

## Supporting information for

### **Rational design of anti-freezing electrolyte concentrations via freeze concentration process**

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**This file includes:**

Experimental and Computational Methods

Figs. S1 to S13

Tables S1 to S14

References 1-23

## Methods

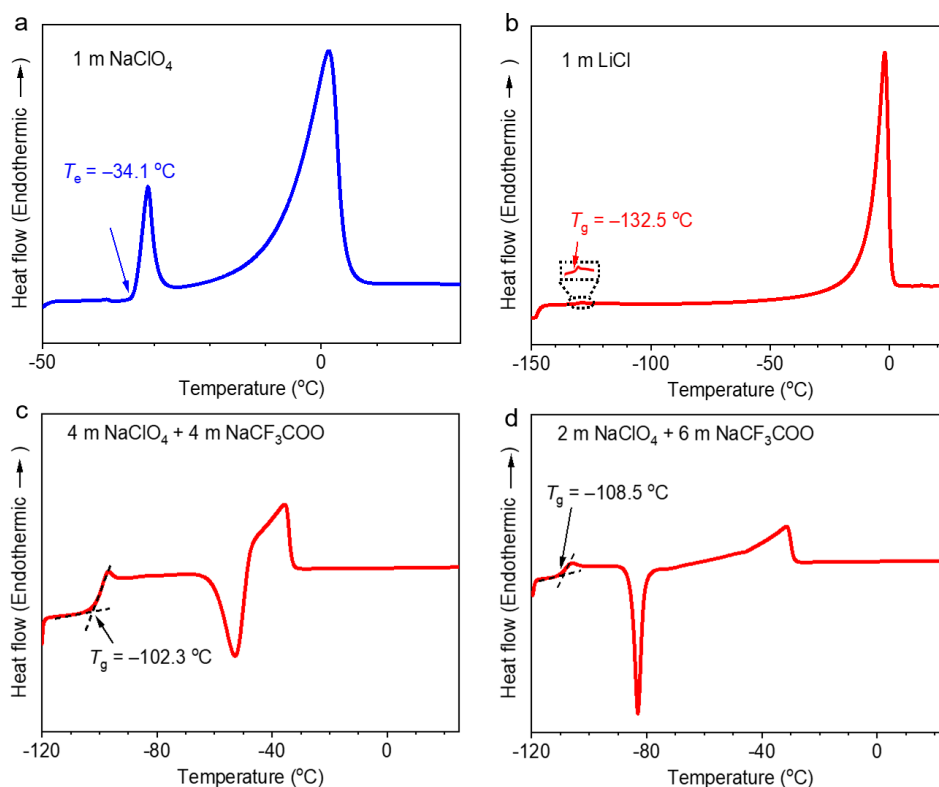
**Material fabrication.** The  $\text{LiMn}_2\text{O}_4$  cathode and PTCDI anode are purchased from MTI and Alfa Aesar corporations, respectively. The NaCoHCF cathode was prepared by a simple precipitation approach according to the literature<sup>1</sup>. The cathode (anode) composite electrodes were fabricated by compressing cathode (anode), carbon black, and polytetrafluoroethylene (PTFE) at weight ratio of 7:2:1 (6:3:1). The Ti mesh is used as the electrode current collector. The 3.85 m  $\text{NaClO}_4$  + 5.92 m  $\text{NaCF}_3\text{COO}$  electrolyte is obtained by dissolving 3.85 mmol  $\text{NaClO}_4$  and 5.92 mmol  $\text{NaCF}_3\text{COO}$  into 1 g  $\text{H}_2\text{O}$ . The  $\text{H}_{36}\text{EG}_{64}$ -0.5 m  $\text{NaClO}_4$  electrolyte is obtained by dissolving 0.5 mmol  $\text{NaClO}_4$  into 0.36 g  $\text{H}_2\text{O}$  and 0.64 g ethylene glycol (EG).

**Syringe-filtration method in FCE approach.** In the syringe-filtration method, the dilute solution of single-solute (such as the  $\text{H}_2\text{O}$ -LiCl or  $\text{H}_2\text{O}$ - $\text{NaClO}_4$ ) system is usually kept in the chamber at  $T_i$  for several hours or longer time before the FCE is filtered (**Fig. S2a, ESI†**). For the multiple-solute  $\text{H}_2\text{O}$ - $\text{NaClO}_4$ - $\text{NaCF}_3\text{COO}$  and  $\text{LiPF}_6$ -EC-DEC system, the dilute solution is first frozen in liquid nitrogen (**Fig. S2b, ESI†**) to eliminate the supercooling during hydrate precipitation, followed by the same procedure as in above single-solute system. The equilibrium of FCEs in  $\text{H}_2\text{O}$ -LiCl,  $\text{H}_2\text{O}$ - $\text{NaClO}_4$ ,  $\text{H}_2\text{O}$ - $\text{NaClO}_4$ - $\text{NaCF}_3\text{COO}$ , and  $\text{LiPF}_6$ -EC-DEC systems can be reached after keeping dilute solution at  $T_i$  for 2 hours, 3 hours, 6 hours, and 24 hours, respectively, because the refractive index of obtained FCE does not change even after keeping the dilute solution at  $T_i$  for longer time. Here, the dilute solution is the one that has a concentration less than eutectic-point concentration  $X_e$  and will precipitate ice or hydrate at  $T_i$ . In the single-solute system, the electrolyte refractive index usually increases as the concentration increases. Therefore, one can identify the preselected solution as a dilute solution when the refractive index of FCE obtained at  $T_i$  is higher than that of preselected solution. The FCE concentrations in  $\text{H}_2\text{O}$ -LiCl and  $\text{H}_2\text{O}$ - $\text{NaClO}_4$  systems were determined by the refractive index method<sup>2</sup> (**Figs. S2c-d, ESI†**). The FCE concentrations in  $\text{H}_2\text{O}$ - $\text{NaClO}_4$ - $\text{NaCF}_3\text{COO}$  system were determined by the inductively coupled plasma atomic emission spectrometry<sup>3</sup> (to determine the concentration of  $\text{Na}^+$ ) and ion chromatography (to determine the concentration of  $\text{ClO}_4^-$ )<sup>4, 5</sup>. The FCE concentration in  $\text{LiPF}_6$ -EC-DEC system was determined by ICP test (for  $\text{Li}^+$ ) and organic elemental analyzer vario EL cube (for carbon mass ratio).

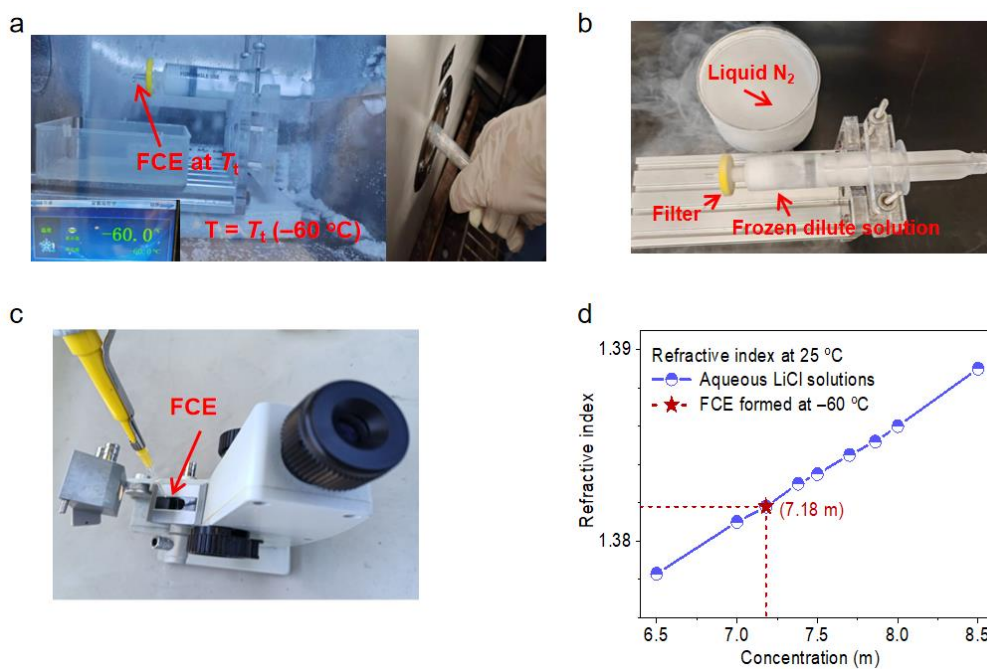
**Electrochemical measurements.** The three-electrode cell consists of cathode (anode) composite working electrode, active carbon counter electrode, and Ag/AgCl-7.18 m LiCl (0.205 V vs. standard hydrogen electrode), with the mass ratio of counter electrode to working electrode being around 8-10. Swagelok-type cells were used to assemble the Li-based full cell, with Ti foil used to protect against halogen corrosion. Coin cells were used to assemble the Na-based full cell. The mass loadings of cathode and anode in Li-based Swagelok-type cells are  $6.3 \text{ mg cm}^{-2}$  and  $7.2 \text{ mg cm}^{-2}$  respectively. The mass loadings of cathode and anode in Na-based coin cells are  $5.4 \text{ mg cm}^{-2}$  and  $7.6 \text{ mg cm}^{-2}$  respectively. The amount of electrolyte in Li-based Swagelok-type cell and Na-based coin cell was 0.2 mL. The mass loading of cathode and anode in Li-based pouch cell are  $13.3 \text{ mg cm}^{-2}$  and  $15.2 \text{ mg cm}^{-2}$  respectively. The mass loading of cathode and anode in Na-based pouch cell are  $11.4 \text{ mg cm}^{-2}$  and  $14.6 \text{ mg cm}^{-2}$  respectively. The amount of electrolyte in Li-based and Na-based pouch cells were 1.0 mL. The charge-discharge tests of cells were performed on the Landt battery test systems (CT3001A, Wuhan Land Electronic Co., Ltd.) and Neware battery test systems (CT-4008-5V50mA-164, Neware technology limited). The full cell specific capacities are showed based on cathode mass and all the current rates are calculated based on a theoretical capacity of  $120 \text{ mAh g}^{-1}$  in both Li- and Na-based cells. The mass ratio of cathode/anode is 1/0.9 for both Li-based and Na-based full cells. The energy densities of full cells are calculated based on total active material mass of cathode and anode. For low-temperature tests, the cell performance was measured in a ShangHai BoYi B-T-107D oven.

**Characterization.** The refractive index was measured by the Abbe refractometer (WAY-2WAJ) with high accuracy ( $\pm 0.0002$ ). The ionic conductivities of the electrolytes were measured by electrochemical impedance spectroscopy (EIS) using BioLogic. The chemical formula ( $\text{Na}_{1.4}\text{Co}[\text{Fe}(\text{CN})_6]_{0.84} \cdot 2.5\text{H}_2\text{O}$ ) of NaCoHCF cathode was determined by inductively coupled plasma atomic emission spectrometry. The Raman spectra for electrolytes were conducted on HORIBA HR evolution microscope using a 532 nm excitation laser. The Raman spectra of  $\text{H}_2\text{O}-\text{NaClO}_4$  system at  $-34.1 \text{ }^\circ\text{C}$  and  $\text{H}_2\text{O}-\text{NaClO}_4-\text{NaCF}_3\text{COO}$  system at  $-50 \text{ }^\circ\text{C}$  were tested after experiencing a cooling process from  $25 \text{ }^\circ\text{C}$  to  $-150 \text{ }^\circ\text{C}$ . DSC tests were carried out in DSC200F3 with cooling and heating rates of  $10 \text{ K min}^{-1}$  from  $25 \text{ }^\circ\text{C}$  to  $-150 \text{ }^\circ\text{C}$ . The linear sweep voltammetry (LSV) is tested at scan rate of  $10 \text{ mV s}^{-1}$  using BioLogic.

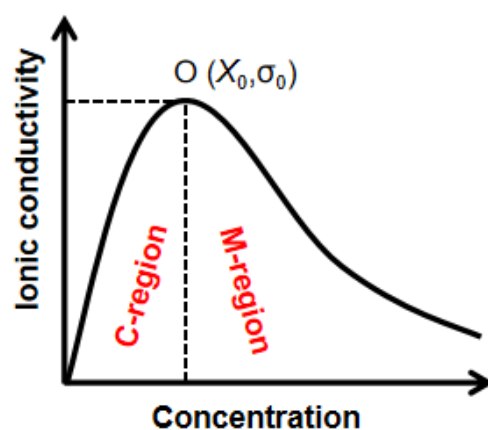
**AIMD simulations.** The AIMD simulations were carried out by using the Vienna ab initio simulation package (VASP)<sup>6</sup>. The projector augmented-wave (PAW) potentials<sup>7</sup> generated with Perdew–Burke–Ernzerhof (PBE) generalized gradient approximation (GGA)<sup>8</sup>were used. The van der Waals (vdW) interaction was taken into account by using the rev-vdWDF2 functional<sup>9</sup>. The plane wave cut-off energy was set to 400 eV and the  $\Gamma$  point was used for the Brillouin zone sampling. The AIMD simulations were performed in a canonical ensemble (NVT)<sup>10, 11</sup> by using a Nose-Hoover thermostat at 300 K (H<sub>2</sub>O, 7.18 m LiCl, 9.07 m NaClO<sub>4</sub>, 3.85 m NaClO<sub>4</sub> + 5.92 m NaCF<sub>3</sub>COO), with a time step of 1 fs. All the AIMD simulations were run for 60-100 ps to yield the data for analysis. The H<sub>2</sub>O AIMD model contains 165 atoms (55 H<sub>2</sub>O) within 11.8 Å x 11.8 Å x 11.8 Å cubic supercell. The 7.18 m LiCl electrolyte AIMD model contains 181 atoms (8 LiCl and 55 H<sub>2</sub>O) within 12.5 Å x 12.5 Å x 12.5 Å cubic supercell. The 9.07 m NaClO<sub>4</sub> electrolyte AIMD model contains 96 atoms (4 NaClO<sub>4</sub> and 24 H<sub>2</sub>O) within 10.5 Å x 10.5 Å x 10.5 Å cubic supercell. The 3.85 m NaClO<sub>4</sub> + 5.92 m NaCF<sub>3</sub>COO electrolyte AIMD model contains 117 atoms (2 NaClO<sub>4</sub>, 3 NaCF<sub>3</sub>COO, and 27 H<sub>2</sub>O) within 11.5 Å x 11.5 Å x 11.5 Å cubic supercell. The initial structures of liquid electrolyte models were constructed using the Packmol software<sup>12</sup>.



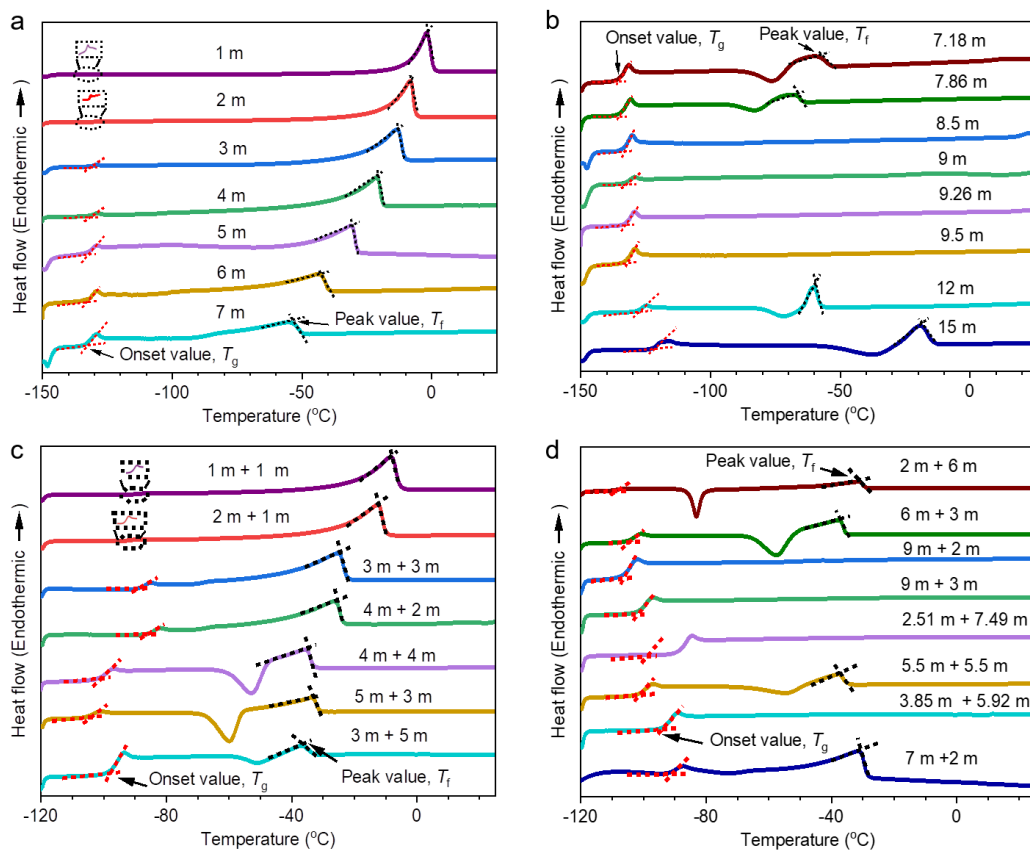
**Fig. S1. Determine the liquid-to-solid low-temperature limits of H<sub>2</sub>O-solute systems by DSC heating curves of dilute solutions. (a)** The DSC heating curve of 1 m NaClO<sub>4</sub> electrolyte in H<sub>2</sub>O-NaClO<sub>4</sub> system. The eutectic heat-flow peak on the DSC curve demonstrates that the thermodynamic liquid-to-solid low-temperature limit  $T_e$  of the H<sub>2</sub>O-NaClO<sub>4</sub> system is  $-34.1$  °C.  $T_e$  is usually determined by the onset temperature of  $T_e$  peak<sup>13</sup>. **(b)** The DSC heating curve of 1 m LiCl electrolyte in H<sub>2</sub>O-LiCl system. The DSC curve shows the glass-transition step (see the enlarged picture in the dotted rectangle) rather than the eutectic heat-flow peak, demonstrating that the DSC test can only determine the kinetic liquid-to-solid low-temperature limit  $T_g$  ( $-132.5$  °C) rather than the  $T_e$  value of H<sub>2</sub>O-LiCl system.  $T_g$  is usually determined by the onset temperature of  $T_g$  peak<sup>14</sup>. **(c-d)** The DSC heating curves of 4 m NaClO<sub>4</sub> + 4 m NaCF<sub>3</sub>COO ( $T_g = -102.3$  °C) **(c)** and 2 m NaClO<sub>4</sub> + 6 m NaCF<sub>3</sub>COO ( $T_g = -108.5$  °C) **(d)** electrolytes in H<sub>2</sub>O-NaClO<sub>4</sub>-NaCF<sub>3</sub>COO system.



**Fig. S2. The syringe-filtration method for the FCE approach. (a)** keep the dilute solution in the chamber at  $T_t$  (e.g.  $-60^\circ\text{C}$ ) to reach chemical equilibrium before filtering the FCE by manually squeezing the syringe. **(b)** Illustration of a dilute solution of  $\text{H}_2\text{O}$ - $\text{NaClO}_4$ - $\text{NaCF}_3\text{COO}$  system being frozen in liquid  $\text{N}_2$ . **(c)** Measure the refractive index of FCE with the Abbe refractometer. **(d)** Determine the concentration of FCE obtained at  $-60^\circ\text{C}$  by the refractive index method.

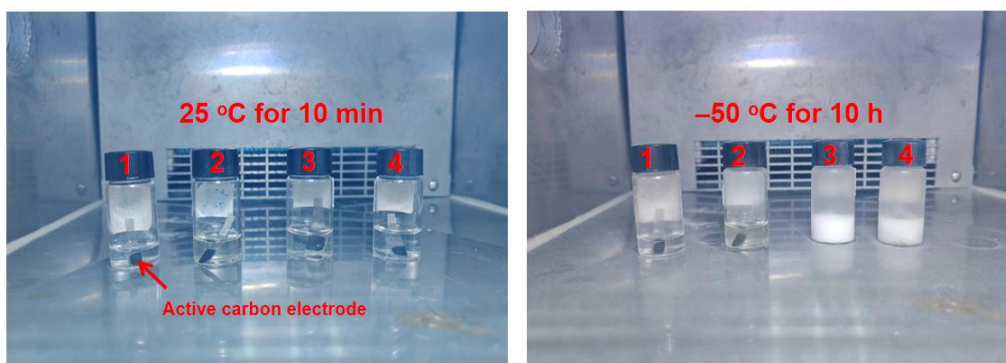


**Fig. S3. Typical concentration-conductivity curve in an H<sub>2</sub>O-solute system.** The point O ( $X_0, \sigma_0$ ) is the maximum conductivity point. The concentration-conductivity curve can be divided into two regions<sup>15, 16</sup>: concentration-controlled region (C-region) below concentration  $X_0$  and mobility-controlled region (M-region) above concentration  $X_0$ . The FCE obtained at ultralow  $T_f$  usually locate at the M-region and therefore has the lowest electrolyte concentration (therefore the lowest cost) and the highest ionic conductivity without being frozen at  $T_f$ .

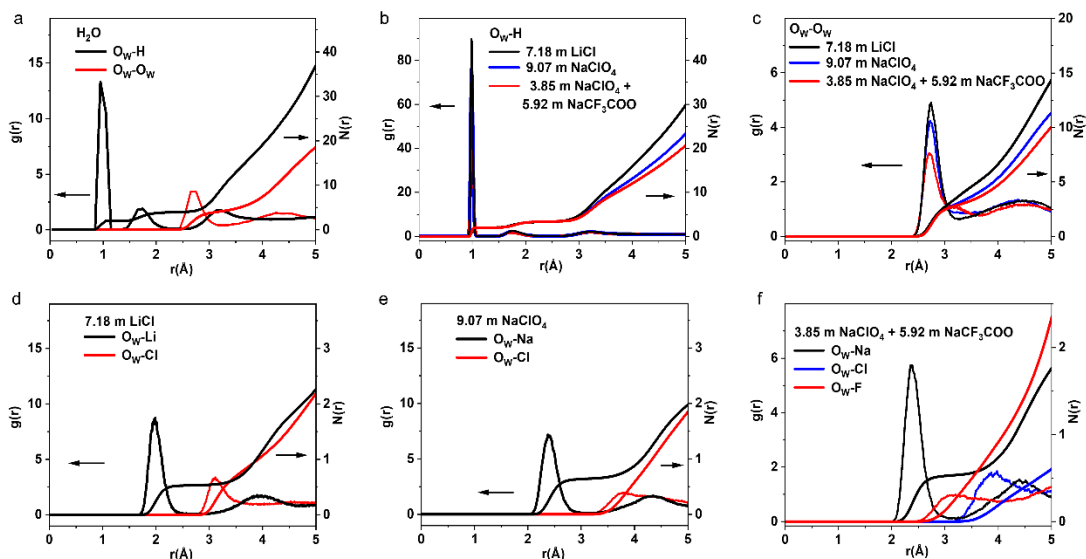


**Fig. S4.** The DSC heating curves of aqueous solutions in  $\text{H}_2\text{O-LiCl}$  and  $\text{H}_2\text{O-NaClO}_4\text{-NaCF}_3\text{COO}$  systems at heating rate of  $10 \text{ K min}^{-1}$ . **a-b**, 1 m to 15 m LiCl. **c-d**, Various electrolyte concentrations. The “1 m + 1 m” represents the “1 m  $\text{NaClO}_4$  + 1 m  $\text{NaCF}_3\text{COO}$ ”. See all the  $T_g$  and  $T_f$  values in **Tables S2 and S8**.

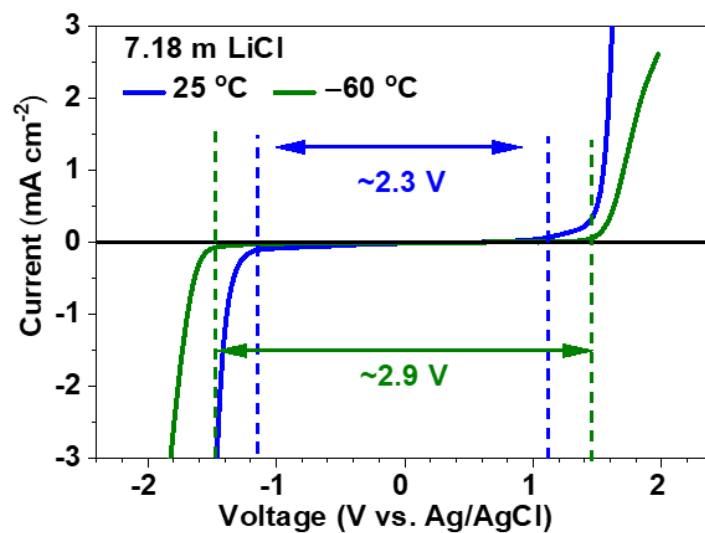




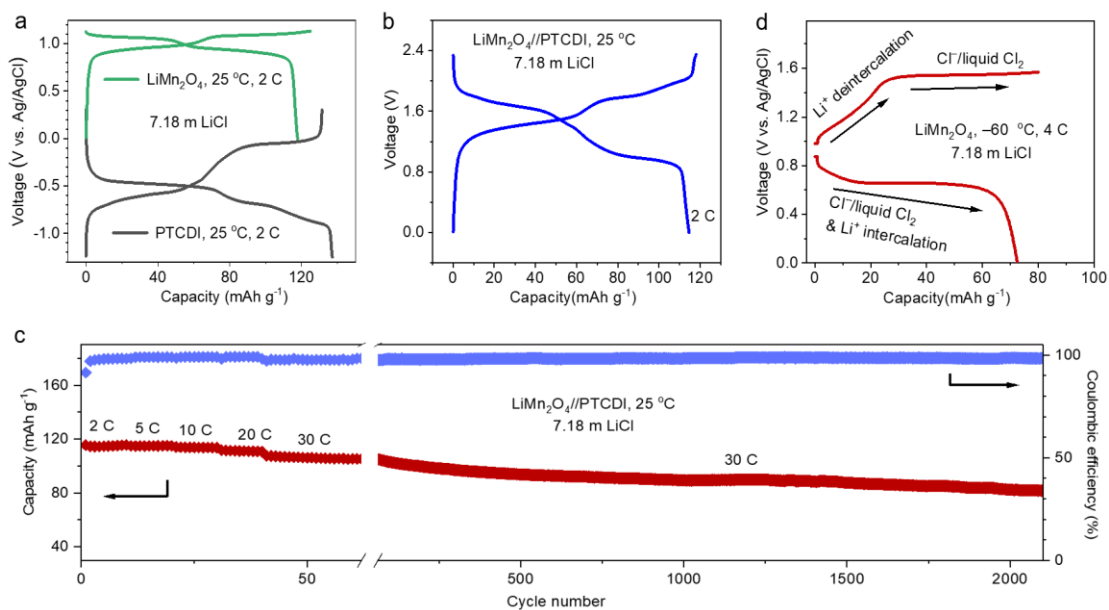
**Fig. S5. The photographs of various electrolytes in  $\text{H}_2\text{O}-\text{NaClO}_4-\text{NaCF}_3\text{COO}$  system at 25 °C (10 min) and -50 °C (10 h). The active carbon electrodes are used to inhibit supercooling phenomenon and promote electrolyte crystallization. No. 1: 3.85 m  $\text{NaClO}_4$  + 5.92 m  $\text{NaCF}_3\text{COO}$ , No. 2: 7.49 m  $\text{NaClO}_4$  + 2.51 m  $\text{NaCF}_3\text{COO}$ , No. 3: 9 m  $\text{NaClO}_4$  + 2 m  $\text{NaCF}_3\text{COO}$ , No. 4: 9 m  $\text{NaClO}_4$  + 3 m  $\text{NaCF}_3\text{COO}$ .**



**Fig. S6.** The radial distribution function  $g(r)$  and coordination number  $N(r)$  for pure  $\text{H}_2\text{O}$ , 7.18 m LiCl, 9.07 m  $\text{NaClO}_4$ , 3.85 m  $\text{NaClO}_4$  + 5.92 m  $\text{NaCF}_3\text{COO}$  AIMD models. (a)  $\text{O}_w\text{-H}$  and  $\text{O}_w\text{-O}_w$  in pure  $\text{H}_2\text{O}$ . (b)  $\text{O}_w\text{-H}$  in the designed FCEs. (c)  $\text{O}_w\text{-O}_w$  in the designed FCEs. (d)  $\text{O}_w\text{-Li}$  and  $\text{O}_w\text{-Cl}$  in 7.18 m LiCl. (e)  $\text{O}_w\text{-Na}$  and  $\text{O}_w\text{-Cl}$  in 9.07 m  $\text{NaClO}_4$ . (f)  $\text{O}_w\text{-Na}$ ,  $\text{O}_w\text{-Cl}$ , and  $\text{O}_w\text{-F}$  in 3.85 m  $\text{NaClO}_4$  + 5.92 m  $\text{NaCF}_3\text{COO}$ .  $\text{O}_w$ : oxygen atom in  $\text{H}_2\text{O}$ .



**Fig. S7.** The linear sweep voltammetry (Scan rate: 10 mV s<sup>-1</sup>) of 7.18 m LiCl electrolyte at 25 °C and -60 °C.



**Fig. S8. Performances of Li-based electrodes and cells in 7.18 m LiCl electrolyte. (a-b),** Typical charge-discharge curves of  $\text{LiMn}_2\text{O}_4$  cathode (a), PTCDI anode (a), and  $\text{LiMn}_2\text{O}_4$ //PTCDI full cell (b) at 25 °C. (c) Rate capability and cycling stability of  $\text{LiMn}_2\text{O}_4$ //PTCDI full cell at 25 °C. (d) Typical charge-discharge curve of  $\text{LiMn}_2\text{O}_4$  cathode at -60 °C. The reversible capacity at -60 °C is contributed by  $\text{Li}^+$ -(de)intercalation mechanism and  $\text{Cl}^-/\text{liquid Cl}_2$  redox mechanism.

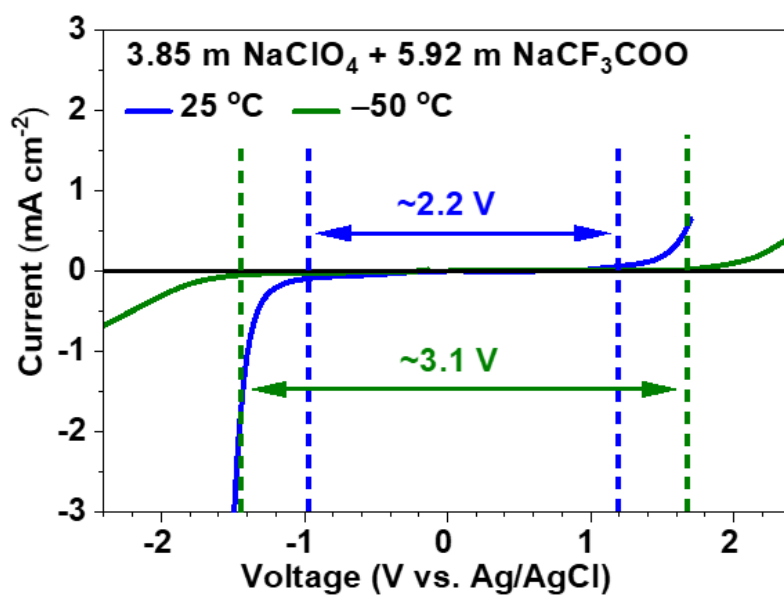
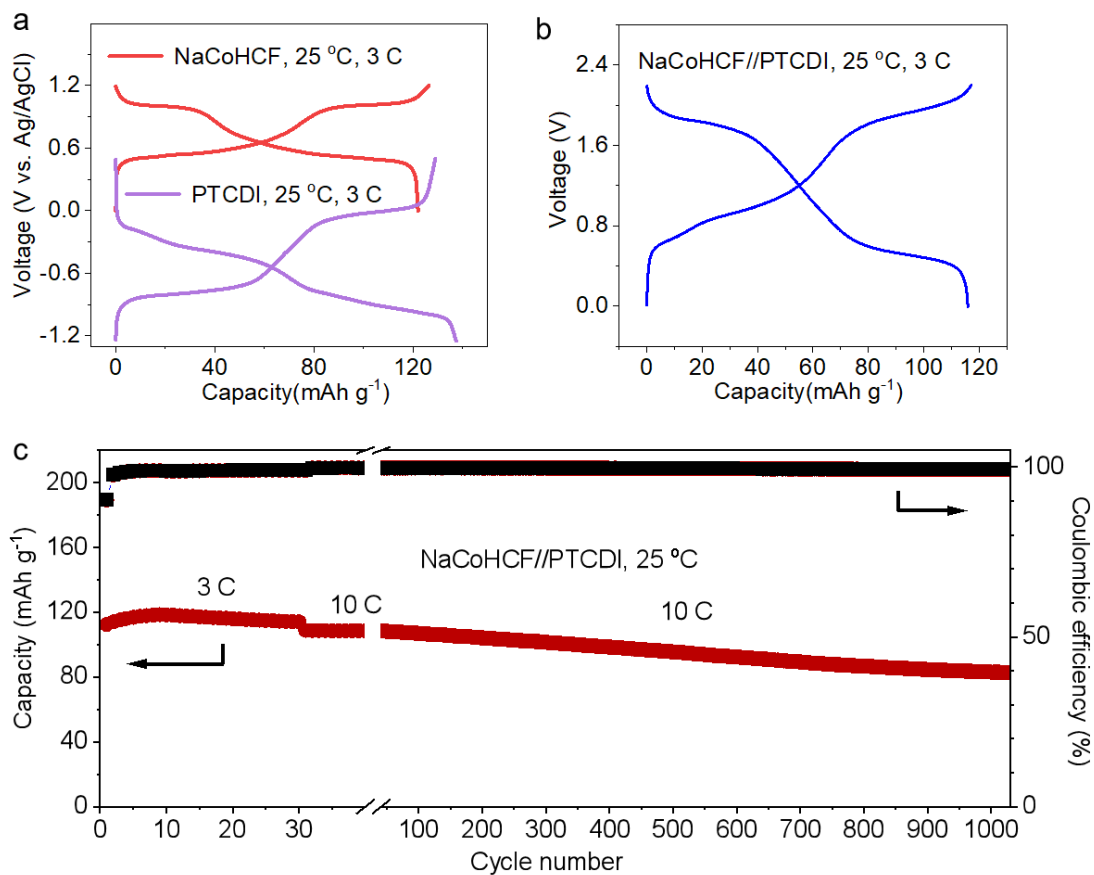
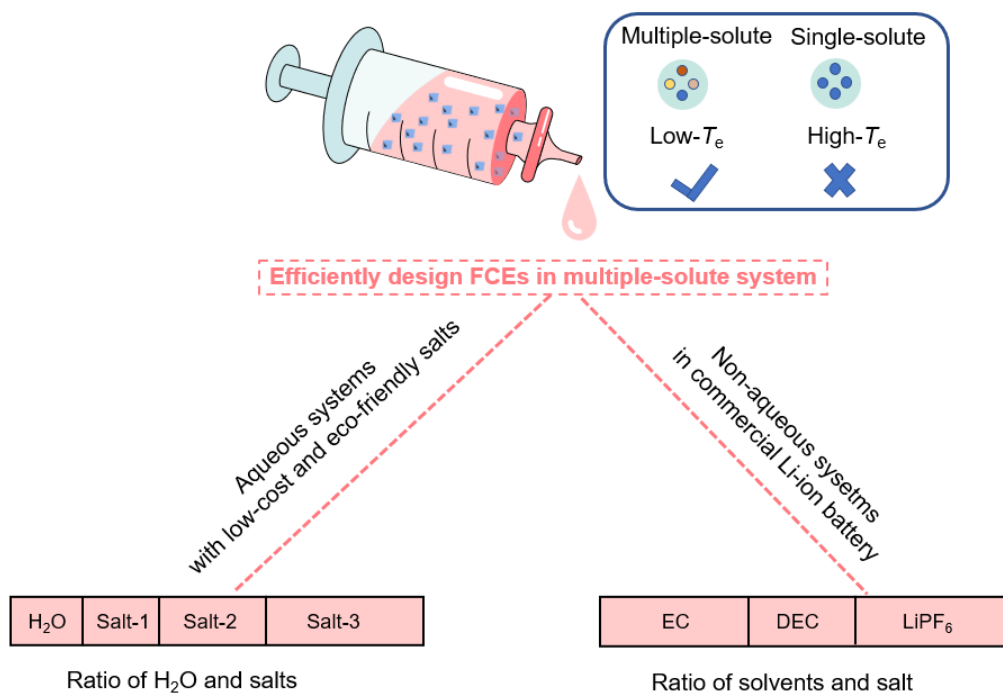


Fig. S9. The linear sweep voltammetry (Scan rate: 10 mV s<sup>-1</sup>) of 3.85 m NaClO<sub>4</sub> + 5.92 m NaCF<sub>3</sub>COO electrolyte at 25 °C and -50 °C.

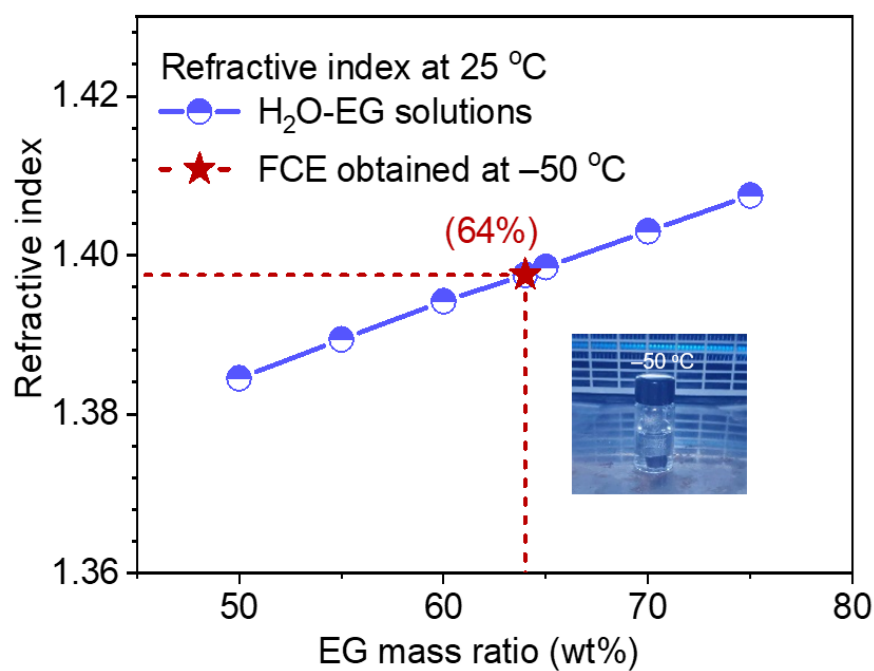


**Fig. S10.** Performances of Na-based electrodes and cells in 3.85 m NaClO<sub>4</sub> + 5.92 m NaCF<sub>3</sub>COO electrolyte. **(a-b)** Typical charge-discharge curves of NaCoHCF cathode **(a)**, PTCDI anode **(a)**, and NaCoHCF//PTCDI full cell **(b)** at 25 °C. **(c)** Rate capability and cycling stability of NaCoHCF//PTCDI full cell at 25 °C.

Freeze concentration at target low temperature



**Fig. S11. Future applications of the FCE approach in designing anti-freezing electrolytes.** EC: ethylene carbonate. DEC: dimethyl carbonate.



**Fig. S12. Design anti-freezing electrolyte in H<sub>2</sub>O-EG-NaClO<sub>4</sub> system using FCE approach when  $T_t$  is  $-50$  °C.** Here, we firstly determined the lowest EG amount (64 wt%) needed to keep unfrozen state in H<sub>2</sub>O-EG system, and then prepared the H<sub>36</sub>EG<sub>64</sub>-0.5 m NaClO<sub>4</sub> electrolyte. The electrolyte can maintain unfrozen state at  $-50$  °C, as shown in the inset photograph (The active carbon electrode is used to inhibit supercooling phenomenon and promote electrolyte crystallization).





**Fig. S13.** The picture of dilute solution (left) and determined FCE (right) after keeping at  $-20\text{ }^{\circ}\text{C}$  for 24 h (firstly being frozen in liquid  $\text{N}_2$ ). The dilute solution is the typical commercial formula, 1M  $\text{LiPF}_6$  in EC-DEC (1:1, vol) (mole ratio of  $\text{LiPF}_6/\text{EC}/\text{DEC}$  is 1/7.50/4.10). The FCE component mole ratio  $\text{LiPF}_6/\text{EC}/\text{DEC}$  is determined as 1/3.23/6.18 (Table S14, ESI†).

**Table S1. The definition of the symbols in the main text.**

Symbols	Definition
$T_f$	Freezing point
$T_e$	Eutectic temperature
$T_t$	The target low temperature
$T_g$	Glass-transition temperature
$T_D$	Freezing point of dilute solution
$X_e$	Eutectic-point concentration
$X_D$	Concentration of dilute solution
$X_F$	Concentration of FCE
$X_{\text{salt-1}}, X_{\text{salt-2}},$ and $X_{\text{H}_2\text{O}}$	Concentration percentages of FCE concentration in ternary systems

**Table S2. The  $T_g$  and  $T_f$  values of aqueous solutions in H<sub>2</sub>O-LiCl system based on the DSC data in Figs. S4a-b and the design efficiency in conventional approach.**

The “\*” means that the  $T_f$  values of these electrolytes cannot be determined by DSC curves owing to the lack of melting peaks, but their  $T_f$  are lower than  $-60$  °C according to the reported H<sub>2</sub>O-LiCl phase diagram<sup>17</sup>.

Preselected concentration	$T_g$ determined by DSC	$T_f$ determined by DSC	Preselected numbers	Qualifying numbers	Design efficiency
1 m	$-132.5$ °C	$-1.5$ °C	15	5	33.3%
2 m	$-132.5$ °C	$-8.1$ °C			
3 m	$-132.5$ °C	$-12.8$ °C			
4 m	$-132.5$ °C	$-20.4$ °C			
5 m	$-132.6$ °C	$-30.5$ °C			
6 m	$-132.4$ °C	$-42.5$ °C			
7 m	$-132.5$ °C	$-53.3$ °C			
7.18 m	$-135.3$ °C	$-56.8$ °C			
7.86 m	$-134.5$ °C	$-66.5$ °C			
8.5 m*	$-133.4$ °C	\			
9 m*	$-132.9$ °C	\			
9.26 m*	$-132.5$ °C	\			
9.5 m*	$-132.1$ °C	\			
12 m	$-128.5$ °C	$-58.9$ °C			
15 m	$-121.3$ °C	$-18.9$ °C			

**Table S3. The anti-freezing electrolyte design using FCE approach when  $T_t$  is set as  $-60\text{ }^\circ\text{C}$  in  $\text{H}_2\text{O-LiCl}$  system and the design efficiency in FCE approach.**

<b>Preselected concentration</b>	<b>Refractive index of FCE at <math>25\text{ }^\circ\text{C}</math></b>	<b>FCE concentration</b>	<b>Qualifying / Preselected numbers</b>	<b>Design efficiency</b>
3 m	1.3818	7.18 m	4/4	100%
4 m	1.3818	7.18 m		
5 m	1.3818	7.18 m		
6 m	1.3818	7.18 m		

**Table S4. The ionic conductivities of various aqueous LiCl electrolytes at  $-60\text{ }^{\circ}\text{C}$ .**

<b>Concentration</b>	<b>Ionic conductivity at <math>-60\text{ }^{\circ}\text{C}</math> (<math>\text{mS cm}^{-1}</math>)</b>
5 m	3.44
6 m	4.27
6.75 m	5.08
7.18 m	6.09
7.86 m	5.87
8.5 m	5.56
9.26 m	5.12
10 m	4.81

**Table S5. The eutectic-point concentration  $X_e$  of H<sub>2</sub>O-NaClO<sub>4</sub> system identified via FCE approach ( $T_t = -34.1$  °C).**

Preselected concentration	Refractive index of FCE at 25 °C	$X_e$
4 m	1.3745	9.07 m
5 m	1.3745	9.07 m
6 m	1.3745	9.07 m

**Table S6. The eutectic-point concentration  $X_e$  for various H<sub>2</sub>O-solute system determined by FCE approach. All the  $T_e$  values of H<sub>2</sub>O-solute systems are determined by DSC tests.**

System	Targeted temperature ( $T_e$ )	Refractive index of FCE at 25 °C	$X_e$
H <sub>2</sub> O-NaCF <sub>3</sub> SO <sub>3</sub>	-20.5 °C	1.3470	4.54 m
H <sub>2</sub> O-KCF <sub>3</sub> SO <sub>3</sub>	-20.5 °C	1.3530	8.30 m
H <sub>2</sub> O-LiBF <sub>4</sub>	-28.5 °C	1.3206	4.53 m
H <sub>2</sub> O-KCl	-12.2 °C	1.3610	3.42 m
H <sub>2</sub> O-LiTFSI	-42.5 °C	1.3584	5.41 m
H <sub>2</sub> O-NaCl	-21.1 °C	1.3705	5.11 m

**Table S7. The anti-freezing electrolyte design using FCE approach when  $T_t$  is set as  $-50\text{ }^\circ\text{C}$  in  $\text{H}_2\text{O}-\text{NaClO}_4-\text{NaCF}_3\text{COO}$  system and the design efficiency in FCE approach.**

<b>Preselected concentration (NaClO<sub>4</sub> + NaCF<sub>3</sub>COO)</b>	<b>Refractive index of FCE at 25 °C</b>	<b>FCE concentration</b>	<b>Qualifying / Preselected numbers</b>	<b>Design efficiency</b>
4 m + 4 m	1.3615	3.85 m + 5.92 m	2/2	100%
2 m + 6 m		2.51m + 7.49 m		

**Table S8. The  $T_g$  and  $T_f$  values of aqueous solutions in  $H_2O$ - $NaClO_4$ - $NaCF_3COO$  system based on the DSC data in Figs. S4c-d and the design efficiency in conventional approach.** The “\*” means that the  $T_f$  values of these electrolytes cannot be determined by DSC curves owing to the lack of melting peaks. According to our crystallization acceleration test in Fig. S5, the two electrolytes (9 m + 2 m, 9 m + 3 m) freeze at  $-50$  °C, whereas another two electrolytes (3.85 m + 5.92 m, 2.51 m + 7.49 m) do not freeze at  $-50$  °C.

Preselected concentration $NaClO_4$ + $NaCF_3COO$	$T_g$ determined by DSC	$T_f$ determined by DSC	Qualifying /Preselected numbers	Design efficiency
1 m + 1 m	$-91.4$ °C	$-8.1$ °C	2/15	13.3%
2 m + 1 m	$-93.6$ °C	$-12.3$ °C		
3 m + 3 m	$-88.6$ °C	$-24.3$ °C		
4 m + 2 m	$-85.3$ °C	$-25.6$ °C		
4 m + 4 m	$-100.6$ °C	$-34.7$ °C		
5 m + 3 m	$-104.1$ °C	$-32.9$ °C		
3 m + 5 m	$-97.5$ °C	$-36.2$ °C		
2 m + 6 m	$-108.5$ °C	$-30.8$ °C		
6 m + 3 m	$-104.4$ °C	$-37.1$ °C		
9 m + 2 m*	$-106.2$ °C	\		
9 m + 3 m*	$-101.5$ °C	\		
7 m + 2 m*	$-99.1$ °C	$-30.8$ °C		
5.5 m + 5.5 m	$-101.4$ °C	$-36.9$ °C		
3.85 m + 5.92 m*	$-93.7$ °C	\		
2.51 m + 7.49 m*	$-88.2$ °C	\		



**Table S9.** The ionic conductivities of FCEs ( $T_t = -50\text{ }^\circ\text{C}$ ) in  $\text{H}_2\text{O}$ - $\text{NaClO}_4$ - $\text{NaCF}_3\text{COO}$  systems.

<b>Electrolytes (<math>\text{NaClO}_4 + \text{NaCF}_3\text{COO}</math>)</b>	<b>Ionic conductivity at <math>25\text{ }^\circ\text{C}</math> (<math>\text{mS cm}^{-1}</math>)</b>	<b>Ionic conductivity at <math>-50\text{ }^\circ\text{C}</math> (<math>\text{mS cm}^{-1}</math>)</b>
3.85 m + 5.92 m	96.9	0.31
2.51 m + 7.49 m	86.7	0.24

**Table S10. The coordination species and numbers within cutoff radius of 4 Å based on AIMD results.**

Liquid structures	Coordination species and numbers (cutoff radius: 4 Å)					
	O <sub>w</sub> -H	O <sub>w</sub> -O <sub>w</sub>	O <sub>w</sub> -Li	O <sub>w</sub> -Cl	O <sub>w</sub> -Na	O <sub>w</sub> -F
H <sub>2</sub> O	19.7	7.4	\	\	\	\
7.18 m LiCl	15.9	6.6	1.16	1.07	\	\
9.07 m NaClO <sub>4</sub>	13.1	5.3	\	0.88	0.58	\
3.85 m NaClO <sub>4</sub> + 5.92 m NaCF <sub>3</sub> COO	12.0	4.7	\	0.19	0.73	0.91

**Table S11. Compared Li-based FCE to reported electrolytes in terms of ionic conductivity, battery operating low-temperature limit (OLTL), energy density at 25 °C, and lifespan.**

<b>Systems</b>	<b>Electrolyte</b>	<b>Ionic Conductivity</b>	<b>OLTL, Energy density, lifespan</b>
LiMn <sub>2</sub> O <sub>4</sub> //PTCDI <b>(This work)</b>	7.18 m LiCl	6.09 mS cm <sup>-1</sup> , – 60 °C	–60 °C, 80 Wh kg <sup>-1</sup> , >2000 cycles
LiMn <sub>2</sub> O <sub>4</sub> //Mo <sub>6</sub> S <sub>8</sub> (Literature) <sup>18</sup>	5 m LiTFSI-CO <sub>2</sub>	~1.5 mS cm <sup>-1</sup> , – 40 °C	–40 °C, ~80 Wh kg <sup>-1</sup> , 2000 cycles
LiMn <sub>2</sub> O <sub>4</sub> //CuSe (Literature) <sup>19</sup>	7.86 m LiCl	5.00 mS cm <sup>-1</sup> , –78 °C,	–78 °C, 109 Wh kg <sup>-1</sup> , 100 cycles
LiMn <sub>2</sub> O <sub>4</sub> //LiTi <sub>5</sub> O <sub>12</sub> (Literature) <sup>20</sup>	H <sub>2</sub> O-DOL- LiTFSI (BSiS-DOL <sub>0.5</sub> )	0.1 mS cm <sup>-1</sup> , – 50 °C,	–50 °C, /, 100 cycles

**Table S12. Compared Na-based FCE to reported electrolytes in terms of other cation, co-solvent, battery operating low-temperature limit (OLTL), energy density at 25 °C, and lifespan.**

<b>Systems</b>	<b>Electrolyte</b>	<b>Other cation or Co-solvent</b>	<b>OLTL, Energy density, lifespan</b>
NaCoHCF//PTCDI <b>(This work)</b>	3.85 m NaClO <sub>4</sub> + 5.92 m NaCF <sub>3</sub> COO	No	−50 °C, 62 Wh kg <sup>−1</sup> , >1000 cycles
Na <sub>3</sub> (VOPO <sub>4</sub> ) <sub>2</sub> F//NaTi <sub>2</sub> (PO <sub>4</sub> ) <sub>3</sub> (Literature) <sup>21</sup>	25 m NaFSI + 10 m NaFTFSI	No	−10 °C, 64 Wh Kg <sup>−1</sup> , 500 cycles
NaCoHCF//AC (Literature) <sup>22</sup>	1 m NaClO <sub>4</sub> + 3.86 m CaCl <sub>2</sub>	Yes (Ca <sup>2+</sup> )	−30 °C, 28 Wh kg <sup>−1</sup> , 1000 cycles
AC//NaTi <sub>2</sub> (PO <sub>4</sub> ) <sub>3</sub> (Literature) <sup>23</sup>	H <sub>2</sub> O <sub>0.7</sub> DMSO <sub>0.3</sub> -2 m NaClO <sub>4</sub>	Yes (DMSO)	−50 °C, 36 Wh kg <sup>−1</sup> , 100 cycles

**Table S13. The anti-freezing electrolyte design using FCE approach when  $T_i$  is set as  $-50\text{ }^\circ\text{C}$  in  $\text{H}_2\text{O}$ -EG- $\text{NaClO}_4$  system.**

<b>Preselected concentration (mass ratio)</b>	<b>FCE concentration (mass ratio)</b>	<b>Prepared electrolyte concentration</b>
H <sub>2</sub> O-EG (60:40)	H <sub>2</sub> O-EG (36:64)	H <sub>36</sub> EG <sub>64</sub> -0.5 m NaClO <sub>4</sub>

**Table S14. The anti-freezing electrolyte design using FCE approach when  $T_i$  is set as  $-20\text{ }^\circ\text{C}$  in  $\text{LiPF}_6$ -EC-DEC system.**

<b>Preselected concentration (mole ratio)</b>	<b>FCE concentration (mole ratio)</b>
$\text{LiPF}_6$ -EC-DEC (1:7.50:4.10)	$\text{LiPF}_6$ -EC-DMC (1:3.23:6.18)

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