

## Supporting Information

# Interfacial processing engineering of co-grinding agent for recycling of spent lithium-ion batteries

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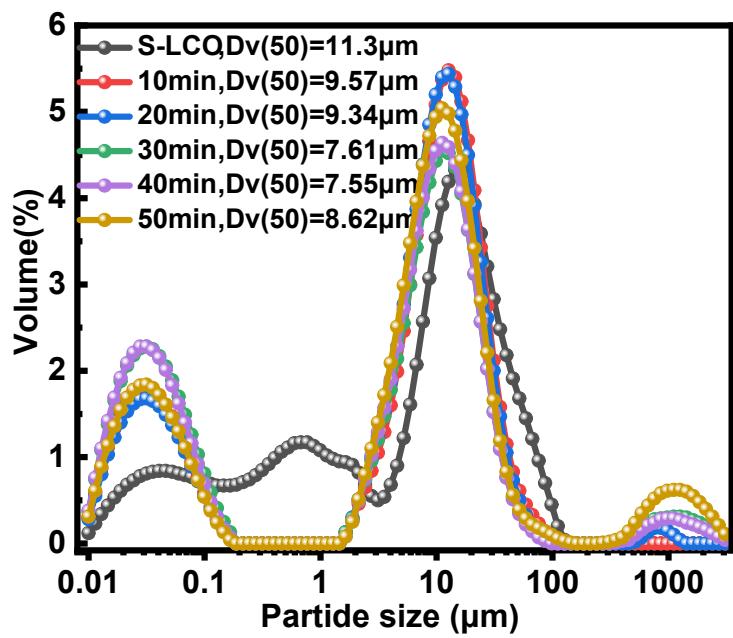
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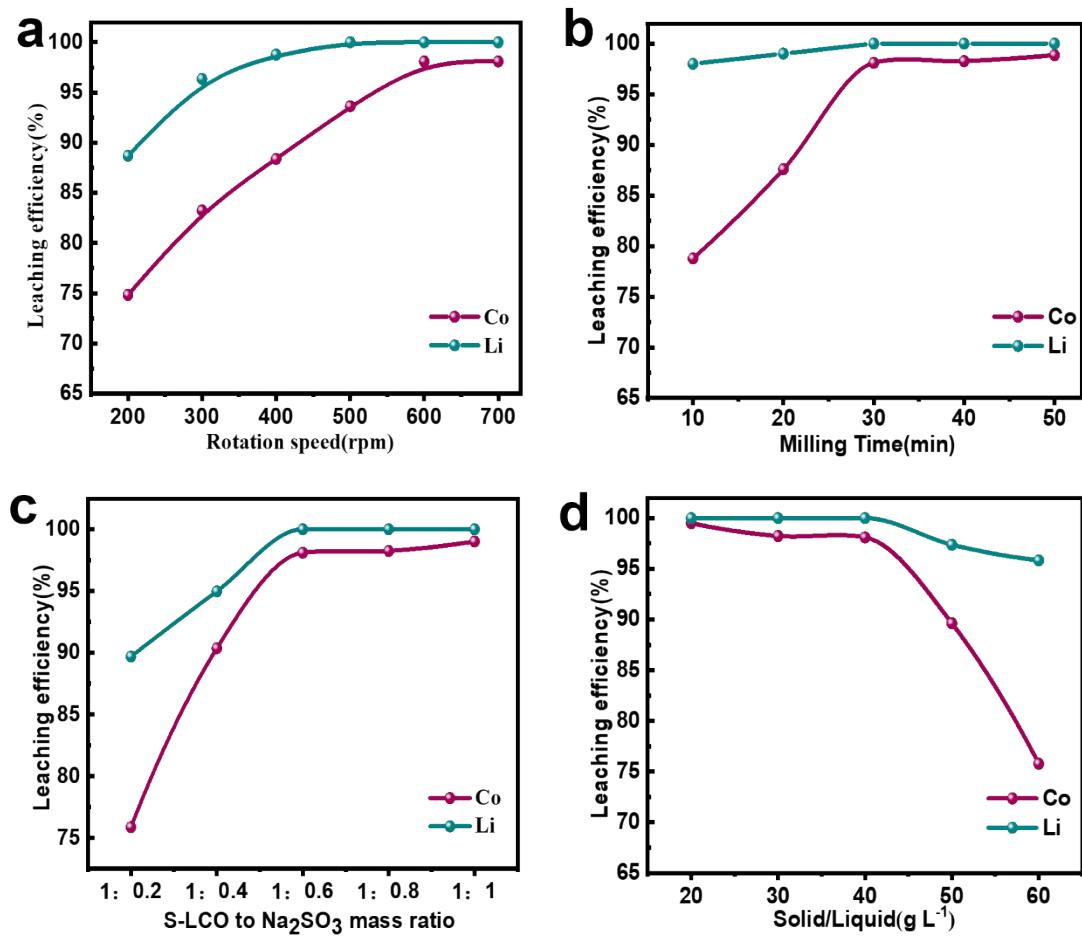
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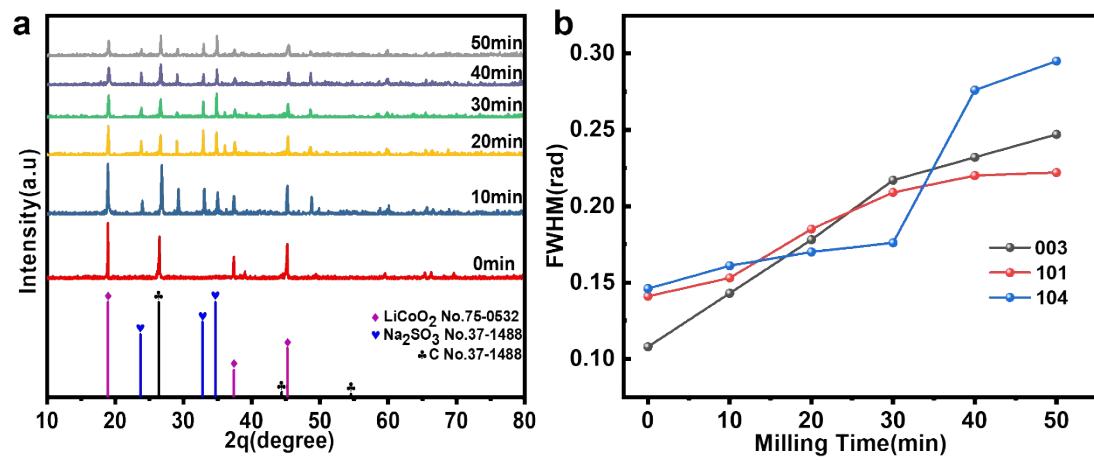
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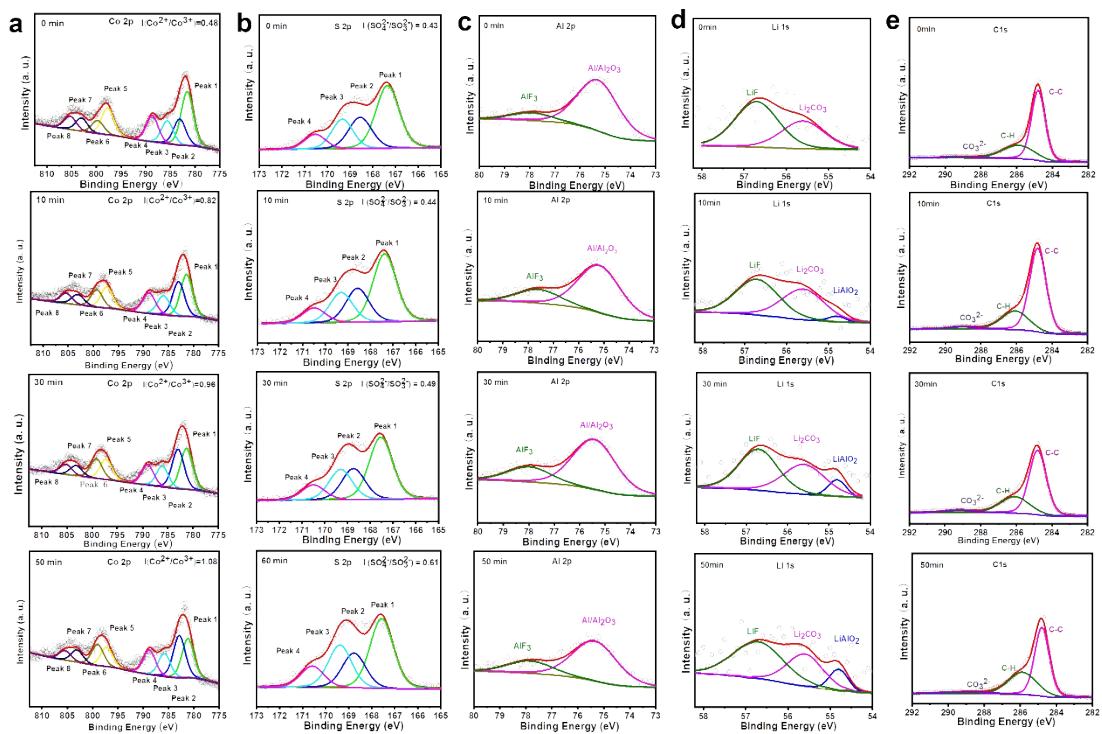
**Figure S1.** Particle size distribution of S-LCO powders activated at 600 rpm for different milling times.



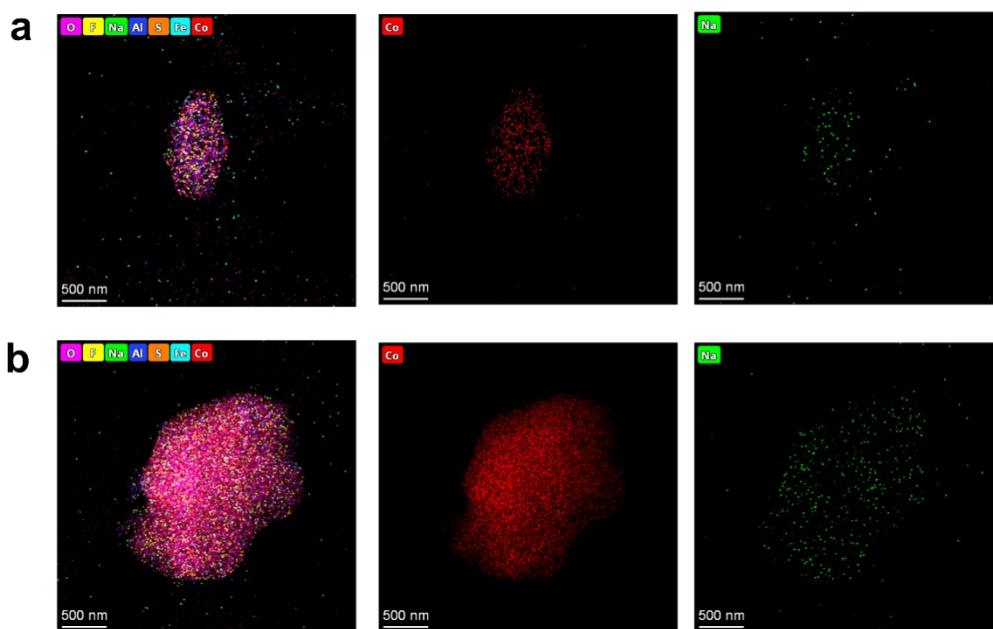
**Figure S2.** Effect of (a) rotation speed, (b) milling time, (c) mass ratio and (d) solid/liquid on the leaching efficiencies of valuable metals in S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders.



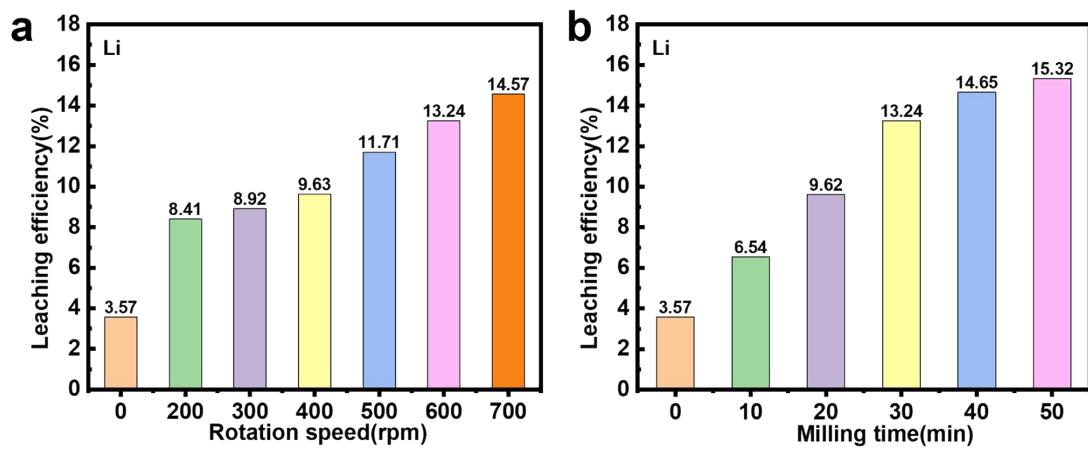
**Figure S3.** (a) XRD patterns, (b) FWHM of S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders activated at 600 rpm for different milling times.



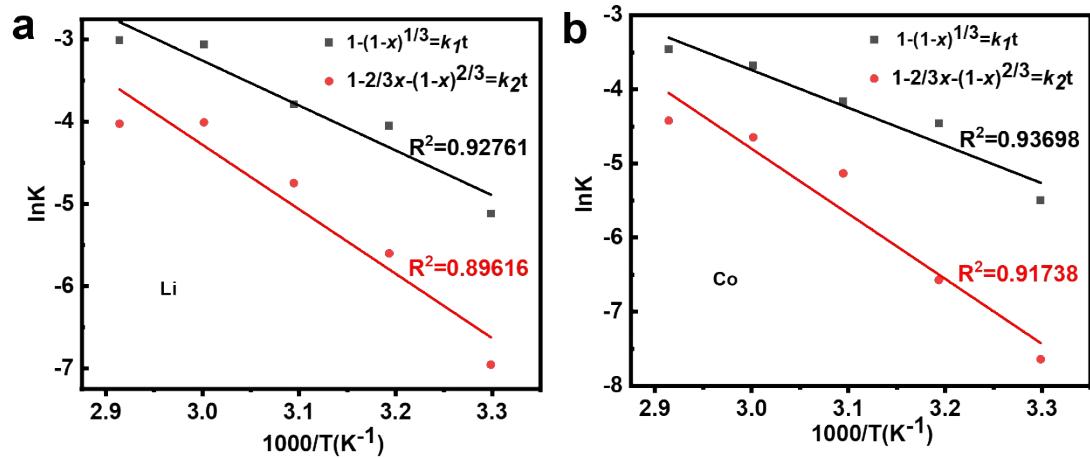
**Figure S4.** High-resolution XPS spectra of (a) Co 2p, (b) S 2p, (c) Al 2p, (d) Li 1s and (e) C 1s of the S-LCO/Na<sub>2</sub>SO<sub>3</sub> (mass ratio of 1:0.6) powders activated at 600 rpm for different milling times.



**Figure S5.** EDS mapping of elements Co and Na of the S-LCO/Na<sub>2</sub>SO<sub>3</sub> (mass ratio of 1:0.6) powders before activation (0 min) and after activated at 600 rpm for 30 min.



**Figure S6.** The leaching efficiency of Li in water from S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders under different activation conditions: (a) milling 30 min at different rotation speeds, (b) milling different times at 600 rpm (Leaching conditions: after the mechanochemical reaction, using deionized water as the leaching agent, Li<sup>+</sup> was directly leached at room temperature with a solid-liquid ratio of 40 g L<sup>-1</sup>).



**Figure S7.** Arrhenius plots for leaching of (a) Li and (b) Co from the S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders activated at 600 rpm for 30 min.

**Table S1.** Fitting peaks of XPS spectra for the Co 2p of S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders activated at 600 rpm for different milling times.

		Co 2p <sub>3/2</sub>				Co 2p <sub>1/2</sub>				I(Co <sup>2+</sup> /Co <sup>3+</sup> )
		Peak1 Co <sup>3+</sup>	Peak2 Co <sup>2+</sup>	Peak3 Co <sup>2+</sup> Sat	Peak4 Co <sup>3+</sup> Sat	Peak5 Co <sup>3+</sup>	Peak6 Co <sup>2+</sup>	Peak7 Co <sup>2+</sup> Sat	Peak8 Co <sup>3+</sup> Sat	
0	Position(eV)	781.60	783.11	785.61	788.65	797.70	799.71	802.99	805.33	0.48
	Aera (%)	27.74	13.45	11.48	13.19	13.87	6.72	6.59	6.93	
10min	Position(eV)	781.40	782.97	785.96	788.86	797.3	799.29	803.09	805.41	0.83
	Aera (%)	23.44	19.84	11.88	12.73	12.07	9.92	6.36	6.03	
30min	Position(eV)	781.31	782.98	786.09	788.97	797.24	799.15	803.16	805.18	0.96
	Aera (%)	22.42	21.54	11.49	11.29	11.21	10.77	5.64	5.60	
50min	Position(eV)	781.20	782.90	785.83	788.81	797.23	799.03	803.09	805.47	1.08
	Aera (%)	20.36	22.06	12.03	12.82	10.18	11.03	6.41	5.09	

The data of the fitting peaks of the Co 2p XPS spectra was calculated by the XPS peak software.

$$\text{Content of Co}^{2+} = (\text{Aera}_{\text{peak}2} + \text{Aera}_{\text{peak}6}) / (\text{Aera}_{\text{peak}1} + \text{Aera}_{\text{peak}2} + \text{Aera}_{\text{peak}5} + \text{Aera}_{\text{peak}6})$$

$$\text{Content of Co}^{3+} = (\text{Aera}_{\text{peak}1} + \text{Aera}_{\text{peak}5}) / (\text{Aera}_{\text{peak}1} + \text{Aera}_{\text{peak}2} + \text{Aera}_{\text{peak}5} + \text{Aera}_{\text{peak}6})$$

$$I(\text{Co}^{2+}/\text{Co}^{3+}) = \text{Content of Co}^{2+} / \text{Content of Co}^{3+}$$

**Table S2.** Fitting peaks of XPS spectra for the S 2p of S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders activated at 600 rpm for different milling times.

		S 2p <sub>3/2</sub>		S 2p <sub>1/2</sub>		I(SO <sub>4</sub> <sup>2-</sup> /SO <sub>3</sub> <sup>2-</sup> )
		Peak1	Peak3	Peak2	Peak4	
		SO <sub>3</sub> <sup>2-</sup>	SO <sub>4</sub> <sup>2-</sup>	SO <sub>3</sub> <sup>2-</sup>	SO <sub>4</sub> <sup>2-</sup>	
0	Position(eV)	167.35	169.32	168.55	170.52	0.43
	Aera (%)	46.50	20.16	23.25	10.08	
10min	Position(eV)	167.37	169.29	168.57	170.49	0.44
	Aera (%)	46.20	20.46	23.10	10.23	
30min	Position(eV)	167.54	169.30	168.74	170.50	0.49
	Aera (%)	44.82	21.85	22.41	10.92	
50min	Position(eV)	167.57	169.38	168.77	170.58	0.61
	Aera (%)	41.41	25.26	20.70	12.63	

The data of the fitting peaks of the S 2p XPS spectra was calculated by the XPS peak software.

$$\text{Content of SO}_3^{2-} = (\text{Aera}_{\text{peak1}} + \text{Aera}_{\text{peak2}}) / (\text{Aera}_{\text{peak1}} + \text{Aera}_{\text{peak2}} + \text{Aera}_{\text{peak3}} + \text{Aera}_{\text{peak4}})$$

$$\text{Content of SO}_4^{2-} = (\text{Aera}_{\text{peak3}} + \text{Aera}_{\text{peak4}}) / (\text{Aera}_{\text{peak1}} + \text{Aera}_{\text{peak2}} + \text{Aera}_{\text{peak3}} + \text{Aera}_{\text{peak4}})$$

$$I(\text{SO}_4^{2-}/\text{SO}_3^{2-}) = \text{Content of SO}_4^{2-} / \text{Content of SO}_3^{2-}$$

**Table S3.** Fitting peaks of XPS spectra for the Al 2p of S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders activated at 600 rpm for different milling times.

	Al/Al <sub>2</sub> O <sub>3</sub>	AlF <sub>3</sub>	
		Peak1	Peak2
0	Position(eV)	75.29	77.89
	Aera (%)	86.73	13.27
10min	Position(eV)	75.16	77.57
	Aera (%)	77.50	22.50
30min	Position(eV)	75.42	77.97
	Aera (%)	76.77	23.23
50min	Position(eV)	75.34	77.84
	Aera (%)	76.17	23.83

**Table S4.** Fitting peaks of XPS spectra for the C 1S of S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders activated at 600 rpm for different milling times.

	Position(eV)	C-C	C-H	CO <sub>3</sub> <sup>2-</sup>
		Peak1	Peak2	Peak3
0	Position(eV)	284.80	285.90	289.15
	Aera (%)	67.26	29.97	2.77
10min	Position(eV)	284.80	286.07	289.01
	Aera (%)	70.89	25.90	3.21
30min	Position(eV)	284.80	286.08	289.21
	Aera (%)	66.68	29.07	4.25
50min	Position(eV)	284.80	285.88	289.02
	Aera (%)	57.68	36.23	6.09

**Table S5.** The rate constant ( $k$ ) and the coefficient of determination ( $R^2$ ) for Li and Co leaching from the S-LCO/Na<sub>2</sub>SO<sub>3</sub> powders activated at 600 rpm (30 min) for different temperatures.

Model	Equation	$T(k)$	Li		Co		Ea (kJ mol <sup>-1</sup> )	
			$k$ (min <sup>-1</sup> )	$R^2$	$k$ (min <sup>-1</sup> )	$R^2$	Li	Co
Chemical reaction control	$\frac{1}{(1-x)^{\frac{1}{3}}} = k_1 t$	303.15	0.0060	0.9844	0.0041	0.9941		
		313.15	0.0175	0.9950	0.0116	0.9929		
	$\frac{1}{3}x - \frac{1}{3}(1-x)^{\frac{2}{3}} = k_1 t$	323.15	0.0227	0.9927	0.0156	0.9919	45.40	42.32
		333.15	0.0470	0.9926	0.0253	0.9955		
		343.15	0.0494	0.9888	0.0314	0.9925		
Internal diffusion control	$\frac{2}{3}x - \frac{1}{3}(1-x)^{\frac{2}{3}} = k_1 t$	303.15	9.5626E-4	0.9889	4.8076E-4	0.9979		
		313.15	0.0037	0.9973	0.0014	0.9831		
	$\frac{2}{3}x - \frac{1}{3}(1-x)^{\frac{2}{3}} = k_1 t$	323.15	0.0087	0.9846	0.0059	0.9804	65.15	72.95
		333.15	0.0182	0.9670	0.0096	0.9721		
		343.15	0.0179	0.9698	0.0120	0.9817		

**Table S6.** Test liquids and their surface tension<sup>[1-3]</sup>

Liquids	Total surface tension (mN/m)	Dispersive component (mN/m)	Polar component (mN/m)
deionized water	72.8	21.8	51.0
n-hexadecane	27.6	27.6	0.0

According to the Owens–Wendt–Rabel–Kaelble (OWRK) method, the interfacial tension of each phase can be divided into two parts: a polar component,  $\gamma^p$ , and a non-polar component (dispersion component),  $\gamma^d$ . The surface free energy between the solids and liquids is  $\gamma_{sl}$ . The relationship between  $\gamma_{sl}$ ,  $\gamma^p$  and  $\gamma^d$  can be expressed by OWRK as follows:

$$\gamma_{sl} = \gamma_l + \gamma_s - 2(\gamma_l^d \gamma_s^d)^{1/2} - 2(\gamma_l^p \gamma_s^p)^{1/2} \quad (\text{Eq. S1})$$

According to Young's equation (Eq. S2), the relationship between the contact angle of a liquid on a solid surface ( $\theta$ ) and the free energy between solid, liquid and gas can be expressed as:

$$\cos \theta = (\gamma_s - \gamma_{sl}) / \gamma_l \quad (\text{Eq. S2})$$

where  $\gamma_l$ ,  $\gamma_s$  and  $\gamma_{sl}$ , are the surface free energy of liquids, the surface free energy of solids, and the free energy at the solid–liquid interface, respectively. Substituting Eq. S1 into Eq. S2 gives:

$$\gamma_l(1 + \cos \theta) = 2(\gamma_l^d \gamma_s^d)^{1/2} + 2(\gamma_l^p \gamma_s^p)^{1/2} \quad (\text{Eq. S3})$$

$$\frac{\gamma_l(1 + \cos \theta)}{2\sqrt{\gamma_l^d}} = \sqrt{\gamma_s^p} \cdot \sqrt{\frac{\gamma_l^p}{\gamma_l^d} + \frac{\gamma_s^d}{\gamma_l^d}} \quad (\text{Eq. S4})$$

According to Eq. S4, using the data from Table S6, by plotting  $\frac{\gamma_l(1 + \cos \theta)}{2\sqrt{\gamma_l^d}}$  versus  $\sqrt{\frac{\gamma_l^p}{\gamma_l^d}}, \gamma_s^p$  and

$\gamma_s^d$  can be calculated from the slope and the intercept of the fitted line, respectively. The value of  $\gamma_s^d$  can be determined as a sum of the two surface free energy components (Eq. S5).

$$\gamma_s = \gamma_s^p + \gamma_s^d \quad (\text{Eq. S5})$$

**Table S7.** Summary of leaching parameters for leaching S-LCO in different references.

Leaching agent	Leaching condition				Leaching efficiency		Ref.
	Concentration (mol L <sup>-1</sup> )	Temperature (°C)	Time (min)	Solid-liquid ratio (g L <sup>-1</sup> )	Li (%)	Co (%)	
H <sub>2</sub> SO <sub>4</sub>	0.5	60	30	40	99.9	98.95	<b>This work</b>
H <sub>2</sub> SO <sub>4</sub>	2	80	240	35	92	88	49
H <sub>2</sub> SO <sub>4</sub>	2	60	120	33	87.5	96.3	50
H <sub>2</sub> SO <sub>4</sub>	3	95	120	25	96	98	51
H <sub>2</sub> SO <sub>4</sub>	1	95	240	20	96.7	91.6	52
HCl	4	80	120	30	97	99	53
HCl	4	80	120	20	99	99	54
HNO <sub>3</sub>	1	75	30	20	95	95	55

## References [4-8]

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