls_shift/su_mean       0
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_refine_diff_density_min      -2.742
_refine_diff_density_rms       0.446

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Pt Pt -1.7033 8.3905 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
YY YY -2.7962 3.5667 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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  _atom_site_occupancy
  _atom_site_symmetry_multiplicity
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  _atom_site_refinement_flags
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Ga1 Ga 0.25 0.25 0.25 0.0076(3) Uani 1 12 d S ..

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  _atom_site_aniso_U_-13
  _atom_site_aniso_U_12
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Pt1 0.00388(17) 0.00646(12) 0.00646(12) 0.00154(10) 0 0
Y1 0.0063(6) 0.0058(3) 0.0058(3) 0 0 0
Ga1 0.0076(3) 0.0076(3) 0.0076(3) 0.0029(4) 0.0029(4) 0.0029(4)

#-----#
#      MOLECULAR GEOMETRY      #
#-----#

```

```

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All esds (except the esd in the dihedral angle between two l.s. planes)
are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
and torsion angles; correlations between esds in cell parameters are only
used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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Ga1 Y1 3.3737(4) 81 ?
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Ga1 Y1 3.3737(4) 5 ?
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Pt1 Y1 Pt1 53.434(8) 27\_554 9 ?  
Pt1 Y1 Pt1 120.27(3) 25\_544 9 ?  
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Pt1 Y1 Pt1 120.27(3) 73 53 ?  
Pt1 Y1 Pt1 120.27(3) 75\_545 53 ?  
Pt1 Y1 Pt1 53.434(8) 27\_554 53 ?

Pt1 Y1 Pt1 53.434(8) 25\_544 53 ?  
Pt1 Y1 Pt1 89.692(3) 9 53 ?  
Pt1 Y1 Pt1 171.60(5) 7 53 ?  
Pt1 Y1 Pt1 89.692(3) 11 53 ?  
Pt2 Y1 Ga1 81.88(2) . 2 ?  
Pt1 Y1 Ga1 149.36(4) 73 2 ?  
Pt1 Y1 Ga1 95.074(11) 75\_545 2 ?  
Pt1 Y1 Ga1 95.074(11) 27\_554 2 ?  
Pt1 Y1 Ga1 46.884(5) 25\_544 2 ?  
Pt1 Y1 Ga1 135.112(4) 9 2 ?  
Pt1 Y1 Ga1 135.112(4) 7 2 ?  
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Pt2 Y1 Ga1 81.88(2) . . ?  
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Pt2 Y1 Ga1 81.88(2) . 28\_545 ?  
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Pt1 Y1 Ga1 46.545(2) 11 28\_545 ?  
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Ga1 Y1 Ga1 88.857(6) 2 28\_545 ?  
Ga1 Y1 Ga1 88.857(6) . 28\_545 ?  
Pt1 Ga1 Pt1 64.532(5) . 81 ?  
Pt1 Ga1 Pt1 115.468(5) . 9 ?  
Pt1 Ga1 Pt1 180 81 9 ?  
Pt1 Ga1 Pt1 180 . 73 ?  
Pt1 Ga1 Pt1 115.468(5) 81 73 ?  
Pt1 Ga1 Pt1 64.532(5) 9 73 ?  
Pt1 Ga1 Pt1 115.468(5) . 7 ?  
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Pt1 Ga1 Pt1 115.468(5) 9 7 ?  
Pt1 Ga1 Pt1 64.532(5) 73 7 ?  
Pt1 Ga1 Pt1 64.532(5) . 79 ?  
Pt1 Ga1 Pt1 115.468(5) 81 79 ?  
Pt1 Ga1 Pt1 64.532(5) 9 79 ?  
Pt1 Ga1 Pt1 115.468(5) 73 79 ?  
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Pt1 Ga1 Y1 120.91(2) . . ?  
Pt1 Ga1 Y1 119.494(7) 81 . ?  
Pt1 Ga1 Y1 60.506(7) 9 . ?  
Pt1 Ga1 Y1 59.09(2) 73 . ?  
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Pt1 Ga1 Y1 60.506(7) 79 73 ?  
Y1 Ga1 Y1 180.00(4) . 73 ?  
Y1 Ga1 Y1 73.01(3) 81 73 ?  
Pt1 Ga1 Y1 60.506(7) . 5 ?  
Pt1 Ga1 Y1 119.494(7) 81 5 ?  
Pt1 Ga1 Y1 60.506(7) 9 5 ?  
Pt1 Ga1 Y1 119.494(7) 73 5 ?  
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Y1 Ga1 Y1 106.99(3) 81 5 ?  
Y1 Ga1 Y1 106.99(3) 73 5 ?  
Pt1 Ga1 Y1 119.494(7) . 77 ?  
Pt1 Ga1 Y1 60.506(7) 81 77 ?  
Pt1 Ga1 Y1 119.494(7) 9 77 ?  
Pt1 Ga1 Y1 60.506(7) 73 77 ?  
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Y1 Ga1 Y1 106.99(3) . 77 ?  
Y1 Ga1 Y1 73.01(3) 81 77 ?  
Y1 Ga1 Y1 73.01(3) 73 77 ?  
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Pt1 Ga1 Y1 60.506(7) . 9 ?  
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Pt1 Ga1 Y1 119.494(7) 73 9 ?  
Pt1 Ga1 Y1 60.506(7) 7 9 ?  
Pt1 Ga1 Y1 119.494(7) 79 9 ?  
Y1 Ga1 Y1 73.01(3) . 9 ?  
Y1 Ga1 Y1 180 81 9 ?  
Y1 Ga1 Y1 106.99(3) 73 9 ?  
Y1 Ga1 Y1 73.01(3) 5 9 ?  
Y1 Ga1 Y1 106.99(3) 77 9 ?