

## Supplementary Information

### Thermal Deactivation of Pd/Al<sub>2</sub>O<sub>3</sub>-Cu/Al<sub>2</sub>O<sub>3</sub>-combined Three-way Catalysts via Cu Migration and Alloying

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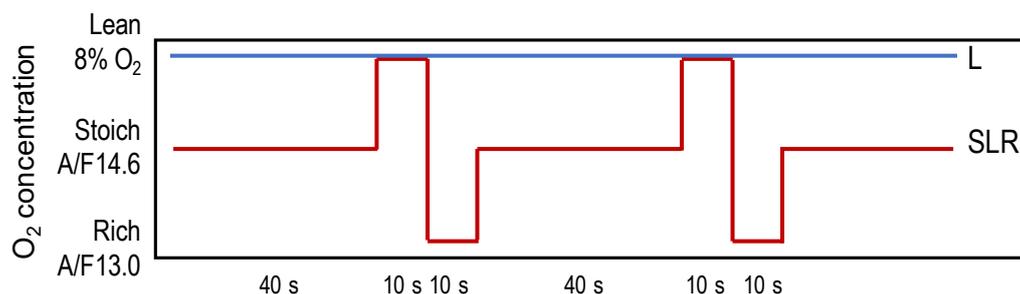
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**Figure S1.** Schematic diagram of the gas feeds for thermal aging under SLR and L conditions. SLR: three simulated gas feeds, that is, a stoichiometric gas (S, 40 s), a fuel-lean gas (L, 10 s), and a fuel-rich gas (R, 10 s), were cycled sequentially. L: constant lean condition. Detailed gas compositions are shown below. The gas feed was supplied at a total flow rate of 100 mL min<sup>-1</sup>. Gas compositions for each condition are shown below.

| Aging                                | Stoichiometric (S) <sup>b</sup> | Lean (L) <sup>b</sup> | Rich (R) <sup>b</sup> | Air     |
|--------------------------------------|---------------------------------|-----------------------|-----------------------|---------|
| Air-to-fuel ratio (A/F) <sup>a</sup> | 14.6                            | -                     | 13.0                  | -       |
| Excess oxygen ratio                  | 1.0                             | 18.2                  | 0.06                  | -       |
| CO/%                                 | 0.50                            | 0.50                  | 0.50                  | -       |
| C <sub>3</sub> H <sub>6</sub> /ppm   | 400                             | 400                   | 400                   | -       |
| NO/ppm                               | 500                             | 500                   | 500                   | -       |
| O <sub>2</sub> /%                    | 0.4                             | 8                     | 0                     | 18      |
| H <sub>2</sub> O/%                   | 10                              | 10                    | 10                    | 10      |
| N <sub>2</sub>                       | balance                         | balance               | balance               | balance |

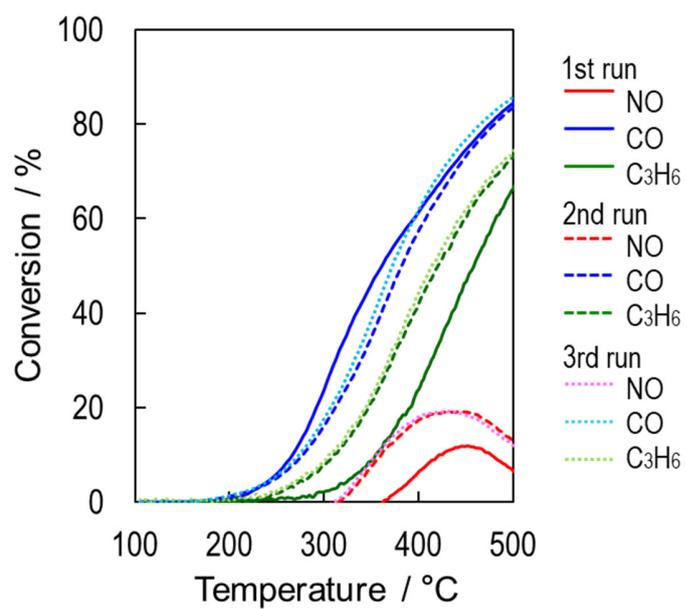
<sup>a</sup> The A/F value was calculated in accordance with a reported study<sup>1</sup> using the excess oxygen ratio of the simulated gas feed, which is calculated as follows:

$$\text{Excess oxygen ratio} = \frac{\text{Amount of oxygen in gas feed}}{\text{Amount of oxygen required for complete oxidation}} = \frac{2 \times p_{\text{O}_2} + p_{\text{NO}}}{9 \times p_{\text{C}_3\text{H}_6} + p_{\text{CO}}}$$

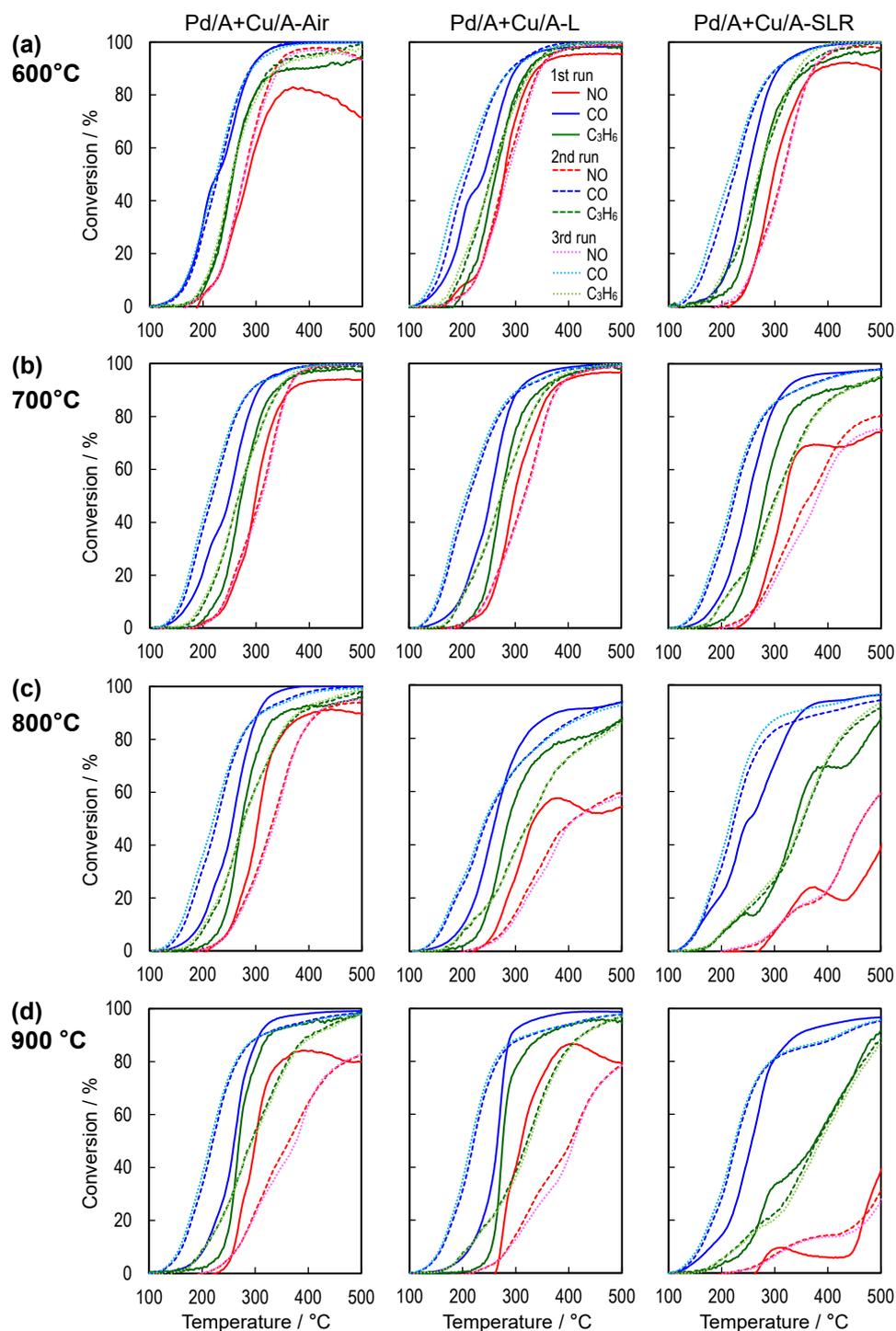
<sup>b</sup> During SLR cycle aging, three gas feeds, that is, S (40 s), L (10 s), and R (10 s), were cycled sequentially.

Exposure to 10% H<sub>2</sub>O/air flow without any exhaust gas mixture leads to an Air-aged Pd–Cu composite catalyst (Pd/A+Cu/A-Air). For Air aging, approximately 0.2 g of catalysts was placed into a preheated tubular furnace at the desired temperature. Following a 5-h exposure to 10% H<sub>2</sub>O/air stream, the catalyst was removed from the furnace and cooled in air at room temperature. For L and SLR aging, approximately 0.2 g of catalysts was heated from room temperature to each

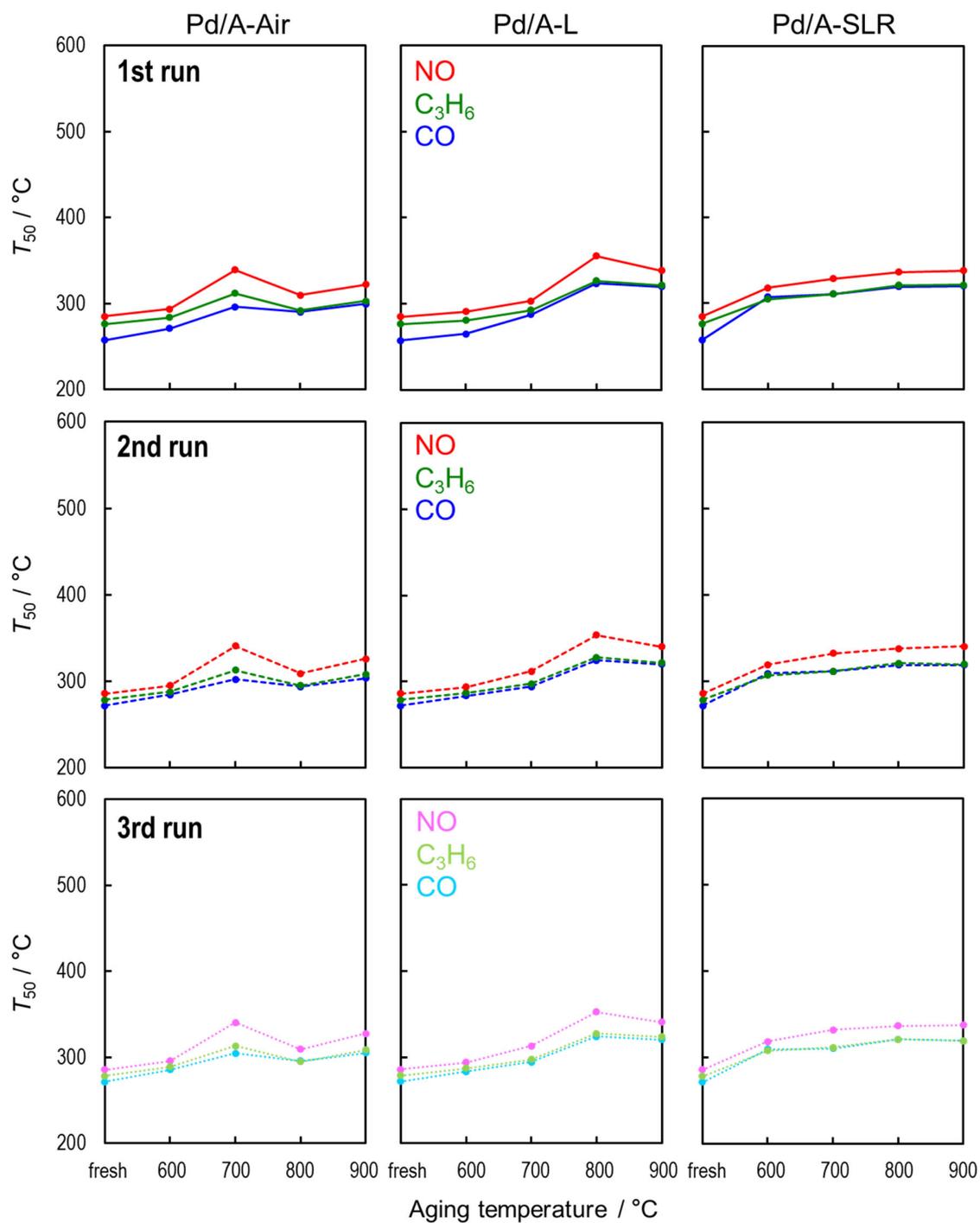
aging temperature (600°C–900°C) for 2 h under N<sub>2</sub> flow. When the desired aging temperature was achieved, N<sub>2</sub> was replaced by a simulated exhaust gas mixture as shown in the above table. Three different gas feeds, including a stoichiometric gas (A/F = 14.6, 40 s), a lean gas (8% O<sub>2</sub>, 10 s), and a rich gas (A/F = 13.0, 10 s), were cycled sequentially, ending with the stoichiometric portion of the cycle at the end of the aging period of 5 h for L and SLR aging. After L and SLR aging, the catalyst bed was cooled under N<sub>2</sub> flow, and Pd/A+Cu/A-L and Pd/A+Cu/A-SLR catalysts were obtained, respectively.



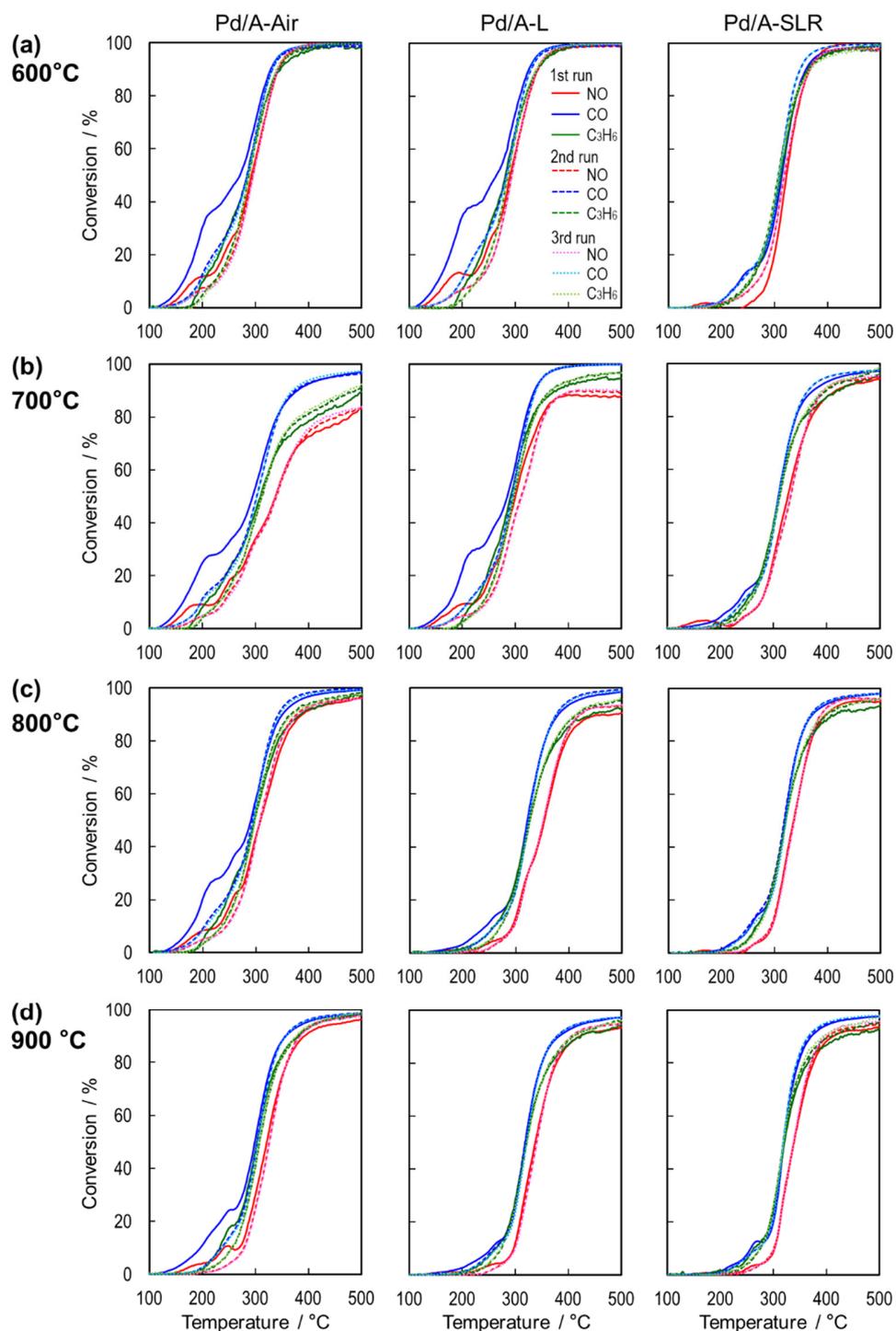
**Figure S2.** Light-off curves of NO, CO, and C<sub>3</sub>H<sub>6</sub> during the first, second, and third light-off runs in the simulated TWC reaction over Cu/A after thermal aging under air.



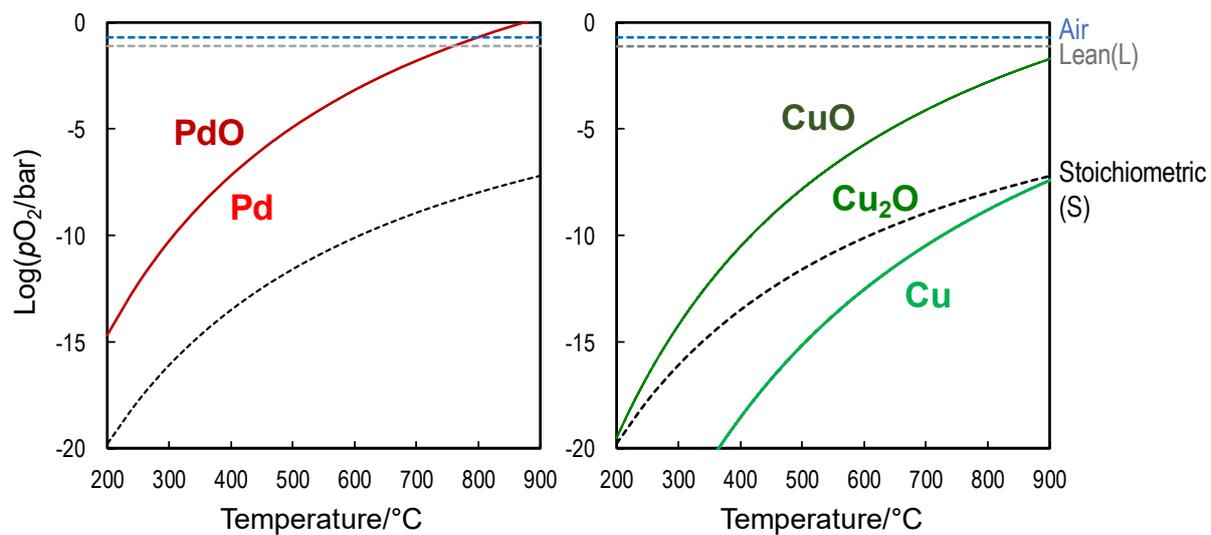
**Figure S3.** Light-off curves of NO, CO, and C<sub>3</sub>H<sub>6</sub> during the first, second, and third light-off runs in the simulated TWC reaction over Pd/A+Cu/A-Air, Pd/A+Cu/A-L, and Pd/A+Cu/A-SLR catalysts with different aging temperatures: (a) 600°C, (b) 700°C, (c) 800°C, and (d) 900°C.



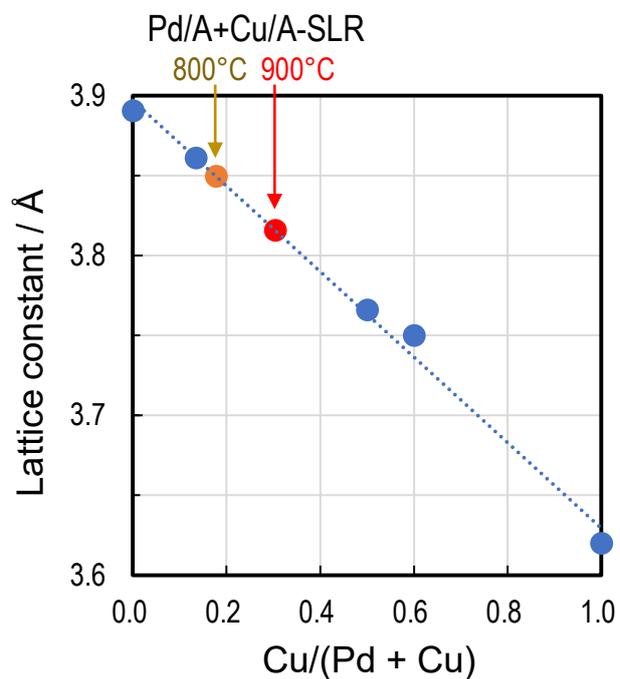
**Figure S4.**  $T_{50}$  values of NO, CO, and  $C_3H_6$  during the first, second, and third light-off runs in the simulated TWC reaction for Pd/A catalysts after thermal aging at elevated temperatures under Air, L, and SLR conditions. The light-off curves for each plot are shown in Figure S5.



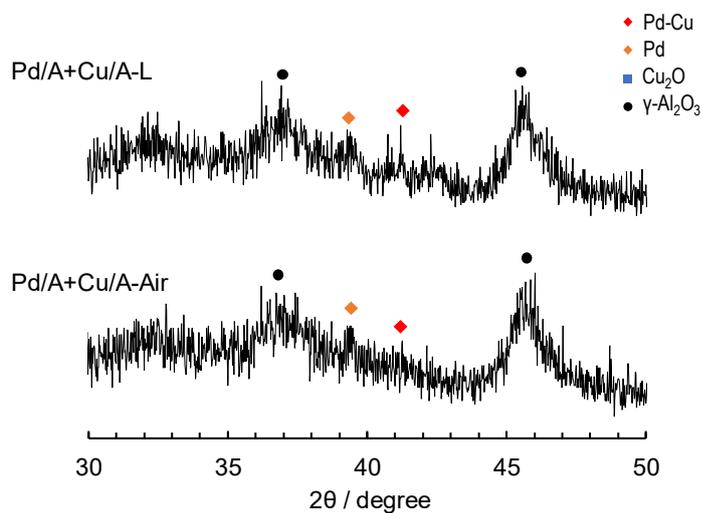
**Figure S5.** Light-off curves of NO, CO, and C<sub>3</sub>H<sub>6</sub> during the first, second, and third light-off runs in the simulated TWC reaction over Pd/A-Air, Pd/A-L, and Pd/A-SLR catalysts with different aging temperatures: (a) 600°C, (b) 700°C, (c) 800°C, and (d) 900°C.



**Figure S6.** Phase relationships in the partial oxygen pressure versus temperature plots of the Pd–O and Cu–O systems. Red and green curves represent the equilibrium of PdO–Pd and CuO–Cu<sub>2</sub>O–Cu, respectively, and other dashed curves correspond to the thermal aging atmosphere.



**Figure S7.** Lattice constant estimation of the Pd–Cu alloys formed in Pd/A+Cu/A-SLR after aging at 800°C and 900°C. The blue circles correspond to Pd–Cu alloys found in the literature data.<sup>2-5</sup> Pd–Cu alloys observed in Pd/A+Cu/A-SLR are shown as yellow and red circles.



**Figure S8.** XRD patterns of Pd/A+Cu/A-Air and Pd/A+Cu/A-L catalysts (aged at 800°C) after stoichiometric TWC light-off runs (three runs).

## REFERENCES

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