Supplementary Information

An efficient, green, and residual oxidant-free wastewater treatment technology enabled by coupling dual-cathode heterogeneous electro-Fenton and UV radiation in tandem

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Text S1. Chemicals

Carbon black (CB, Vulcan XC-72), polytetrafluoroethylene (PTFE, 60%), 1,10phenanthroline (C₁₂H₈N₂, 99%), and potassium titanium (IV) oxalate (K₂TiO(C₂O₄)₂, \geq 98%) were purchased from Shanghai Aladdin Biological Technology Co., Ltd. Anhydrous sodium sulfate (Na₂SO₄, 99%), iron(III) chloride hexahydrate (FeCl₃·6H₂O, 99%), sodium hydroxide (NaOH, 96%), tert-butyl alcohol (TBA, \geq 99%), methanol (MeOH, 99.5%), dimethyl sulfoxide (DMSO, >99.8%), pbenzoquinone (BQ, \geq 99%), oxytetracycline (OTC, 95%), tetracycline (TC, \geq 98), ranitidine (RNTD, \geq 98%), sulfamethoxazole (SMX, 98%), 2,2,6,6-tetramethyl-4piperidinoland (TEMP, 99%), and 5,5-dimethylpyrroline-1-oxide (DMPO, 97%) were supplied by Shanghai Macklin Biochemical Co., Ltd. Graphite felt (GF, Shanghai Hongjun Industry Co., Ltd.) was used in the preparation of air-diffusion cathode (ADC) and FeOCl/GF catalytic cathode. Ti mesh electrode coated with noble metal Pt was used as the anode material and was bought from Suzhou Shuertai Industrial Technology Co., Ltd.

Text S2. Characterizations

The contact angle of ADC was recorded using a contact angle instrument (Kruss DSA30). The morphology and elemental distribution of ADC and FeOCI/GF was characterized by scanning electron microscopy (SEM) (Tescan Mira4) coupled with X-ray energy dispersive spectroscopy (EDS) (Oxford). The crystalline structures of different materials were analyzed using an X-ray diffractometer (XRD) (Rigaku Ultima IV) with a Cu kα radiation. X-ray photoelectron spectroscopy (XPS) (Thermo Scientific) was used to determine the changes in the relative concentrations of different iron species on the FeOCI/GF surface before and after the reaction.



Fig. S1. Schematic illustration of the UV system.



Fig. S2. Cross-sectional SEM image of ADC electrode and contact angle of the catalytic layer (inset).



Fig. S3. Fe, O, Cl, and C elemental mapping of the FeOCl/GF catalytic cathode.



Fig. S4. Comparison of the accumulation concentration of H_2O_2 in the dual-cathode system with no current applied to the FeOCl/GF cathode and the ADC single-cathode system.



Fig. S5. High-resolution XPS spectra of Fe 2p for FeOCl/GF pre- and post-degradation reaction.



Fig. S6. Comparison of the total Fe leaching of FeOCl/GF catalytic cathode with or without PTFE post-treatment in three runs.



Fig. S7. OTC degradation performance of homogeneous EF driven by Fe^{2+} (1.4 mg/L) leached from FeOCl/GF catalytic cathode (conditions: ADC cathode, Ti/Pt mesh anode, [OTC] = 20 mg/L, pH = 4, and $I_{ADC} = 25 \text{ mA/cm}^2$).



Fig. S8. Apparent reaction kinetic curve for OTC degradation at a current density of 5 mA/cm^2 applied to both ADC and FeOCl/GF cathodes.



Fig. S9. Comparison of the decomposition rate of H_2O_2 by FeOCl/GF catalytic cathode and UV radiation: (a) ~50 mg/L, (b) ~100 mg/L, and (c) ~200 mg/L.



Fig. S10. Effect of different initial solution pH on process efficiency: (a–c) pH = 4, (d–f) pH = 6, and (g–i) pH = 8. OTC degradation performance in different systems (first row), corresponding H₂O₂ concentration evolution (second row), and comparison of apparent rate constant *k* (third row) (conditions: [OTC] = 20 mg/L, $I_{ADC} = 100 \text{ mA/cm}^2$, $I_{FeOCI/GF} = 5 \text{ mA/cm}^2$, and UV = 6 W).

For the UV system, it can be observed that the degradation rate of OTC by direct photolysis gradually increases from 40.0% at pH 4 (Fig. S10a) to 53.6% at pH 8 (Fig. S10g), which may be related to the different predominant OTC species at different pH values. In fact, there are many dissociated forms of OTC at pH range of 3–8.5 $(H_3OTC^+, H_2OTC, HOTC^-, and OTC^{2-})$ with distinct physicochemical properties.¹ And OTC²⁻ was found to be the fastest degradable form for the photolysis followed

by HOTC⁻, H₂OTC, and H₃OTC⁺ by the increasing molar absorptivity at 254 nm,² which explained the accelerated degradation of OTC with increasing pH in the UV system. In contrast, the degradation kinetics of OTC in the HEF system showed a tendency to decrease with pH (0.04114 min⁻¹ at pH 4 and 0.01373 min⁻¹ at pH 8), which was because the alkaline microenvironment on the surface of the catalytic cathode aggravated the hydrolysis reaction of the active Fe center, thereby reducing the Fenton activity of the cathode to H₂O₂.³ This is supported by the increase in the residual unactivated concentration of H₂O₂ in the HEF effluent from 201.8 mg/L at pH 4 (Fig. S10b) to 615.2 mg/L at pH 8 (Fig. S10h). In addition, an increase in solution alkalinity also resulted in decreased total iron leaching from the FeOCI/GF interface, which could attenuate the contribution of homogeneous EF (albeit weak overall) to the degradation of OTC, as demonstrated in Fig. S11.

Unlike both the HEF and UV systems, the best OTC degradation efficiency in the UV/H₂O₂ system was found to be achieved at pH 6. Alkaline media are well known to facilitate the formation of hydroperoxide anion (HO₂⁻, a deprotonated form of H₂O₂) in H₂O₂ solution, which was reported to have higher molar absorptivity than H₂O₂ and therefore has the potential to produce more •OH under UV irradiation.⁴ Indeed, the residual concentration of H₂O₂ in the UV/H₂O₂ system decreased from 416.4 mg/L at pH 4 (Fig. S10b) to 181.1 mg/L at pH 8 (Fig. S10h). Furthermore, as well established by Liu et al., the reactivity of different dissociated forms of OTC toward •OH follows the following order: OTC²⁻ > HOTC⁻ > H₂OTC > H₃OTC⁺ (i.e., increases with increasing pH).¹ Notwithstanding the above, an increase in pH simultaneously leads to a significant decrease in the redox potential of •OH according to the Nernst equation (Eq. (S1)).⁵ In addition, considering that •OH react with HO₂⁻ (Eq. (S2)) two orders of magnitude faster than with H₂O₂ (Eq.(11) in the main text),¹ the risk of •OH being scavenged by predominant HO₂⁻ at circumneutral and basic pH conditions will be increased. Taking these together, the *k* value was found to be highest at pH 6 for the UV/H₂O₂ system. Similarly, the HEF/UV tandem system also achieved optimal coupling and degradation efficiency at pH 6, which was considered to be a compromise between the different reaction characteristics of each subprocess in terms of initial solution pH.

$$E_{\bullet OH} = E^{0}_{\bullet OH} - 0.059 pH$$
 (S1)

$$HO_2^- + \bullet OH \to OH^- + HO_2^{\bullet} \quad k = 7.5 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$$
 (S2)



Fig. S11. (a) Concentration of total Fe leached from FeOCl/GF surface at different initial solution pH and (b) corresponding OTC degradation performance by induced homogeneous EF (conditions: ADC cathode, Ti/Pt mesh anode, [OTC] = 20 mg/L, and $I_{ADC} = 100 \text{ mA/cm}^2$).



Fig. S12. Evolution of TEMP- $^{1}O_{2}$ signal intensity with reaction time in the HEF/UV tandem system.



Fig. S13. Effect of different Na₂SO₄ electrolyte concentrations on OTC degradation (conditions: $[OTC] = 20 \text{ mg/L}, \text{ pH} = 4, I_{ADC} = 100 \text{ mA/cm}^2, I_{FeOCI/GF} = 5 \text{ mA/cm}^2, \text{ and}$ UV = 6 W).



Fig. S14. OTC degradation in the presence of various quenching agents ([TBA] = 100 mM, [MeOH] = 100 mM, [BQ] = 2.5 mM, and [TEMP] = 1.0 mM).



Fig. S15. Effect of DMSO concentration on OTC degradation in the dual-cathode HEF and UV tandem system.



Fig. S16. Total Fe concentration leached from the FeOCl/GF catalytic cathode in the HEF/UV tandem system during 10 consecutive runs.



Fig. S17. MS spectra of intermediates detected during OTC degradation by the HEF/UV tandem system at different reaction times: (a) 0 min and (b) 10 min.



Fig. S18. Possible transformation pathways of OTC in the dual-cathode HEF and UV

tandem system.

Cathode	Electrolyte	Current density (mA/cm ²)	O ₂ source	H ₂ O ₂ yield (mg/cm ² /h)	CE (%)	EEC (kWh/kg)	Ref.
GDE	0.05 M Na ₂ SO ₄	28.9	O ₂ aeration	19.2	88.1	11.6	6
GDE	0.05 M Na ₂ SO ₄	35.7	Air aeration	12.2	51-88	15.9	7
GDE	0.05 M Na ₂ SO ₄	65	Air aeration	13.9	33.8	53.9	8
GDE	0.1 M K ₂ SO ₄	-1.1 V vs. SCE	O ₂ aeration	1.1	-	18.8	9
GDE	Solid electrolyte	3-50	Air aeration	1.8-20.3	79.1– 58.4	3.7-34.6	10
INAC	0.1 M Na ₂ SO ₄	14.3	Open air	6.5	~70	7.6	11
ABC	0.05 M Na ₂ SO ₄	30	Open air	16.1	~80	10.4	12
GDE	0.1 M Na ₂ SO ₄	-1.0 V vs. Ag/AgCl	O ₂ aeration	5.1	57.3	7.2	13
GDE	0.05 M H ₂ SO ₄	8	O ₂ aeration	_	40	<8	14
ADC	0.05 M Na ₂ SO ₄	5-100	Open air	3.3-54.1	85.3– 100	5.3-44.2	This work

Table S1. Comparison of energy consumption for H_2O_2 production with literature.

GDE: gas diffusion electrode; INAC: integrated natural air-diffusion cathode; ABC: air breathing cathode; ADC: air-diffusion cathode.

Samples	Tap water	River water	Lake water
pH	7.04	6.82	6.91
COD (mg/L)	-	<15	<15
NH ₃ (mg/L)	-	0.30	0.09
NO_3^- (mg/L)	1.40	2.73	0.11
PO_4^{3-} (mg/L)	-	0.01	< 0.01
$Cl^{-}(mg/L)$	15.90	22.77	4.19
CO_3^{2-} (mg/L)	-	98.20	16.90
Conductivity (µS/cm)	182.80	356.00	47.20

 Table S2. Specific water quality parameters for different real water matrices.

Note: "-" means that the parameter was undetected or the concentration of the target parameter is below the detection limit. River water and lake water were collected from Dasha river of Shenzhen city and Tsinghua SIGS campus, respectively.

Compounds	Formula	m/z	Proposed structure
OTC	$C_{22}H_{24}N_2O_9$	461.1	HO CH ₃ OH OH OH O OH O O OH O OH O O
P1	$C_{22}H_{24}N_2O_{10}$	476.3	$HO \qquad CH_3 \qquad OH \qquad O$
P2	C ₂₂ H ₂₃ NO ₉	446.2	HO CH ₃ OH
Р3	$C_{20}H_{20}N_2O_9$	433.2	HO CH ₃ OH NH ₂ OH O OH O NH ₂
P4	C ₂₁ H ₂₁ NO ₉	432.3	HO CH ₃ OH NH OH OH OH OH O OH O
Р5	$C_{20}H_{18}N_2O_8$	415.2	CH ₃ O NH ₂ OH O OH O NH ₂
P6	C ₂₀ H ₁₉ NO ₈	401.3	HO CH ₃ OH NH ₂ OH O O OH O

 Table S3. Mass spectrometry information and structures of the possible intermediates.



P14	$C_{16}H_{14}O_{6}$	302.3	O OH OH OH OH
P15	$C_{11}H_{20}O_4$	217.2	OH OH OH OH

C 1	Acute toxicity (mg/L)			Chronic toxicity (mg/L)			II 1 4
Compounds	Fish (LC ₅₀)	Daphnid (LC ₅₀)	Algae (EC ₅₀)	Fish (ChV)	Daphnid (ChV)	Algae (ChV)	Hazard category
OTC	178	9.34	45.8	3.36	2.36	7.91	Toxic ^a
P1	60.7	3.04	8.35	0.466	0.666	1.30	Very toxic
P2	170	8.95	43.5	3.20	2.26	7.54	Toxic
Р3	1.40×10^{3}	11.9	104	5.37	3.13	12.1	Toxic
P4	190	9.54	51.5	3.66	2.44	8.50	Toxic
Р5	174	4.54	19.0	1.03	1.06	2.67	Toxic
Р6	110	3.62	13.1	0.716	0.828	1.90	Very toxic
Р7	1.02×10^{3}	452	93.5	96.4	42.7	392	Harmful
P8	35.6	2.08	5.17	0.290	0.449	0.826	Very toxic
Р9	46.1	2.31	6.33	0.354	0.505	0.987	Very toxic
P10	6.33	4.80	1.48	0.832	0.679	7.36	Very toxic
P11	30.9	1.87	4.53	0.255	0.401	0.728	Very toxic
P12	168	520	18.3	160	53.0	141	Harmful
P13	56.5	2.36	7.28	0.403	0.526	1.10	Very toxic
P14	270	132	24	27.5	15.1	54.4	Harmful
P15	9.94×10^{4}	4.25×10^4	9.85×10^{3}	6.96×10^{3}	1.89×10^{3}	1.38×10^{3}	Not harmful

Table S4. Acute and chronic toxicity of OTC and its degradation intermediates predicted by ECOSAR software.

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lowest of

acute toxicity values between and within the different trophic levels (fish, daphnid and algae) were used to define the appropriate hazard category of the compounds. According to the system established by the Globally Harmonized System of Classification and Labeling of Chemicals (GHS), the predicted toxicity values of TC and all intermediates can be divided into four categories: very toxic ($LC_{50}/EC_{50}/ChV < 1$ mg/L), toxic ($1 \text{ mg/L} < LC_{50}/EC_{50}/ChV < 10 \text{ mg/L}$), harmful ($10 \text{ mg/L} < LC_{50}/EC_{50}/ChV < 100 \text{ mg/L}$), and not harmful ($LC_{50}/EC_{50}/ChV > 100 \text{ mg/L}$).

TOC	ъU	Conductivity	SS	TN	NH ₃ -N	TDS
(mg/L)	рп	(µS/cm)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
237	7.15	5030	226	78	18	3144

 Table S5. Specific water quality parameters for real antibiotic wastewater.

SS: suspended solids; TN: total nitrogen; TDS: total dissolved solids.

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