

Supplementary Information for:

Surfactant Control of Interfacial Reaction Rates in Aqueous Microdroplets

Alexander M. Prophet,¹ David T. Limmer,^{1,2,3,4} & Kevin R. Wilson^{1*}

¹*Chemical Sciences Division, Lawrence Berkeley National Laboratory, Berkeley, CA 94720*

²*Department of Chemistry, University of California, Berkeley, CA 94720*

³*Materials Science Division, Lawrence Berkeley National Laboratory, Berkeley, California 94720*

⁴*Kavli Energy NanoScience Institute, Berkeley, California 94720*

*Correspondence to krwilson@lbl.gov

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SI-1: Experimental

Here we provide additional information about the experimental setup and reaction conditions. Fig. S1 provides a brief schematic of the experimental apparatus, indicating the major components of the electrodynamic balance and open-port sampling interface (OPSI). An example mass spectrum is provided in Fig. S2 showing the strong signal intensity at $m/z = 126.9$ resulting from the iodide ion. The citric acid (CA) buffer can also be observed both before and after the reaction.

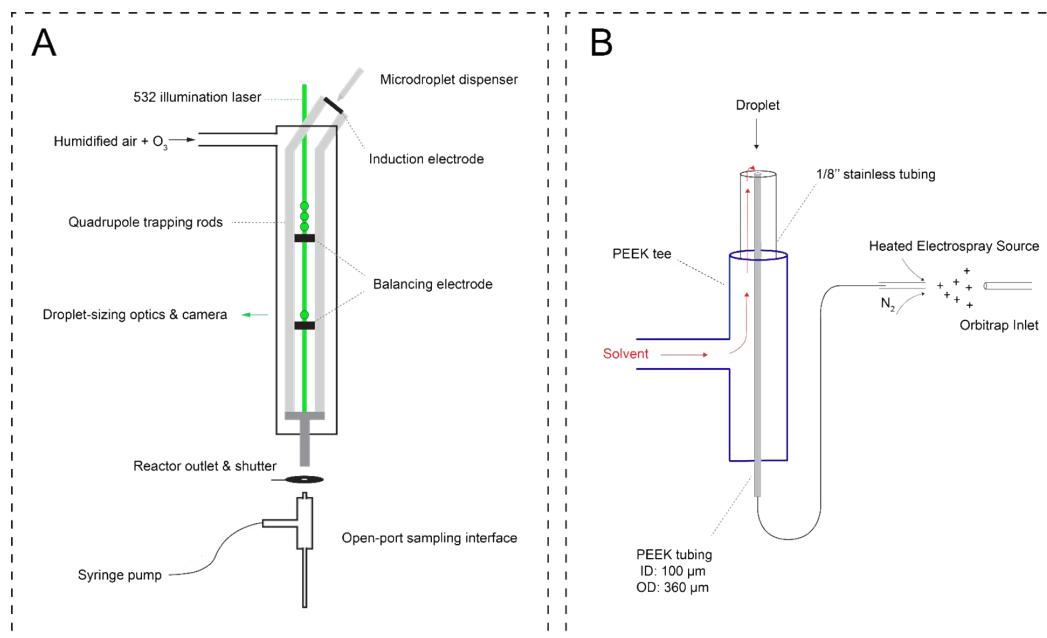


Fig. S1: Experimental diagram for (A) quadrupole electrodynamic trap (QET) with major components labeled and (B) open-port sampling interface (OPSI) for electrospray ionization mass spectrometry (ESI-MS).

An example of the Mie scattering phase function used to quantify the droplet radii for each experiment is shown in Fig. S3. The angular spacing between peaks in the interference pattern is used to identify the radius of a given microdroplet by referencing a library of simulated peak positions and spacings. The details of this approach and the algorithm employed can be found in previous work¹ and by Davies and co-workers.^{2,3}

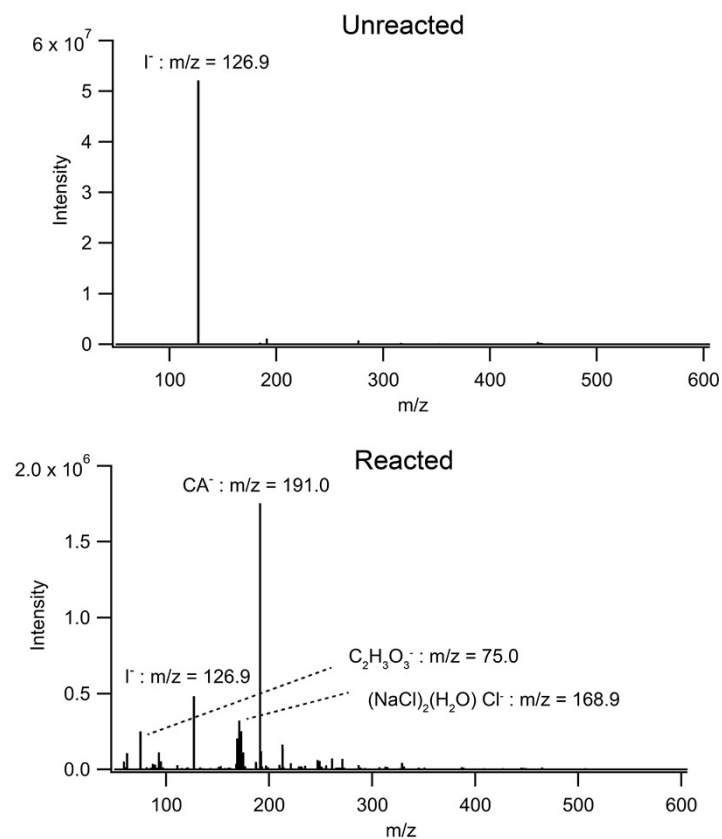


Fig. S2: Mass spectra for unreacted and reacted microdroplets containing NaI, NaCl, citric acid buffer at pH 3 with 32 μM of Triton X-100. The only noticeable change in the spectra is loss of I^- due to oxidation by O_3 and a more visible background.

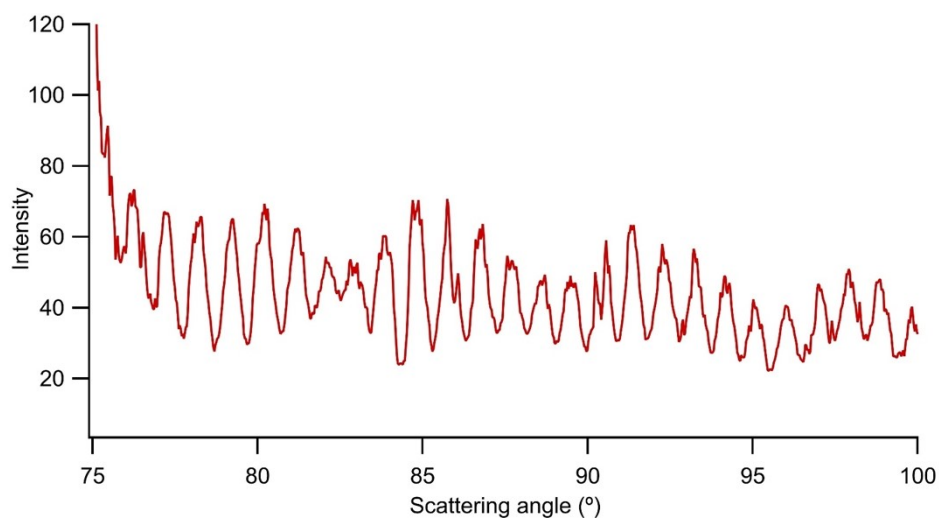


Fig. S3: Scattering intensity vs. collection angle for Mie scattering from a 17 μm radius droplet.

SI-2: Model Framework & Kinetic Simulations

The kinetic model used in the present analysis has been discussed extensively in recent publications.⁴⁻⁶ For details on the conceptual model framework, we reference the reader to a previous work, which provides an overview of the updated framework to include sub-surface reactivity.⁷ Each elementary reaction step used to generate the simulated kinetic profiles is also provided therein. The underlying chemical mechanism for this reaction system, including its pH dependence, was explored in more detail in previous work.⁶ The current model framework follows exactly that described by Prophet *et al.*⁷, reproduced here in Table S1, with addition of the Triton X-100 adsorption step as introduced in the main text, section IV. This additional adsorption step was included in the surface-compartment of the kinetic description to run all simulations.

Table S1: Elementary kinetic steps used to simulate the model in Kinetiscope©. Steps defined in the surface compartment are labeled S, diffusion coefficients for transfer between adjacent compartments are labeled D, steps defined in both the reaction-diffusion and inner-bulk compartment are labeled B, and the maximum coverage terms for each species are labeled G. As explored in the main text section IV, integers $n = 3$ and $m = 5$ are used to correct desolvation coefficients for TX and I⁻, respectively, allowing TX and I⁻ to adsorb to the same set of surface sites (with maximum Γ_{∞}^C).

#	Step	Rate coefficient	Reference
S1	$O_{3(g)} \xrightleftharpoons[k_{diff}]{k_{diff}} O_{3(diff)}$	$k_{diff} = 1.06 \times 10^9 s^{-1}$	7,8
S2	$O_{3(diff)} + site_{O_3} \xrightleftharpoons[k_{des}]{k_{ads}} O_{3(ads)}$	$k_{ads} = 1.77 \times 10^{-11} cm^3 molec.^{-1} s^{-1}$ $k_{des} = 1.93 \times 10^{10} s^{-1}$	6
S3	$O_{3(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} O_{3(b)} + site_{O_3}$	$k_{solv} = 1.9 \times 10^8 s^{-1}$ $k_{desolv} = 1.2 \times 10^{-12} cm^3 molec.^{-1} s^{-1}$	6
S4	$I_{(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} I_{(blk)} + m site$	$k_{solv} = 10^3 s^{-1}$ § $k_{desolv} = 1.66 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	9,10
S5	$IO_{(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} IO_{(b)} + m site$	$k_{solv} = 1 \times 10^3 s^{-1}$ § $k_{desolv} = 1.66 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	9,10
S6	$IO_{2(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} IO_{2(b)} + m site$	$k_{solv} = 1 \times 10^3 s^{-1}$ § $k_{desolv} = 1.66 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	9,10
S7	$TX_{(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} TX_{(blk)} + n site$	$k_{solv} = 1 s^{-1}$ †† $k_{desolv} = 1.1 \times 10^{-15} cm^3 molec.^{-1} s^{-1}$	see section IV

S8	$I_{2(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} I_{2(blk)} + m \text{ site}$	$k_{solv} = 1 \times 10^3 s^{-1}$ § $k_{desolv} = 1.66 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	9,10
S9	$HOI_{(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} HOI_{(blk)} + m \text{ site}$	$k_{solv} = 1 \times 10^3 s^{-1}$ § $k_{desolv} = 1.66 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	9,10
S10	$I_{3(ads)} \xrightleftharpoons[k_{desolv}]{k_{solv}} I_{3(blk)} + m \text{ site}$	$k_{solv} = 1 \times 10^3 s^{-1}$ § $k_{desolv} = 1.66 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	9,10
S11	$I_{(ads)} + O_{3(ads)} \xrightarrow{k_f} IO_{(ads)} + site_{O_3}$	$k_f = 1 \times 10^{-13} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	7
S12	$IO_{(ads)} + O_{3(ads)} \xrightarrow{k_f} IO_{2(ads)} + site_{O_3}$	$k_f = 1.66 \times 10^{-11} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	11
S13	$IO_{2(ads)} + O_{3(ads)} \xrightarrow{k_f} IO_{3(blk)} + m \text{ site} + site_{O_3}$	$k_f = 1.66 \times 10^{-11} cm^3 \cdot molec.^{-1} \cdot s^{-1}$	11
S14	$IO_{(ads)} + H^+ \xrightleftharpoons[k_r]{k_f} HOI_{(ads)}$	$k_f = 1.66 \times 10^{-10} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ * $k_r = 1.58 s^{-1}$	12,13
S15	$HOI_{(ads)} + I_{(ads)} \xrightleftharpoons[k_r]{k_f} I_2OH_{(ads)} + m \text{ site}$	$k_f = 6.64 \times 10^{-17} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ $k_r = 1.34 \times 10^2 s^{-1}$	14
S16	$I_2OH_{(ads)} + H^+ \xrightleftharpoons[k_r]{k_f} I_{2(ads)}$	$k_f = 3.32 \times 10^{-11} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ * $k_r = 3.2 s^{-1}$	14
S17	$HOI_{(ads)} + I_{(ads)} \xrightleftharpoons[k_r]{k_f} I_{2(ads)} + OH^- + m \text{ site}$	$k_f = 3.5 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ $k_r = 1.16 \times 10^{-16} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ *	15
S18	$HOI_{(ads)} + Cl^- + H^+ \xrightleftharpoons[k_r]{k_f} ICl_{(ads)}$	$k_f = 8 \times 10^{-32} cm^6 molec.^{-2} s^{-1}$ *‡ $k_r = 2.4 \times 10^6 s^{-1}$	16
S19	$ICl_{(ads)} + Cl^- \xrightleftharpoons[k_r]{k_f} ICl_{2(ads)}$	$k_f = 1.66 \times 10^{-13} cm^3 molec.^{-1} s^{-1}$ ‡ $k_r = 6 \times 10^5 s^{-1}$	17
S20	$I_{2(ads)} + Cl^- \xrightleftharpoons[k_r]{k_f} I_2Cl_{(ads)}$	$k_f = 1.38 \times 10^{-16} cm^3 molec.^{-1} s^{-1}$ ‡ $k_r = 5 \times 10^4 s^{-1}$	17
S21	$I_{(ads)} + ICl_{(ads)} \xrightleftharpoons[k_r]{k_f} I_2Cl_{(ads)}$	$k_f = 1.83 \times 10^{-12} cm^3 molec.^{-1} s^{-1}$ $k_r = 1.5 s^{-1}$	17
S22	$I_{2(ads)} + I_{(ads)} \leftrightarrow I_{3(ads)} + m \text{ site}$	$k_f = 1 \times 10^{-11} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ ¶ $k_r = 8.64 \times 10^6 s^{-1}$	18

S23	$I_{2(ads)} \xrightarrow{k_{evap}} I_{2(g)} + m \text{ site}$	$k_{evap} = 5.32 \times 10^8 s^{-1}$	#	19
S24	$ICl_{(ads)} \xrightarrow{k_{evap}} ICl_{(g)} + m \text{ site}$	$k_{evap} = 1.81 \times 10^7 s^{-1}$	#	20
S25	$HOI_{(ads)} \xrightarrow{k_{evap}} HOI_{(g)} + m \text{ site}$	$k_{evap} = 5.16 \times 10^6 s^{-1}$	#	21
B1	$I_{(ads)} + O_{3(ads)} \xrightarrow{k_f} IO_{(ads)} + site_{O_3}$	$k_f = 2 \times 10^{-12} cm^3 \cdot molec.^{-1} \cdot s^{-1}$		22
B2	$IO_{(blk)} + O_{3(blk)} \xrightarrow{k_f} IO_{2(blk)}$	$k_f = 2.65 \times 10^{-15} cm^3 \cdot molec.^{-1} \cdot s^{-1}$		13
B3	$IO_{2(blk)} + O_{3(blk)} \xrightarrow{k_f} IO_{3(blk)}$	$k_f = 2.65 \times 10^{-15} cm^3 \cdot molec.^{-1} \cdot s^{-1}$		13
B4	$IO_{(blk)} + H^+ \xrightleftharpoons[k_r]{k_f} HOI_{(blk)}$	$k_f = 1.66 \times 10^{-10} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ $k_r = 1.58 s^{-1}$	*	12,13
B5	$HOI_{(blk)} + I_{(blk)} \xrightleftharpoons[k_r]{k_f} I_2OH_{(blk)}$	$k_f = 6.64 \times 10^{-17} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ $k_r = 1.34 \times 10^2 s^{-1}$		14
B6	$I_2OH_{(blk)} + H^+ \xrightleftharpoons[k_r]{k_f} I_{2(blk)}$	$k_f = 3.32 \times 10^{-11} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ $k_r = 3.2 s^{-1}$	*	14
B7	$HOI_{(blk)} + I_{(b)} \xrightleftharpoons[k_r]{k_f} I_{2(blk)} + OH^-$	$k_f = 3.5 \times 10^{-18} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ $k_r = 1.16 \times 10^{-16} s^{-1}$	*	15
B8	$HOI_{(blk)} + Cl^- + H^+ \xrightleftharpoons[k_r]{k_f} ICl_{(blk)}$	$k_f = 8 \times 10^{-32} cm^6 molec.^{-2} s^{-1}$ $k_r = 2.4 \times 10^6 s^{-1}$	*‡	16
B9	$ICl_{(blk)} + Cl^- \xrightleftharpoons[k_r]{k_f} ICl_{2(blk)}$	$k_f = 1.66 \times 10^{-13} cm^3 molec.^{-1} s^{-1}$ $k_r = 6 \times 10^5 s^{-1}$	‡	17
B10	$I_{2(blk)} + Cl^- \xrightleftharpoons[k_r]{k_f} I_2Cl_{(blk)}$	$k_f = 1.38 \times 10^{-16} cm^3 molec.^{-1} s^{-1}$ ‡ $k_r = 5 \times 10^4 s^{-1}$		17
B11	$I_{(blk)} + ICl_{(blk)} \xrightleftharpoons[k_r]{k_f} I_2Cl_{(blk)}$	$k_f = 1.83 \times 10^{-12} cm^3 molec.^{-1} s^{-1}$ ‡ $k_r = 1.5 s^{-1}$		17
B12	$I_{2(blk)} + I_{(blk)} \xrightleftharpoons[k_r]{k_f} I_{3(blk)}$	$k_f = 1 \times 10^{-11} cm^3 \cdot molec.^{-1} \cdot s^{-1}$ $k_r = 8.64 \times 10^6 s^{-1}$	¶	18
D1	$I_{(blk)}$	$D = 1.53 \times 10^{-5} cm^2 \cdot s^{-1}$	¶	23
D2	$IO_{(blk)}$	$D = 1.53 \times 10^{-5} cm^2 \cdot s^{-1}$ ¶¶		23
D3	$IO_{2(blk)}$	$D = 1.53 \times 10^{-5} cm^2 \cdot s^{-1}$		23

		$\dagger\dagger$	
D4	$IO_{3(blk)}^-$	$D = 1.53 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$ $\dagger\dagger$	23
D5	$I_2OH_{(blk)}^-$	$D = 1.53 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$ $\dagger$	23
D6	$I_2Cl_{(blk)}^-$	$D = 1.53 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$ $\dagger$	23
D7	$Cl_2I_{(blk)}^-$	$D = 1.53 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$ $\dagger$	23
D6	$I_{3(blk)}^-$	$D = 1.07 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$	24
D7	$I_{2(blk)}$	$D = 1.15 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$	25
D8	$HOI_{(blk)}$	$D = 1.15 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$ $\dagger$	25
D9	$ICl_{(blk)}$	$D = 1.15 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$ $\dagger$	25
D10	$O_{3(blk)}$	$D = 1.76 \times 10^{-5} \text{ cm}^2 \cdot \text{s}^{-1}$	26
G1	O_3	$\Gamma_{\infty}^{O_3} = 5.42 \times 10^{14} \text{ molec. cm}^{-2}$	27
G2	I^-	$\Gamma_{\infty}^{I^-} = 1.2 \times 10^{14} \text{ molec. cm}^{-2}$	7
G3	TX	$\Gamma_{\infty}^{TX} = 2 \times 10^{14} \text{ molec. cm}^{-2}$	see section IV
G4	All non- O_3 solutes	$\Gamma_{\infty}^C = 6 \times 10^{14} \text{ molec. cm}^{-2}$	see section IV

§ Values of k_{desolv} found in these steps are divided by $m = 5$ in the Kinetiscope model to account for the larger maximum site value Γ_{∞}^C as explored in section IV.

†† The value of k_{desolv} found in the Triton X-100 adsorption step is divided by $n = 3$ in the Kinetiscope model to account for the larger maximum site value Γ_{∞}^C as explored in section IV.

* Simulated H^+ or OH^- are not explicitly included in the model, but rather, a pseudo-order rate condition is used by multiplying the reported rate coefficient with $[H^+]$ or $[OH^-]$ directly.

‡ As with the simulation of H^+ , Cl^- is not included explicitly and initial $[Cl^-]$ for each experiment is used to calculate a pseudo-first order rate for each step involving Cl^- .

¶ These steps—either chemical or diffusional—involve a rapid equilibrium which can inhibit the stochastic simulation when run in concert. For many simulations, the corresponding constants shown in the table are decreased by ~ 100 - 1000 in order to allow for reasonable simulation times. However, we have verified that the model results have no observable sensitivity to these coefficients in the range we can observe.

† Diffusion coefficients for these species are estimated using the D for I^- for ions, and the D for I_2 for neutrals.

Evaporation steps have also been defined in surface compartment as first order in the “bulk” species rather than adsorbed. This effectively allows I₂, for example, to evaporate from either the adsorbed or solvated state. While the model should technically only allow for adsorbed volatiles to evaporate, we define evaporation from the entire surface compartment to avoid potential coupling of evaporation rates with the solvation/desolvation rates of these volatiles, which we have largely treated as unknowns.

SI-3: Steady-state analysis methods

Here we provide further detail on the steady-state approach used to derive the analytical expressions. The core assumption used in this approach is that once the droplet is dispensed and the reaction has begun, a quasi-steady-state condition is quickly attained, which can be approximated by defining instantaneous concentrations of each species defined in the kinetic model framework. We briefly outline the derivation of the surfactant adsorption equations governing the “bulk-depletion” effect in microdroplets to demonstrate the utility of this approach and the origin of Eqs. 8-10a in section IV. Subsequently, we demonstrate how the same approach is used to quantify steady-state concentration of reactants [O₃] in the two relevant kinetic domains (*i.e.*, the surface and the subsurface “reaction-diffusion” region).

(i) Surfactant Adsorption

As illustrated in the main text, surfactant adsorption is treated as a set of elementary kinetic steps,



where the concentrations are described by a standard Langmuir-adsorption isotherm:

$$[TX_{(ads)}] = \frac{\Gamma_{\infty}^{TX} K_{eq}^{TX} \cdot [TX_{(blk)}]}{\delta \cdot 1 + K_{eq}^{TX} \cdot [TX_{(blk)}]} \quad \text{Eq. S1}$$

Recall that $K_{eq}^{TX} = \frac{k_{TX_{desolv}}}{k_{TX_{solv}}}$ and that $\frac{\Gamma_{\infty}^{TX}}{\delta}$ represents the maximum concentration of available surface sites for Triton X-100. Because this derivation neglects the interfacial concentration of I⁻, TX adsorption can be modeled as occupying a single site where Γ_{∞}^{TX} is used to define the maximum site number rather

than Γ_{∞}^C as discussed in section IV. The kinetics of surfactant adsorption in the microdroplet (Step S1) can be expressed as,

$$\frac{d[TX_{(ads)}]}{dt} = k_{TX_desolv} [site][TX_{(blk)}] - k_{TX_solv}[TX_{(ads)}] \quad \text{Eq. S3}$$

We now use the steady-state assumption, $\frac{d[TX_{(ads)}]}{dt} = 0$, to relate the concentrations of $[TX_{(ads)}]$ and $[TX_{(blk)}]$,

$$k_{TX_solv}[TX_{(ads)}] = k_{TX_desolv} [site][TX_{(blk)}] \quad \text{Eq. S4}$$

Where the available site concentration is,

$$[site] = \frac{\Gamma_{\infty}^{TX}}{\delta} - [TX_{(ads)}]. \quad \text{Eq. S5}$$

Furthermore, $[TX_{(ads)}]$ and $[TX_{(blk)}]$ are related through the conservation of the total number of TX molecules present in the microdroplet, which provides the constraint,

$$[TX_{(blk)}]_0 = [TX_{(blk)}] + \frac{3\delta}{r}[TX_{(ads)}] \quad \text{Eq. S6}$$

where δ is the thickness of the droplet interface (1 nm) and r is the droplet radius. In Eq. S6, $[TX_{(blk)}]_0$ is the bulk concentration at $t = 0$, where we assume $[TX_{(ads)}] = 0$. Solving Eqs. S4-S6 provides expressions for $[TX_{(ads)}]$ and $[TX_{(blk)}]$, presented in the main text as Eqs. 4 and 5. Lastly, we note that the approach outlined here assumes a static droplet radius r . Allowing r to change (due to evaporation or condensation of water, for example), provides similar equations, but with additional geometric factors.

(ii) Surface-Adsorbed and Solvated Ozone concentrations

An analogous approach is used to obtain expressions for ozone concentrations at the interface and within the sub-surface layer. While we do not provide an extensive discussion of how steady-state concentrations are derived, we provide a brief conceptual overview of the approach—while reserving a larger discussion to future work. The steady-state concentrations of O_3 at the interface and within the sub-surface are conceptually grounded in the kinetic model built in Kinetiscope. In the mechanics of this model, the surface adsorbed $O_{3(ads)}$ and the subsurface (or reaction-diffusion compartment) species $O_{3(rd)}$

are related through a solvation/desolvation process occurring in the top nm of solution, and a liquid diffusion description extending the length of the reaction-diffusion region. This is conceptually outlined in Fig. S4. As shown, this description invokes an intermediate “surface-to-bulk” species, termed $O_{3(sb)}$ that represents the O_3 , which has undergone solvation across the interface but has yet to diffuse into the reaction-diffusion compartment. As such, no reaction for $O_{3(sb)}$ is defined as the species acts mostly as a bookkeeping concentration to define solvation and diffusion from the interface. In parallel, on the other side of the interface, a very similar approach is used to define another “gas-to-surface” species $O_{3(gs)}$, indicating ozone, which has diffused from the gas-phase to the droplet interface but has yet to undergo actual adsorption and thermal accommodation to the interface (or equivalently, O_3 which has desorbed from the interface, but has yet to diffuse away from the droplet surface). $O_{3(sb)}$ and $O_{3(gs)}$ are necessary to fully implement the steady state approach but are eliminated when solving for the species of interest $O_{3(ads)}$ and $O_{3(rd)}$. As noted in section IV, we choose to ignore the ozone reactivity in the inner bulk compartment, $[O_{3(bulk)}]$ since the vast majority of reactivity occurs at the surface or in the reaction-diffusion region.

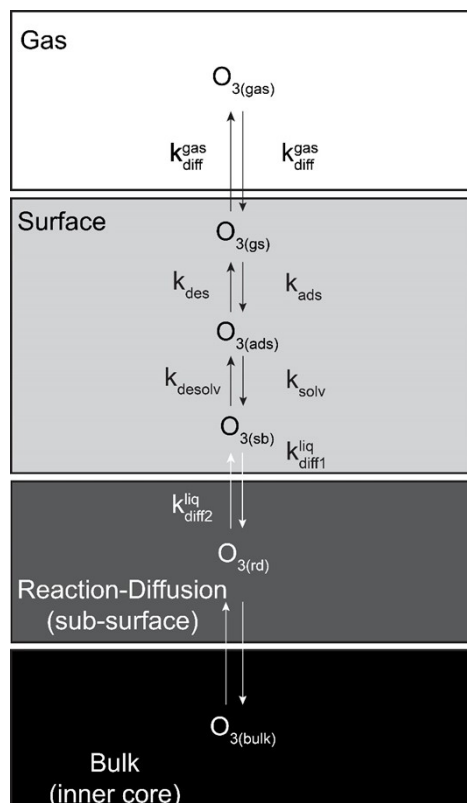


Fig. S4: Kinetic scheme showing mass transport pathways in model framework. The five related species can be used to create steady-state concentrations of $O_{3(ads)}$ and $O_{3(rd)}$ in the current work. As noted in the text, $O_{3(bulk)}$ is found to be negligible and so omitted in the analysis.

To solve for $[O_{3(ads)}]$ and $[O_{3(rd)}]$, rate equations are first defined for the four species identified, where $[O_{3(gas-\infty)}]$ represents the static gas phase concentration arbitrarily far from the droplet surface:

$$\frac{d[O_{3(gs)}]}{dt} = k_{diff}^{gas}[O_{3(gas)}] + k_{des}[O_{3(ads)}] - k_{diff}^{gas}[O_{3(gs)}] - \frac{\Gamma_{\infty}(O_3)}{\delta} k_{ads}[O_{3(gs)}] \quad \text{Eq. S7}$$

$$\frac{d[O_{3(ads)}]}{dt} = \frac{\Gamma_{\infty}(O_3)}{\delta} k_{ads}[O_{3(gs)}] + \frac{\Gamma_{\infty}(O_3)}{\delta} k_{desolv}[O_{3(sb)}] - k_{des}[O_{3(ads)}] - k_{solv}[O_{3(ads)}] - k_{rxn}^{srf}[I_{(ads)}^-][O_{3(ads)}] \quad \text{Eq. S8}$$

$$\frac{d[O_{3(sb)}]}{dt} = k_{solv}[O_{3(ads)}] + k_{diff1}^{liq}[O_{3(rd)}] - \frac{\Gamma_{\infty}(O_3)}{\delta} k_{desolv}[O_{3(sb)}] - k_{diff1}^{liq}[O_{3(sb)}] \quad \text{Eq. S9}$$

$$\frac{d[O_{3(rd)}]}{dt} = k_{diff2}^{liq}[O_{3(sb)}] - k_{diff2}^{liq}[O_{3(rd)}] - k_{rxn}^{blk}[I_{(rd)}^-][O_{3(rd)}] \quad \text{Eq. S10}$$

Kinetic coefficients found in Eq. S7-S10 can be found in the associated kinetic simulation description. The liquid diffusion rate coefficients k_{diff}^{liq1} and k_{diff}^{liq2} have not been defined in the previous work, but are simply defined through the application of Fick's first law,

$$k_{diff1}^{liq} = \frac{2D}{(L_{RD} + \delta)\delta}$$

$$k_{diff2}^{liq} = \frac{2D}{(L_{RD} + \delta)L_{RD}}$$

where L_{rxn} is the reaction diffusion length of O_3 in solution given the initial $[I^-]$, (which also defines the length of the RD compartment).

Applying a steady-state assumption, all differentials Eq. S7-S10 are assumed to be zero, enabling one to solve for each of the four concentrations in terms of the overall gas concentration $[O_{3(gas)}]$ and the iodide concentration, (where $[I_{(rd)}^-]$ and $[I_{(ads)}^-]$) are related through a Langmuir isotherm as outlined in the

main text. Solving in this manner produces expressions for $[O_{3(\text{ads})}]$ and $[O_{3(\text{rd})}]$ as given in Eq. 11 and Eq. 12 in the main text.

SI-4: Experimental data

Tables S2 and S3 below contain the data found in the main text Fig. 3 and Fig. 4, respectively.

Table S2: Remaining iodide fraction $[I]/[I_0]$ vs. time for the 9 [Triton X-100] conditions shown in Figure 3.

[TX] = 3.2 mM		[TX] = 1.6 mM		[TX] = 795 μ M	
t(s)	$[I]/[I_0]$	t(s)	$[I]/[I_0]$	t(s)	$[I]/[I_0]$
0	1	0	1	0	1
90.36041	0.972053	68.60367	0.941108	94.29367	0.943313
91.49917	0.899438	91.87155	0.933417	100.418	0.964155
92.00317	0.872377	161.8164	0.925311	117.6859	0.915194
180.2768	0.922999	162.2201	0.901734	181.2616	0.899957
181.5986	0.828855	182.0457	0.849768	203.1313	0.892552
183.9115	0.817199	252.8746	0.902986	206.5912	0.932396
271.9432	0.773728	276.4327	0.836434	269.311	0.829525
272.355	0.753597	278.9972	0.74914	284.671	0.829321
273.4548	0.863109	341.7416	0.874727	294.5551	0.893031
360.0527	0.740351	359.7966	0.762889	370.1999	0.840027
360.2116	0.780914	361.3009	0.799444	379.4746	0.686441
361.5614	0.765594	429.3405	0.812103	388.0181	0.771322
451.539	0.661134	447.53	0.736387	460.4424	0.730769
452.4257	0.721418	461.2344	0.695196	468.9614	0.594975
457.5618	0.696534	524.0389	0.656049	474.2812	0.76145
539.8215	0.799057	538.0863	0.659208	550.044	0.680043
541.063	0.631975	541.1395	0.674262	554.5338	0.661559
542.9855	0.675093	610.2761	0.634606	569.4648	0.700266
633.7419	0.704659	625.4366	0.649227	642.9516	0.649709
633.8693	0.629868	630.3615	0.637886	646.661	0.606163
643.3516	0.614147	702.2406	0.624691	655.8139	0.693108
723.0465	0.493621	714.5723	0.600461	731.7766	0.607016
725.1078	0.630106	723.2701	0.534502	738.2686	0.594143
776.2303	0.465749	790.2938	0.582197	744.0001	0.614738
809.8386	0.610455	816.9949	0.426392	822.8745	0.439042
814.5882	0.404689	834.2558	0.506673	833.0949	0.593173
871.6723	0.468558	881.1767	0.489662	836.2871	0.494198
901.665	0.550426	899.6164	0.474819	923.3287	0.403795
905.3548	0.36423	979.9073	0.479508	923.7123	0.313782
955.2658	0.401825	989.0462	0.368439	924.8827	0.490657
993.6517	0.453267	1061.559	0.413941	1002.768	0.280267
1035.28	0.311521	1078.317	0.319998	1014.197	0.433962
1042.395	0.329933	1165.632	0.300649	1016.068	0.371003
1080.24	0.438545			1099.097	0.217132
1112.144	0.256738			1108.174	0.294165
1171.14	0.420848			1180.427	0.230549
1261.089	0.384586			1186.182	0.215913
				1190.362	0.310158
				1279.029	0.135969
				1285.178	0.274864
				1292.997	0.258373
				1402.529	0.192369
				1438.198	0.145476
				1495.386	0.106903
				1565.89	0.112603

$$[TX] = 480 \mu M$$

t(s)	$[I]/[I_0]$
0	1
84.69891	0.942126
88.46592	0.957325
104.3051	0.952368
172.0875	0.890933
179.2902	0.912095
193.1422	0.904611
268.4698	0.79633
283.9406	0.795035
286.39	0.865337
358.5783	0.74533
377.369	0.75913
386.1213	0.673887
449.0538	0.712881
466.4496	0.734347
472.074	0.746857
537.4401	0.558204
549.6645	0.738501
564.5766	0.52448
627.0767	0.540835
647.9009	0.554333
674.394	0.539036
719.6438	0.401638
735.8426	0.557874
786.4938	0.529982
824.94	0.461542
879.8166	0.423068
931.6089	0.409995
1026.396	0.319377
1129.791	0.296788
1219.285	0.141129
1326.382	0.201688
1416.13	0.186981

$$[TX] = 320 \mu M$$

t(s)	$[I]/[I_0]$
0	1
63.27279	0.929419
74.73716	0.832809
75.34892	0.867284
79.35129	0.834247
88.61755	0.898669
152.3515	0.784934
154.3175	0.636998
155.8921	0.795828
159.7847	0.711462
179.4089	0.784911
230.2467	0.540799
233.6644	0.69982
233.814	0.655915
247.6168	0.703501
268.4765	0.627282
301.9635	0.541274
309.0907	0.602519
311.7306	0.52393
334.1739	0.611554
359.4927	0.541619
383.7213	0.468159
385.6816	0.370835
395.9027	0.406359
430.0726	0.472355
447.9742	0.392043
461.9475	0.29808
462.285	0.31389
468.3296	0.3078
517.765	0.426404
535.9505	0.273737
538.3924	0.340694
603.7854	0.269392
614.9093	0.193318
627.8123	0.26315
683.1727	0.104275
694.1448	0.237401
718.0181	0.090287
783.2732	0.153139

$$[TX] = 160 \mu M$$

t(s)	$[I]/[I_0]$
0	1
16.98968	0.972285
70.0993	0.887987
103.9617	0.860194
154.5488	0.802265
159.2003	0.771595
219.9647	0.589775
246.1819	0.580405
255.2953	0.610692
310.4597	0.344354
334.3647	0.376014
341.3823	0.423031
384.3336	0.241218
425.0009	0.164256
425.7025	0.260175
477.9844	0.07881
507.7503	0.065203
516.784	0.111471
605.5523	0.024869

[TX] = 64 μ M		[TX] = 32 μ M		[TX] = 6 μ M	
t(s)	[I]/[I ₀]	t(s)	[I]/[I ₀]	t(s)	[I]/[I ₀]
0	1	0	1	0	1
63.51167	0.878363	19.23641	0.963451	54.18542	0.919309
65.60404	0.931542	27.14305	0.943681	66.70231	0.894943
66.67746	0.934786	75.37341	0.819437	105.588	0.779931
89.52655	0.774935	75.87229	0.779135	143.8691	0.773078
151.4541	0.6674	96.42572	0.78981	160.8622	0.59645
151.619	0.725185	118.138	0.74866	195.247	0.620364
155.1347	0.728459	148.9261	0.672176	232.0792	0.586559
185.8525	0.486738	155.4217	0.56953	248.266	0.521944
242.6117	0.482232	174.096	0.670361	298.6154	0.462556
246.9751	0.460082	208.6014	0.439933	326.2488	0.386493
247.48	0.434373	222.2936	0.584967	344.7067	0.372628
270.7734	0.28479	233.9087	0.429919	388.8573	0.30658
334.9728	0.301194	259.3312	0.453048	411.2404	0.230212
336.5328	0.233271	297.9865	0.342982	456.0869	0.139764
340.9347	0.294633	299.1205	0.409948	484.5432	0.156118
366.7276	0.105533	309.395	0.304532	507.9547	0.079761
424.3504	0.095543	375.8073	0.191398	573.1509	0.062965
425.6941	0.107537	389.2492	0.120193	598.6583	0.032752
432.6504	0.08602	390.887	0.155641		
450.8464	0.038953	447.1145	0.11648		
511.306	0.039346	474.8565	0.088448		
522.7744	0.025746	525.7865	0.056933		
		618.3368	0.014785		

Table S3: Experimental uptake coefficients vs [Triton X-100] as shown in Figure 4.

[TX] (mM)	Uptake	[TX] (mM)	Uptake
0.0064	5.42E-03	0.4771	2.37E-03
0.0064	5.48E-03	0.4771	1.89E-03
0.0064	5.68E-03	0.4771	1.71E-03
0.0318	5.72E-03	0.4771	1.93E-03
0.0318	5.42E-03	0.6361	1.38E-03
0.0318	5.19E-03	0.6361	1.42E-03
0.0636	5.60E-03	0.6361	1.43E-03
0.0636	5.56E-03	0.7951	1.40E-03
0.0636	5.56E-03	0.7951	1.60E-03
0.0636	5.57E-03	0.7951	1.73E-03
0.0636	5.71E-03	1.5902	1.59E-03
0.0636	5.64E-03	1.5902	1.69E-03
0.1590	4.40E-03	1.5902	1.45E-03
0.1590	4.76E-03	3.1803	1.50E-03
0.1590	4.84E-03	3.1803	1.68E-03
0.3180	3.77E-03	3.1803	1.37E-03
0.3180	3.45E-03		
0.3180	3.90E-03		
0.3180	3.31E-03		
0.3180	3.53E-03		

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