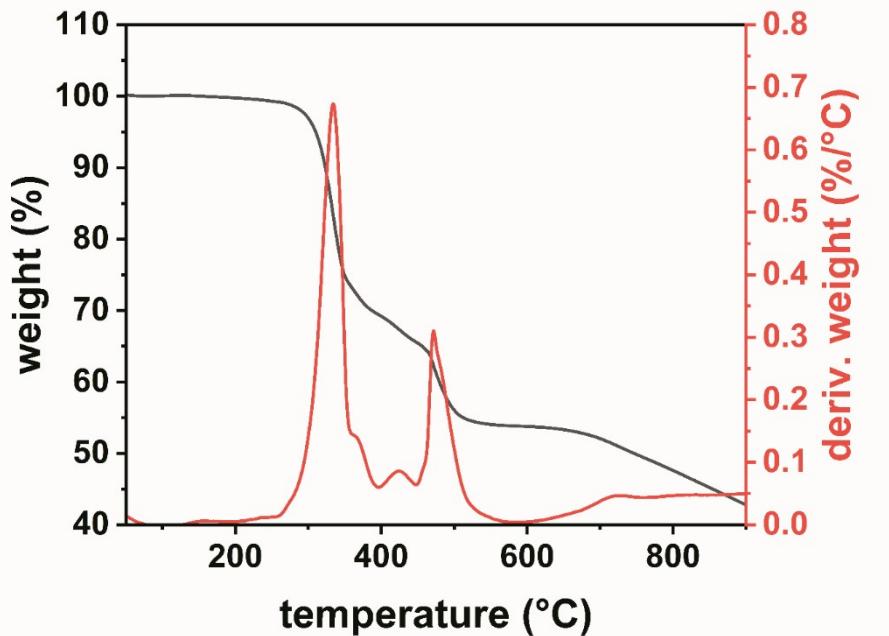


## Supplementary Material

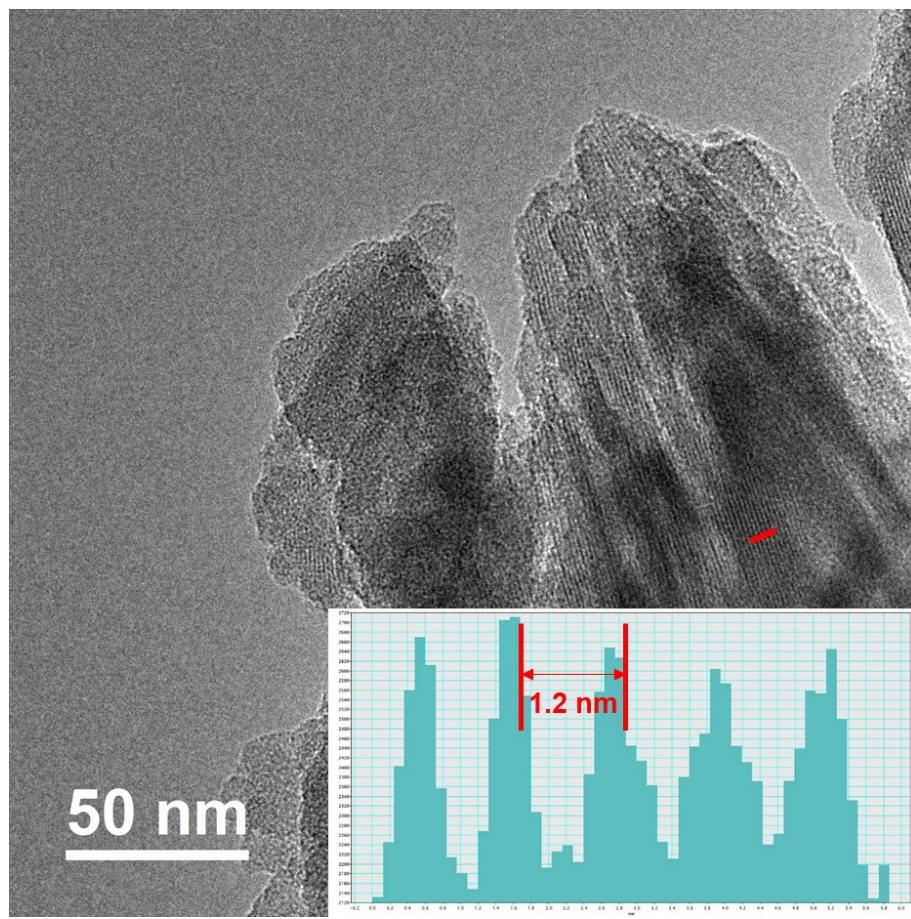
**High metal loaded Cu(I)N<sub>3</sub> single-atom catalysts: superior methane conversion activity and selectivity under mild conditions**

Hyesung Lee and Sang-Yup Lee\*

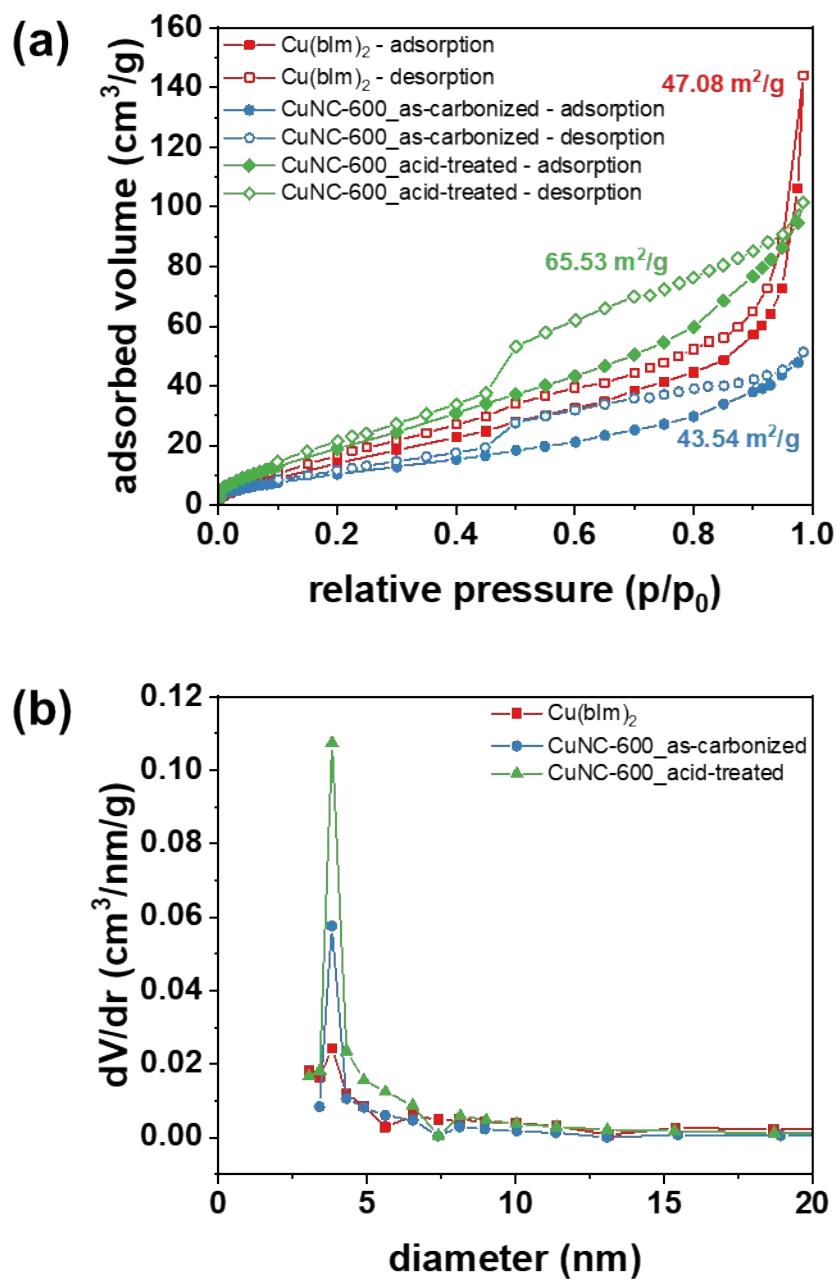
Department of Chemical and Biomolecular Engineering, Yonsei University, Seoul  
03722 Republic of Korea



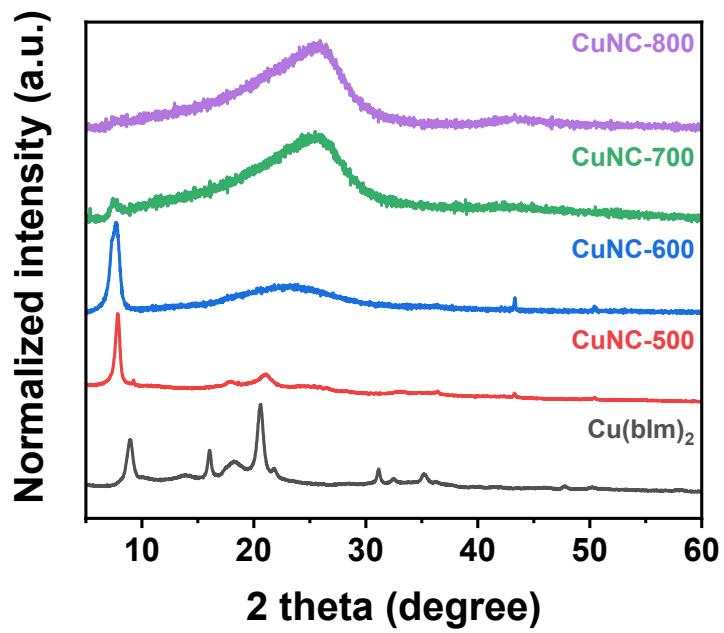
**Figure S1.** TGA and 1<sup>st</sup> derivation profiles of Cu(bIm)<sub>2</sub>.



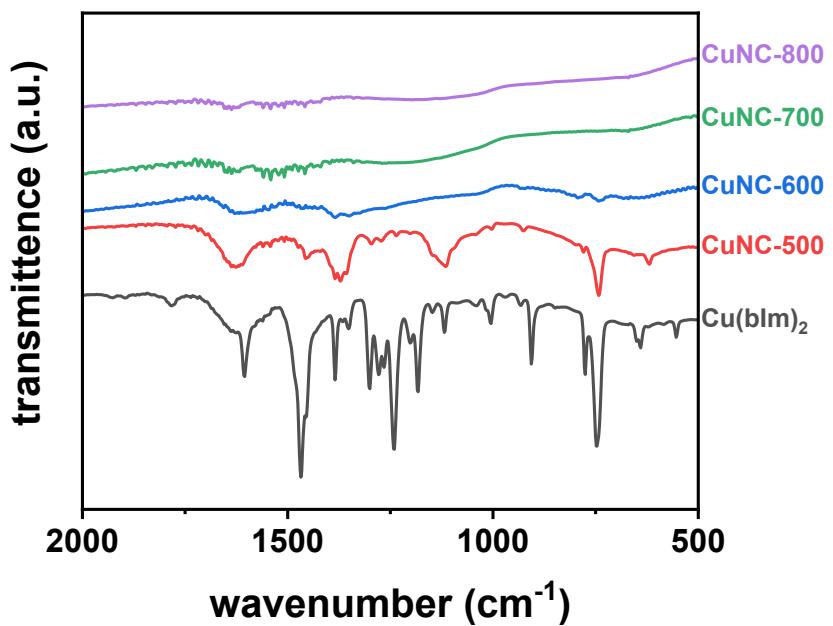
**Figure S2.** TEM image of the CuNC-600 showing carbon layers (inset: intensity profile of the region marked in red line).



**Figure S3.** BET analyses of  $\text{Cu(blm)}_2$ , as-carbonized and acid-treated CuNC-600. (a)  $\text{N}_2$  isotherm at 77 K and (b) pore size distribution.



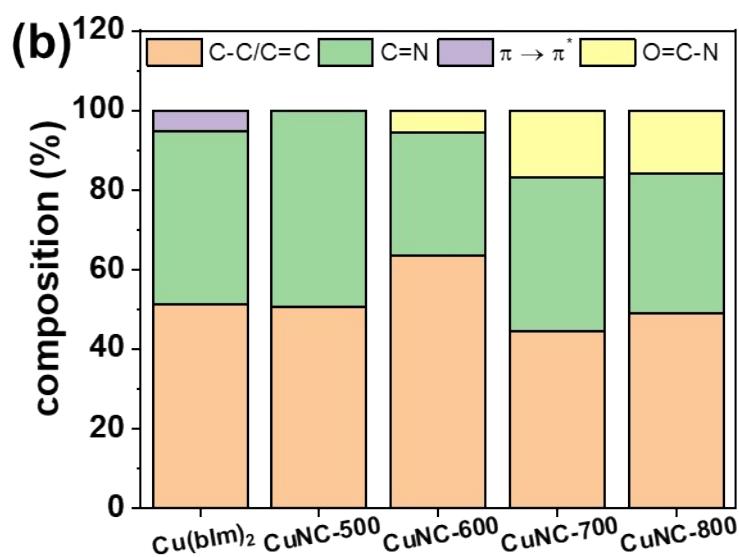
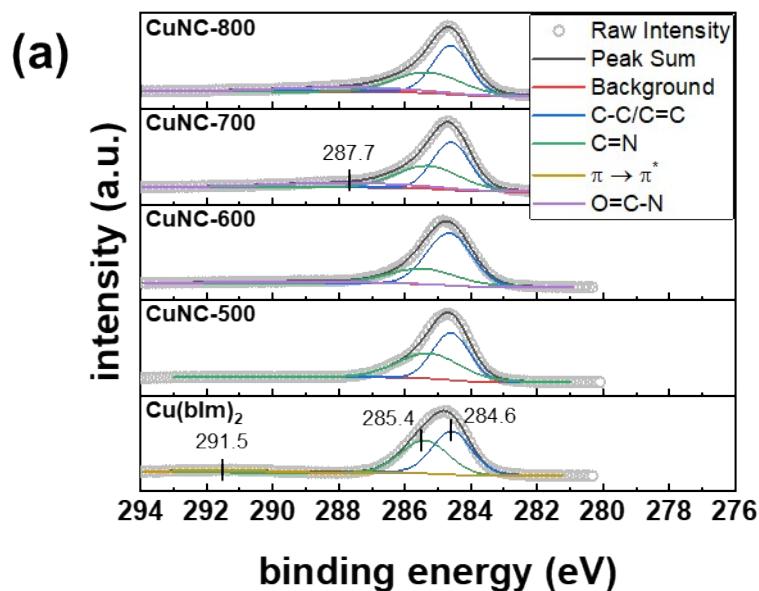
**Figure S4.** XRD patterns of  $\text{Cu}(\text{bIm})_2$  and CuNC catalysts carbonized at various temperatures.



**Figure S5.** FT-IR spectra of  $\text{Cu}(\text{bIm})_2$  and CuNC catalysts carbonized at various temperatures.

**Table S1.** Wavenumbers and assignments of Raman and FT-IR peaks of Cu(blm)<sub>2</sub>.

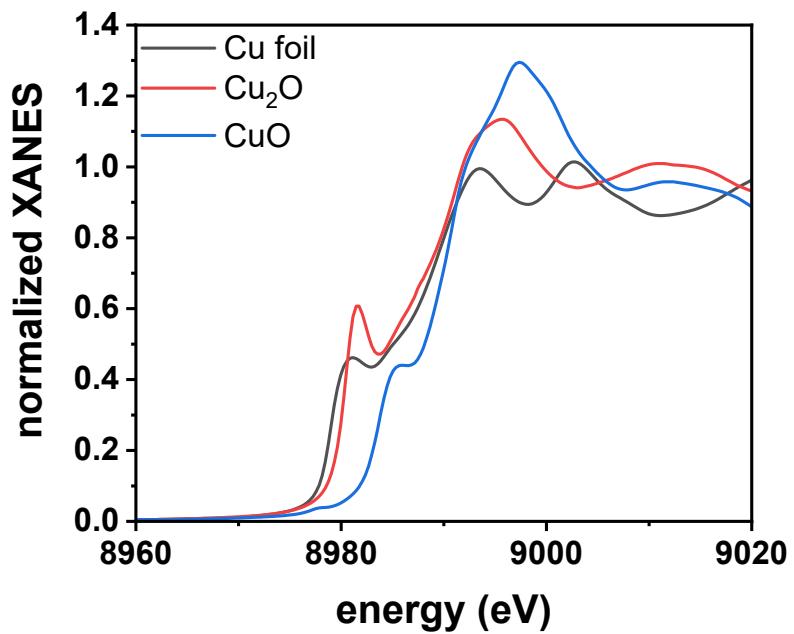
FT-IR (cm <sup>-1</sup> )	Raman (cm <sup>-1</sup> )	Assignment
554	553	ring torsion
	583	
640	640	Imidazole ring torsion
650		
746		benzimidazole C-H out-of-plane bending
775	776	Imidazole plane ring bending
907		Benzimidazole in-plane ring bending
932		Benzimidazole in-plane ring bending
970		Imidazole C-H in-plane bending
1005		Benzimidazole in-plane ring bending
1016		Benzimidazole in-plane ring bending
1119		benzimidazole C-H out-of-plane bending
1148		Benzimidazole in-plane C-H bending
1182		Benzimidazole in-plane C-H bending
1202		Benzimidazole in-plane C-H bending
1240	1240	ring stretching
1265	1260	Benzimidazole in-plane bending
1279	1275	Benzimidazole in-plane bending
1300	1300	ring stretching
1350	1350	ring stretching
1385		ring stretching
1468	1466	ring stretching
1605	1609	ring stretching



**Figure S6.** (a) High-resolution XPS C 1s spectra of Cu(blm)<sub>2</sub> and CuNC catalysts, and the corresponding compositions of carbon species.

**Table S2.** Element analysis results determined by XPS analysis.

	Elements (wt%)				
	C	N	O	Cu	Sum
<b>Cu(bIm)<sub>2</sub></b>	55.7	17.2	1.9	25.2	100
<b>CuNC-500</b>	61.0	14.6	5.8	18.6	100
<b>CuNC-600</b>	61.1	14.9	6.3	17.7	100
<b>CuNC-700</b>	64.8	13.5	8.9	12.8	100
<b>CuNC-800</b>	69.4	10.6	9.0	11.0	100

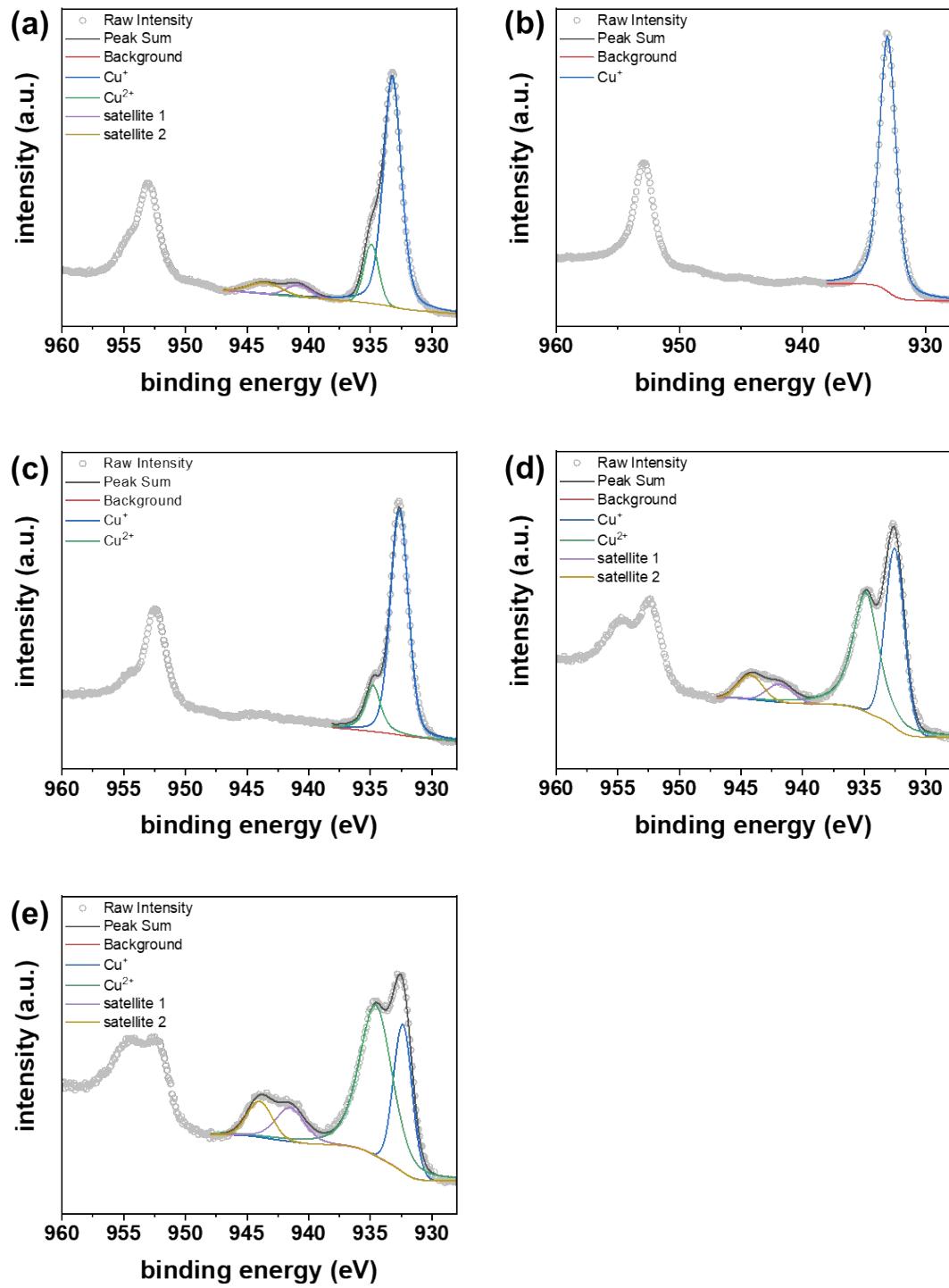


**Figure S7.** Cu-XANES spectra of Cu foil, Cu<sub>2</sub>O, CuO.

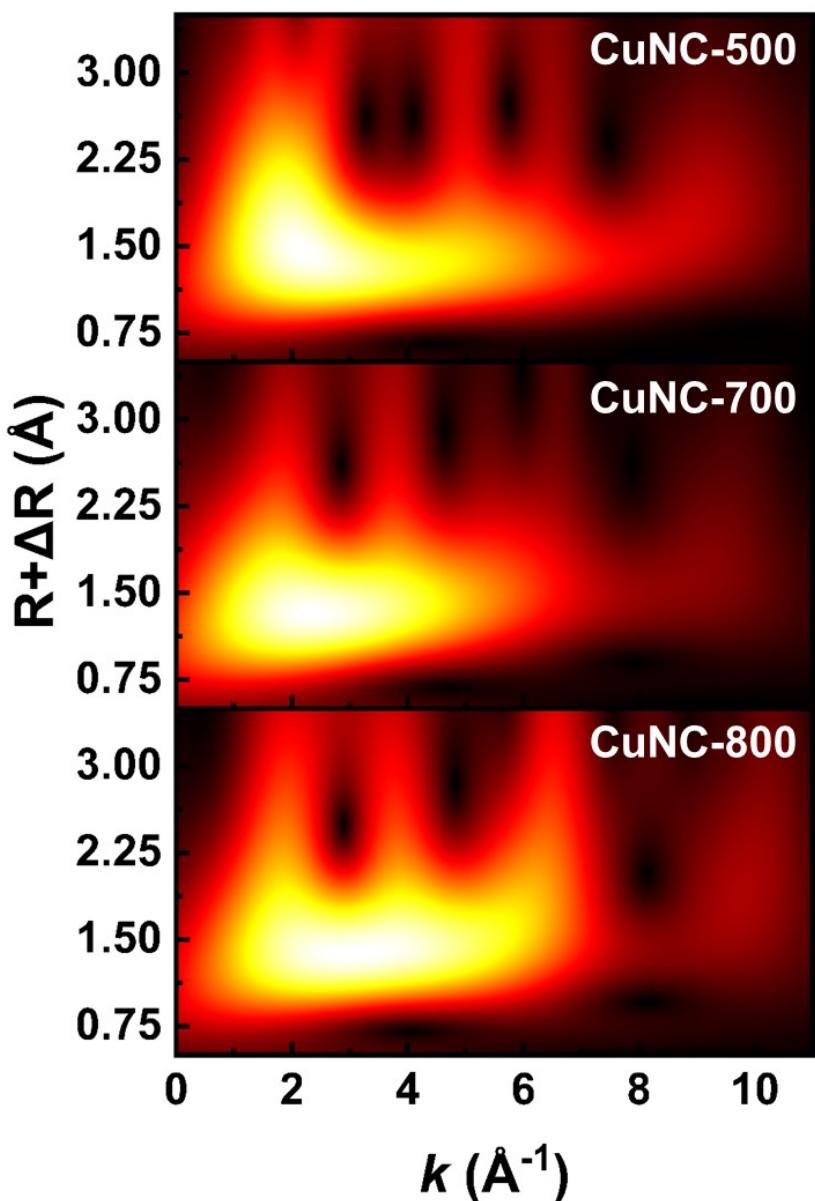
**Table S3.** Detailed Cu-EXAFS fitting results of Cu(bIm)<sub>2</sub> and CuNC catalysts.

Catalyst	Path	Coordination number <sup>a</sup>	Distance (Å)	Debye-Waller Factor (Å <sup>2</sup> )	R-Factor <sup>b</sup>
<b>Cu(bIm)<sub>2</sub></b>	Cu-N	4.22	1.97 ( $\pm 0.006$ )	0.004 ( $\pm 0.001$ )	0.007
	Cu-C	8.44	2.99 ( $\pm 0.02$ )	0.009 ( $\pm 0.002$ )	
	Cu-N-C	16.88	3.19 ( $\pm 0.037$ )	0.017 ( $\pm 0.007$ )	
<b>CuNC-500</b>	Cu-N	2.67	1.87 ( $\pm 0.012$ )	0.005 ( $\pm 0.002$ )	0.019
	Cu-C	3	2.92 ( $\pm 0.029$ )	0.004 ( $\pm 0.003$ )	
	Cu-C	2.67	3.18 ( $\pm 0.046$ )	0.009 ( $\pm 0.008$ )	
<b>CuNC-600</b>	Cu-N	2.77	1.91 ( $\pm 0.010$ )	0.006 ( $\pm 0.002$ )	0.003
	Cu-C	1.84	3.16 ( $\pm 0.060$ )	0.016 ( $\pm 0.012$ )	
	Cu-Cu	0.07	2.54 ( $\pm 0.012$ )	0.007 ( $\pm 0.004$ )	
<b>CuNC-700</b>	Cu-N	3.34	1.93 ( $\pm 0.022$ )	0.008 ( $\pm 0.003$ )	0.014
	Cu-C	9.02	3.00 ( $\pm 0.093$ )	0.020 ( $\pm 0.016$ )	
	Cu-C-N	18.9	3.17 ( $\pm 0.079$ )	0.016 ( $\pm 0.015$ )	
	Cu-Cu	0.35	2.56 ( $\pm 0.063$ )	0.0077 ( $\pm 0.0076$ )	
<b>CuNC-800</b>	Cu-N	3.79	1.95 ( $\pm 0.014$ )	0.006 ( $\pm 0.002$ )	0.019
	Cu-C	3.67	3.05 ( $\pm 0.055$ )	0.010 ( $\pm 0.008$ )	
	Cu-Cu	0.6	2.54 ( $\pm 0.020$ )	0.003 ( $\pm 0.002$ )	
	Cu-C	11	3.40 ( $\pm 0.039$ )	0.018 ( $\pm 0.005$ )	

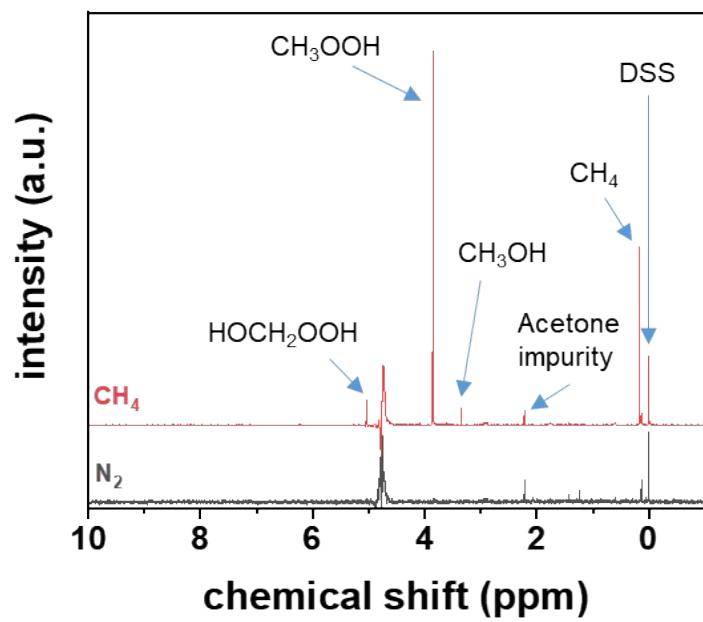
<sup>a</sup>The error was within 20%. <sup>b</sup>a measure of the mean square sum of the misfit at each data point. Fit range:  $2 < k < 11 \text{ \AA}^{-1}$ ;  $1 < R < 3 \text{ \AA}$ ; Fit window: Hanning



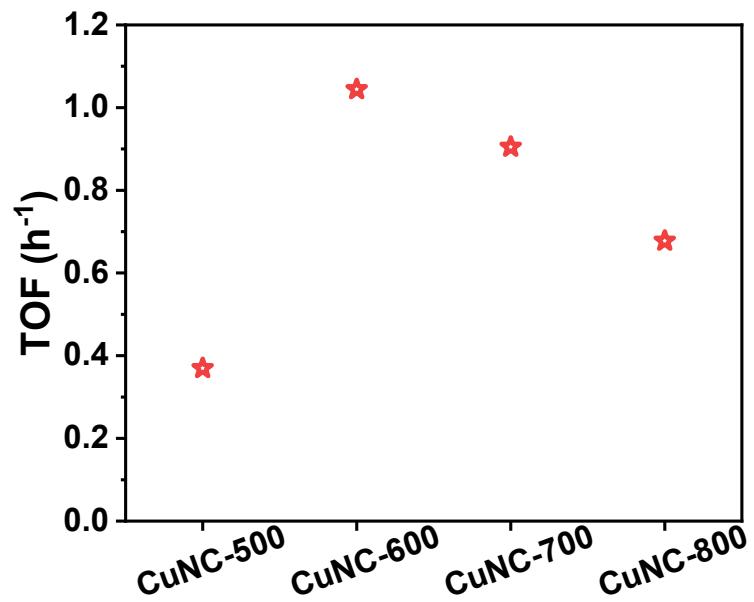
**Figure S8.** High-resolution Cu 2p XPS spectra of (a) Cu(bIm)2, (b-e) CuNC-500, -600, -700, and -800, respectively.



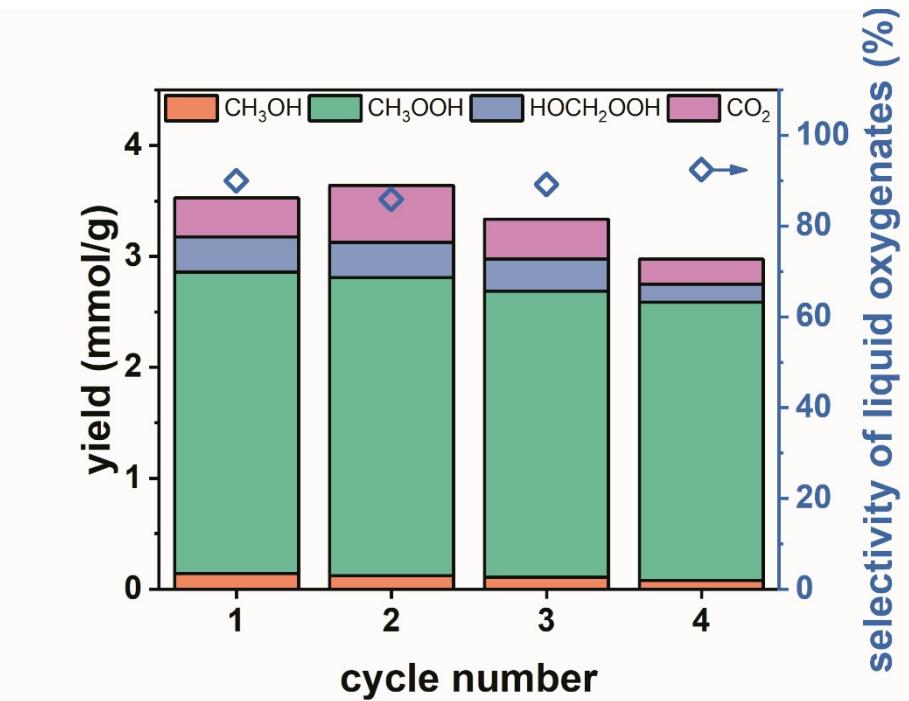
**Figure S9.** WT-EXAFS contour plots of CuNC-500, -700, and -800.



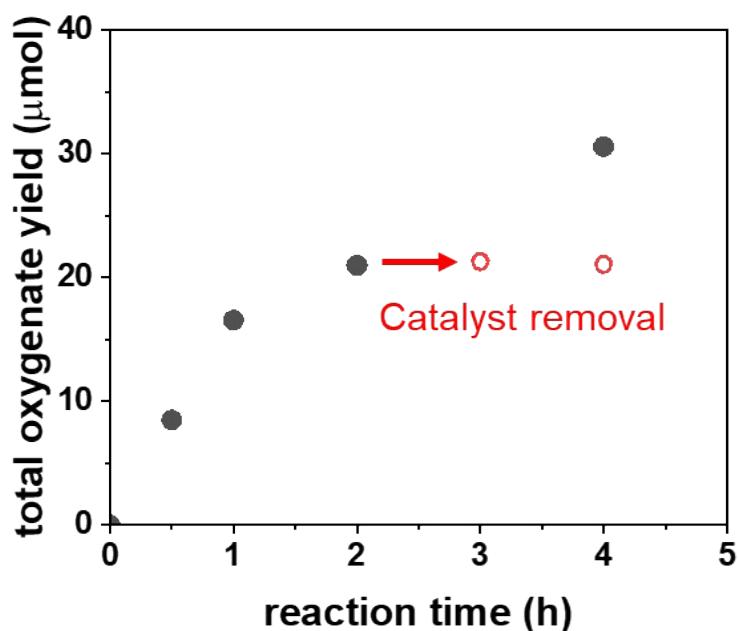
**Figure S10.** Typical <sup>1</sup>H-NMR spectra of the product solutions using (a) CH<sub>4</sub> and (b) N<sub>2</sub>.



**Figure S11.** Turnover frequency (TOF) of C1 liquid products using  $\text{Cu}(\text{bIm})_2$  and CuNC-T catalysts.



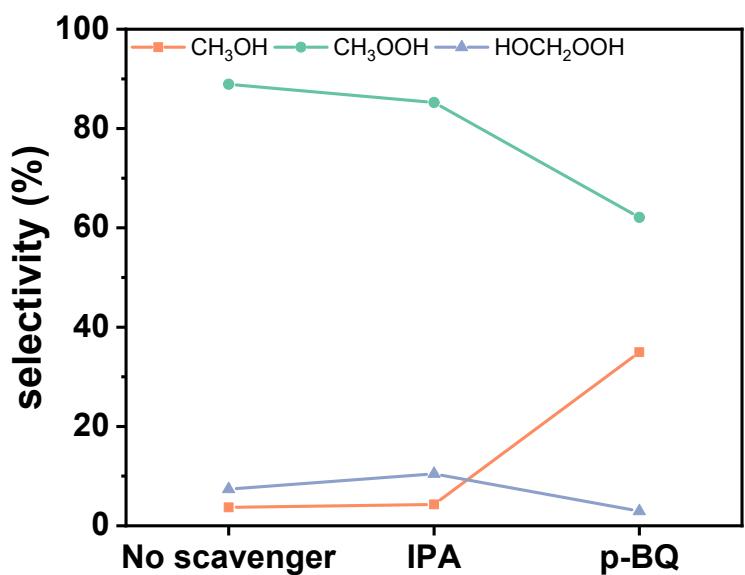
**Figure S12.** Reuse test of CuNC-600 catalyst. Reaction condition: initial amount of catalyst 5 mg, H<sub>2</sub>O 10 mL, reaction time = 0.5 h, 50 °C, [H<sub>2</sub>O<sub>2</sub>] = 0.5 M, CH<sub>4</sub> 28.5 bar, He 1.5 bar.



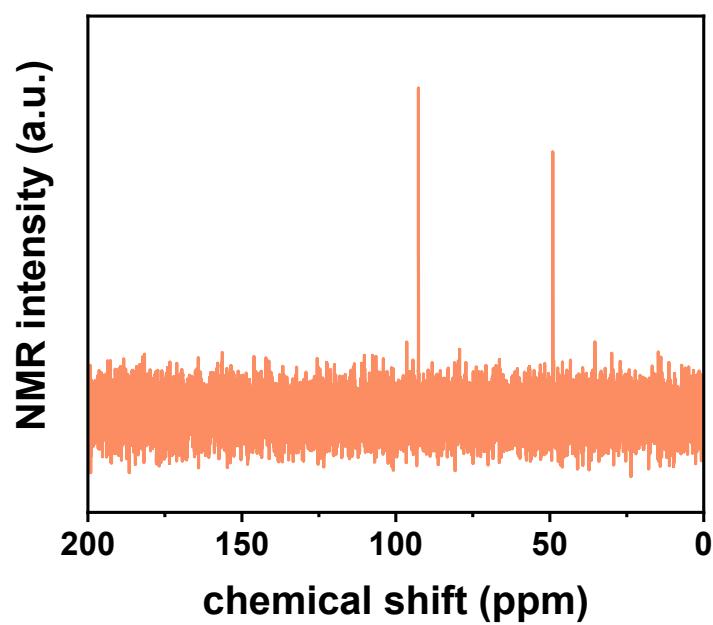
**Figure S13.** Hot filtration test result.

Reaction condition : CuNC-600 5 mg,  $\text{H}_2\text{O}$  10 mL, reaction time = 0.5 - 4 h. 40 °C,  $[\text{H}_2\text{O}_2]$  = 0.5 M,  $\text{CH}_4$  28.5 bar, He 1.5 bar.

The catalyst was separated from the reaction mixture through filtration after 2 hours, after which 1 mL of the liquid solution was collected for product quantification. Subsequently, the reaction vessel was replenished with methane gas up to 30 bar and the reaction continued for an additional hour. Another 1 mL liquid sample was taken, and the reaction proceeded for a further hour following a recharge of the reaction vessel with methane.

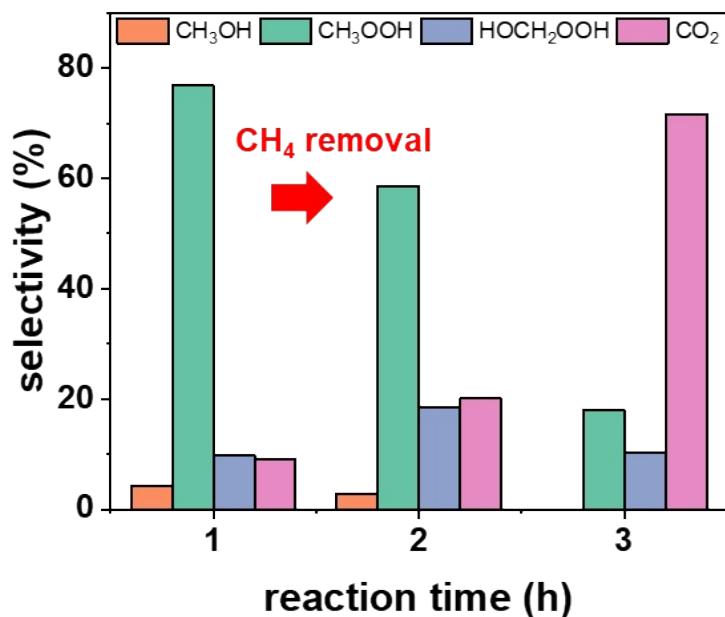


**Figure S14.** Liquid product selectivity during radical scavenger tests.



**Figure S15.** <sup>13</sup>C-NMR spectrum of the liquid product after the oxidation of <sup>13</sup>CH<sub>3</sub>OH.

Reaction condition: CuNC-600 5 mg, H<sub>2</sub>O<sub>2</sub> 5 mmol, H<sub>2</sub>O 10 mL, CH<sub>4</sub> 28.5 bar, He 1.5 bar, 40 °C, 1 h.



**Figure S16.** CH<sub>3</sub>OOH oxidation result. CH<sub>4</sub> was removed from the reaction vessel after 1 h of reaction under standard conditions. The vessel was re-pressurized to 30 bar with N<sub>2</sub> and the reaction was continued for another 1 and 2 hours.

**Table S4.** Performances comparison of the thermocatalysts for methane oxidation using H<sub>2</sub>O<sub>2</sub>.

Catalytic template	Catalyst	Metal-loading (wt%)	Active site structure	P <sup>a</sup> (bar)	T <sup>b</sup> (°C)	Productivity [μmol / g <sub>cat</sub> / h]					C1 liquid product selectivity (%)	Turnover Frequency (mol <sub>C1</sub> liquid products /mol <sub>metal</sub> /h)	Ref.
						CH <sub>3</sub> OH	CH <sub>3</sub> OOH	HOCH <sub>2</sub> OOH	HCOOH	CO <sub>2</sub>			
Carbon	CuNC-600	17.7	CuN3	30	50	285	5429	633	0	766	89.2	2.3	This work
	FeN4/GN	2.7	FeN4	20	25	11	83	63	71	31	88.1	0.34	[S1]
	Cu <sub>1</sub> @C <sub>3</sub> N <sub>4</sub>	0.35	CuN2	30	50	26	-	0	0	-	-	0.7	[S2]
	Cu <sub>2</sub> @C <sub>3</sub> N <sub>4</sub>	0.35	Cu2O-N4	30	50	260	-	0	0	16	89.4	4.73	
Metal Oxide	AuPd/TiO <sub>2</sub> (1 wt%)	1	AuPd	30.5	50	76	146	0	0	30	88.1	3.4	[S3]
	Rh/ZrO <sub>2</sub>	0.3	Rh <sub>1</sub> O <sub>5</sub>	30	70	31	7	0	0	10	78	1.7	[S4]
	CuCHA	2.5	-	35	60	13	101	-	-	-	-	0.3	
	CuFAU	1.1	-	35	60	13	224	-	-	-	-	1.3	
	CuMOR	0.4	-	35	60	6	98	-	-	-	-	1.6	[S5]
	CuFER	2.3	-	35	60	104	85	-	-	-	-	0.4	
	CuBEA	1.1	-	35	60	6	126	-	-	-	-	0.7	

<sup>a</sup>Pressure;

<sup>b</sup>Temperature.

**Table S5.** Carbon balance of the reactant and products with time.

t <sup>a</sup> (h)	CH <sub>4</sub> consumption (μmol)	Products (μmol)				Carbon balance <sup>b</sup> (%)
		CH <sub>3</sub> OH	CH <sub>3</sub> OOH	HOCH <sub>2</sub> OOH	CO <sub>2</sub>	
0.5	8.44	0.27	6.46	0.54	1.21	100.5
1	14.85	0.44	11.33	1.19	2.32	102.9
2	19.83	0.74	15.22	1.69	3.16	105.0
4	30.26	0.77	20.87	3.61	5.34	101.1
10	38.42	1.03	15.65	2.46	20.23	102.5
16	47.53	1.59	16.50	2.69	25.65	97.7

<sup>a</sup>Reaction time; <sup>b</sup>Carbon balance = Total yield of the products / CH<sub>4</sub> consumption \* 100 %.

**Table S6.** Reaction rate equations of the proposed reaction equations.

No.	Reaction rate equation	Initial condition
1	$\frac{d[CH_4]}{dt} = -k_1[CH_4][H_2O_2] - k_2[CH_4][H_2O_2]^2$	$[CH_4]_0 = 33.8 \text{ mM}^a$
2	$\frac{d[CH_3OH]}{dt} = k_1[CH_4][H_2O_2] - k_3[CH_3OH][H_2O_2]$	$[CH_3OH]_0 = 0 \text{ mM}$
3	$\frac{d[CH_3OOH]}{dt} = k_2[CH_4][H_2O_2]^2 - k_4[CH_3OOH][H_2O_2]$	$[CH_3OOH]_0 = 0 \text{ mM}$
4	$\frac{d[HOCH_2OOH]}{dt} = k_3[CH_3OH][H_2O_2]^2 + k_4[CH_3OOH][H_2O_2]$	$[HOCH_2OOH]_0 = 0 \text{ mM}$
5	$\frac{d[CO_2]}{dt} = k_5[CH_3OOH][H_2O_2]^2 + k_6[HOCH_2OOH][H_2O_2]$	$[CO_2]_0 = 0 \text{ mM}$

<sup>a</sup>The initial methane concentration was calculated by the interpolation of experimental data provided in the literature.<sup>S6</sup>

**Table S7.** Best fit results of the reaction rate constants.

Reaction rate constants	
$k_1$ [M <sup>-1</sup> h <sup>-1</sup> ]	0.0015755
$k_2$ [M <sup>-2</sup> h <sup>-1</sup> ]	0.1510500
$k_3$ [M <sup>-2</sup> h <sup>-1</sup> ]	0.0000241
$k_4$ [M <sup>-1</sup> h <sup>-1</sup> ]	0.5423146
$k_5$ [M <sup>-2</sup> h <sup>-1</sup> ]	0.0000002
$k_6$ [M <sup>-1</sup> h <sup>-1</sup> ]	3.015652

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