

Electronic Supplementary Materials for

Non-fouling polymer brush grafted fluorine-doped tin oxide enabled optical and chemical enhancement for sensitive label-free antibody microarrays

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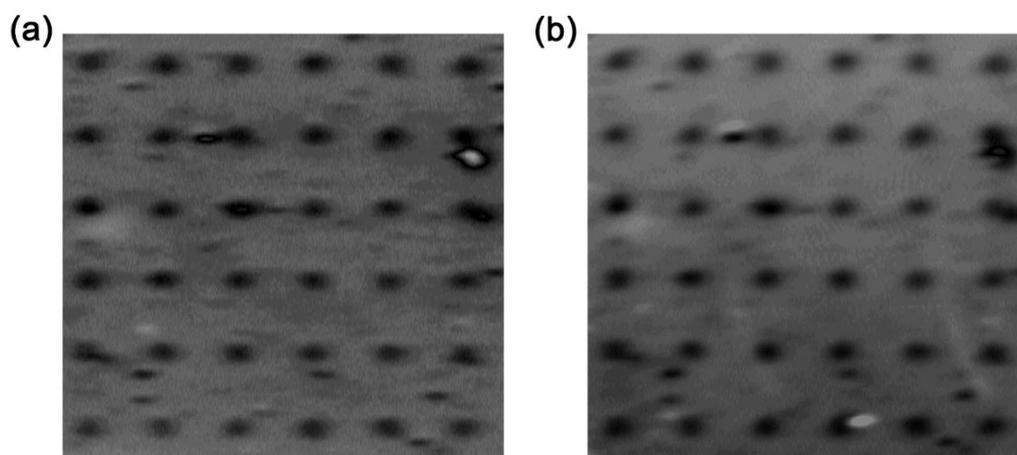


Fig. S1. OIRD images of microarray before (a) and after (b) reacting with 1 μg mL⁻¹ CRP.

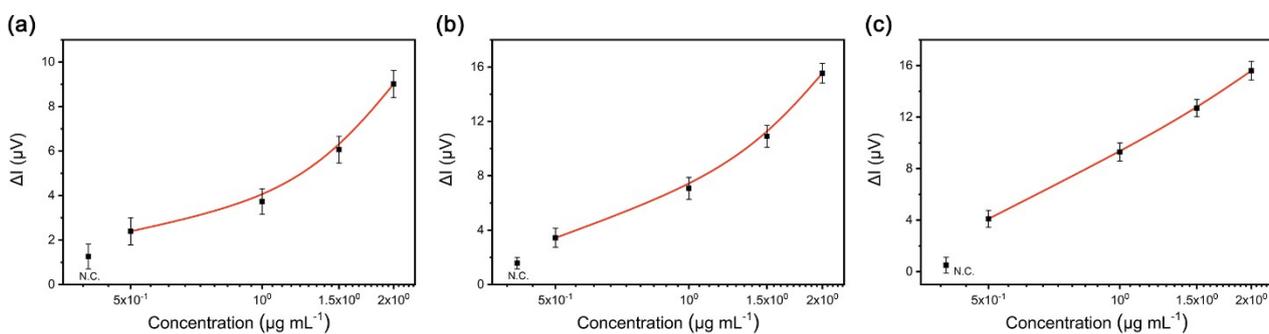


Fig. S2. Dose-response curve for detection of CRP on GPTES-glass (a), on GPTES-FTO (b) and on POEGMA-co-GMA-glass (c).

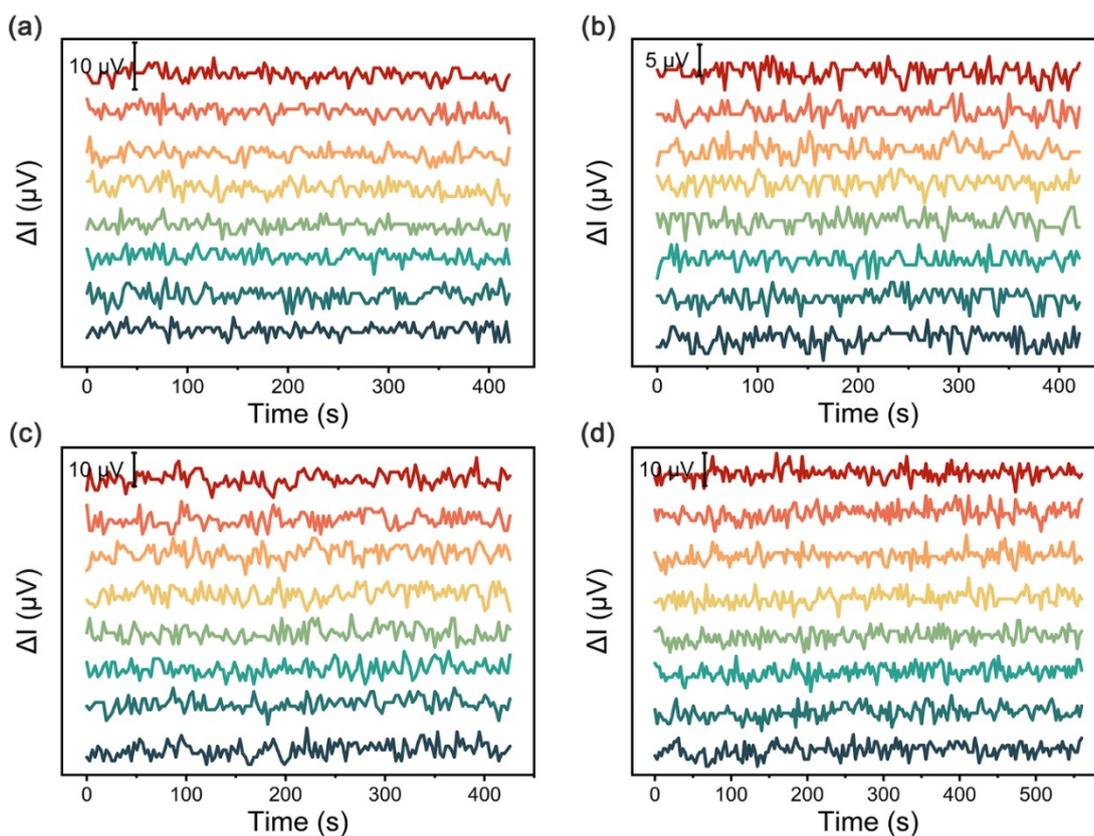


Fig. S3. *In situ* OIRD signals collected on POEGMA-co-GMA-FTO (a), POEGMA-co-GMA-glass (b), GPTES-FTO (c) and GPTES-glass (d) in 0.01 M PBS buffer. For each chip, the signals collected on 8 spots were shown.

Table S1. Thickness of POEGMA-co-GMA brush growth on FTO surface measured by ellipsometer.

| Site | a | b | c | d | e |
|----------------|-------|-------|-------|-------|-------|
| Thickness (nm) | 58.11 | 58.56 | 57.96 | 59.11 | 58.31 |

Table S2. Performance of POEGMA-co-GMA brush based microarray for clinical samples.

| Sample | Initial concentration ($\mu\text{g mL}^{-1}$) ^a | Dilution multiples ^b | Measured concentration ($\mu\text{g mL}^{-1}$) ^c | Recovery (%) ^d |
|--------|--|---------------------------------|---|---------------------------|
| 10E99 | 27 | 27 | 0.79 | 79.68 |
| 10E150 | 25.4 | 20 | 0.80 | 80.08 |

^a the concentration determined by ELISA; ^b dilution multiple at which the sample was diluted before detecting with POEGMA-co-GMA-glass OIRD chip; ^c the concentration determined by POEGMA-co-GMA-glass OIRD chip; ^d Recovery = measured concentration \times Dilution multiple / initial concentration \times 100%.

Optical computation

OIRD achieves real time monitoring of surface/interface processes by measuring the time-lapsed difference between the relative changes in the reflectivity of p-polarized light and s-polarized light.

According to the OIRD principle, the OIRD signal of $I(2\Omega)$ from a certain interface is described by eqn (E1):

$$I(2\Omega) = I_0(|r_{p0}|^2 \cos^2 \alpha - |r_{s0}|^2 \sin^2 \alpha) J_2(A) \quad (E1)$$

where Ω is the modulation frequency of the photoelastic modulator. I_0 is the initial light intensity of the laser. r_{p0} and r_{s0} are the p-polarized and s-polarized reflectivity of the surface, respectively. α is the angle between the optical axis of the polarization analyzer and the p-polarized light. $J_2(A)$ is the second kind Bessel function, where A is the amplitude of the modulation phase of the photoelastic modulator.

For microarray chips with functional layer, the reflective interface before detection can be described with a glass/functional layer/solution three-layer model (Figure 6a). The probe attached to the surface of the chip is treated as a part of the functional layer for simplification. ϵ_s , ϵ_p and ϵ_0 represent the dielectric constants of glass, functional layer and solution, respectively. φ_s , φ_p and φ_0 represent the angles of incidence in glass, functional layer and solution. h represents the thickness of functional layer.

The OIRD signal ($I_b(2\Omega)$) collected on the surface of the microarray chip before detection is described as:

$$I_b(2\Omega) = I_0(|r_{3p}|^2 \cos^2 \alpha - |r_{3s}|^2 \sin^2 \alpha) J_2(A) \quad (E2)$$

Among them, r_{3p} and r_{3s} represent the reflectance of p-polarized light and s-polarized light at the functional layer/solution interface, respectively. $|r_{3p}|$ and $|r_{3s}|$ are the amplitudes of r_{3p} and r_{3s} .

After detection, the reflective interface can be described with a glass/functional layer/target/solution four-layer model (Figure 6a). The captured target biomolecules are scattered on the surface of the chip, which we have assumed to be a thin layer with an average thickness of d for analysis. ϵ_d and φ_d represent the dielectric constant and incident angle of the target protein, respectively.

Similarly, the OIRD signal ($I_a(2\Omega)$) collected on the surface of the microarray chip after detection can be described as:

$$I_a(2\Omega) = I_0(|r_{4p}|^2 \cos^2 \alpha - |r_{4s}|^2 \sin^2 \alpha) J_2(A) \quad (E3)$$

Among them, r_{4p} and r_{4s} represent the reflectance of p-polarized light and s-polarized light at the target/solution interface, respectively. $|r_{4p}|$ and $|r_{4s}|$ are the amplitudes of r_{4p} and r_{4s} .

The $\Delta I(2\Omega)$ signal originates from the glass/functional layer/solution three-layer to glass/functional layer /target/solution four-layer transformation. According to eqn (E1), the differential OIRD signal of $\Delta I(2\Omega)$ could be calculated by subtracting the original $I_b(2\Omega)$ signal before detection from the final $I_a(2\Omega)$ signal after detection as follows:

$$\Delta I(2\Omega) = I_a(2\Omega) - I_b(2\Omega) = I_0[(|r_{4p}|^2 - |r_{3p}|^2) \cos^2 \alpha - (|r_{4s}|^2 - |r_{3s}|^2) \sin^2 \alpha] J_2(A) \quad (E4)$$

According to the Fresnel formula, the reflectivity of p-polarized light and s-polarized light in the glass/functional layer /solution three-layer model respectively are:

$$r_{3p} = \frac{r_{sp}^{(p)} + r_{p0}^{(p)} e^{2i\psi_1}}{1 + r_{sp}^{(p)} r_{p0}^{(p)} e^{2i\psi_1}} \quad (E5)$$

$$r_{3s} = \frac{r_{sp}^{(s)} + r_{p0}^{(s)} e^{2i\psi_1}}{1 + r_{sp}^{(s)} r_{p0}^{(s)} e^{2i\psi_1}} \quad (E6)$$

Here,

$$\psi_1 = \frac{2\pi}{\lambda} h \sqrt{\varepsilon_p} \cos \varphi_p \quad (E7)$$

Among them, $r_{sp}^{(p)}$ and $r_{sp}^{(s)}$ represents the reflectance of p-polarized light and s-polarized light at the glass/functional layer interface, respectively. $r_{p0}^{(p)}$ and $r_{p0}^{(s)}$ represent the reflectance of p-polarized light and s-polarized light at the functional layer/solution interface, respectively.

According to the optical transmission matrix theory, the reflectivity of p-polarized light and s-polarized light in the glass/functional layer/target/solution four-layer model respectively are:

$$r_{4p} = \frac{r_{sp}^{(p)} + r_{pd}^{(p)} e^{2i\psi_1} + r_{d0}^{(p)} e^{2i(\psi_1 + \psi_2)} + r_{sp}^{(p)} r_{pd}^{(p)} r_{d0}^{(p)} e^{2i\psi_2}}{1 + r_{sp}^{(p)} r_{pd}^{(p)} e^{2i\psi_1} + r_{sp}^{(p)} r_{d0}^{(p)} e^{2i(\psi_1 + \psi_2)} + r_{pd}^{(p)} r_{d0}^{(p)} e^{2i\psi_2}} \quad (E8)$$

$$r_{4s} = \frac{r_{sp}^{(s)} + r_{pd}^{(s)} e^{2i\psi_1} + r_{d0}^{(s)} e^{2i(\psi_1 + \psi_2)} + r_{sp}^{(s)} r_{pd}^{(s)} r_{d0}^{(s)} e^{2i\psi_2}}{1 + r_{sp}^{(s)} r_{pd}^{(s)} e^{2i\psi_1} + r_{sp}^{(s)} r_{d0}^{(s)} e^{2i(\psi_1 + \psi_2)} + r_{pd}^{(s)} r_{d0}^{(s)} e^{2i\psi_2}} \quad (E9)$$

Here,

$$\psi_2 = \frac{2\pi}{\lambda} d \sqrt{\varepsilon_d} \cos \varphi_d \quad (E10)$$

Among them, $r_{pd}^{(p)}$ and $r_{pd}^{(s)}$ represents the reflectance of p-polarized light and s-polarized light at the functional layer/target interface, respectively. $r_{d0}^{(p)}$ and $r_{d0}^{(s)}$ represent the reflectance of p-polarized light and s-polarized light at the target/solution interface, respectively.

In general, the reflectivity of p-polarized light and s-polarized light at the a/b interface can be calculated by the

following equation:

$$r_{ab}^{(p)} = \frac{\sqrt{\varepsilon_a} \cos \varphi_b - \sqrt{\varepsilon_b} \cos \varphi_a}{\sqrt{\varepsilon_a} \cos \varphi_b + \sqrt{\varepsilon_b} \cos \varphi_a} \quad (\text{E11})$$

$$r_{ab}^{(s)} = \frac{\sqrt{\varepsilon_a} \cos \varphi_a - \sqrt{\varepsilon_b} \cos \varphi_b}{\sqrt{\varepsilon_a} \cos \varphi_a + \sqrt{\varepsilon_b} \cos \varphi_b} \quad (\text{E12})$$

Among them, $r_{ab}^{(p)}$ and $r_{ab}^{(s)}$ represent the reflectance of p-polarized light and s-polarized light at the a/b interface of the substance. ε_a and ε_b represent the dielectric constants of substances a and b, respectively. φ_a and φ_b represent the angles of incidence in media a and b, respectively.

Substitute the equation E5-E12 into the equation E4, and ignore the initial light intensity I_0 and give the corresponding parameters, the variation law of the frequency-doubling signal intensity with the thickness of the functional layer can be calculated. Some parameters are assigned to facilitate the calculation: the wavelength of the incident laser $\lambda=632.8$ nm; the angle between the optical axis of the polarization analyzer and the p-polarized light $\alpha = \pi/2$; the modulation frequency of the photoelastic modulator $\Omega=50$ kHz; the amplitude of the modulation phase of the photoelastic modulator $A=\pi$; the refractive index of the glass slide $n_s = 1.50$; the refractive index of the solution $n_0 = 1.33$; the refractive index of FTO layer $n_p = 2.10$; the refractive index of the bound target protein $n = 1.5$.

The results shown in Fig. 7b are obtained by using different n_p and h for four chips. For GPTES-glass chip, use GPTES layer as the functional layer: $n_{p1} = 1.2$, $h_1 = 2$ nm. For GPTES-FTO chip: $n_{p2} = 2.1$, $h_2 = 350$ nm. For POEGMA-co-GMA-glass chip: $n_{p3} = 1.46$, $h_3 = 58$ nm. For POEGMA-co-GMA-FTO chip: $n_{p4} = 1.976$, $h_4 = 58 + 350 = 408$ nm.

We note that in this calculation, a single “functional layer” is used to model the FTO-brush layer for POEGMA-co-GMA-FTO chip to facilitate the four-layer model; a more accurate model should consider FTO and polymer brush as separated layers as their dielectric constants are different. Unfortunately the high-level five-layer calculation is complicated and we currently do not have the infrastructure and knowledge required for this simulation. Therefore, FTO-brush is treated as a single layer in POEGMA-co-GMA-FTO chip and its effective dielectric constant is calculated with the following formula:

$$\varepsilon_p = \frac{(h_a + h_b)\varepsilon_{pa} * \varepsilon_{pb}}{h_a * \varepsilon_{pb} + h_b * \varepsilon_{pa}} \quad (\text{E13})$$

Where, h_a and ε_{pa} are the thickness and dielectric constant of the first sensing layer, and h_b and ε_{pb} are the thickness and dielectric constant of the second sensing layer. For POEGMA-co-GMA-FTO based chip, the refractive index of POEGMA-co-GMA brush layer $n_{PEG} = 1.46$, and that of FTO layer $n_{FTO} = 2.10$. According to Formula E13, the refractive index of the sensing layer can be calculated as 1.976.

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