

## From microkinetic model to process: Understanding the role of the boron nitride surface and gas phase chemistry in the oxidative dehydrogenation of propane

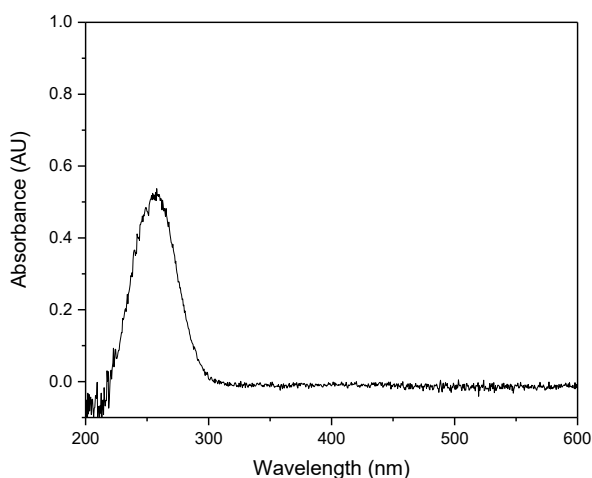
### Electronic Supplementary Information

*ESI Table 1 available from MINDS@UW Subcollection entitled "MINDS@UW Madison / College of Engineering, University of Wisconsin--Madison / Department of Chemical and Biological Engineering / Data and Supplementary Materials."*

#### Ozone Generation and Measurement

Ozone was generated using a VMUS-DG ozone generator. In a typical experiment, ca. 2L/min of UHP O<sub>2</sub> was flown through the ozone generator to produce an ozonated oxygen feed with ca. 10 psig of backpressure. This feed was then directed into the reactor through a Bronkhorst EL-Flow Select mass flow controller.

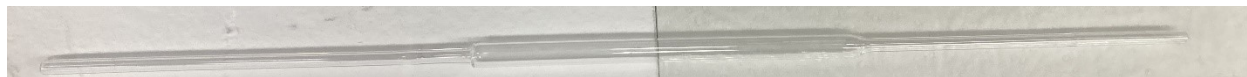
Ozone concentration was measured prior to reaction using UV-Vis absorbance measurements with a Maya 2000Pro spectrometer using a combined deuterium and halogen light source. A 0.1cm path length quartz cuvette was placed in line with the generator outlet prior to any heated sections of the reactor. Ozonated oxygen was introduced to the cuvette via mass flow controllers and decomposed using an ozone destroyer after the cuvette. O<sub>3</sub> absorption measurements at 253.6 nm were collected for at least 500 seconds. An exemplar spectrum is shown in Figure 1. Absorptivity at 253.6 nm was taken to be 1130E-20 molecules cm<sup>-2</sup>.<sup>1</sup> The Beer-Lambert law was used to estimate the O<sub>3</sub> concentration.



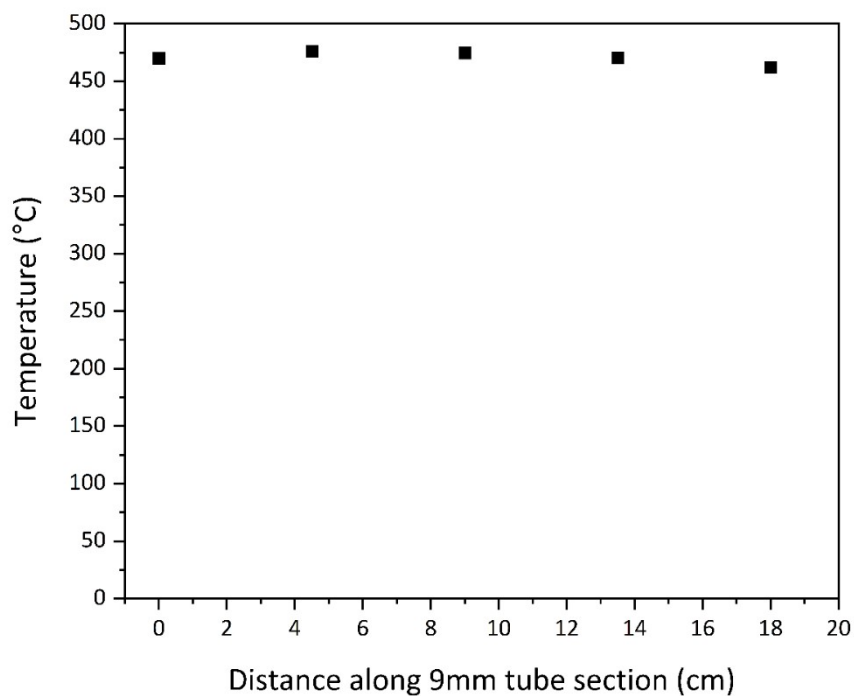
**Figure 1:** Exemplar absorbance measurement for undiluted ozonated O<sub>2</sub> stream.

## Ozone Reactor Tube

Ozone is highly reactive and decomposes rapidly. To minimize non-isothermal reactivity, a reactor tube was constructed that had minimal dead-volume outside the isothermal region. The tube consisted of a central 9mm ID reactor portion and two 4mm ID quartz tube sections that were packed either with a thermowell or a quartz spacer rod to minimize dead volume. This tube was used for  $O_3$ , NO, and some background reactions. The temperature profile was found to vary within a 14°C range within this region at a setpoint of 475°C.

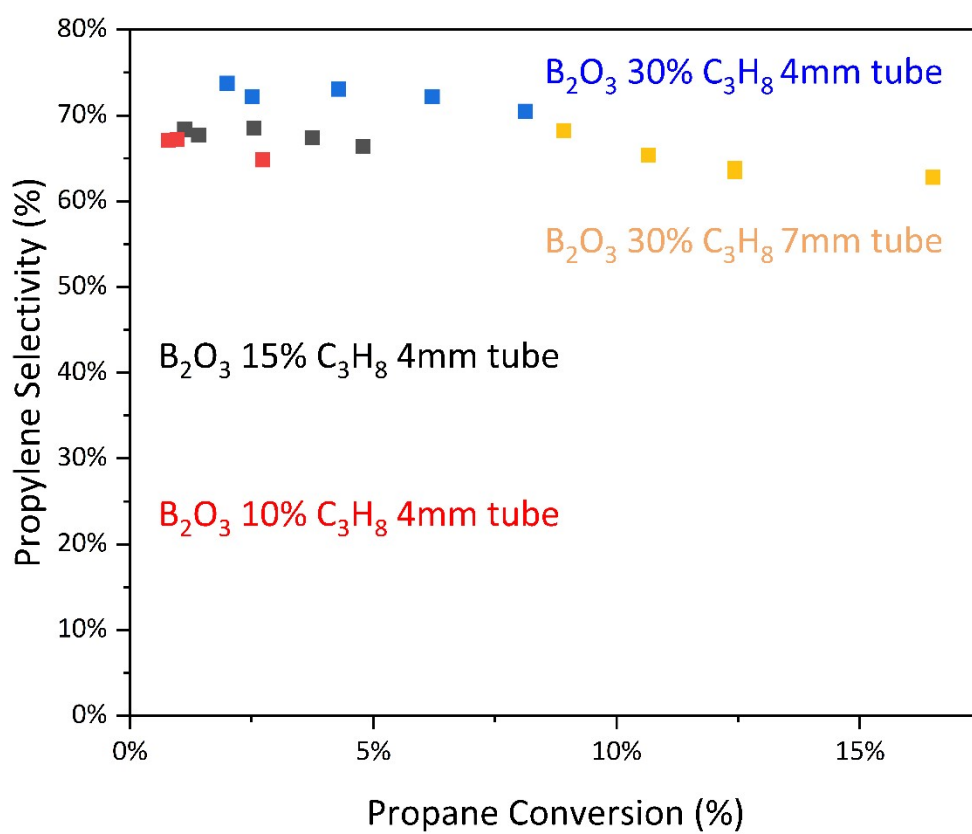


**Figure 2:** Tube used for ozone reactions. Central tube portion where gas-phase reactions occurred is 18cm in length and 9mm in inner diameter.

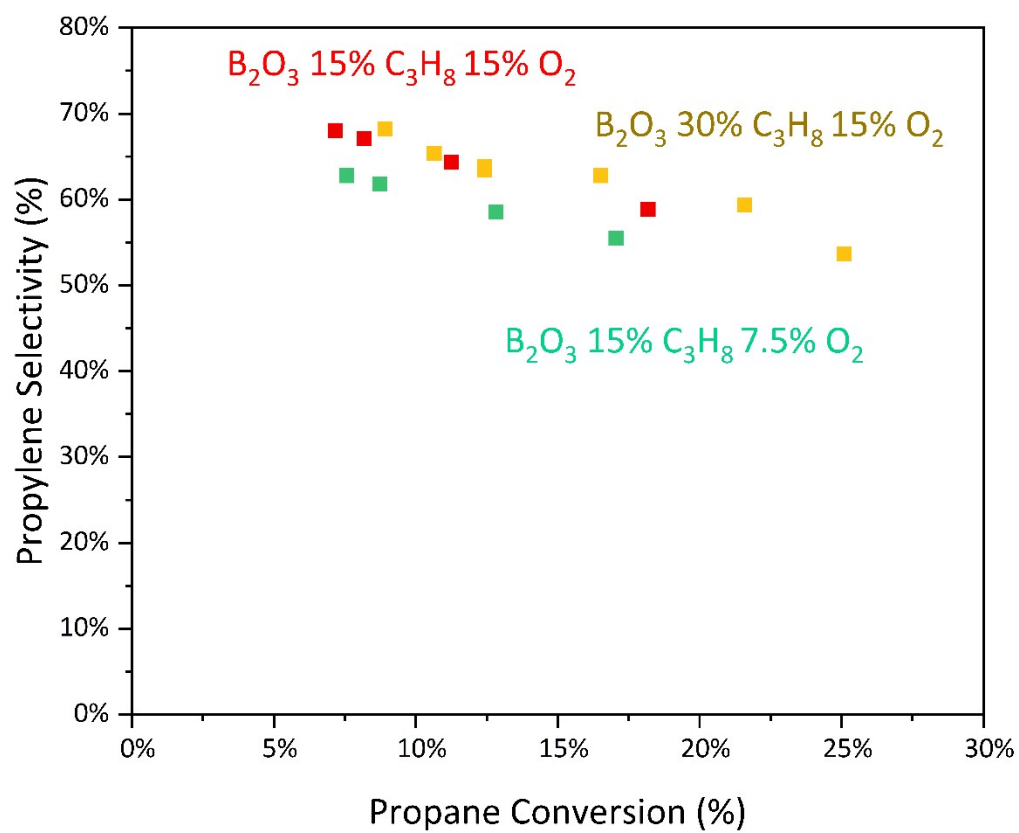


**Figure 3:** Temperature along 9mm section of reactor tube at 475°C setpoint.

## $B_2O_3$ Reactivity

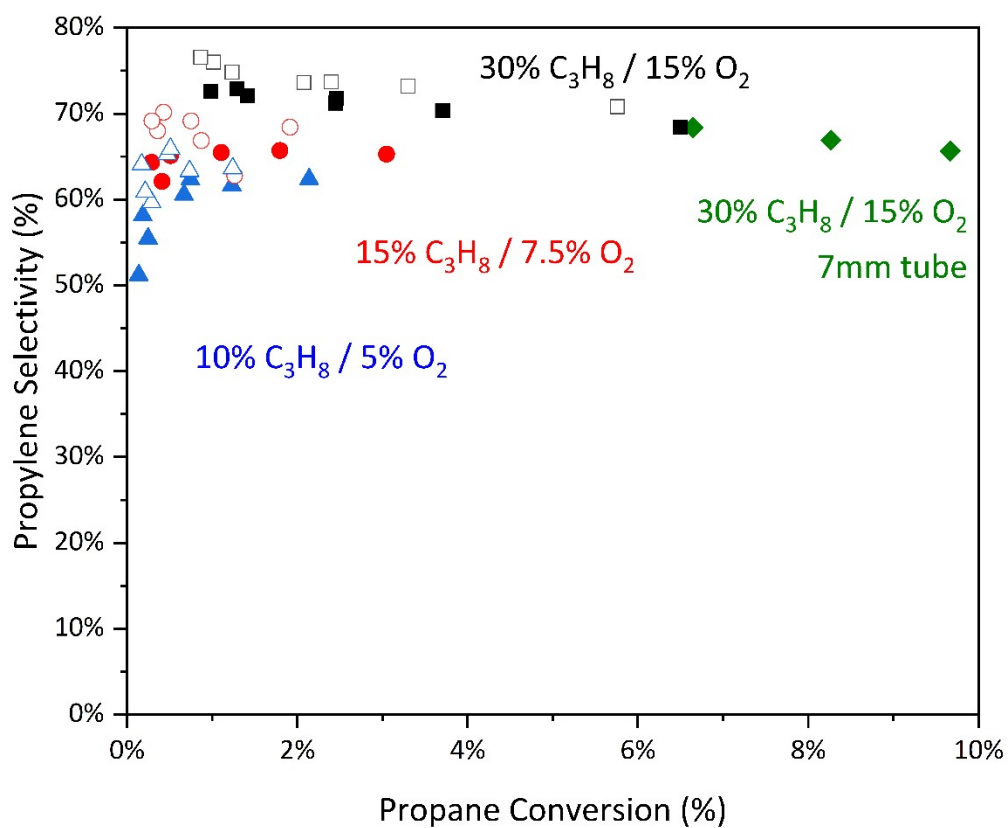


**Figure 4:**  $B_2O_3$  reactivity in 4mm and 7mm tubes. Conditions: 550°C, 25-70 mLn min<sup>-1</sup> total flow, 2:1  $C_3H_8$ : $O_2$  ratio with various dilutions in  $N_2$ .



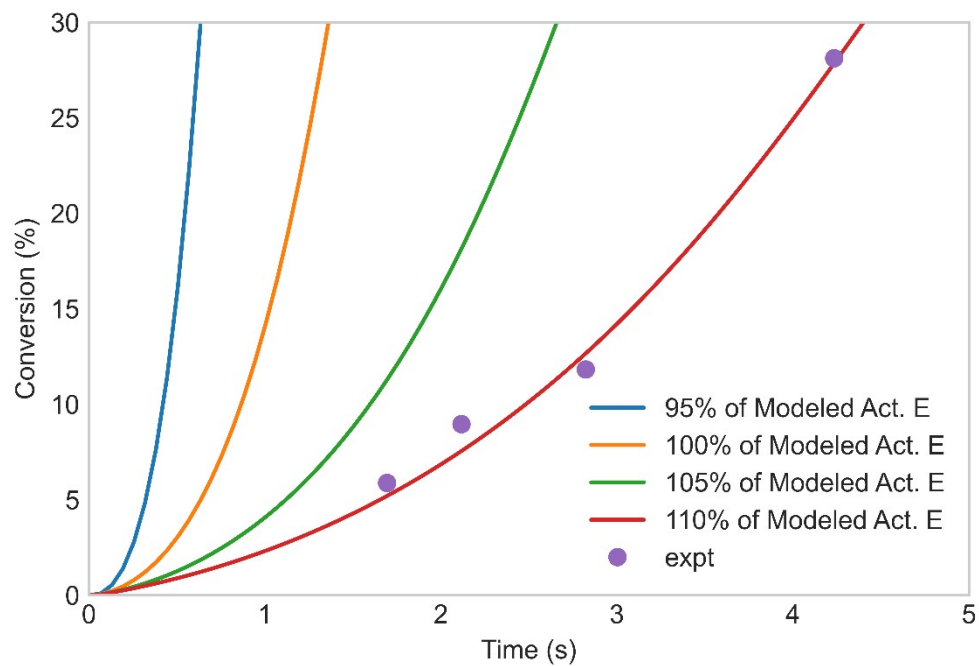
**Figure 5:**  $B_2O_3$  reactivity in 7mm tube. Conditions: 550°C, 30-80 mL min<sup>-1</sup> total flow, 50mg  $B_2O_3$  diluted in 950mg quartz chips.  $C_3H_8$  and  $O_2$  feed fractions specified in figure with balance of feed containing  $N_2$ .

## Effect of low Partial Pressure of Propane

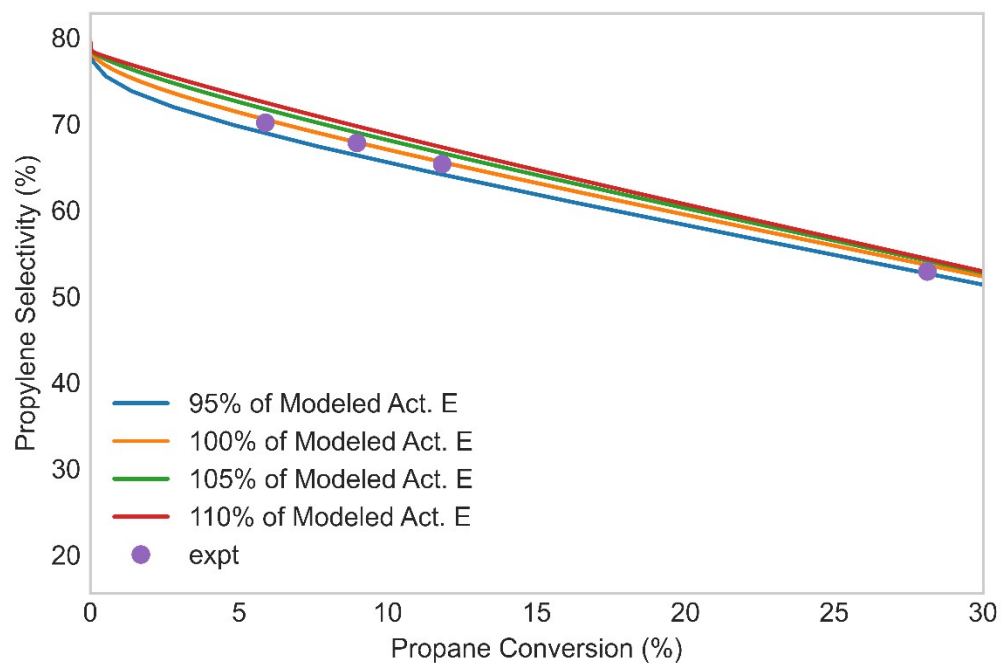


**Figure 6:** Propylene selectivity vs propane conversion over boron nitride (solid) and in empty tube (hollow) at various feed dilutions. Each run maintained a 2:1 C<sub>3</sub>H<sub>8</sub> : O<sub>2</sub> ratio but with a different feed dilution to achieve the stated feed fraction of C<sub>3</sub>H<sub>8</sub>. Conditions: 550°C, 20-80 mLn min<sup>-1</sup>, 1:5 dilution of boron nitride in passivated silicon carbide (50mg hBN in 4mm tube and 100mg hBN in 7mm tube) or 9cm of empty tube. All runs were performed in a 4mm tube unless otherwise noted.

## Role of hydrogen peroxide dissociation

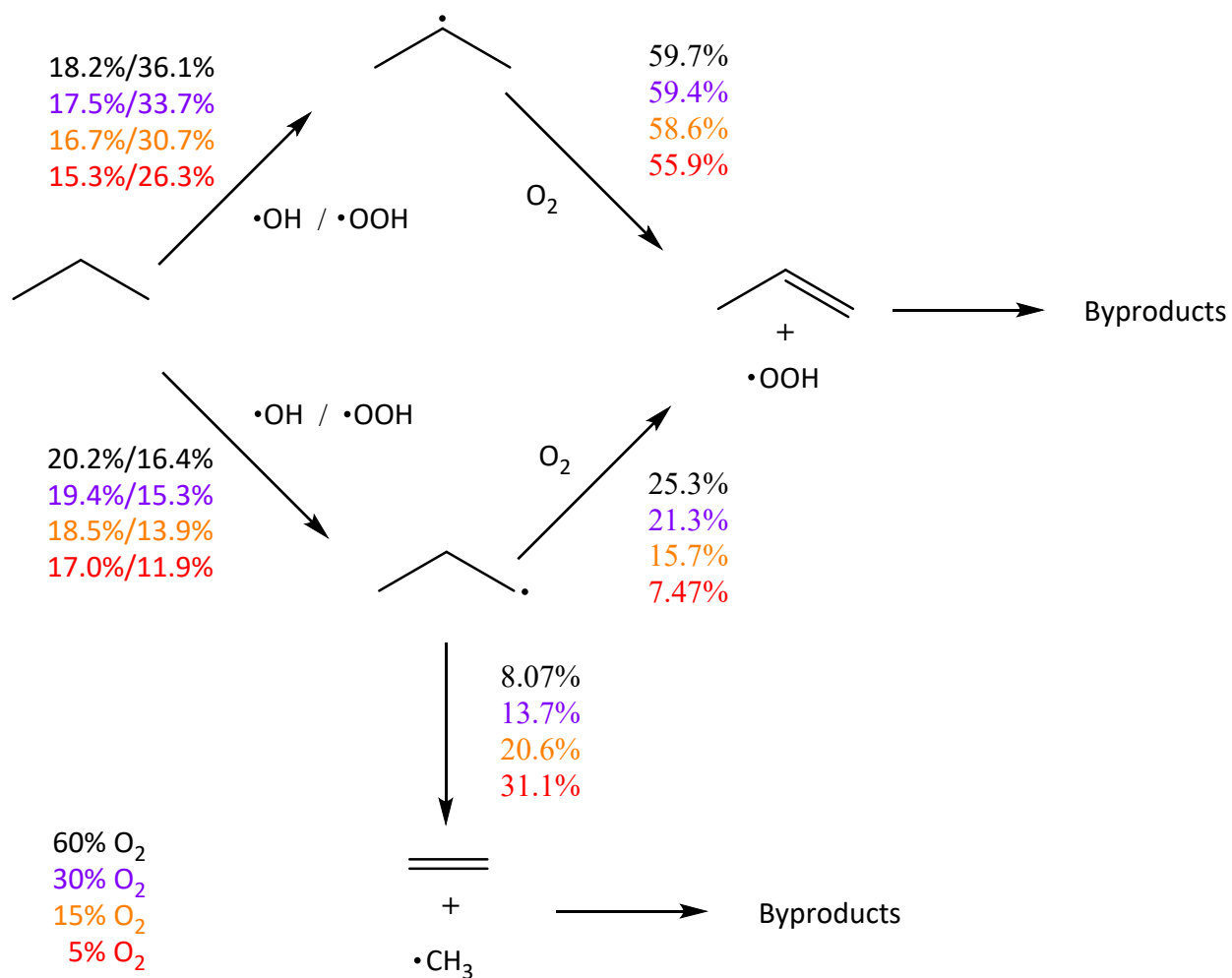


**Figure 7:** Conversion versus time in reactor tube, experiment vs model with different multipliers applied to the modeled activation energies for hydrogen peroxide dissociation. Modifying the activation energy improves the accuracy of the model in capturing the conversion as a function of contact time. Conditions: 550°C, 30% C<sub>3</sub>H<sub>8</sub> / 15% O<sub>2</sub> / 55% N<sub>2</sub>. Figure generated using Matplotlib.<sup>2</sup>



**Figure 8:** Selectivity versus conversion in reactor tube, experiment vs model with different multipliers applied to the modeled activation energies for hydrogen peroxide dissociation. Modifying the activation energy reduces the accuracy of the model in capturing the selectivity vs conversion. Conditions: 550°C, 30% C<sub>3</sub>H<sub>8</sub> / 15% O<sub>2</sub> / 55% N<sub>2</sub>. Figure generated using Matplotlib.<sup>2</sup>

### Effect of O<sub>2</sub> Feed Percentage



**Figure 9:** Major pathways for carbon flux in the gas-phase as predicted by the microkinetic model. Percentages represent the percentage of total carbon flux from C<sub>3</sub>H<sub>8</sub> that goes through a specific pathway when measured at 5 % conversion. Note that minor flux pathways are not included in this simplified diagram. Conditions: 550°C, 30 % C<sub>3</sub>H<sub>8</sub> / x% O<sub>2</sub> / balance % N<sub>2</sub>.



## Works Cited

- (1) Orphal, J.; Staehelin, J.; Tamminen, J.; Braathen, G.; De Backer, M.-R.; Bais, A.; Balis, D.; Barbe, A.; Bhartia, P. K.; Birk, M.; Burkholder, J. B.; Chance, K.; von Clarmann, T.; Cox, A.; Degenstein, D.; Evans, R.; Flaud, J.-M.; Flittner, D.; Godin-Beekmann, S.; Gorshelev, V.; Gratien, A.; Hare, E.; Janssen, C.; Kyrölä, E.; McElroy, T.; McPeters, R.; Pastel, M.; Petersen, M.; Petropavlovskikh, I.; Picquet-Varraut, B.; Pitts, M.; Labow, G.; Rotger-Languereau, M.; Leblanc, T.; Lerot, C.; Liu, X.; Moussay, P.; Redondas, A.; Van Roozendaal, M.; Sander, S. P.; Schneider, M.; Serdyuchenko, A.; Veefkind, P.; Viallon, J.; Viatte, C.; Wagner, G.; Weber, M.; Wielgosz, R. I.; Zehner, C. Absorption Cross-Sections of Ozone in the Ultraviolet and Visible Spectral Regions: Status Report 2015. *Journal of Molecular Spectroscopy* **2016**, 327, 105–121. <https://doi.org/10.1016/j.jms.2016.07.007>.
- (2) Hunter, J. D. Matplotlib: A 2D Graphics Environment. *Comput. Sci. Eng.* **2007**, 9 (3), 90–95. <https://doi.org/10.1109/MCSE.2007.55>.