## Supporting Information

## Enhancing Continuous-Flow Reaction via Compression-Molding of Solid Catalysts and Dilutants in Packed-Bed Systems

Kwihwan Kobayashi, ${ }^{1}$ Teruhiko Tanaka, ${ }^{1}$ Kon Yoshihiro, ${ }^{1}$ Hajime Kawanami, ${ }^{* 1}$ and Nagatoshi Koumura*1
1 Interdisciplinary Research Center for Catalytic Chemistry, National Institute of Advanced Industrial Science and Technology Central 5, Higashi 1-1-1, Tsukuba, Ibaraki 305-8565, Japan
E-mail: h-kawanami@aist.go.jp, n-koumura@aist.go.jp

## Contents

## 1. General

2. Experimental setup for the flow reaction
3. Preparation of the reaction column for MCR-1000 and HCR-1000
4. Procedure for EDX analysis of Pt in the column before/after the flow reaction

## 5. Images of SEM and EDX mapping

6. Procedure and calculation for the void volume of the catalyst column
7. Results of particle size distribution
8. Procedure for ICP-AES analysis of Pt with/without compression molding
9. XPS analysis (Figure 4)
10. Procedure for the scale-up experiment for the flow reaction

## 1. General

Gas chromatography was measured on Shimadzu GC-2014 spectrometer with $\mathrm{N}_{2}$ gas as a career, using Shimadzu SH-Stabilwax-DA (Length: 30 m , I.D.: 0.250 mm , Film: $0.25 \mu \mathrm{~m}$ ). A dual plunger pump (UI-22 series) was purchased from EYELA, and flow reactor (MCR-1000, HCR-1000), Teflon filter, SUS laminated metal filter, and fraction collector (DC-1000) were purchased from EYELA. ICP-AES was measured by HORIBA ULTIMA2. Particle size distribution was measured by MICROTRACBELL MT3000II. SEM was measured by JEOL JSM-IT800. XPS was measured by Shimadzu KRATOS ULTRA2. Press machine (CDM-5PA) was purchased from RIKEN KIKI CO., Ltd. Molds (mold for heat press machine $\varphi 14$ and LD-3025) were purchased from AS ONE CORPORATION and Labonect CO., Ltd. $\mathrm{H}_{2} \mathrm{O}_{2}$ and Wakogel C-200 were purchased from FUJIFILM Wako pure chemicals. $t$-AmylOH and benzyl alcohol were purchased from Tokyo Chemical Industry Co., Ltd. $\mathrm{SiO}_{2}$-60-S was purchased from KANTO CHEMICAL CO., INC. Pt black powder was purchased from N.E. Chemcat.

## 2. Experimental setup for the flow reaction

- Reaction setup for MCR-1000 (column size ID: 10 mm , L: 100 mm )


Pump: UI-22 110P, EYELA
Flow reactor (heating controller and column reactor): MCR-1000, EYELA Fraction collector: DC-1500, EYELA

- Reaction setup for HCR-1000 (column size ID: 37 mm , L: 300 mm )


Pump for $\mathrm{H}_{2} \mathrm{O}_{2}$ aq.: UI-22 110P, EYELA
Pump for $t$-amylOH solution: LC-20AD, Shimadzu
Flow reactor (heating controller and column reactor): HCR-1000, EYELA

- Press machine and molds


Press machine: RIKEN KIKI CO., Ltd, CDM-5PA
Mold for small scale: AS ONE CORPORATION, mold for heat press machine $\varphi 14$
Mold for large scale: Labonect, LD-3025, $\varphi 30 \times 25 \mathrm{~mm}$
3. Preparation of the reaction column for MCR-1000 and HCR-1000

- Preparation of the reaction column for MCR-1000 without the compression molding

- Preparation of the reaction column for MCR-1000 with the compression molding

- Preparation of the reaction column for HCR-1000 without the compression molding

- Preparation of the reaction column for HCR-1000 with the compression molding



## 4. Procedure for EDX analysis of Pt in the column before/after the flow reaction (Table 1)

Pt black powder was pre-mixed with silica-gel and then packed into a column (ID: 10 mm , L: 100 mm . In the cases of entries 5 and 6 , the compression molding was conducted for the pre-mixed catalysts using a press machine (RIKEN KIKI CO., Ltd, CDM-5PA) and mold (AS ONE CORPORATION, mold for heat press machine $\varphi 14$ ) before packing to the reaction column. The catalyst column was set onto the reactor (EYELA, MCR-1000), and $\mathrm{H}_{2} \mathrm{O}$ was flowed at each $0.4 \mathrm{~mL} / \mathrm{min}$ (pump: EYELA, UI22110 P ) for 1 h . The catalyst column was heated at $90^{\circ} \mathrm{C}$ (heating controller and column reactor: MCR-1000). After stabilization the reaction was started by changing into feed solution of $2 \mathrm{wt} \% \mathrm{H}_{2} \mathrm{O}_{2}$ aq. and benzyl alcohol $(1,0.05 \mathrm{M})$ solution in $t$-amylOH. After 24 hours, feed solutions were changed into blank solvent, and reactor was cooled to room temperature. The catalysts were taken out from the reaction column and dried up in vacuo. The EDX of a part of dried catalysts was measured, and the amount of Pt in the reaction column was calculated.


Yields of benzaldehyde using Pt catalyst with and without CM (Table 1 entry 2 vs. entry 3 )

## 5. Images of SEM and EDX mapping (Figure 1)


(a-1): SEM image of pre-mixed Pt and $\mathrm{SiO}_{2}-60-\mathrm{S}$. (b-1): SEM image of compression molded Pt and $\mathrm{SiO}_{2}-60-\mathrm{S}$. (c): EDX mapping of pre-mixed Pt and $\mathrm{SiO}_{2}-60-\mathrm{S}$. (d): EDX mapping of compression molded Pt and $\mathrm{SiO}_{2}-60-\mathrm{S}$.

## 6. Procedure and calculation for the void volume of the catalyst column

$0.4 \mathrm{wt} \% \mathrm{Pt}$ with $\mathrm{SiO}_{2}-60-\mathrm{S}$ was packed into a column (I.D. $\varphi 10 \times 100 \mathrm{~mm}$ ). The catalyst column was sealed with plugs and weighted. Sealed plugs were removed, and the catalyst column was set onto the flow reactor. The catalyst column was filled with $t$-amylOH by the pump at $0.5 \mathrm{~mL} / \mathrm{min}$ for 30 min . After the solvent filling, the catalyst column was sealed with plugs again and weighted. Therefore, the void volume of the catalyst column was calculated as follows with the density of $t$-amylOH at $20^{\circ} \mathrm{C}$ $(0.81 \mathrm{~g} / \mathrm{mL})$.


## 7. Results of particle size distribution (Figure S1, 2, 3)



| 28.5 | 0.7 | 28.5 | 2.0 | 28.5 | 3.8 | 28.5 | 0.6 | 28.5 | 2.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26.2 | 0.4 | 26.2 | 1.5 | 26.2 | 4.0 | 26.2 | 0.4 | 26.2 | 1.5 |
| 24.0 | 0.3 | 24.0 | 1.2 | 24.0 | 4.1 | 24.0 | 0.3 | 24.0 | 1.2 |
| 22.0 | 0.2 | 22.0 | 1.0 | 22.0 | 4.2 | 22.0 | 0.2 | 22.0 | 1.0 |
| 20.2 | 0.1 | 20.2 | 0.9 | 20.2 | 4.2 | 20.2 | 0.2 | 20.2 | 0.9 |
| 18.5 | 0.0 | 18.5 | 0.9 | 18.5 | 4.1 | 18.5 | 0.2 | 18.5 | 0.9 |
| 17.0 | 0.0 | 17.0 | 1.0 | 17.0 | 4.0 | 17.0 | 0.3 | 17.0 | 0.9 |
| 15.6 | 0.1 | 15.6 | 1.0 | 15.6 | 3.8 | 15.6 | 0.3 | 15.6 | 1.0 |
| 14.3 | 0.2 | 14.3 | 1.1 | 14.3 | 3.6 | 14.3 | 0.4 | 14.3 | 1.1 |
| 13.1 | 0.2 | 13.1 | 1.1 | 13.1 | 3.5 | 13.1 | 0.5 | 13.1 | 1.1 |
| 12.0 | 0.3 | 12.0 | 1.2 | 12.0 | 3.3 | 12.0 | 0.5 | 12.0 | 1.1 |
| 11.0 | 0.3 | 11.0 | 1.1 | 11.0 | 3.1 | 11.0 | 0.6 | 11.0 | 1.1 |
| 10.1 | 0.3 | 10.1 | 1.1 | 10.1 | 3.0 | 10.1 | 0.6 | 10.1 | 1.1 |
| 9.3 | 0.3 | 9.3 | 1.0 | 9.3 | 2.9 | 9.3 | 0.6 | 9.3 | 1.0 |
| 8.5 | 0.3 | 8.5 | 0.9 | 8.5 | 2.7 | 8.5 | 0.6 | 8.5 | 1.0 |
| 7.8 | 0.2 | 7.8 | 0.8 | 7.8 | 2.6 | 7.8 | 0.6 | 7.8 | 0.9 |
| 7.1 | 0.2 | 7.1 | 0.6 | 7.1 | 2.4 | 7.1 | 0.6 | 7.1 | 0.8 |
| 6.5 | 0.2 | 6.5 | 0.5 | 6.5 | 2.2 | 6.5 | 0.5 | 6.5 | 0.7 |
| 6.0 | 0.1 | 6.0 | 0.4 | 6.0 | 2.0 | 6.0 | 0.4 | 6.0 | 0.6 |
| 5.5 | 0.0 | 5.5 | 0.3 | 5.5 | 1.8 | 5.5 | 0.4 | 5.5 | 0.5 |
| 5.0 | 0.0 | 5.0 | 0.3 | 5.0 | 1.6 | 5.0 | 0.3 | 5.0 | 0.4 |
| 4.6 | 0.0 | 4.6 | 0.2 | 4.6 | 1.4 | 4.6 | 0.3 | 4.6 | 0.3 |
| 4.2 | 0.0 | 4.2 | 0.1 | 4.2 | 1.2 | 4.2 | 0.3 | 4.2 | 0.3 |
| 3.9 | 0.0 | 3.9 | 0.0 | 3.9 | 1.0 | 3.9 | 0.2 | 3.9 | 0.2 |
| 3.6 | 0.0 | 3.6 | 0.0 | 3.6 | 0.9 | 3.6 | 0.2 | 3.6 | 0.1 |
| 3.3 | 0.0 | 3.3 | 0.0 | 3.3 | 0.8 | 3.3 | 0.0 | 3.3 | 0.0 |
| 3.0 | 0.0 | 3.0 | 0.0 | 3.0 | 0.7 | 3.0 | 0.0 | 3.0 | 0.0 |
| 2.8 | 0.0 | 2.8 | 0.0 | 2.8 | 0.6 | 2.8 | 0.0 | 2.8 | 0.0 |
| 2.5 | 0.0 | 2.5 | 0.0 | 2.5 | 0.5 | 2.5 | 0.0 | 2.5 | 0.0 |
| 2.3 | 0.0 | 2.3 | 0.0 | 2.3 | 0.5 | 2.3 | 0.0 | 2.3 | 0.0 |
| 2.1 | 0.0 | 2.1 | 0.0 | 2.1 | 0.4 | 2.1 | 0.0 | 2.1 | 0.0 |
| 1.9 | 0.0 | 1.9 | 0.0 | 1.9 | 0.4 | 1.9 | 0.0 | 1.9 | 0.0 |
| 1.8 | 0.0 | 1.8 | 0.0 | 1.8 | 0.3 | 1.8 | 0.0 | 1.8 | 0.0 |
| 1.6 | 0.0 | 1.6 | 0.0 | 1.6 | 0.3 | 1.6 | 0.0 | 1.6 | 0.0 |
| 1.5 | 0.0 | 1.5 | 0.0 | 1.5 | 0.3 | 1.5 | 0.0 | 1.5 | 0.0 |
| 1.4 | 0.0 | 1.4 | 0.0 | 1.4 | 0.2 | 1.4 | 0.0 | 1.4 | 0.0 |
| 1.3 | 0.0 | 1.3 | 0.0 | 1.3 | 0.2 | 1.3 | 0.0 | 1.3 | 0.0 |
| 1.2 | 0.0 | 1.2 | 0.0 | 1.2 | 0.2 | 1.2 | 0.0 | 1.2 | 0.0 |


| 1.1 | 0.0 | 1.1 | 0.0 | 1.1 | 0.1 | 1.1 | 0.0 | 1.1 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.0 | 0.0 | 1.0 | 0.0 | 1.0 | 0.0 | 1.0 | 0.0 | 1.0 | 0.0 |
| 0.9 | 0.0 | 0.9 | 0.0 | 0.9 | 0.0 | 0.9 | 0.0 | 0.9 | 0.0 |
| 0.8 | 0.0 | 0.8 | 0.0 | 0.8 | 0.0 | 0.8 | 0.0 | 0.8 | 0.0 |
| 0.8 | 0.0 | 0.8 | 0.0 | 0.8 | 0.0 | 0.8 | 0.0 | 0.8 | 0.0 |

## 8. Procedure for ICP-AES analysis of Pt with/without compression molding (Table 2)

Pt black powder was pre-mixed with silica-gel and then packed into a column (ID: $10 \mathrm{~mm}, \mathrm{~L}: 100 \mathrm{~mm}$. In the case of enry 2 , the compression molding was conducted for the pre-mixed catalysts using a press machine (RIKEN KIKI CO., Ltd, CDM-5PA) and mold (AS ONE CORPORATION, mold for heat press machine $\varphi 14$ ) before packing to the reaction column. The catalyst column was set onto the reactor (EYELA, MCR-1000), and the catalyst column was heated at $90^{\circ} \mathrm{C}$ (heating controller and column reactor: MCR-1000). Water was flowed at $0.4 \mathrm{~mL} / \mathrm{min}$ (Pump: UI-22 110P, EYELA). After 3 hours, pumps were stopped. The whole liquid which passed through the reaction column was evaporated. Obtained powder was dissolved by aqua regia, and the solution was analyzed the amount of Pt by the inductivity coupled plasma atomic emission spectroscopy (ICP-AES: HORIBA ULTIMA2).


## 9. XPS analysis (Figure 4)



| without compression molding |  | with compression molding |  |
| :---: | :---: | :---: | :---: |
| Binding energy (eV) | Counts per second | Binding energy (eV) | Counts per second |
| 84 | 5164.382562 | 84 | 5604.213 |
| 83.9 | 5140.777145 | 83.9 | 5592.674 |
| 83.8 | 5092.661311 | 83.8 | 5558.812 |
| 83.7 | 5070.639644 | 83.7 | 5546.896 |
| 83.6 | 5022.674643 | 83.6 | 5518.238 |
| 83.5 | 4977.273809 | 83.5 | 5482.264 |
| 83.4 | 4941.149226 | 83.4 | 5455.717 |
| 83.3 | 4930.138392 | 83.3 | 5463.862 |
| 83.2 | 4890.393808 | 83.2 | 5444.48 |
| 83.1 | 4839.864641 | 83.1 | 5433.318 |
| 83 | 4786.394224 | 83 | 5403.529 |
| 82.9 | 4767.841724 | 82.9 | 5395.761 |
| 82.8 | 4781.642974 | 82.8 | 5356.393 |
| 82.7 | 4725.759223 | 82.7 | 5346.212 |
| 82.6 | 4691.520056 | 82.6 | 5358.43 |
| 82.5 | 4663.389639 | 82.5 | 5353.226 |
| 82.4 | 4625.455055 | 82.4 | 5320.57 |
| 82.3 | 4600.793805 | 82.3 | 5277.357 |
| 82.2 | 4606.902555 | 82.2 | 5278.111 |
| 82.1 | 4577.414638 | 82.1 | 5290.856 |
| 82 | 4548.454638 | 82 | 5270.569 |
| 81.9 | 4534.879637 | 81.9 | 5255.486 |
| 81.8 | 4499.358387 | 81.8 | 5234.218 |
| 81.7 | 4489.931304 | 81.7 | 5253.6 |
| 81.6 | 4485.25547 | 81.6 | 5201.035 |
| 81.5 | 4501.394637 | 81.5 | 5234.143 |
| 81.4 | 4464.968387 | 81.4 | 5217.023 |
| 81.3 | 4441.061303 | 81.3 | 5206.163 |
| 81.2 | 4425.902553 | 81.2 | 5163.93 |
| 81.1 | 4397.395052 | 81.1 | 5193.493 |
| 81 | 4394.001302 | 81 | 5182.332 |
| 80.9 | 4401.467552 | 80.9 | 5154.126 |
| 80.8 | 4364.890469 | 80.8 | 5180.069 |
| 80.7 | 4332.235052 | 80.7 | 5171.245 |
| 80.6 | 4327.860885 | 80.6 | 5135.95 |


| 80.5 | 4322.204635 | 80.5 | 5132.858 |
| :---: | :---: | :---: | :---: |
| 80.4 | 4315.190885 | 80.4 | 5142.361 |
| 80.3 | 4301.389635 | 80.3 | 5120.339 |
| 80.2 | 4282.082968 | 80.2 | 5133.99 |
| 80.1 | 4309.006718 | 80.1 | 5130.671 |
| 80 | 4303.048801 | 80 | 5150.883 |
| 79.9 | 4298.071301 | 79.9 | 5100.731 |
| 79.8 | 4300.861718 | 79.8 | 5104.125 |
| 79.7 | 4284.345468 | 79.7 | 5112.043 |
| 79.6 | 4230.950467 | 79.6 | 5091.907 |
| 79.5 | 4272.052551 | 79.5 | 5142.135 |
| 79.4 | 4270.921301 | 79.4 | 5117.85 |
| 79.3 | 4253.877134 | 79.3 | 5100.429 |
| 79.2 | 4223.936717 | 79.2 | 5100.58 |
| 79.1 | 4245.430467 | 79.1 | 5110.761 |
| 79 | 4209.682967 | 79 | 5115.362 |
| 78.9 | 4197.314633 | 78.9 | 5120.49 |
| 78.8 | 4226.877967 | 78.8 | 5096.357 |
| 78.7 | 4236.154217 | 78.7 | 5106.161 |
| 78.6 | 4232.68505 | 78.6 | 5128.786 |
| 78.5 | 4216.319634 | 78.5 | 5124.035 |
| 78.4 | 4212.020884 | 78.4 | 5127.127 |
| 78.3 | 4210.135467 | 78.3 | 5128.71 |
| 78.2 | 4205.3088 | 78.2 | 5131.501 |
| 78.1 | 4186.228383 | 78.1 | 5131.953 |
| 78 | 4184.644633 | 78 | 5145.905 |
| 77.9 | 4183.5888 | 77.9 | 5164.307 |
| 77.8 | 4181.627967 | 77.8 | 5160.008 |
| 77.7 | 4189.094217 | 77.7 | 5128.56 |
| 77.6 | 4211.6438 | 77.6 | 5174.488 |
| 77.5 | 4212.0963 | 77.5 | 5183.689 |
| 77.4 | 4184.644633 | 77.4 | 5158.349 |
| 77.3 | 4192.563383 | 77.3 | 5166.042 |
| 77.2 | 4224.841717 | 77.2 | 5191.08 |
| 77.1 | 4212.699634 | 77.1 | 5181.351 |
| 77 | 4217.224634 | 77 | 5191.985 |
| 76.9 | 4221.1463 | 76.9 | 5173.583 |


| 76.8 | 4234.872134 | 76.8 | 5217.551 |
| :---: | :---: | :---: | :---: |
| 76.7 | 4209.909217 | 76.7 | 5224.188 |
| 76.6 | 4208.325467 | 76.6 | 5199.753 |
| 76.5 | 4225.595884 | 76.5 | 5193.87 |
| 76.4 | 4241.961301 | 76.4 | 5251.79 |
| 76.3 | 4239.170884 | 76.3 | 5257.296 |
| 76.2 | 4297.166301 | 76.2 | 5261.821 |
| 76.1 | 4280.046718 | 76.1 | 5251.941 |
| 76 | 4273.259218 | 76 | 5245.983 |
| 75.9 | 4284.873384 | 75.9 | 5324.04 |
| 75.8 | 4263.907551 | 75.8 | 5321.551 |
| 75.7 | 4338.720885 | 75.7 | 5344.176 |
| 75.6 | 4359.234219 | 75.6 | 5372.533 |
| 75.5 | 4371.979635 | 75.5 | 5396.817 |
| 75.4 | 4383.518386 | 75.4 | 5395.308 |
| 75.3 | 4400.788802 | 75.3 | 5439.201 |
| 75.2 | 4428.315886 | 75.2 | 5463.108 |
| 75.1 | 4479.37297 | 75.1 | 5500.138 |
| 75 | 4501.09297 | 75 | 5578.269 |
| 74.9 | 4522.134221 | 74.9 | 5610.472 |
| 74.8 | 4546.116721 | 74.8 | 5645.164 |
| 74.7 | 4586.238388 | 74.7 | 5665.602 |
| 74.6 | 4582.769221 | 74.6 | 5664.772 |
| 74.5 | 4551.471304 | 74.5 | 5699.841 |
| 74.4 | 4559.390054 | 74.4 | 5699.992 |
| 74.3 | 4543.100054 | 74.3 | 5714.698 |
| 74.2 | 4579.752555 | 74.2 | 5724.2 |
| 74.1 | 4540.611304 | 74.1 | 5716.282 |
| 74 | 4493.023387 | 74 | 5671.635 |
| 73.9 | 4505.316304 | 73.9 | 5666.507 |
| 73.8 | 4482.917553 | 73.8 | 5668.995 |
| 73.7 | 4468.135887 | 73.7 | 5670.881 |
| 73.6 | 4447.094636 | 73.6 | 5611.453 |
| 73.5 | 4434.424636 | 73.5 | 5576.459 |
| 73.4 | 4427.410886 | 73.4 | 5559.566 |
| 73.3 | 4417.078803 | 73.3 | 5557.077 |
| 73.2 | 4361.949219 | 73.2 | 5544.558 |


| 73.1 | 4350.033385 | 73.1 | 5510.847 |
| :---: | :---: | :---: | :---: |
| 73 | 4335.628802 | 73 | 5462.655 |
| 72.9 | 4347.242968 | 72.9 | 5479.85 |
| 72.8 | 4313.757968 | 72.8 | 5447.27 |
| 72.7 | 4294.903801 | 72.7 | 5439.427 |
| 72.6 | 4278.462968 | 72.6 | 5435.732 |
| 72.5 | 4290.755884 | 72.5 | 5491.54 |
| 72.4 | 4319.565051 | 72.4 | 5502.702 |
| 72.3 | 4330.274218 | 72.3 | 5521.179 |
| 72.2 | 4361.949219 | 72.2 | 5542.899 |
| 72.1 | 4386.836719 | 72.1 | 5566.806 |
| 72 | 4402.674219 | 72 | 5623.595 |
| 71.9 | 4427.712553 | 71.9 | 5665.526 |
| 71.8 | 4486.38672 | 71.8 | 5661.378 |
| 71.7 | 4522.435887 | 71.7 | 5714.019 |
| 71.6 | 4537.519221 | 71.6 | 5790.793 |
| 71.5 | 4556.675054 | 71.5 | 5795.243 |
| 71.4 | 4573.568388 | 71.4 | 5846.828 |
| 71.3 | 4580.431305 | 71.3 | 5920.51 |
| 71.2 | 4616.706722 | 71.2 | 5953.316 |
| 71.1 | 4593.101305 | 71.1 | 5940.42 |
| 71 | 4602.302138 | 71 | 5917.569 |
| 70.9 | 4575.227555 | 70.9 | 5885.818 |
| 70.8 | 4555.694638 | 70.8 | 5856.858 |
| 70.7 | 4533.597554 | 70.7 | 5838.23 |
| 70.6 | 4515.045054 | 70.6 | 5832.348 |
| 70.5 | 4508.55922 | 70.5 | 5805.877 |
| 70.4 | 4474.998803 | 70.4 | 5770.205 |
| 70.3 | 4420.397136 | 70.3 | 5769.375 |
| 70.2 | 4405.841719 | 70.2 | 5694.185 |
| 70.1 | 4374.091302 | 70.1 | 5642.147 |
| 70 | 4313.003801 | 70 | 5613.338 |
| 69.9 | 4276.879218 | 69.9 | 5571.18 |
| 69.8 | 4263.455051 | 69.8 | 5506.774 |
| 69.7 | 4230.1963 | 69.7 | 5469.066 |
| 69.6 | 4206.967967 | 69.6 | 5447.874 |
| 69.5 | 4222.352967 | 69.5 | 5394.479 |


| 69.4 | 4170.617133 | 69.4 | 5382.865 |
| :---: | :---: | :---: | :---: |
| 69.3 | 4134.266299 | 69.3 | 5368.158 |
| 69.2 | 4133.361299 | 69.2 | 5332.713 |
| 69.1 | 4089.619632 | 69.1 | 5349.153 |
| 69 | 4110.660882 | 69 | 5360.39 |
| 68.9 | 4101.309216 | 68.9 | 5348.55 |
| 68.8 | 4129.665883 | 68.8 | 5338.972 |
| 68.7 | 4132.154633 | 68.7 | 5339.953 |
| 68.6 | 4129.741299 | 68.6 | 5350.285 |
| 68.5 | 4117.448382 | 68.5 | 5338.218 |
| 68.4 | 4133.059633 | 68.4 | 5352.924 |
| 68.3 | 4137.282966 | 68.3 | 5363.407 |
| 68.2 | 4161.340883 | 68.2 | 5361.446 |
| 68.1 | 4134.115466 | 68.1 | 5340.103 |
| 68 | 4163.603383 | 68 | 5362.728 |
| 67.9 | 4170.994216 | 67.9 | 5356.243 |
| 67.8 | 4147.388799 | 67.8 | 5337.087 |
| 67.7 | 4160.435883 | 67.7 | 5319.665 |
| 67.6 | 4162.09505 | 67.6 | 5326.528 |
| 67.5 | 4183.664217 | 67.5 | 5366.424 |
| 67.4 | 4190.60255 | 67.4 | 5380.904 |
| 67.3 | 4178.535883 | 67.3 | 5385.429 |
| 67.2 | 4196.862133 | 67.2 | 5368.46 |
| 67.1 | 4182.155883 | 67.1 | 5370.572 |
| 67 | 4187.43505 | 67 | 5344.704 |
| 66.9 | 4180.8738 | 66.9 | 5357.525 |
| 66.8 | 4181.401717 | 66.8 | 5338.821 |
| 66.7 | 4171.974633 | 66.7 | 5338.595 |
| 66.6 | 4206.44005 | 66.6 | 5353.603 |
| 66.5 | 4213.4538 | 66.5 | 5356.77 |
| 66.4 | 4220.090467 | 66.4 | 5354.583 |
| 66.3 | 4225.6713 | 66.3 | 5336.333 |
| 66.2 | 4251.312967 | 66.2 | 5337.011 |
| 66.1 | 4234.872134 | 66.1 | 5323.813 |
| 66 | 4211.040467 | 66 | 5325.85 |

## 10. Procedure for the scale-up experiment for the flow reaction

Pt black powder ( 700 mg ) was pre-mixed with silica-gel ( 140 g ) and then packed into a column (ID: 37 mm , L: 300 mm . The compression molding was conducted for the pre-mixed catalysts using a press machine (RIKEN KIKI CO., Ltd, CDM-5PA) and mold (Labonect, LD-3025, $\varphi 30 \times 25 \mathrm{~mm}$ ) under 40 MPa for 2 hours before packing to the reaction column. The catalyst column was set onto the reactor (EYELA, HCR-1000), and $\mathrm{H}_{2} \mathrm{O}$ was flowed at each $3.0 \mathrm{~mL} / \mathrm{min}$ (Pump for $\mathrm{H}_{2} \mathrm{O}_{2}$ aq.: UI-22 110P, EYELA, Pump for $t$-amylOH solution: LC-20AD, Shimadzu). The catalyst column was heated at 90 ${ }^{\circ} \mathrm{C}$ (heating controller and column reactor: HCR-1000). After stabilization the reaction was started by changing into feed solution of $10 \mathrm{wt} \% \mathrm{H}_{2} \mathrm{O}_{2}$ aq. and benzyl alcohol $(1,0.67 \mathrm{M})$ solution in $t$-amylOH. The resulted solution was fractionated for every 5 minutes ( 30 mL ) (Fraction collector: DC-1500, EYELA), and selected fractions were analyzed by GC-FID ( $\mathrm{N}_{2}: 34.0 \mathrm{~cm} / \mathrm{s}$, column temperature: $50{ }^{\circ} \mathrm{C}$ for $2 \mathrm{~min}, 10^{\circ} \mathrm{C} / \mathrm{min}$ heating then $240^{\circ} \mathrm{C}$ for 12 min ) to determine GC conversion and yield.


