# Novel Covalent Adaptable Networks (CANs) of Ethylene/1-Octene Copolymers (EOCs) Made by Free-Radical Processing: <br> Comparison of Structure-Property Relationships of EOC CANs with EOC Thermosets 

## Supporting Information

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## Synthesis of BiTEMPS Methacrylate (BTMA) Cross-Linker for Reprocessing Studies Via Extrusion.

For reprocessing studies via extrusion, BTMA was synthesized using a modified method. In a nitrogenfilled glove box, TMPM ( $80.0 \mathrm{~g}, 355 \mathrm{mmol}$ ) was dissolved in 440 mL of pre-dried, degassed tetrahydrofuran (THF). Triethylamine ( $247.4 \mathrm{~mL}, 1775 \mathrm{mmol}$ ) was added, and the stirring solution was cooled to $-35^{\circ} \mathrm{C}$ in an acetone/dry ice bath. $\mathrm{S}_{2} \mathrm{Cl}_{2}(14.2 \mathrm{~mL}, 178 \mathrm{mmol})$ was dissolved in 40 mL of THF and added dropwise to the cooled solution via syringe pump over 15 min . A yellow suspension formed; this suspension was warmed to room temperature and left to stir for 30 min . After, the suspension was poured into 3 L of DI water and stirred overnight. The resulting precipitate was dissolved in diethyl ether, and two liquid-liquid extractions were performed with brine. The organic layers were combined, dried over $\mathrm{MgSO}_{4}$, and filtered. Solvent was removed under vacuum to give an oil which was mixed with 500 mL of methanol and cooled at $-20^{\circ} \mathrm{C}$ overnight. After, the recrystallized white solid was dried under vacuum overnight to give BTMA ( $52.9 \mathrm{~g}, 55 \%$ ).


Figure S1. Possible chemistries during the preparation of EOC CANs, including single cross-links, crosslinks of a run of multiple BTMA units, dangling BTMA units or runs, intra-chain loops, and permanent crosslinks.


Figure S2. Normalized shear storage modulus ( $G^{\prime}$ ) as a function of curing time at $180^{\circ} \mathrm{C}$ obtained by small-amplitude oscillatory shear experiment with 1.0 Hz frequency and $0.1 \%$ strain (normalization is done relative to final $G^{\prime}$ value during curing).


Figure S3. FTIR spectra of neat EOC-38-1, $1^{\text {st }}$-molded EOCX-38-1, and $1^{\text {st }}$-molded EOC CAN-38-1 before and after washing in boiling xylene via Soxhlet extraction. The carbonyl stretch at $\sim 1720 \mathrm{~cm}^{-1}$ indicates that BTMA was grafted to EOC backbones during reactive processing.


Figure S4. (a) FTIR spectra of blends of EOC-30-1 with varying amounts of BTMA and washed EOC CAN-30-1. (b) FTIR calibration curve: intensity of BTMA C=O ( $1720 \mathrm{~cm}^{-1}$ ) normalized by C-H (1470 $\mathrm{cm}^{-1}$ ) as a function of BTMA wt \% in blends of EOC-30-1 with varying amounts of BTMA.


Figure S5. (a) FTIR spectra of blends of EOC-38-1 with varying amounts of BTMA and washed EOC CAN-38-1. (b) FTIR calibration curve: intensity of BTMA C=O $\left(1720 \mathrm{~cm}^{-1}\right)$ normalized by C-H (1470 $\mathrm{cm}^{-1}$ ) as a function of BTMA wt $\%$ in blends of EOC-38-1 with varying amounts of BTMA.


Figure S6. (a) FTIR spectra of blends of EOC-45-1 with varying amounts of BTMA and washed EOC CAN-45-1. (b) FTIR calibration curve: intensity of BTMA $\mathrm{C}=\mathrm{O}\left(1720 \mathrm{~cm}^{-1}\right)$ normalized by $\mathrm{C}-\mathrm{H}(1470$ $\mathrm{cm}^{-1}$ ) as a function of BTMA wt\% in blends of EOC-45-1 with varying amounts of BTMA.


Figure S7. (a) FTIR spectra of blends of EOC-38-5 with varying amounts of BTMA and washed EOC CAN-38-5. (b) FTIR calibration curve: intensity of BTMA C=O $\left(1720 \mathrm{~cm}^{-1}\right)$ normalized by C-H (1470 $\mathrm{cm}^{-1}$ ) as a function of BTMA wt\% in blends of EOC-38-5 with varying amounts of BTMA.


Figure S8. Tensile storage modulus ( $E^{\prime}$ ) as a function of temperature and molding of (a) EOC CAN-31-30 with $5 \mathrm{wt} \%$ BTMA and $1 \mathrm{wt} \%$ DCP and (b) EOC CAN-31-30 with $10 \mathrm{wt} \%$ BTMA and $2 \mathrm{wt} \%$ DCP alongside neat EOC-31-30.


Figure S9. Storage modulus ( $E^{\prime}$ ) at $100^{\circ} \mathrm{C}$ as a function of frequency for EOCXs (filled symbols) and EOC CANs (open symbols) made from (a) EOC-30-1, (b) EOC-38-1, (c) EOC-45-1, and (d) EOC-38-5.


Figure S10. Tensile storage modulus ( $E^{\prime}$ ) as a function of temperature for neat PEC as well as its failed cross-linking attempt (PEC CAN $1^{\text {st }}$ Mold).


Figure S11. Room-temperature stress-elongation curves of EOCXs and EOC CANs made from (a) EOC-30-1, (b) EOC-38-1, (c) EOC-45-1, and (d) EOC-38-5 with their corresponding neat counterparts.


Figure S12. Strain as a function of time for EOC CAN-45-1 at $50^{\circ} \mathrm{C}$ under a tensile load of 0.33 MPa .


Figure S13. Strain as a function of time for EOC-45-1 and EOC CAN-45-1 at $90^{\circ} \mathrm{C}$ under a shear load of 3.0 kPa .

## EOC CAN-30-1 EOC CAN-38-1 EOC CAN-45-1 EOC CAN-38-5



Figure S14. Reprocessing of $1^{\text {st }}$-molded EOC CANs (top) by cutting and compression-molding ( $180^{\circ} \mathrm{C}$, 8 MPa, 5 min ) pieces into healed films as the $2^{\text {nd }}$-mold samples (bottom). Another reprocessing step to prepare the $3^{\text {rd }}$-molded samples was performed in a similar manner.


Figure S15. Tan $\delta$ as a function of temperature and molding of EOC CANs made from (a) EOC-30-1, (b) EOC-38-1, (c) EOC-45-1, and (d) EOC-38-5 with their corresponding EOCXs and neat counterparts.


Figure S16. Extrusion of EOC CAN-38-1 at $200^{\circ} \mathrm{C}$. Note the surface defects from melt fracture.

Table S1. Thermal properties by DSC of neat EOCs, EOCXs, EOC CANs, and PEC as a function of molding step.

| Material | Sample | Mold | $\boldsymbol{T}_{\text {m,peak }}\left({ }^{\circ} \mathbf{C}\right)$ | $\boldsymbol{T}_{\text {m,endpoint }}\left({ }^{\circ} \mathbf{C}\right)$ | Crystallinity (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| EOC-30-1 | Neat | -- | 81 | 98 | 23 |
|  | EOCX-30-1 | -- | 78 | 95 | 20 |
|  | EOC CAN-30-1 | $1{ }^{\text {st }}$ | 78 | 95 | 21 |
|  |  | $2^{\text {nd }}$ | 78 | 94 | 21 |
|  |  | $3{ }^{\text {rd }}$ | 78 | 94 | 20 |
| EOC-38-1 | Neat | -- | 63 | 85 | 18 |
|  | EOCX-38-1 | -- | 64 | 80 | 14 |
|  | EOC CAN-38-1 | $1^{\text {st }}$ | 63 | 83 | 17 |
|  |  | $2^{\text {nd }}$ | 62 | 82 | 16 |
|  |  | $3{ }^{\text {rd }}$ | 64 | 82 | 17 |
| EOC-45-1 | Neat | -- | 50 | 67 | 11 |
|  | EOCX-45-1 | -- | 41 | 64 | 7 |
|  | EOC CAN-45-1 | $1{ }^{\text {st }}$ | 39 | 62 | 7 |
|  |  | $2^{\text {nd }}$ | 40 | 63 | 8 |
|  |  | $3{ }^{\text {rd }}$ | 40 | 62 | 8 |
| EOC-38-5 | Neat | -- | 63 | 85 | 19 |
|  | EOCX-38-5 | -- | 60 | 81 | 17 |
|  | EOC CAN-38-5 | $1^{\text {st }}$ | 60 | 85 | 17 |
|  |  | $2^{\text {nd }}$ | 61 | 82 | 18 |
|  |  | $3{ }^{\text {rd }}$ | 61 | 81 | 17 |
| EOC-31-30 | Neat | -- | 84 | 96 | 15 |
| PEC | Neat | -- | 142 | 154 | 14 |

Table S2. Times in which $G^{\prime}(t) / G^{\prime}{ }_{0}=0.95\left(t_{95}\right)$ during SAOS curing tests for EOC CANs and EOCXs.

| Sample | $\boldsymbol{t}_{\mathbf{9 5}}(\mathbf{m i n})$ |
| :---: | :---: |
| EOCX-30-1 | 23 |
| EOCX-38-1 | 23 |
| EOCX-45-1 | 27 |
| EOCX-38-5 | 24 |
| EOC CAN-30-1 | 27 |
| EOC CAN-38-1 | 29 |
| EOC CAN-45-1 | 30 |
| EOC CAN-38-5 | 24 |

Table S3. $E^{\prime}$ as a function of temperature and molding step for neat EOCs, EOCXs, and EOC CANs.

| Material | Sample | Mold | $E^{\prime}(\mathbf{M P a})^{\mathbf{a}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $100{ }^{\circ} \mathrm{C}$ | $120{ }^{\circ} \mathrm{C}$ | $140{ }^{\circ} \mathrm{C}$ | $160{ }^{\circ} \mathrm{C}$ |
| EOC-30-1 | Neat | -- | 0.13 | 0.0033 | 0.0011 | 0.0009 |
|  | EOCX-30-1 | -- | $1.4 \pm 0.3$ | $1.4 \pm 0.2$ | $1.3 \pm 0.2$ | $1.54 \pm 0.01$ |
|  | EOC CAN-30-1 | $1^{\text {st }}$ | $1.10 \pm 0.09$ | $0.99 \pm 0.07$ | $0.90 \pm 0.04$ | $0.79 \pm 0.04$ |
|  |  | $2^{\text {nd }}$ | $1.14 \pm 0.06$ | $1.05 \pm 0.03$ | $1.01 \pm 0.02$ | $0.95 \pm 0.01$ |
|  |  | $3{ }^{\text {rd }}$ | $1.14 \pm 0.04$ | $1.03 \pm 0.03$ | $0.96 \pm 0.05$ | $0.86 \pm 0.09$ |
| EOC-38-1 | Neat | -- | 0.0092 | 0.0015 | 0.0016 | 0.0014 |
|  | EOCX-38-1 | -- | $1.3 \pm 0.2$ | $1.3 \pm 0.2$ | $1.2 \pm 0.1$ | $1.2 \pm 0.1$ |
|  | EOC CAN-38-1 | $1^{\text {st }}$ | $0.76 \pm 0.08$ | $0.65 \pm 0.04$ | $0.56 \pm 0.02$ | $0.48 \pm 0.03$ |
|  |  | $2^{\text {nd }}$ | $0.91 \pm 0.04$ | $0.76 \pm 0.01$ | $0.66 \pm 0.02$ | $0.58 \pm 0.06$ |
|  |  | $3{ }^{\text {rd }}$ | $0.84 \pm 0.04$ | $0.74 \pm 0.02$ | $0.65 \pm 0.05$ | $0.59 \pm 0.05$ |
| EOC-45-1 | Neat | -- | 0.0013 | 0.0013 | 0.0010 | 0.0010 |
|  | EOCX-45-1 | -- | 0.90 | 0.81 | 0.80 | 0.80 |
|  | EOC CAN-45-1 | $1^{\text {st }}$ | $0.69 \pm 0.03$ | $0.58 \pm 0.03$ | $0.52 \pm 0.04$ | $0.44 \pm 0.05$ |
|  |  | $2^{\text {nd }}$ | $0.75 \pm 0.01$ | $0.63 \pm 0.02$ | $0.56 \pm 0.02$ | $0.52 \pm 0.01$ |
|  |  | $3{ }^{\text {rd }}$ | $0.72 \pm 0.07$ | $0.62 \pm 0.09$ | $0.57 \pm 0.05$ | $0.56 \pm 0.01$ |
| EOC-38-5 | Neat | -- | 0.0011 | 0.0011 | 0.0010 | 0.0007 |
|  | EOCX-38-5 | -- | $0.42 \pm 0.03$ | $0.39 \pm 0.01$ | $0.37 \pm 0.02$ | $0.36 \pm 0.04$ |
|  | EOC CAN-38-5 | $1^{\text {st }}$ | $0.37 \pm 0.04$ | $0.29 \pm 0.03$ | $0.23 \pm 0.03$ | $0.15 \pm 0.04$ |
|  |  | $2^{\text {nd }}$ | $0.42 \pm 0.04$ | $0.32 \pm 0.02$ | $0.23 \pm 0.02$ | $0.17 \pm 0.03$ |
|  |  | $3{ }^{\text {rd }}$ | $0.45 \pm 0.03$ | $0.34 \pm 0.03$ | $0.25 \pm 0.03$ | $0.18 \pm 0.05$ |

${ }^{\text {a }}$ Determined by DMA. Error bars represent $\pm$ one standard deviation of three or four measurements.

Table S4. Characteristic relaxation times, stretching exponents, average relaxation times, and KWW decay function fits as a function of temperature for EOC CANs.

| EOC CAN | $\boldsymbol{T}\left({ }^{\circ} \mathbf{C}\right)$ | $\boldsymbol{\tau}^{*}(\mathbf{s})$ | $\boldsymbol{\beta}$ | $\langle\boldsymbol{\tau}\rangle(\mathbf{s})$ | $\mathbf{R}^{\mathbf{2}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| EOC CAN-30-1 | 100 | 208 | 0.26 | 3820 | 0.98 |
|  | 120 | 123 | 0.32 | 869 | 0.98 |
|  | 140 | 59 | 0.42 | 170 | 0.98 |
|  | 160 | 26 | 0.49 | 55 | 0.99 |
|  | 100 | 234 | 0.28 | 2960 | 0.97 |
|  | 120 | 132 | 0.34 | 716 | 0.98 |
|  | 140 | 63 | 0.45 | 160 | 0.98 |
|  | 160 | 27 | 0.52 | 49 | 0.99 |
| EOC CAN-45-1 | 100 | 33 | 0.23 | 1330 | 0.98 |
|  | 120 | 29 | 0.30 | 280 | 0.98 |
|  | 140 | 17 | 0.39 | 61 | 0.98 |
|  | 160 | 8 | 0.54 | 14 | 0.99 |
|  | 80 | 34 | 0.25 | 730 | 0.98 |
|  | 100 | 30 | 0.34 | 160 | 0.97 |
|  | 120 | 14 | 0.40 | 48 | 0.98 |
|  | 140 | 7.6 | 0.55 | 13 | 0.98 |
|  | 160 | $<1$ | -- | -- |  |

Table S5. Room-temperature tensile properties of $1^{\text {st }}$, , $2^{\text {nd }}-$, and $3^{\text {rd }}$-molded EOC CANs.

| Sample | Mold | Young's modulus <br> $(\mathbf{M P a})^{\mathbf{a}}$ | Tensile strength <br> $(\mathbf{M P a})^{\mathbf{a}}$ | Elongation at break <br> $(\%)^{\mathbf{a}}$ |
| :---: | :---: | :---: | :---: | :---: |
| EOC CAN-30-1 | $1^{\text {st }}$ | $21.7 \pm 1.1$ | $13.4 \pm 2.1$ | $650 \pm 70$ |
|  | $2^{\text {nd }}$ | $18.6 \pm 3.5$ | $14.4 \pm 0.7$ | $660 \pm 30$ |
|  | $3^{\text {rd }}$ | $18.7 \pm 3.3$ | $16.7 \pm 3.1$ | $670 \pm 30$ |
|  | $1^{\text {st }}$ | $7.6 \pm 3.5$ | $14.9 \pm 1.9$ | $700 \pm 110$ |
|  | $2^{\text {nd }}$ | $8.5 \pm 0.8$ | $12.1 \pm 4.0$ | $670 \pm 60$ |
|  | $3^{\text {rd }}$ | $8.3 \pm 0.3$ | $13.0 \pm 0.6$ | $710 \pm 50$ |
| EOC CAN-45-1 | $1^{\text {st }}$ | $3.0 \pm 0.1$ | $5.1 \pm 1.2$ | $830 \pm 120$ |
|  | $2^{\text {nd }}$ | $3.0 \pm 0.6$ | $5.0 \pm 1.3$ | $790 \pm 80$ |
|  | $3^{\text {rd }}$ | $2.6 \pm 0.3$ | $5.4 \pm 1.2$ | $850 \pm 130$ |
| EOC CAN-38-5 | $1^{\text {st }}$ | $7.8 \pm 0.9$ | $8.7 \pm 1.2$ | $760 \pm 80$ |
|  | $2^{\text {nd }}$ | $8.4 \pm 0.8$ | $7.9 \pm 2.4$ | $800 \pm 190$ |
|  | $3^{\text {rd }}$ | $8.2 \pm 1.0$ | $10.8 \pm 2.2$ | $910 \pm 220$ |

${ }^{\text {a }}$ Determined by tensile testing. Error bars represent $\pm$ one standard deviation of three measurements.

