Supplementary Information

Core-shell Si₃N₄@WS₂ porous ceramics with improved electromagnetic wave absorption performance

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Preparation of porous Si₃N₄ ceramics

A mixture of Si₃N₄ powder, mono-dispersed poly methyl methacrylate (PMMA, d₅₀=~50 μ m), and Lu₂O₃, (Si₃N₄:PMMA:Lu₂O₃ = 67.2:30:2.8) was wet-milled for 4 h by a planetary ball milling at 300 rpm using Si₃N₄ balls as the milling media and ethanol as a liquid medium to obtain mixture slurry. The mass ratio for powder mixture:Si₃N₄ balls:liquid medium was 1:2:1. After drying at 70 °C for 24 h, the uniformly-mixed powders were uniaxially pressed into a square die using a uniaxial compactor machine under the 20 MPa to obtain green bodies. The green bodies were heated at 600 °C for 2 h in the air to remove the PMMA by oxidation, and then sintered at 1670 °C for 3 h in a 0.3 MPa nitrogen atmosphere.

Characterization:

The phase composition of the samples was analyzed via X-ray diffraction (XRD, Cu K α as radiation, Germany). The morphology of the fracture surface was observed using field emission scanning electron microscope (SEM, Hitachi SU8220, Japan) and transmission electron microscopy (TEM, JEM-2100F). Apparent porosity was measured by the Archimedes method. Raman spectra were obtained on a LabRam HR800 with a visible laser (532 nm) to characterize the structure of the samples. The vector network analyzer (VNA, Agilent E5071C; China) was carried out to test the complex permittivity of the samples with dimensions of 22.86 mm × 10.16 mm × 3 mm in the frequency range of 8.2-12.4 GHz

Electromagnetic Formulas:

The complex permittivity $(\varepsilon_r = \varepsilon' - j\varepsilon'')$ and complex permeability $(\mu_r = \mu' - j\mu'')$

were tested using the wave-guide method. The ε' and μ' values represent the capacity to store electromagnetic energy, while ε'' and μ'' represent the inner dissipation. Based on transmission line theory, the reflection loss (RL) was calculated using ε_r and μ_r as following equations:

$$RL = 20\log_{10} \frac{|Z_{in} - Z_0|}{|Z_{in} + Z_0|}$$
(1)
$$Z_{in} = Z_0 \sqrt{\frac{\mu_r}{\varepsilon_r}} tanh[j\frac{2\pi f d}{c} \sqrt{\mu_r \varepsilon_r}]$$
(2)

where Z_{in} is the input impedance of the microwave absorber layer, Z_0 is the impedance of the EMW in free space. *c*, *f*, and *d* are the light speed, frequency, and matching thickness of the absorber, respectively.

The attenuation constant (α) can be calculated through:

$$\alpha = \frac{\sqrt{2}\pi f}{c} \left[\left(\mu \ddot{\varepsilon} - \mu \dot{\varepsilon} \right) + \sqrt{\left(\mu \ddot{\varepsilon} - \mu \dot{\varepsilon} \right)^2 + \left(\mu \dot{\varepsilon} + \mu \ddot{\varepsilon} \right)^2} \right]^{\frac{1}{2}}$$
(3)

The matching impedance ratio Z need to be the following the equation:

$$Z = \left| \frac{Z_{in}}{Z_0} \right| = \left| \sqrt{\frac{\mu_r}{\varepsilon_r} tanh[j \frac{2\pi f d}{c} \sqrt{\mu_r \varepsilon_r}]} \right|$$
(4)

The $|\Delta|$ value can be calculated by the following equation:

$$|\Delta| = |\sinh^{2}(Kfd) - M|$$

$$K = \frac{4\pi \sqrt{\mu \epsilon} \cdot \sin(\frac{\delta_{\epsilon} + \delta_{\mu}}{2})}{c \cdot \cos \delta_{\epsilon} \cdot \cos \delta_{\mu}}$$

$$(6)$$

$$4\mu' \cdot \cos \delta_{\epsilon} \cdot \epsilon' \cdot \cos \delta_{\mu}$$

$$M = \frac{\mu^{2} \cos \delta_{\varepsilon} - \varepsilon \cos \delta_{\mu}}{(\mu^{2} \cos \delta_{\varepsilon} - \varepsilon^{2} \cos \delta_{\mu})^{2} + \left[\tan^{\frac{2}{100}}\left(\frac{\delta_{\mu} - \delta_{\varepsilon}}{2}\right)\right]^{2} \cdot \left(\mu^{2} \cos \delta_{\varepsilon} + \varepsilon^{2} \cos \delta_{\mu}\right)^{2}}$$
(7)

where δ_{ε} and δ_{μ} are dielectric loss angle and magnetic loss angle, respectively.

CST simulation:

CST Studio Suite 2020 was employed to simulate the radar cross section (RCS). A double-layer metal back model (the upper layer is a 4.20 mm absorbent layer, and the bottom layer is a perfect conductive layer (PEC) of 2.00 mm was designed for RCS simulation analysis. The simulation frequency in all simulation conditions was set as 9.30 GHz. The frame of the model is set to a square of 180×180 mm.

Figures



Fig. S1. SEM images of $Si_3N_4@WS_2-1$.



Fig. S2. SEM images of $Si_3N_4@WS_2$ -2.



Fig. S3. SEM images of $Si_3N_4@WS_2-4$.



Fig. S4. XRD patterns of Si_3N_4 , $Si_3N_4@WS_2-1$, $Si_3N_4@WS_2-2$, $Si_3N_4@WS_2-3$, and $Si_3N_4@WS_2-4$.



Fig. S5. Raman spectra of Si_3N_4 , $Si_3N_4@WS_2-1$, $Si_3N_4@WS_2-2$, $Si_3N_4@WS_2-3$, and $Si_3N_4@WS_2-4$.



Fig. S6. Porosity of Si_3N_4 , $Si_3N_4@WS_2-1$, $Si_3N_4@WS_2-2$, $Si_3N_4@WS_2-3$, and $Si_3N_4@WS_2-4$.



Fig. S7. Frequency-dependent (a) $\varepsilon', \varepsilon''$, and (b) $\tan \delta_{\varepsilon}$ of Si₃N₄ porous ceramics.