Novel Covalent Adaptable Networks (CANs) of Ethylene/1-Octene Copolymers (EOCs)

## Made by Free-Radical Processing:

Comparison of Structure-Property Relationships of EOC CANs with EOC Thermosets

## **Supporting Information**

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## Synthesis of BiTEMPS Methacrylate (BTMA) Cross-Linker for Reprocessing Studies Via Extrusion. For reprocessing studies via extrusion, BTMA was synthesized using a modified method. In a nitrogenfilled glove box, TMPM (80.0 g, 355 mmol) was dissolved in 440 mL of pre-dried, degassed tetrahydrofuran (THF). Triethylamine (247.4 mL, 1775 mmol) was added, and the stirring solution was cooled to -35 °C in an acetone/dry ice bath. $S_2Cl_2$ (14.2 mL, 178 mmol) was dissolved in 40 mL of THF and added dropwise to the cooled solution via syringe pump over 15 min. A yellow suspension formed; this suspension was warmed to room temperature and left to stir for 30 min. After, the suspension was poured into 3 L of DI water and stirred overnight. The resulting precipitate was dissolved in diethyl ether, and two liquid-liquid extractions were performed with brine. The organic layers were combined, dried over MgSO<sub>4</sub>, and filtered. Solvent was removed under vacuum to give an oil which was mixed with 500 mL of methanol and cooled at -20 °C overnight. After, the recrystallized white solid was dried under vacuum overnight to give BTMA (52.9 g, 55%).



**Figure S1.** Possible chemistries during the preparation of EOC CANs, including single cross-links, cross-links of a run of multiple BTMA units, dangling BTMA units or runs, intra-chain loops, and permanent crosslinks.



**Figure S2.** Normalized shear storage modulus (G') as a function of curing time at 180 °C obtained by small-amplitude oscillatory shear experiment with 1.0 Hz frequency and 0.1% strain (normalization is done relative to final G' value during curing).



**Figure S3.** FTIR spectra of neat EOC-38-1, 1<sup>st</sup>-molded EOCX-38-1, and 1<sup>st</sup>-molded EOC CAN-38-1 before and after washing in boiling xylene via Soxhlet extraction. The carbonyl stretch at ~1720 cm<sup>-1</sup> indicates that BTMA was grafted to EOC backbones during reactive processing.



**Figure S4.** (a) FTIR spectra of blends of EOC-30-1 with varying amounts of BTMA and washed EOC CAN-30-1. (b) FTIR calibration curve: intensity of BTMA C=O (1720 cm<sup>-1</sup>) normalized by C–H (1470 cm<sup>-1</sup>) as a function of BTMA wt% in blends of EOC-30-1 with varying amounts of BTMA.



**Figure S5.** (a) FTIR spectra of blends of EOC-38-1 with varying amounts of BTMA and washed EOC CAN-38-1. (b) FTIR calibration curve: intensity of BTMA C=O (1720 cm<sup>-1</sup>) normalized by C–H (1470 cm<sup>-1</sup>) as a function of BTMA wt% in blends of EOC-38-1 with varying amounts of BTMA.



**Figure S6.** (a) FTIR spectra of blends of EOC-45-1 with varying amounts of BTMA and washed EOC CAN-45-1. (b) FTIR calibration curve: intensity of BTMA C=O (1720 cm<sup>-1</sup>) normalized by C–H (1470 cm<sup>-1</sup>) as a function of BTMA wt% in blends of EOC-45-1 with varying amounts of BTMA.



**Figure S7.** (a) FTIR spectra of blends of EOC-38-5 with varying amounts of BTMA and washed EOC CAN-38-5. (b) FTIR calibration curve: intensity of BTMA C=O (1720 cm<sup>-1</sup>) normalized by C–H (1470 cm<sup>-1</sup>) as a function of BTMA wt% in blends of EOC-38-5 with varying amounts of BTMA.



**Figure S8.** Tensile storage modulus (*E*') as a function of temperature and molding of (a) EOC CAN-31-30 with 5 wt% BTMA and 1 wt% DCP and (b) EOC CAN-31-30 with 10 wt% BTMA and 2 wt% DCP alongside neat EOC-31-30.



**Figure S9.** Storage modulus (*E*') at 100 °C as a function of frequency for EOCXs (filled symbols) and EOC CANs (open symbols) made from (a) EOC-30-1, (b) EOC-38-1, (c) EOC-45-1, and (d) EOC-38-5.



**Figure S10.** Tensile storage modulus (E') as a function of temperature for neat PEC as well as its failed cross-linking attempt (PEC CAN 1<sup>st</sup> Mold).



**Figure S11.** Room-temperature stress-elongation curves of EOCXs and EOC CANs made from (a) EOC-30-1, (b) EOC-38-1, (c) EOC-45-1, and (d) EOC-38-5 with their corresponding neat counterparts.



Figure S12. Strain as a function of time for EOC CAN-45-1 at 50 °C under a tensile load of 0.33 MPa.



**Figure S13.** Strain as a function of time for EOC-45-1 and EOC CAN-45-1 at 90 °C under a shear load of 3.0 kPa.



**Figure S14.** Reprocessing of  $1^{st}$ -molded EOC CANs (top) by cutting and compression-molding (180 °C, 8 MPa, 5 min) pieces into healed films as the  $2^{nd}$ -mold samples (bottom). Another reprocessing step to prepare the  $3^{rd}$ -molded samples was performed in a similar manner.



**Figure S15.** Tan  $\delta$  as a function of temperature and molding of EOC CANs made from (a) EOC-30-1, (b) EOC-38-1, (c) EOC-45-1, and (d) EOC-38-5 with their corresponding EOCXs and neat counterparts.



Figure S16. Extrusion of EOC CAN-38-1 at 200 °C. Note the surface defects from melt fracture.

Material	Sample	Mold	T <sub>m,peak</sub> (°C)	T <sub>m,endpoint</sub> (°C)	Crystallinity (%)
	Neat		81	98	23
	EOCX-30-1		78	95	20
EOC-30-1		$1^{st}$	78	95	21
	EOC CAN-30-1	$2^{nd}$	78	94	21
		3 <sup>rd</sup>	78	94	20
	Neat		63	85	18
	EOCX-38-1		64	80	14
EOC-38-1		$1^{st}$	63	83	17
	EOC CAN-38-1	$2^{nd}$	62	82	16
		3 <sup>rd</sup>	64	82	17
	Neat		50	67	11
	EOCX-45-1		41	64	7
EOC-45-1	EOC CAN-45-1	$1^{st}$	39	62	7
		2 <sup>nd</sup>	40	63	8
		3 <sup>rd</sup>	40	62	8
EOC-38-5	Neat		63	85	19
	EOCX-38-5		60	81	17
	EOC CAN-38-5	$1^{st}$	60	85	17
		$2^{nd}$	61	82	18
		3 <sup>rd</sup>	61	81	17
EOC-31-30	Neat		84	96	15
PEC	Neat		142	154	14

**Table S1.** Thermal properties by DSC of neat EOCs, EOCXs, EOC CANs, and PEC as a function of molding step.

**Table S2.** Times in which  $G'(t)/G'_0 = 0.95$  ( $t_{95}$ ) during SAOS curing tests for EOC CANs and EOCXs.

Sample	<i>t</i> <sub>95</sub> (min)	
EOCX-30-1	23	
EOCX-38-1	23	
EOCX-45-1	27	
EOCX-38-5	24	
EOC CAN-30-1	27	
EOC CAN-38-1	29	
EOC CAN-45-1	30	
EOC CAN-38-5	24	

M-4	Sample	Mala	<i>E</i> ' ( <b>MP</b> a) <sup>a</sup>				
Material		NIOIO	100 °C	120 °C	140 °C	160 °C	
EOC-30-1	Neat		0.13	0.0033	0.0011	0.0009	
	EOCX-30-1		$1.4 \pm 0.3$	$1.4 \pm 0.2$	$1.3 \pm 0.2$	$1.54\pm0.01$	
	EOC CAN-30-1	1 <sup>st</sup>	$1.10\pm0.09$	$0.99\pm0.07$	$0.90\pm0.04$	$0.79\pm0.04$	
		$2^{nd}$	$1.14\pm0.06$	$1.05\pm0.03$	$1.01\pm0.02$	$0.95\pm0.01$	
		3 <sup>rd</sup>	$1.14\pm0.04$	$1.03\pm0.03$	$0.96\pm0.05$	$0.86\pm0.09$	
	Neat		0.0092	0.0015	0.0016	0.0014	
	EOCX-38-1		$1.3 \pm 0.2$	$1.3 \pm 0.2$	$1.2 \pm 0.1$	$1.2 \pm 0.1$	
EOC-38-1	EOC CAN-38-1	1 <sup>st</sup>	$0.76\pm0.08$	$0.65\pm0.04$	$0.56\pm0.02$	$0.48\pm0.03$	
		2 <sup>nd</sup>	$0.91\pm0.04$	$0.76\pm0.01$	$0.66\pm0.02$	$0.58\pm0.06$	
		3 <sup>rd</sup>	$0.84\pm0.04$	$0.74\pm0.02$	$0.65\pm0.05$	$0.59\pm0.05$	
EOC-45-1	Neat		0.0013	0.0013	0.0010	0.0010	
	EOCX-45-1		0.90	0.81	0.80	0.80	
	EOC CAN-45-1	1 <sup>st</sup>	$0.69\pm0.03$	$0.58\pm0.03$	$0.52\pm0.04$	$0.44\pm0.05$	
		$2^{nd}$	$0.75\pm0.01$	$0.63\pm0.02$	$0.56\pm0.02$	$0.52\pm0.01$	
		3 <sup>rd</sup>	$0.72\pm0.07$	$0.62\pm0.09$	$0.57\pm0.05$	$0.56\pm0.01$	
EOC-38-5	Neat		0.0011	0.0011	0.0010	0.0007	
	EOCX-38-5		$0.42\pm0.03$	$0.39\pm0.01$	$0.37\pm0.02$	$0.36\pm0.04$	
	EOC CAN-38-5	1 <sup>st</sup>	$0.37\pm0.04$	$0.29\pm0.03$	$0.23\pm0.03$	$0.15\pm0.04$	
		$2^{nd}$	$0.42\pm0.04$	$0.\overline{32\pm0.02}$	$0.23\pm0.02$	$0.17\pm0.03$	
		3 <sup>rd</sup>	$0.45 \pm 0.03$	$0.34 \pm 0.03$	$0.25 \pm 0.03$	$0.18 \pm 0.05$	

Table S3. E' as a function of temperature and molding step for neat EOCs, EOCXs, and EOC CANs.

<sup>a</sup>Determined by DMA. Error bars represent  $\pm$  one standard deviation of three or four measurements.

**Table S4.** Characteristic relaxation times, stretching exponents, average relaxation times, and KWW decay function fits as a function of temperature for EOC CANs.

EOC CAN	<i>T</i> (°C)	$\tau^{*}\left(s ight)$	β	< <b>\tau &gt;</b> (s)	<b>R</b> <sup>2</sup>
	100	208	0.26	3820	0.98
FOC CAN 20 1	120	123	0.32	869	0.98
EUC CAN-50-1	140	59	0.42	170	0.98
	160	26	0.49	55	0.99
	100	234	0.28	2960	0.97
FOC CAN 28 1	120	132	0.34	716	0.98
EUC CAN-30-1	140	63	0.45	160	0.98
	160	27	0.52	49	0.99
	100	33	0.23	1330	0.98
FOC CAN 45 1	120	29	0.30	280	0.98
EUC CAN-45-1	140	17	0.39	61	0.98
	160	8	0.54	14	0.99
	80	34	0.25	730	0.98
	100	30	0.34	160	0.97
EOC CAN-38-5	120	14	0.40	48	0.98
	140	7.6	0.55	13	0.98
	160	< 1		< 1	

**Table S5.** Room-temperature tensile properties of 1<sup>st</sup>-, 2<sup>nd</sup>-, and 3<sup>rd</sup>-molded EOC CANs.

Sample	Mold	Young's modulus (MPa) <sup>a</sup>	Tensile strength (MPa) <sup>a</sup>	Elongation at break (%) <sup>a</sup>
	1 <sup>st</sup>	$21.7\pm1.1$	$13.4 \pm 2.1$	$650\pm70$
EOC CAN-30-1	2 <sup>nd</sup>	$18.6\pm3.5$	$14.4\pm0.7$	$660 \pm 30$
	3 <sup>rd</sup>	$18.7 \pm 3.3$	$16.7 \pm 3.1$	$670 \pm 30$
	$1^{st}$	$7.6 \pm 3.5$	$14.9\pm1.9$	$700 \pm 110$
EOC CAN-38-1	2 <sup>nd</sup>	$8.5\pm0.8$	$12.1\pm4.0$	$670 \pm 60$
	3 <sup>rd</sup>	$8.3 \pm 0.3$	$13.0\pm0.6$	$710 \pm 50$
	1 <sup>st</sup>	$3.0 \pm 0.1$	$5.1 \pm 1.2$	$830 \pm 120$
EOC CAN-45-1	2 <sup>nd</sup>	$3.0\pm0.6$	$5.0 \pm 1.3$	$790 \pm 80$
	3 <sup>rd</sup>	$2.6 \pm 0.3$	$5.4 \pm 1.2$	$850 \pm 130$
	1 <sup>st</sup>	$7.8\pm0.9$	$8.7\pm1.2$	$760\pm80$
EOC CAN-38-5	2 <sup>nd</sup>	$8.4 \pm 0.8$	$7.9 \pm 2.4$	$800 \pm 190$
	3 <sup>rd</sup>	$8.2 \pm 1.0$	$10.8 \pm 2.2$	$910 \pm 220$

<sup>a</sup>Determined by tensile testing. Error bars represent  $\pm$  one standard deviation of three measurements.