Supporting information

Size-Dependent Magnetomechanically Enhanced Photothermal

Antibacterial Effect of Fe₃O₄@Au/PDA NanoDurian

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Simulation model: Modified formulae for the magnetic dipolar force, van der Waals force, and hydrodynamic drag force were employed in the simulation model.

Table S1. The weight percentage of the Au and Fe elements in the different samples

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Video S2: With or without sample constantly move under the influence of a magnetic field.

Video S3: Observation of the structure of $S-Fe_3O_4$ (aAu/PDA under a rotating magnetic field.

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Simulation model

Simulation set-up

Periodic boundary conditions were applied in the x-z and y-z planes, while shear boundary conditions were applied in the x-y plane. The number of particles was kept constant at N=2,000. Initially, the particles were randomly distributed in the simulation box with a fixed direction along the Z-axis. An external magnetic field along the Z-axis and a steady shear flow along the X-axis were suddenly applied. The simulation started and continued until the shear stress reached an equilibrium state. To reduce computational time, the simulation terminated at t=40 ms.

Inter-particle forces

The relationship between magnetization M and external field strength H of superparamagnetic Fe₃O₄ and Fe₃O₄@Au/PDA can be characterized by the Langevin function:

$$M = M_{\rm s} \left[\coth\left(\frac{H}{x}\right) - \frac{x}{H} \right] \tag{1}$$

where $x = M_s V_p / k_B T$. M_s means the saturation magnetization. Thus, the magnetic moment induced by the external field can be determined as:

$$\boldsymbol{m}_i = M \boldsymbol{V}_{\mathrm{p}} \frac{\boldsymbol{H}}{\boldsymbol{H}} \tag{2}$$

where $V_{\rm p}$ represents the volume of the particles. $H = |\mathbf{H}|$.

After magnetized by the external field, particle *i* will generate a magnetic field at the position of particle *j*:

$$\boldsymbol{H}_{i} = -\frac{1}{4\pi r_{ij}^{3}} \left[\boldsymbol{m}_{i} - 3 \left(\boldsymbol{m}_{i} \cdot \hat{\boldsymbol{r}} \right) \hat{\boldsymbol{r}} \right]$$
(3)

where r_{ij} denotes a spatial vector from the center of particle i to the spatial point. r = |r| and $\hat{r} = r/r$.

According to the point-dipole model, the magnetic force imposed on particle *i* exerted by particle *j* is given by:

$$\boldsymbol{F}_{ij}^{\mathrm{m}} = \frac{3\mu_0}{4\pi r_{ij}^4} \boldsymbol{c}_{\mathrm{m}} \Big[\Big(-\boldsymbol{m}_i \cdot \boldsymbol{m}_j + 5\boldsymbol{m}_i \cdot \hat{\boldsymbol{r}} \, \boldsymbol{m}_j \cdot \hat{\boldsymbol{r}} \Big) \hat{\boldsymbol{r}} - \big(\boldsymbol{m}_i \cdot \hat{\boldsymbol{r}} \big) \boldsymbol{m}_j - \big(\boldsymbol{m}_j \cdot \hat{\boldsymbol{r}} \big) \boldsymbol{m}_i \Big]$$
(4)

Here, the magnetic permeability of the matrix is approximately equal to $\mu_0 = 4\pi \times 10^{-7}$ N/A². c_m is a factor to correct the dipole model when two particles are very close to each other.

The van der Waals force between two particles is expressed as:

$$\boldsymbol{F}_{ij}^{\rm vdW} = \frac{A}{6} L_{ij} d^2 \left[\frac{1}{L_{ij}^2 - d^2} - \frac{1}{L_{ij}^2} \right]^2 \hat{\boldsymbol{r}}$$
(5)

The Hamaker constant is $A=3\times10^{-20}$ J. $L_{ij}=\max[r_{ij}, 1.01d]$. *d* is the average diameter of magnetic particles. In order to avoid the overlap of particles, an exponential repulsive force is introduced as:

$$\boldsymbol{F}_{ij}^{r} = -\left(\frac{3\mu_{0}M_{s}^{2}V_{p}^{2}}{2\pi d^{4}} + \boldsymbol{F}_{ij}^{vdw}\right)10^{-10\left(\frac{r_{ij}}{d}-1\right)}\hat{\boldsymbol{r}}$$
(6)

The random Brownian force acting on each particle is described as:

$$\boldsymbol{F}_{i}^{\mathrm{B}} = \boldsymbol{R} \sqrt{\frac{6\pi k_{\mathrm{B}} T d\eta}{\delta t}}$$
(7)

where **R** is a unit random vector whose components are Gaussian numbers with zero mean. $k_{\rm B}$ is the Boltzmann constant. The time interval of the Brownian force is chosen as $\delta_t = 0.1\tau_{\rm p}$. $\tau_{\rm p} = d^2\rho_{\rm p}/18\eta$ is the characteristic time of particles and $\rho_{\rm p}$ is the density of particles. η is the viscosity of the matrix. It is noted that the integral of this random force over a long time is independent on the choice of δt .

Governing equations

In a magnetic fluid, the motion of magnetic particles relative to the matrix belongs to Stokes flow with a Reynolds number of Re=0. Therefore, the hydrodynamic drag force can be modelled by Stokes law:

$$\boldsymbol{F}_{i}^{\mathrm{h}} = -3\pi\eta d\boldsymbol{c}_{\mathrm{h}} \left(\boldsymbol{v}_{i} - \boldsymbol{u}_{i} \right)$$

$$\tag{8}$$

where *vi-ui* is the velocity of particle i relative to the matrix. In concentrated magnetic fluid, the surrounding particles will enlarge the drag force. c_h is a correction factor for F_i^h , presented as:

$$c_{\rm h} = \frac{1+5.81\varphi}{\left(1-\varphi\right)^3} + 0.48 \frac{\sqrt[3]{\varphi}}{\left(1-\varphi\right)^4} + \varphi^3 \operatorname{Re}\left[0.95 + \frac{0.61\varphi^3}{\left(1-\varphi\right)^2}\right]$$
(9)

Here, φ is the volume fraction of magnetic fluid. The magnetic torque acting on a single particle is so exiguous that the rotational motion is neglectable. Considering the forces mentioned above, the equation of motion is constructed as:

$$\sum_{j\neq i} \left(\boldsymbol{F}_{ij}^{\mathrm{m}} + \boldsymbol{F}_{ij}^{\mathrm{vdW}} + \boldsymbol{F}_{ij}^{\mathrm{r}} \right) + \boldsymbol{F}_{i}^{\mathrm{B}} + \boldsymbol{F}_{i}^{\mathrm{h}} = m_{\mathrm{p}i} \boldsymbol{a}_{i}$$
(10)

Where m_{pi} is the mass of particle *i*.

The modified velocity-Verlet algorithm is employed to solve Eq. 10, in which the empirical parameter is chosen as 0.65. The magneto-induced stress tensor σ and magnetic potential energy $U_{\rm m}$ are presented as:

$$\boldsymbol{\sigma} = \frac{1}{V} \sum_{i} \left[\sum_{j>i} \boldsymbol{r}_{ij} \boldsymbol{F}_{ij} - \boldsymbol{m}_{pi} \left(\boldsymbol{v}_{i} - \boldsymbol{u}_{i} \right) \left(\boldsymbol{v}_{i} - \boldsymbol{u}_{i} \right) \right]$$
(11)

$$U_{\rm m} = \mu_0 \sum_{i} \left[-\boldsymbol{m}_i \cdot \boldsymbol{H} + \sum_{j>i} \frac{1}{4\pi r_{ij}^3} \left(\boldsymbol{m}_i \cdot \boldsymbol{m}_j - 3\boldsymbol{m}_i \cdot \hat{\boldsymbol{r}} \, \boldsymbol{m}_j \cdot \hat{\boldsymbol{r}} \right) \right]$$
(12)

Here, V is the volume of the simulation box. F_{ij} is the total inter-particle force between these two particles. $U_{\rm m}$ consists of the particle-external field section and inter-particle section.



Figure S1. HAADF-STEM images (a) and EDX elemental mapping of Au, Fe, N, O and C (b–g) and the EDX spectrum (h) of the S-Fe₃O₄@Au/PDA. Scale bar is 50 nm.

	Au (wt%)	Fe (wt%)
L-Fe ₃ O ₄		53.35
L-Fe ₃ O ₄ @Au/PDA	18.14	33.83
S-Fe ₃ O ₄		59.25
S-Fe ₃ O ₄ @Au/PDA	19.49	37.07

Table S1. The weight percentage of the Au and Fe elements in the different samples



Figure S2. UV–vis spectra of different concentrations of S-Fe₃O₄ (a), S-Fe₃O₄@Au/PDA (b), L-Fe₃O₄ (d) and L-Fe₃O₄@Au/PDA (e) dispersed in aqueous solution; (c) and (f) the extinction coefficient of different samples.



Figure S3. Temperature elevation of S-Fe₃O₄ (a) and L-Fe₃O₄ (b) with different concentrations. Temperature elevation curves of S-Fe₃O₄ (c) and L-Fe₃O₄ (d) suspension after continuous irradiation and natural cooling and a plot fitting of cooling time *vs* -ln(θ) (100 µg/mL).



Figure S4. Comparison of experimental and simulated results of magnetic field sweep test (25 wt%).



Figure S5. Variation in particle chain length of S-Fe₃O₄@Au/PDA.



Figure S6. Variation in particle chain length of L-Fe₃O₄@Au/PDA.



Figure S7. OD600 values of *S. aureus* treated with S-Fe₃O₄@Au/PDA (a-b) and L-Fe₃O₄@Au/PDA (c-d) at different concentrations and durations.



Figure S8. Photographs of *E. coli* colonies treated with Fe₃O₄, Fe₃O₄@PDA and Fe₃O₄@Au/PDA (200 μ g/mL) for 10 min under various conditions.



Figure S9. Photographs of *S. aureus* colonies treated with Fe₃O₄, Fe₃O₄@PDA and Fe₃O₄@Au/PDA (200 μ g/mL) for 10 min under various conditions.