

1 **Supporting Information**

2 **Robust and flexible composite aerogel films with porous multilayered structures**
3 **toward broadband electromagnetic wave absorption**

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Supporting Information Corresponding Formulas

17 S1. Electromagnetic parameters measurement

18 The electromagnetic parameters including complex permittivity and complex permeability of the
 19 composite aerogel films were measured within the frequency range of 2-18 GHz. The $RL-f$ curve is
 20 calculated using the measured electromagnetic parameters based on the following equations:

$$21 \quad R(d) = 20 \log \left| \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \right| \quad (\text{Eq. S1})$$

$$22 \quad \frac{Z_{in}}{Z_0} = \sqrt{\frac{\mu_r}{\epsilon_r}} \tanh \left[j \frac{2\pi}{c} d \sqrt{\mu_r \epsilon_r} \right] \quad (\text{Eq. S2})$$

23 where Z_{in} represents the input impedance of the absorber, Z_0 is the impedance of free space, ϵ_r is the
 24 relative complex permittivity, μ_r is the relative complex permeability, f is the frequency, d is the sample
 25 thickness, and c is the speed of light.

26 S2. Debye relaxation

27 Dielectric polarization refers to the phenomenon where bound charges migrate along the direction
 28 of an applied electric field, resulting in electron displacement or alignment of dipoles. In high-
 29 frequency electromagnetic fields, when the motion of electrons or the reorientation of dipoles cannot
 30 keep up with the changes under the alternating electric field, a lagging effect of electron or dipole
 31 polarization relaxation occurs. The Cole-Cole semicircle equation based on the Debye relaxation
 32 theory can effectively contribute to understanding the relaxation processes that occur under the
 33 influence of alternating electromagnetic fields based on the following equations:

$$34 \quad \epsilon = \epsilon_\infty + \frac{\epsilon_s - \epsilon_\infty}{1 + \omega^2 \tau^2} \quad (\text{Eq. S3})$$

35
$$\epsilon'' = \frac{\epsilon_s - \epsilon_\infty}{1 + \omega^2 \tau^2} \omega \tau + \frac{\sigma}{\omega \epsilon_0} \quad (\text{Eq. S4})$$

36 where ϵ_∞ represents the relative dielectric constant at high-frequency limit, ϵ_s denotes the static
 37 dielectric constant, ω refers to the angular frequency, τ is the polarization relaxation time, and σ is the
 38 conductivity. From Eq. S3 and Eq. S4, we can obtain the relationship between ϵ' and ϵ'' :²

39
$$\left(\epsilon' - \frac{\epsilon_s + \epsilon_\infty}{2}\right)^2 + \left(\epsilon'' - \frac{\epsilon_s - \epsilon_\infty}{2}\right)^2 = \left(\frac{\epsilon_s - \epsilon_\infty}{2}\right)^2 \quad (\text{Eq. S5})$$

40 It should be noted that each Cole-Cole semicircle corresponds to a Debye relaxation
 41 process.

42 **S3. Quarter-wavelength resonance formula**

43
$$f_m = \frac{(2N - 1)c}{4t_m n} \quad (\text{Eq. S6})$$

44 where f_m is the resonance peak frequency and t_m is the resonance thickness of the sample. While n is
 45 the real part of square root of the product of complex permittivity and permeability, and N is a positive
 46 integer.

47 **S4. Impedance matching**

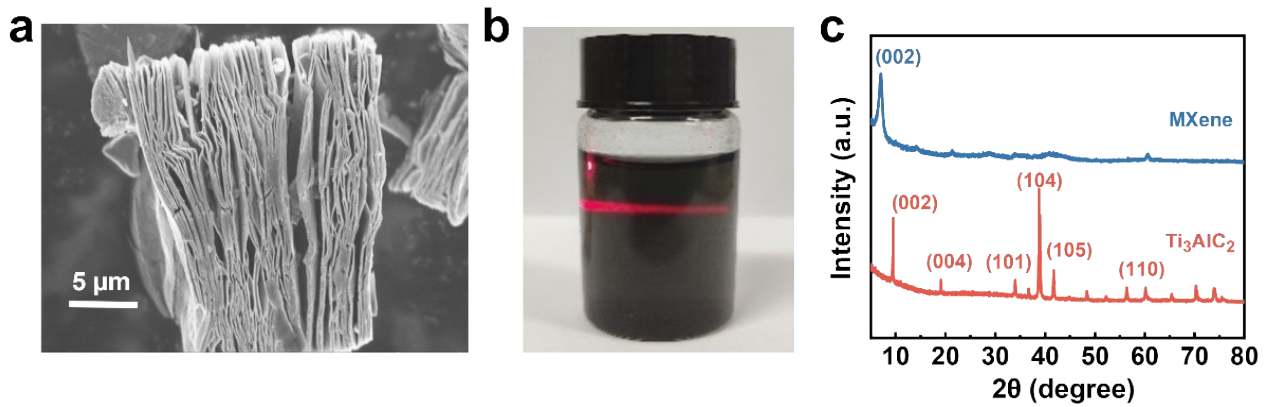
48 The attenuation constant (α), which mainly determines the attenuation capability of
 49 the incident EMWs, can be expressed based on the following equation:

50
$$\alpha = \frac{\sqrt{2}}{c} \pi \sqrt{(\epsilon'' - \mu''^2) + \sqrt{(\epsilon'' - \epsilon\mu'{}^2 + \mu''^2) + \epsilon\mu'{}^2 \mu''^2}} \quad (\text{Eq. S7})$$

51 To achieve high-performance EMW absorption, it is quite important that the incident
 52 EMWs should enter the absorber as much as possible. Therefore, a good impedance
 53 matching at the air-material interface is extremely necessary and critical. According to
 54 Eq. S1 and Eq. S2, the best impedance matching can be obtained when the Z ($|Z_{in}/Z_0|$)
 55 value is close or equal to 1 ($Z_{in} = Z_0$), and the RL will reach its optimal value.³

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Supporting Information Corresponding Figures and Table

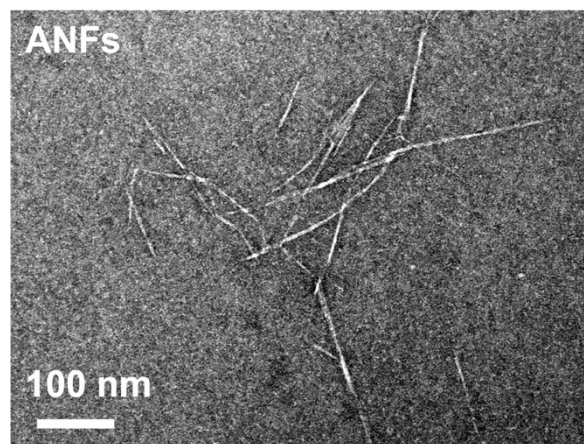


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58 **Fig. S1.** (a) SEM image of the multilayered $\text{Ti}_3\text{C}_2\text{T}_x$. (b) Digital imaging of the Tyndall effect produced

59 by $\text{Ti}_3\text{C}_2\text{T}_x$ suspensions. (c) XRD patterns of MAX phase and $\text{Ti}_3\text{C}_2\text{T}_x$.

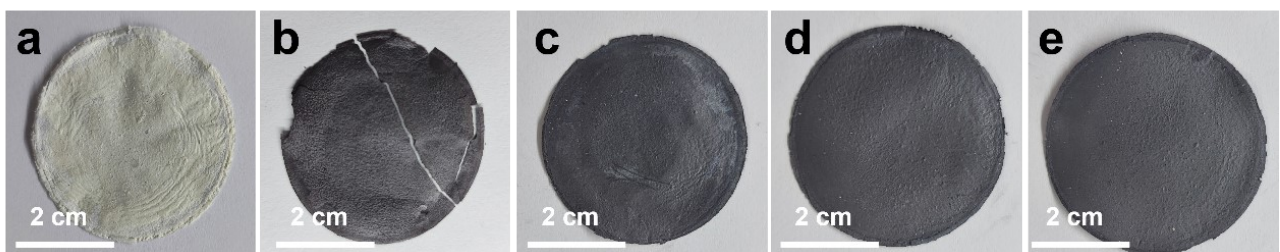
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62 **Fig. S2.** TEM image of ANFs.

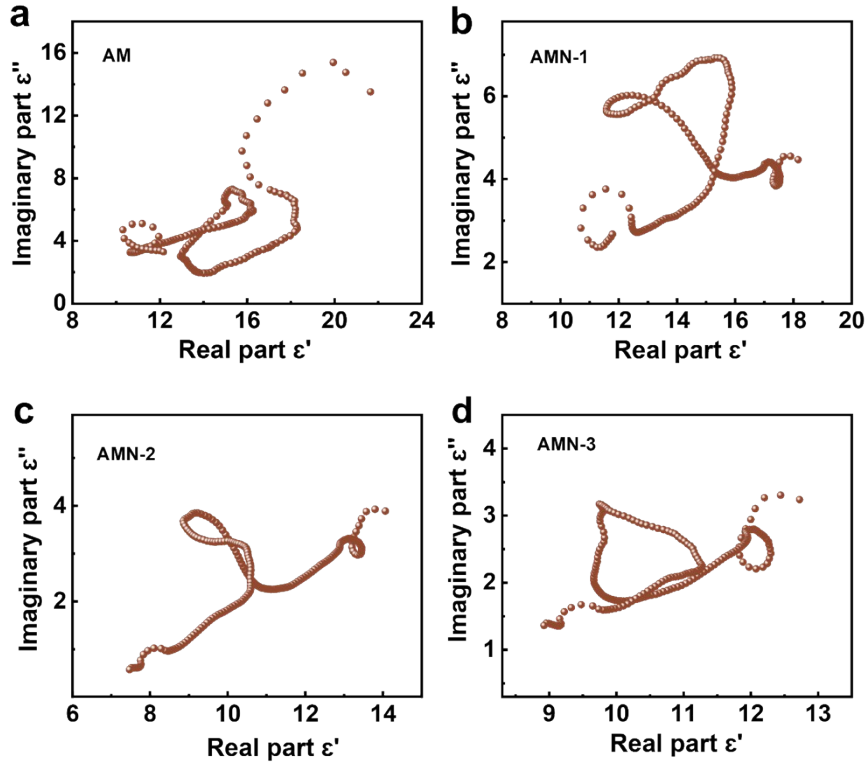
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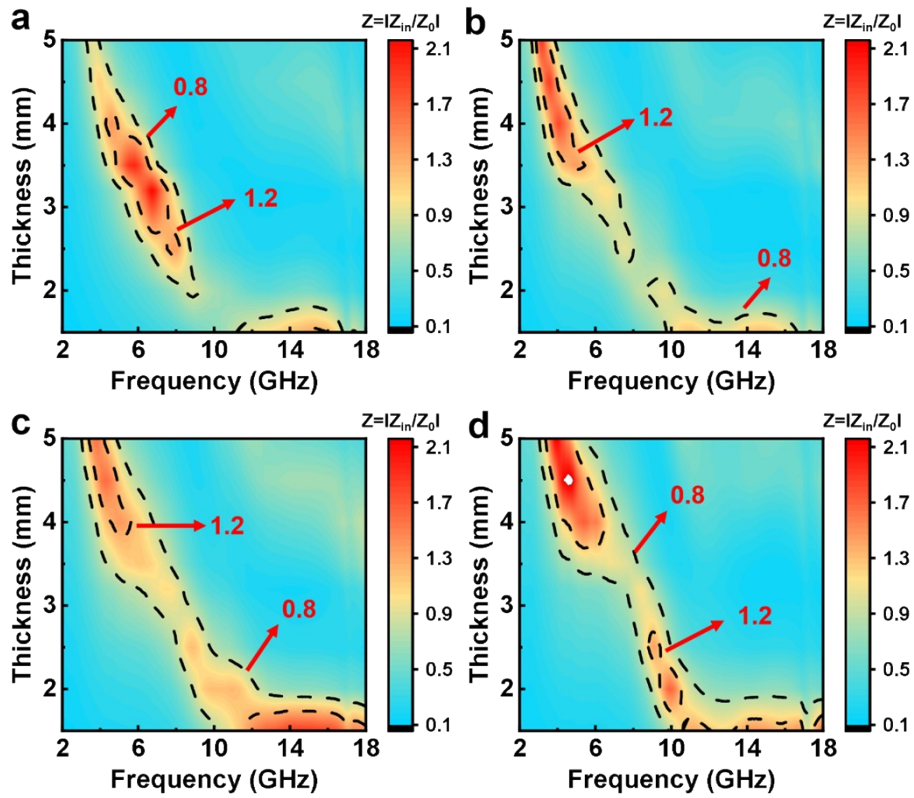
65 **Fig. S3.** Digital images of the (a) pure ANF film, (b) pure MXene film, (c) AM, (d) AMN-1, and (e)

66 AMN-3.



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 68 **Fig. S4.** Cole-Cole curves of (a) AM, (b) AMN-1, (c) AMN-2, and (d) AMN-3.

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 71 **Fig. S5.** The values of $Z = |Z_{in}/Z_0|$ of (a) AM, (b) AMN-1, (c) AMN-2, and (d) AMN-3.

72 **Table S1.** Comparison of EMW absorption properties of the AMN aerogel film with other related
 73 MXene-based composites.

Samples	<i>RL</i> (dB)	<i>EAB</i> (GHz)	Matching thickness (mm)	Ref.
Fe ₃ O ₄ @Ti ₃ C ₂ T _x	-57.2	1.4	4.2	4
MXene/Ni	-49.9	2.1	1.75	5
MXene/Ni	-31.9	2.3	1.0	6
MXene-CoC	-46.48	3.0	1.02	7
Ti ₃ C ₂ T _x /Fe ₃ O ₄	-50.18	3.2	1.3	8
Ni@MXene	-52.6	3.7	3.0	9
MXene-CNTs/Ni	-56.4	3.95	2.4	10
Co/ZnO@CNTs/Ti ₃ C ₂ T _x	-46.0	4.0	1.9	11
MXene/RGO	-44.3	4.84	1.5	12
MXene-rGO/CoNi	-54.1	4.9	2.01	13
MXene/Ni	-50.5	5.28	3.5	14
MXene/RGO	-31.2	5.4	2.05	15
ANF/MXene/Ni	-48.6	5.8	1.5	This work

75 References

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