

Supplemental Information

Electrified CO₂ valorization in emerging nanotechnologies: A technical analysis of gas feedstock purity and nanomaterials in electrocatalytic and bio-electrocatalytic CO₂ conversion

Joshua Jack^{*a}, Aidan Weber^c, Sara Bolzman^a, Stephen McCord^b

^a Department of Civil and Environmental Engineering, University of Michigan, Ann Arbor, MI, 48109, USA

^b Global CO₂ Initiative, University of Michigan, Ann Arbor, MI, 48109, USA

^c Department of Chemical Engineering, University of Michigan, Ann Arbor, MI, 48109, USA

(*) Corresponding author address: Department of Civil and Environmental Engineering, University of Michigan, Ann Arbor, MI 48109, USA

Tel: +1 (734)-764-0452; E-mail: jdjack@umich.edu

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S1.0 Energy inputs and costs calculations

Production costs were estimated for various feed gas scenarios using reported performance metrics from recent literature. Three distinct gas feed scenarios were considered for both electrocatalytic and bio-electrocatalytic CO₂ conversion processes. Brief descriptions of each scenario are provided below.

Scenario 1, 20% CO₂: This scenario evaluated the case where a waste gas stream containing 20% (v/v) CO₂ could be used without pretreatment of the gas stream prior to

CO₂ conversion. This scenario is expected to model the emissions that might be available from a coal fired power plant or industrial cement plant or steel mill.

Scenario 2, 99% CO₂: This scenario demonstrated a case where a high purity gas stream of containing 99% (v/v) CO₂ could be used for direct CO₂ conversion without upstream separation. These calculations are relevant to concentrated emissions reported in industrial bioethanol fermentations or ammonia synthesis plants.

Scenario 3, 20% CO₂ + MEA: This scenario evaluated the case where a waste gas stream containing 30% (v/v) CO₂ is first upgraded to a 99% (v/v) CO₂ feedstock using an on-site MEA separation unit prior to CO₂ conversion. This scenario is assumed to be the standard case if significant scientific advancements are not made in CO₂ conversion operation and catalyst design. For bio-electrocatalytic analyses, 30% (v/v) CO₂ was used rather than 20% (v/v) for Scenarios 1 and 3.

For each scenario, total production costs were taken as the sum of the estimated energy costs required to produce a kg of CO₂-derived product plus the accompanying separation costs to provide the associated mass of initial CO₂ feedstock (Eq. S1). Capital costs were considered outside the scope of this initial analysis.

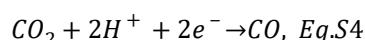
$$\text{Production cost} = \text{Energy Cost} \left(\frac{\$}{\text{kg product}} \right) + \text{Separation Cost} \left(\frac{\$}{\text{kg product}} \right), \text{Eq. S1}$$

When analyzing electrocatalytic CO₂ conversion processes, representative performance values were taken from literature for Ag nanoparticle-based electrodes¹ as these electrocatalysts show excellent potential for scale-up. Specific literature values are listed in Table S1. The first step in approximating the production costs was to estimate the energy costs per kg product via the reported power demand and production rates from the study via Eqs. S2-S6.

$$\text{Power (W)} = \text{Current density} \left(\frac{A}{\text{m}^2} \right) \times \text{Electrode surface area (m}^2\text{)} \times \text{Voltage (V)}, \text{Eq. S2}$$

$$\text{Charge utilization} \left(\frac{e^-}{\text{sec}} \right) = \text{Current (A)} \times \frac{\text{C}}{1\text{A}} \times \frac{6.25 \times 10^{18} e^-}{1\text{C}} \text{Eq. S3}$$

For electrochemical reduction of CO₂ to CO:



This means 1 mol of CO demands 1 mol of CO₂ and 2 electrons as reactants:

$$\text{Synthesis rate} \left(\frac{\text{g CO}}{\text{sec}} \right) = \text{Charge} \left(\frac{e^-}{\text{sec}} \right) \times \left(\frac{1\text{mol CO}}{2 e^-} \right) \times \left(\frac{1\text{mol CO}}{6.022 \times 10^{23}} \right) \times \left(\frac{28 \text{ g}}{1 \text{ mol CO}} \right), \text{Eq. S5}$$

$$\text{Unit power demand} \left(\frac{\text{kWh}}{\text{kg CO}} \right) = \frac{1}{\text{Synthesis Rate}} \left(\frac{\text{day}}{\text{kg CO}} \right) \times \text{Power (kWh)}, \text{Eq. S6}$$

$$\text{Energy costs} \left(\frac{\$}{kg CO} \right) = \text{Unit power demand} \left(\frac{kWh}{kg CO} \right) \times \text{Electricity costs} \left(\frac{\$}{kWh} \right), \text{Eq. S7}$$

Electricity costs were estimated using leveledized costs of energy (LCOE) from a recent U.S. Energy Information Administration (EIA) report². Similar calculations were also used to calculate acetate production costs via a bio-electrocatalytic CO₂ conversion process using values for an RVC NT cathode³. Initially the power demand was estimated using Eq.S2. In this case, the total cell voltage was approximated using Eq.S8 assuming an overpotential for the anode oxygen evolution reaction of 0.27V, as commonly reported in literature⁴.

$$E_{cell} = E_{cathode} - E_{anode}, \text{ Eq.S8}$$

Notably, the acetate synthesis rate was used directly from literature as the columbic efficiency was nearly 100%. As such, the unit power demand and energy costs were calculated using variations of Eq. S6-S7 for acetate production rather than CO.

In Scenario 3, separation costs were included using unit separation costs estimates from a recent IPCC Special Report on Carbon Dioxide Capture and Storage⁵. Assuming the theoretical 1:1 molar ratio of CO₂ to CO (Eq. S7) can be achieved and the separation energy demands can be calculated using Eq. S9. Similar equations can also be derived for acetate production.

$$\begin{aligned} \text{Unit separation energy} \left(\frac{kWh}{kg CO} \right) \\ = \text{Capture energy} \left(\frac{kWh}{kg CO_2} \right) \times MW_{CO_2} \left(\frac{kg CO_2}{mol} \right) \times \left(\frac{1 mol CO_2}{1 mol CO} \right) \times \frac{1}{MW_{CO}} \left(\frac{kg}{mol CO} \right), \text{Eq. S9} \end{aligned}$$

The unit separation energy values were then multiplied by EIA leveledized costs of energy to estimate the total separation costs for Scenario 3. This value was then added directly to the energy costs for CO₂ conversion via Eq. S1.

Table S1: Reported electrochemical performance metrics

Parameter	Value	Units
V_{cell}	3.0	V
J_{CO} , 20% (v/v)	39	$\frac{mA}{cm^2}$
J_{CO} , 99% (v/v)	52	$\frac{mA}{cm^2}$
Surface Area	1	cm^2

Table S2: Reported bio-electrochemical performance metrics

Parameter	Value	Units
$V_{cathode}$	-0.45	V

J_{co} , 30% (v/v)	34	$\frac{A}{cm^2}$
J_{co} , 99% (v/v)	35	$\frac{A}{cm^2}$
Synthesis Rate 30% (v/v)	275	$\frac{g}{m^2 day}$
Synthesis Rate, 99% (v/v)	300	$\frac{g}{m^2 day}$
Surface Area	1.36	cm^2

2.0 Carbon footprint calculations

The expected carbon footprint was predicted for each feedstock scenario described in section S1.0. Overall, the unit power demand (Eq. S6) and unit separation energy (Eq. S9) were used to estimate the energy demand per mass of product generated (e.g. kWh per kg CO) for both the CO₂ conversion and separation processes. The total unit energy demands were then calculated by summing these values (Eq. S10).

$$\begin{aligned} \text{Total unit energy} \left(\frac{kWh}{kg \text{ product}} \right) \\ = \text{Unit power demand} \left(\frac{kWh}{kg \text{ product}} \right) + \text{Unit separation energy} \left(\frac{kWh}{kg \text{ product}} \right), \text{ Eq. S10} \end{aligned}$$

The carbon footprint was then calculated for various energy sources using the carbon intensity for energy source from a recent IPCC Special Report on Carbon Dioxide Capture and Storage via Eq. S11.

$$\begin{aligned} \text{Carbon footprint} \left(\frac{kg \text{ CO}_2 \text{ eq}^-}{kg \text{ product}} \right) \\ = \text{Total unit energy} \left(\frac{kWh}{kg \text{ product}} \right) \times \text{Carbon intensity of energy} \left(\frac{kg \text{ CO}_2 \text{ eq}^-}{kWh} \right), \text{ Eq. S11} \end{aligned}$$

3.0 Energy source abbreviations

Abbreviation	Power Source
Biomass	Conventional biomass energy
CC	Natural gas fired combined cycle energy
Coal	Ultra-supercritical coal energy
GT	Large-scale geothermal energy
Offshore	Off-shore wind energy
Onshore	On-shore wind farm energy
Solar	Solar photovoltaics

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