

## Supplementary Information

Quantitative profiling of lipid mediators in sperm cells through on-line dilution on-line polymer matrix based solid phase extraction liquid chromatography with mass spectrometry detection

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### LC-methods

#### Method 1

Time [min]	Pump 1 (LPG/SPE)			Pump 2 (SPE)		Pump 3 + 4 (binary gradient / analytical)			Trap-Valve
	A [%]	B [%]	C [%]	Flow [mL/min]	0.1 % HCOOH Flow [mL/min]	A [%]	B [%]	Flow [mL/min]	Position
	0.1 % HCOOH	MeOH	Isopro- panol / HCOOH (100/0.2)			MeCN / Water / HCOOH (10/90/0.1)	MeCN / Water (95/5)		
0	60	40	0	0.5	2	90	10	0.4	Trap-load
1.9					2				
2	60	40	0	0.5	0.001	90	10		Trap-inject
2.1									
2.15				0.5					
3	10	45	45	0.3					
5									
11				0.3		50	50	0.4	Trap-load
12				1					
15						0	100	0.4	
16	10	45	45	1					
16.1	60	40	0	0.5					
17						0	100	0.4	
18					0.001	90	10	0.4	
18.5					2				
24	60	40	0	0.5		90	10	0.4	

Table I: Method 1 was used for the determination of the following analytes: 19(*R*)-Hydroxy-prostaglandin E<sub>1</sub> (19(*R*)-HO-PGE<sub>1</sub>), 19(*R*)-Hydroxy-prostaglandin E<sub>2</sub> (19(*R*)-HO-PGE<sub>2</sub>), Prostaglandin E<sub>1</sub> (PGE<sub>1</sub>), Prostaglandin E<sub>2</sub> (PGE<sub>2</sub>), Prostaglandin D<sub>2</sub> (PGD<sub>2</sub>), Prostaglandin F<sub>2α</sub> (PGF<sub>2α</sub>), Thromboxane B<sub>2</sub> (TXB<sub>2</sub>)

## Method 2

Time [min]	Pump 1 (LPG/SPE)			Pump 2 (SPE)		Pump 3 + 4 (binary gradient / analytical)			Trap-Valve
	A [%]	B [%]	C [%]	Flow [mL/min]	0.1 % HCOOH Flow [mL/min]	A [%]	B [%]	Flow [mL/min]	Position
	0.1 % HCOOH	MeOH	Isopro- panol / HCOOH (100/0.2)			MeCN / Water / HCOOH (10/90/0.1)	MeCN / Water (95/5)		
0	40	60	0	0.5	2	50	50	0.4	Trap-load
1.9					2				
2	40	60	0	0.5	0.001	50	50		
2.1									Trap-inject
2.15				0.5					
3	10	45	45	0.3					
9				0.3		0	100	0.4	
10				1					Trap-load
11						0	100	0.4	
13	10	45	45	1					
13.1	40	60	0	1					
14					0.001	50	50	0.4	
14.5				1	2				
15				0.5					
20	40	60	0	0.5		50	50	0.4	

Table II: Method 2 was used for the determination of the following analytes: 15-Hydroxyeicosatetraenoic acid (15(S)-HETE), Arachidonic acid-d<sub>11</sub> (AA-d<sub>11</sub>), Arachidonylethanolamide (AA-EA), 2-Arachidonoylglycerol (2-AG), 2-Arachidonoylglycerol-d<sub>5</sub> (2-AG-d<sub>5</sub>)

## ISTD-Solution

Substanz	Mass [μg]
PGE <sub>1</sub> -d <sub>4</sub>	2
PGE <sub>2</sub> -d <sub>9</sub>	2
PGD <sub>2</sub> -d <sub>4</sub>	2
PGF <sub>2α</sub> -d <sub>4</sub>	2
2-AG-d <sub>8</sub>	4
AA-d <sub>8</sub>	4
AA-EA-d <sub>8</sub>	4
15(S)-HETE-d <sub>8</sub>	4
TXB <sub>2</sub> -d <sub>4</sub>	2

Table III: ISTD-Analytes in 500 mL MeCN:MeOH (50/50, v/v)

# Investigations into the properties of the TurboFlow Cyclone™ SPE column

## Elution behaviour of the eicosanoids on the SPE column

To investigate the elution behaviour of the analytes on the trap column, mobile phase A (acetonitrile / ultrapure water / formic acid (10/90/0.1, v/v/v)) and mobile phase B (acetonitrile / ultrapure water (95/5, v/v)) were mixed in the respective compositions between 10 % and 90 % B. The test solution of the analytes was prepared in 400  $\mu\text{L}$  HTF buffer with 1200  $\mu\text{L}$  ISTD solution at a concentration of 1.25  $\mu\text{g}/\text{mL}$ . In each case, 10  $\mu\text{L}$  of this calibration standard was injected. The LC-MS system shown in Figure 1 was used for the investigations.

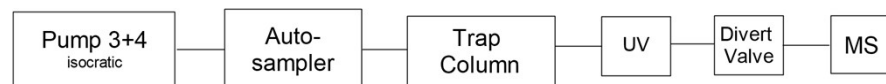


Figure 1: LC-MS system for investigating the elution behaviour of analytes on the SPE column

Figure 2 shows that 19-(*R*)-HO-PGE<sub>2</sub> is eluted quickly and entirely at a mobile phase B concentration of 20%. To maintain an adequate stacking effect on the analytical column, the mobile phase composition was set to 90% A and 10% B as the starting point for the analytical gradient. To ensure that all prostaglandins are completely backflushed from the solid-phase extraction (SPE) column to the analytical column, a backflush time of 9 minutes was selected.

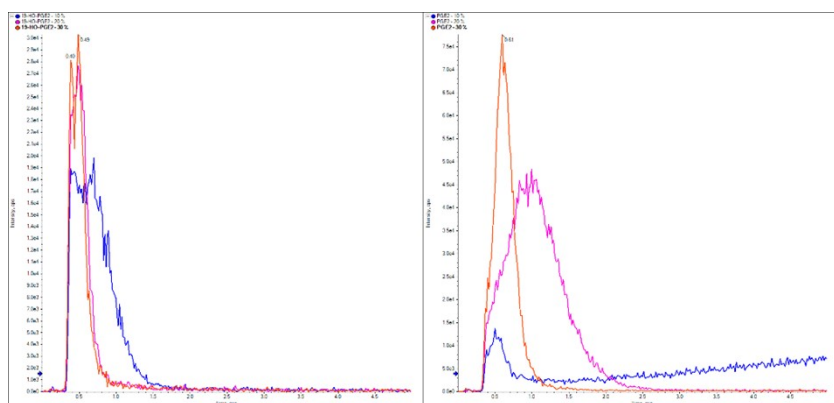


Figure 2: The elution profile of the analytes 19-(*R*)-HO-PGE<sub>2</sub> and PGE<sub>2</sub> on a TurboFlow™ Cyclone column during isocratic elution with 10% (orange), 20% (pink) and 30% (blue) mobile phase B

Figure 3 shows the elution behaviour for the representative analytes 15-HETE and 2-AG. From this, a composition of the mobile phase of the analytical gradient of 50% B can be derived. Due to the increasing proportion of B in backflush mode, all analytes are completely flushed onto the analytical column.

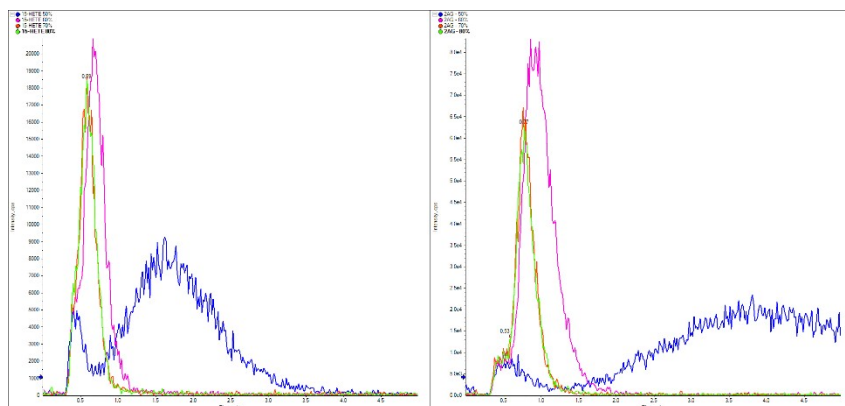


Figure 3: The elution profile of the analytes 15-HETE and 2-AG on a TurboFlow™ Cyclone column during isocratic elution with 50% (blue), 60% (pink), 70% (orange) and 80% (green) mobile phase B.

## Investigation of the retention and recovery behaviour of representative analytes on the SPE column

The chromatographic LC-MS system shown in Figure 4 was used to investigate the retention and recovery behaviour of representative analytes as a function of the composition of the mobile phase of loading pump 2 on the TurboFlow Cyclone™ trap column. The methods were adapted so that the methanol content of the mobile phase of loading pump 1 varied between 20% and 80%. The remaining chromatographic conditions were kept the same in accordance with standard methods 1 and 2. No internal standard was used.

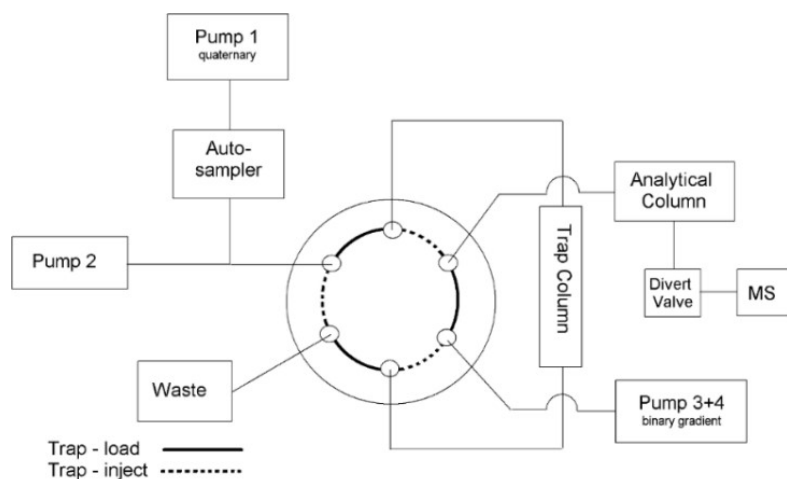


Figure 4: Chromatographic LC-MS system for investigations of retention and recovery behaviour

Figure 5 shows the results for the representative prostaglandins 19-(*R*)-HO-PGE<sub>2</sub> and PGE<sub>2</sub>, and Figure 6 shows the results for 15-HETE, 2-AG and AA-D<sub>11</sub>.

As theoretically expected, the technical recovery increases slightly with decreasing methanol content in the mobile phase. However, since a higher carry-over effect was observed with more lipophilic analytes as the methanol content decreased, a methanol content of 40% was found to be most suitable for the prostaglandins (method 1) and 60% for the other analytes (method 2) proved to be the most suitable.

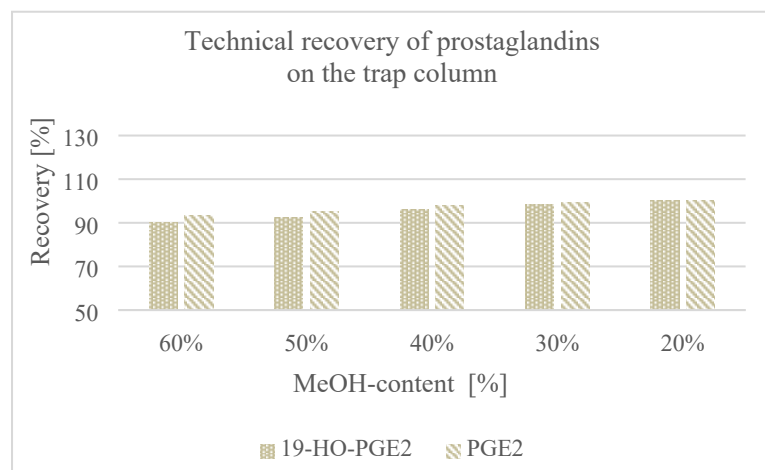


Figure 5: The technical recovery of 19-(*R*)-HO-PGE<sub>2</sub> and PGE<sub>2</sub> on the trap column as a function of the methanol content of the mobile phase of pump 1 is shown. The recovery of the representative prostaglandins increases slightly as the methanol content in the mobile phase of loading pump 1 decreases. The area of the 20% methanol content was set as relative 100% recovery.

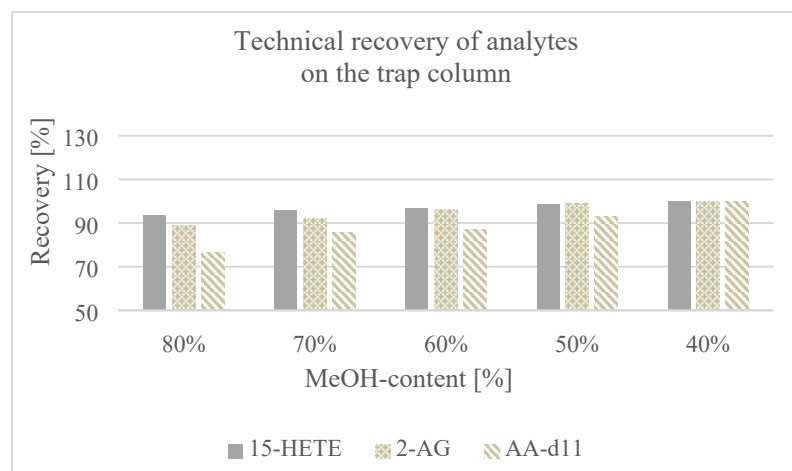


Figure 6: The technical recovery of 15-HETE, 2-AG and AA-d<sub>11</sub> on the trap column as a function of the methanol content of the mobile phase of pump 1 is shown. The recovery of the representative analytes increases slightly as the methanol content in the mobile phase of loading pump 1 decreases. The area of the 20% methanol content was set as relative 100% recovery.

#### Investigation of the injection linearity of the trap column

An analyte solution of 19-(*R*)-HO-PGE<sub>2</sub>, PGE<sub>2</sub>, 15-HETE, 2-AG and AA-d<sub>11</sub> with a concentration of 12.5 ng/mL (ULOQ) was prepared in 400  $\mu$ l HTF buffer and 1200  $\mu$ l MeCN:MeOH (50:50, v/v). Volumes of 50, 100, 150 and 200  $\mu$ l of the analyte solution were injected and analysed using methods 1 and 2. The results were evaluated based on the area.

The result showed an approximately linear relationship with a respective  $r^2$  value of 0.997 to 0.999. Only the residue distribution indicates a slight deviation from linearity. The precision was very high at the same injection volume.

## Accuracy and precision

To determine accuracy and precision, quality control samples were prepared by spiking sperm matrix at four concentration levels (n=5 each) in three different batches that covered the entire calibration range: 0.02 ng (2 x LLOQ- QC), 0.05 ng (low QC), 2 ng (medium QC), 5 ng (high QC).

The within-run accuracy was calculated as the percentage mean of the 5 QC samples of the respective concentration level. The between-run accuracy was calculated as the percentage mean of all 15 QC samples of the respective concentration level of three different batches.

The within-run and between-run precision of the QC-samples is expressed as percent coefficient of variance (CV %).

Analyte / ISTD	pg/10 <sup>6</sup> sperm cells	With-in run				Between-run	
		batch		(n=5 each)	batch		(n=15)
		1	2	3	1-3		
19(R)-HO-PGE <sub>1</sub> / -	20	Mean [%]	158.2	51.2	70.0	MW [%]	100.3
		CV [%]	13.2	21.5	74.2	CV [%]	58.2
	50	Mean [%]	132.9	69.8	91.7	MW [%]	100.3
		CV [%]	11.1	29.0	16.4	CV [%]	31.6
	2000	Mean [%]	102.3	97.0	103.2	MW [%]	100.9
		CV [%]	0.8	4.4	2.9	CV [%]	3.8
	5000	Mean [%]	94.6	99.8	102.3	MW [%]	98.4
		CV [%]	1.4	4.7	1.6	CV [%]	4.4
19(R)-HO-PGE <sub>2</sub> / PGE <sub>2</sub> -d <sub>9</sub>	20	Mean [%]	113.4	96.1	95.6	MW [%]	102.4
		CV [%]	1.5	2.9	8.6	CV [%]	9.7
	50	Mean [%]	108.7	97.5	103.3	MW [%]	103.5
		CV [%]	1.4	1.1	3.5	CV [%]	5.1
	2000	Mean [%]	102.0	93.9	91.7	MW [%]	96.3
		CV [%]	0.8	1.4	4.3	CV [%]	5.4
	5000	Mean [%]	96.5	93.9	94.0	MW [%]	95.0
		CV [%]	1.3	2.5	3.8	CV [%]	2.7
PGD <sub>2</sub> / PGD <sub>2</sub> -d <sub>4</sub>	20	Mean [%]	104.4	98.2	100.0	MW [%]	101.1
		CV [%]	1.3	2.5	2.2	CV [%]	3.3
	50	Mean [%]	103.0	100.6	103.7	MW [%]	102.5
		CV [%]	1.8	1.6	1.9	CV [%]	2.1
	2000	Mean [%]	99.3	95.3	99.7	MW [%]	98.2
		CV [%]	1.0	2.7	1.0	CV [%]	2.6
	5000	Mean [%]	90.0	91.4	94.6	MW [%]	91.7
		CV [%]	1.7	2.1	3.2	CV [%]	3.0

Analyte / ISTD	pg/10 <sup>6</sup> sperm cells	With-in run			Between-run		
		batch	(n=5 each)		batch	(n=15)	
		1	2	3	1-3		
PGE <sub>1</sub> / PGE <sub>1</sub> -d <sub>4</sub>	20	Mean [%]	103.1	94.5	95.3	MW [%]	98.0
		CV [%]	3.9	7.0	5.5	CV [%]	6.4
	50	Mean [%]	103.8	95.7	99.6	MW [%]	99.9
		CV [%]	1.5	2.8	3.1	CV [%]	4.2
	2000	Mean [%]	101.9	93.3	99.3	MW [%]	98.4
		CV [%]	1.5	1.7	2.0	CV [%]	4.1
	5000	Mean [%]	97.3	95.2	95.5	MW [%]	96.1
		CV [%]	1.0	2.1	3.8	CV [%]	2.4
PGE <sub>2</sub> / PGE <sub>2</sub> -d <sub>9</sub>	20	Mean [%]	106.0	97.6	97.9	MW [%]	100.9
		CV [%]	3.5	1.6	1.4	CV [%]	4.7
	50	Mean [%]	104.3	98.2	102.7	MW [%]	101.9
		CV [%]	1.0	1.2	2.3	CV [%]	3.0
	2000	Mean [%]	102.7	94.6	99.0	MW [%]	99.0
		CV [%]	1.7	2.8	2.4	CV [%]	4.1
	5000	Mean [%]	97.1	94.6	95.9	MW [%]	96.0
		CV [%]	1.2	1.9	1.6	CV [%]	1.9
PGF <sub>2</sub> α / PGF <sub>2</sub> α-d <sub>4</sub>	20	Mean [%]	105.2	97.7	93.9	MW [%]	99.3
		CV [%]	2.9	4.2	3.2	CV [%]	5.9
	50	Mean [%]	102.3	96.3	98.0	MW [%]	99.1
		CV [%]	3.8	2.9	2.5	CV [%]	4.0
	2000	Mean [%]	101.9	93.2	96.3	MW [%]	97.4
		CV [%]	1.2	1.9	0.9	CV [%]	4.1
	5000	Mean [%]	97.7	94.8	94.1	MW [%]	95.8
		CV [%]	0.7	1.2	2.0	CV [%]	2.1
TXB <sub>2</sub> / TXB <sub>2</sub> -d <sub>4</sub>	20	Mean [%]	116.7	100.6	101.5	MW [%]	106.9
		CV [%]	0.8	2.3	1.3	CV [%]	7.4
	50	Mean [%]	108.2	100.4	99.9	MW [%]	103.2
		CV [%]	1.6	1.8	10.8	CV [%]	6.8
	2000	Mean [%]	99.6	94.9	100.1	MW [%]	98.3
		CV [%]	0.3	1.3	0.6	CV [%]	2.5
	5000	Mean [%]	95.4	96.1	95.8	MW [%]	95.7
		CV [%]	0.4	0.6	6.2	CV [%]	3.2

Analyte / ISTD	pg/10 <sup>6</sup> sperm cells	With-in run				Between-run	
		batch		(n=5 each)	batch		(n=15)
		1	2	3	1-3		
15-HETE / 15-HETE-d <sub>4</sub>	20	Mean [%]	110.1	95.0	99.6	MW [%]	101.6
		CV [%]	1.2	1.2	3.0	CV [%]	6.7
	50	Mean [%]	106.7	95.2	95.5	MW [%]	99.1
		CV [%]	1.8	1.4	1.3	CV [%]	5.7
	2000	Mean [%]	104.5	95.1	96.9	MW [%]	98.8
		CV [%]	0.7	0.7	0.3	CV [%]	4.3
	5000	Mean [%]	103.6	100.9	101.8	MW [%]	102.1
		CV [%]	0.6	0.5	0.6	CV [%]	1.3
AA-EA / AA-EA-d <sub>8</sub>	20	Mean [%]	99.8	98.5	101.0	MW [%]	99.8
		CV [%]	4.4	5.3	5.5	CV [%]	4.9
	50	Mean [%]	101.1	97.2	98.1	MW [%]	98.8
		CV [%]	3.9	2.8	6.8	CV [%]	4.8
	2000	Mean [%]	101.1	93.6	98.5	MW [%]	97.8
		CV [%]	2.2	1.0	1.3	CV [%]	3.6
	5000	Mean [%]	98.8	97.3	101.6	MW [%]	99.2
		CV [%]	1.7	2.4	1.2	CV [%]	2.5
2-AG / 2-AG-d <sub>8</sub>	20	Mean [%]	108.2	90.6	95.1	MW [%]	98.0
		CV [%]	2.4	6.5	4.8	CV [%]	8.9
	50	Mean [%]	104.0	96.8	101.5	MW [%]	100.8
		CV [%]	2.6	2.6	2.2	CV [%]	3.8
	2000	Mean [%]	97.9	94.0	105.9	MW [%]	99.3
		CV [%]	1.6	1.3	0.6	CV [%]	5.2
	5000	Mean [%]	97.9	98.6	110.9	MW [%]	102.5
		CV [%]	1.3	0.5	1.0	CV [%]	6.1
2-AG-d <sub>5</sub> / 2-AG-d <sub>8</sub>	20	Mean [%]	110.6	90.9	95.1	MW [%]	98.9
		CV [%]	2.7	6.6	3.7	CV [%]	9.7
	50	Mean [%]	104.5	94.2	100.7	MW [%]	99.8
		CV [%]	2.9	1.7	1.8	CV [%]	5.0
	2000	Mean [%]	98.7	91.6	103.4	MW [%]	97.5
		CV [%]	1.3	1.3	0.7	CV [%]	5.2
	5000	Mean [%]	98.4	95.8	109.3	MW [%]	101.2
		CV [%]	1.1	0.6	0.4	CV [%]	6.0



Analyte / ISTD	pg/10 <sup>6</sup> sperm cells	With-in run			Between-run		
		batch	(n=5 each)		batch	(n=15)	
		1	2	3	1-3		
AA-d <sub>11</sub> / AA-d <sub>8</sub>	20	Mean [%]	115.5	102.7	118.1	MW [%]	112.1
		CV [%]	5.4	11.4	11.7	CV [%]	11.1
	50	Mean [%]	106.6	110.2	111.1	MW [%]	109.3
		CV [%]	5.9	8.2	4.1	CV [%]	6.2
	2000	Mean [%]	101.2	95.7	98.0	MW [%]	98.3
		CV [%]	0.6	1.4	1.0	CV [%]	2.5
	5000	Mean [%]	99.7	100.7	101.5	MW [%]	100.6
		CV [%]	1.1	0.8	1.2	CV [%]	1.3

Table IV

## Linearity

Standard curves were prepared for all analytes with 9 calibration points ranging from 0.01 to 5 ng /  $1 \times 10^6$  sperm. For PGD<sub>2</sub>, the calibration range was only covered up to 2 ng /  $1 \times 10^6$  sperm. A 1 / x weighted linear regression analysis of the area ratios (peak area analyte/peak area of the internal deuterated standard) was performed. The calibration for 19(R)-Hydroxy-PGE<sub>1</sub> was performed without considering of an ISTD. The lower limit of quantification (LLOQ) was set at the lowest concentration of the calibration standards. The signal-to-noise ratio of the matrix standards at the LLOQ gives a hint of a detection limit.

Analyte/ISTD		Matrix matched-STD	Matrix-STD	Lösemittel-STD	S/N at LLOQ Matrix-STD
19(R)-HO-PGE <sub>1</sub> / -	Calibration curve	$y = 507.782 x + 192250$ $r = 0.99986$	$y = 496.59 x + 195803$ $r = 0.9996$	$y = 342.76 x + 12940$ $r = 0.9984$	228
19(R)-HO-PGE <sub>2</sub> / PGE <sub>2</sub> -d <sub>9</sub>	Calibration curve	$y = 0.00102 x + 0.02306$ $r = 0.99970$	$y = 0.00103 x + 0.02157$ $r = 0.99990$	$y = 0.000644 x + 0.000897$ $r = 0.9999$	600
PGD <sub>2</sub> / PGD <sub>2</sub> -d <sub>4</sub>	Calibration curve	$y = 0.00189 x + 0.00616$ $r = 0.99981$	$y = 0.00191 x + 0.00202$ $r = 0.9999$	$y = 0.00183 x + 0.00405$ $r = 0.9996$	32
PGE <sub>1</sub> / PGE <sub>1</sub> -d <sub>4</sub>	Calibration curve	$y = 0.00160 x + 0.01193$ $r = 0.9997$	$y = 0.00163 x + 0.00978$ $r = 0.9997$	$y = 0.00162 x + 0.00355$ $r = 0.9994$	74
PGE <sub>2</sub> / PGE <sub>2</sub> -d <sub>9</sub>	Calibration curve	$y = 0.00165 x + 0.01439$ $r = 0.9995$	$y = 0.00167 x + 0.01134$ $r = 0.9998$	$y = 0.00172 x + 0.00249$ $r = 0.9997$	65
PGF <sub>2α</sub> / PGF <sub>2α</sub> -d <sub>4</sub>	Calibration curve	$y = 0.00129 x + 0.00202$ $r = 0.9998$	$y = 0.00131 x + 0.000586$ $r = 0.9999$	$y = 0.00135 x + 0.000421$ $r = 0.9990$	49
TXB <sub>2</sub> -/ TXB <sub>2</sub> -d <sub>4</sub>	Calibration curve	$y = 0.00152 x + 0.00321$ $r = 0.99986$	$y = 0.00157 x + 0.0009798$ $r = 0.9990$	$y = 0.00158 x + 0.00222$ $r = 0.9989$	250
15-HETE/ 15-HETE-d <sub>4</sub>	Calibration curve	$y = 0.00094596 x + 0.00605$ $r = 0.9999$	$y = 0.0009573 x + 0.00421$ $r = 0.9991$	$y = 0.000971692 x + 0.00151$ $r = 0.9987$	250
AA-EA/ AA-EA-d <sub>8</sub>	Calibration curve	$y = 0.00101 x + 0.00637$ $r = 0.99959$	$y = 0.00103 x + 0.00505$ $r = 0.9994$	$y = 0.00106 x + 0.00481$ $r = 0.9990$	57
2-AG/ 2-AG-d <sub>8</sub>	Calibration curve	$y = 0.00845 x + 0.07496$ $r = 0.9997$	$y = 0.00886 x + 0.03984$ $r = 0.9996$	$y = 0.00856 x + 0.02363$ $r = 0.9988$	97
2-AG-d <sub>5</sub> / 2-AG-d <sub>8</sub>	Calibration curve	$y = 0.00449 x + 0.01594$ $r = 0.9999$	$y = 0.00464 x + 0.00562$ $r = 0.99953$	$y = 0.00460 x + 0.01247$ $r = 0.9989$	125
AA-d <sub>11</sub> / AA-d <sub>8</sub>	Calibration curve	$y = 0.0001656 x + 0.0006362$ $r = 0.9999$	$y = 0.0001682 x - 0.00003338$ $r = 0.9993$	$y = 0.00017186 x + 0.0002886$ $r = 0.9993$	28

Table V

## Individual MRM transitions with their measurement parameters

ID	Q 1 Mass	Q3 Mass	RT-method 1	RT-method 2	Polarity	DP (volts)	EP (volts)	CE (volts)	CXP (volts)
19-HO-PGE <sub>2</sub>	367.11	331.20	5.60		neg.	-65.00	-10.00	-20.00	-17.00
19-HO-PGE <sub>2</sub>	367.11	287.20	5.60		neg.	-65.00	-10.00	-26.00	-15.00
19-HO-PGE <sub>1</sub>	369.08	333.10	6.00		neg.	-60.00	-10.00	-22.00	-19.00
19-HO-PGE <sub>1</sub>	369.08	235.00	6.00		neg.	-60.00	-10.00	-24.00	-13.00
TXB <sub>2</sub>	369.14	195.10	8.90		neg.	-40.00	-10.00	-18.00	-11.00
TXB <sub>2</sub>	369.14	169.00	8.90		neg.	-40.00	-10.00	-22.00	-15.00
TXB <sub>2</sub> -d <sub>4</sub>	373.12	173.10	8.90		neg.	-50.00	-10.00	-24.00	-9.00
PGF <sub>2α</sub>	353.13	309.10	8.90		neg.	-65.00	-10.00	-26.00	-12.00
PGF <sub>2α</sub>	353.13	193.00	8.90		neg.	-65.00	-10.00	-34.00	-12.00
PGF <sub>2α</sub> -d <sub>4</sub>	357.12	313.30	8.90		neg.	-65.00	-10.00	-26.00	-15.00
PGE <sub>2</sub>	351.12	271.10	9.20		neg.	-35.00	-10.00	-22.00	-19.00
PGE <sub>2</sub>	351.12	315.00	9.20		neg.	-35.00	-10.00	-16.00	-17.00
PGE <sub>2</sub> -d <sub>9</sub>	360.18	280.20	9.20		neg.	-65.00	-10.00	-24.00	-15.00
PGE <sub>1</sub>	353.14	235.00	9.40		neg.	-55.00	-10.00	-20.00	-25.00
PGE <sub>1</sub>	353.14	317.00	9.40		neg.	-55.00	-10.00	-20.00	-17.00
PGE <sub>1</sub> -d <sub>4</sub>	357.15	239.10	9.40		neg.	-40.00	-10.00	-22.00	-11.00
PGD <sub>2</sub>	351.12	271.20	9.60		neg.	-30.00	-10.00	-24.00	-23.00
PGD <sub>2</sub>	351.12	315.20	9.60		neg.	-30.00	-10.00	-16.00	-15.00
PGD <sub>2</sub> -d <sub>4</sub>	355.10	275.10	9.60		neg.	-40.00	-10.00	-24.00	-15.00
15-HETE	319.12	219.00	14.10	6.30	neg.	-15.00	-10.00	-18.00	-17.00
15-HETE	319.12	257.30	14.10	6.30	neg.	-15.00	-10.00	-20.00	-13.00
15-HETE-d <sub>8</sub>	327.18	226.10	14.10	6.30	neg.	-35.00	-10.00	-18.00	-9.00
AA-EA	348.28	287.30	15.00	7.50	pos.	46.00	10.00	15.00	20.00
AA-EA	348.28	203.20	15.00	7.50	pos.	46.00	10.00	19.00	12.00
AA-EA-d <sub>8</sub>	356.20	294.10	15.00	7.50	pos.	86.00	10.00	27.00	34.00
2-AG	379.25	287.30	15.43	8.10	pos.	50.00	10.00	19.00	20.00
2-AG	379.25	269.30	15.43	8.10	pos.	50.00	10.00	21.00	16.00
2-AG-d <sub>5</sub>	384.35	287.30	15.40	8.10	pos.	71.00	10.00	21.00	18.00
2-AG-d <sub>5</sub>	384.35	269.40	15.40	8.10	pos.	71.00	10.00	23.00	18.00
2-AG d <sub>8</sub>	387.03	294.10	15.43	8.10	pos.	36.00	10.00	17.00	18.00
AA	303.10	259.20	16.00	9.10	neg.	-70.00	-10.00	-18.00	-13.00
AA	303.10	205.00	16.00	9.10	neg.	-70.00	-10.00	-20.00	-9.00
AA-d <sub>11</sub>	314.19	270.30	16.00	9.10	neg.	-30.00	-10.00	-18.00	-15.00
AA-d <sub>11</sub>	314.19	216.20	16.00	9.10	neg.	-30.00	-10.00	-20.00	-13.00
AA-d <sub>8</sub>	311.17	267.30	16.00	9.10	neg.	-40.00	-10.00	-18.00	-13.00

Table VI