## Supporting Information

## Grain Boundary Re-crystallization and Sub-nano Regions Leading to High Plateau

Figure of Merit for Bi<sub>2</sub>Te<sub>3</sub> Nanoflakes

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Section S1. Parallel model

The parallel model for electrical performance analysis of a composite material can be expressed as:<sup>1</sup>

$$\sigma_c = (1 - x_v) \cdot \sigma_m + x_v \cdot \sigma_v \tag{S1-1}$$

$$S_{c} = \frac{(1 - x_{v}) \cdot \sigma_{m} \cdot S_{m} + x_{v} \cdot \sigma_{v} \cdot S_{v}}{(1 - x_{v}) \cdot \sigma_{m} + x_{v} \cdot \sigma_{v}}$$
(S1-2)

 $\sigma$  is the electrical conductivity, *S* is the Seebeck coefficient,  $x_v$  is the volume fraction of secondary phase (vacuum here),  $x_v = r$  (*r* is the relative density), c denotes for composite, m denotes for matrix, and v denotes for vacuum. When  $\sigma_v = 0$  S cm<sup>-1</sup> and  $S_v = 0 \mu V$  K<sup>-1</sup> are taken into account, it can be extracted that:

$$\sigma_c = (1 - r) \cdot \sigma_m \tag{S1-3}$$

$$S_c = S_m \tag{S1-4}$$

As can be seen, the porosity r influence only the  $\sigma_c$  through vacuum compositing.  $S_c$  is still determined by the  $S_m$  of the matrix material.



Fig. S1. High-magnification TEM images of as-sintered  $Bi_2Te_3$  pellets sintered under  $T_{SPS}$  of a) 550, b) and c) 593, and d) 623 K, respectively.



Fig. S2. Measured  $\sigma$  of as-prepared Bi<sub>2</sub>Te<sub>3</sub> pellets under different  $T_{\text{SPS}}$  in comparison with the  $\sigma_{\text{m}}$  extracted by parallel model.



Fig. S3. Comparison between measured (under different  $T_{\text{SPS}}$ )  $\mu$ , extracted  $\mu_{\text{m}}$  and calculated (under different  $E_{\text{def}}$  and  $m^*$ )  $\mu$  as a function of  $n_{\text{e}}$ , at 370 K.



Fig. S4. Measured  $n_e$  of Bi<sub>2</sub>Te<sub>3</sub> pellets sintered under  $T_{SPS}$  of 550, 573, 593 and 623 K, respectively.



Fig. S5. SPB model extracted  $\eta_f$  of Bi<sub>2</sub>Te<sub>3</sub> pellets sintered under  $T_{SPS}$  of 550, 573, 593 and 623 K, respectively.



Fig. S6. Comparison between measured (under different  $T_{\text{SPS}}$ )  $S^2\sigma$ , extracted  $S^2\sigma_{\text{m}}$  and calculated (under different  $E_{\text{def}}$  and  $m^*$ )  $S^2\sigma$  as a function of  $n_{\text{e}}$ , at 370 K.



Fig. S7. Extracted  $\kappa_e$  of Bi<sub>2</sub>Te<sub>3</sub> pellets sintered under  $T_{SPS}$  of 550, 573, 593 and 623 K, respectively.



Fig. S8. Extracted L of Bi<sub>2</sub>Te<sub>3</sub> pellets sintered under  $T_{SPS}$  of 550, 573, 593 and 623 K, respectively.



Fig. S9. Comparison between evaluated  $\kappa_1$  of Bi<sub>2</sub>Te<sub>3</sub> pellets prepared under different  $T_{SPS}$  and the gray medium model-evaluted  $\kappa_{l,nb}$  of nanobulks without pores.



Fig. S10. Measured  $R_{in}$  of the of a single-leg device prepared based on the Bi<sub>2</sub>Te<sub>3</sub> pellet sintered under the  $T_{SPS}$  of 593 K under different  $\Delta T$ , comparing with the theoretical values.

Table S1. Comparison of key carrier transport properties evaluated by SPB model of  $Bi_2Te_3$ pellets prepared under different  $T_{SPS}$  and those of  $Bi_2Te_3$  matrixes (denoted by m) extracted by parallel model.

$T_{\text{SPS}}(\mathbf{K})$	$n_{\rm e} ({\rm cm}^{-3})$	$\mu$ (cm <sup>2</sup> V <sup>-1</sup>	$\mu_{ m m}( m cm^2$	$m^{*}(m_{0})$	<i>m*<sub>m</sub></i>	$E_{def}$	$E_{\rm def,m}$
		s <sup>-1</sup> )	V <sup>-1</sup> s <sup>-1</sup> )		(m <sub>0</sub> )	(eV)	(eV)
550	8.76E+19	24.7	28.1	1.17	1.17	7.68	7.20
573	6.11E+19	51.6	57.6	1.02	1.02	6.51	6.16
593	3.29E+19	99.6	108.4	0.94	0.94	5.44	5.22
623	3.15E+19	91.9	98.0	0.84	0.84	6.58	6.37

## References

1. H. Yao, Z. Fan, H. Cheng, X. Guan, C. Wang, K. Sun and J. Ouyang, *Macromol. Rapid. Comm.*, 2018, **39**, 1700727.