

Ethylene production from shale gas using a dielectric barrier discharge plasma reactor: an integrative circular economy perspective

Seojin Shin^{a,1}, Kyeongjun Seo^{b,1}, Seung-Jun Baek^c, Kyoung-Su Ha^{d,*}, Wangyun Won^{a,*}

- ^a Department of Chemical and Biological Engineering, Korea University, 145 Anam-ro, Seongbuk-gu, Seoul 02841, Republic of Korea
 - ^b Department of Chemical Engineering and Biotechnology, Tech University of Korea, 237 Sangdaehak-ro, Siheung-si, Gyeonggi-do 15073, Republic of Korea
 - ^c Chemical Process Solution Research Center, Korea Research Institute of Chemical Technology, 141 Gajeong-ro, Daejeon 34114, Republic of Korea
 - ^d Department of Chemical and Biomolecular Engineering, Sogang University, 35 Baekbeom-ro, Mapo-gu, Seoul 04107, Republic of Korea
- * Corresponding authors (E-mail: philoseus@sogang.ac.kr (K.-S. Ha), wwon@korea.ac.kr (W. Won))
- ¹ Equally contributed

Supplementary Material

A. Experimental basis for kinetic model development

Table S1. Experimental outlet compositions used for lumped kinetic model development.

Run	Voltage [kV]	Frequency [kHz]	Discharge Power [W]	CH ₄ Inflow [sccm]	H ₂	CH ₄	C ₂ H ₆	C ₂ H ₄	C ₂ H ₂	C ₃ H ₈	C ₃ H ₆	C ₄ H ₁₀	C ₅ H ₁₂	C
0	15	1	37	30	9.804	84.304	2.551	0.174	0.142	0.768	0.043	0.124	0.131	1.96
1	15	1	37	50	6.437	89.628	1.836	0.149	0.119	0.525	0.031	0.078	0.087	1.108
2	15	1	37	70	4.774	92.291	1.399	0.133	0.101	0.382	0.025	0.053	0.062	0.781
3	15	1	37	90	3.774	93.898	1.122	0.121	0.088	0.295	0.02	0.039	0.047	0.597

Table S2. Lumped reaction network and kinetic constants obtained for the DBD methane conversion model.

Run	Reaction	Rate Expression	Rate Constant	Value (mol/s/bar ⁿ /m ³)
0	2CH ₄ -> C ₂ H ₆ + H ₂	$r_0 = k_0 \cdot P_{CH_4}^2$	k ₀	9.51E-02
1	C ₂ H ₆ -> C ₂ H ₄ + H ₂	$r_1 = k_1 \cdot P_{C_2H_6}$	k ₁	3.85E-01
2	C ₂ H ₄ + H ₂ -> C ₂ H ₆	$r_2 = k_2 \cdot P_{C_2H_4} \cdot P_{H_2}$	k ₂	1.96E-07
3	2CH ₄ -> C ₂ H ₄ + 2H ₂	$r_3 = k_3 \cdot P_{CH_4}^2$	k ₃	4.22E-02
4	C ₂ H ₄ + 2H ₂ -> 2CH ₄	$r_4 = k_4 \cdot P_{C_2H_4} \cdot P_{H_2}^2$	k ₄	1.71E-03
5	C ₂ H ₄ -> C ₂ H ₂ + H ₂	$r_5 = k_5 \cdot P_{C_2H_4}$	k ₅	2.97E+00
6	C ₂ H ₄ + CH ₄ -> C ₃ H ₈	$r_6 = k_6 \cdot P_{CH_4} \cdot P_{C_2H_4}$	k ₆	2.48E+01
7	C ₃ H ₈ -> C ₃ H ₆ + H ₂	$r_7 = k_7 \cdot P_{C_3H_8}$	k ₇	2.74E-01
8	C ₃ H ₆ -> C ₂ H ₂ + CH ₄	$r_8 = k_8 \cdot P_{C_3H_6}$	k ₈	2.49E-10
9	2C ₂ H ₄ + H ₂ -> C ₄ H ₁₀	$r_9 = k_9 \cdot P_{C_2H_4}^2 \cdot P_{H_2}$	k ₉	2.04E-02
10	C ₃ H ₈ + CH ₄ -> C ₄ H ₁₀ + H ₂	$r_{10} = k_{10} \cdot P_{C_3H_8} \cdot P_{CH_4}$	k ₁₀	2.10E+00
11	C ₄ H ₁₀ + CH ₄ -> C ₅ H ₁₂ + H ₂	$r_{11} = k_{11} \cdot P_{C_4H_{10}} \cdot P_{CH_4}$	k ₁₁	7.49E+00

Table S3. Electron-impact reaction set considered in the kinetic derivation.

Run	Reaction	Category
0	e+CH ₄ -> e+CH ₄	Elastic/momentum transfer
1	e+CH ₃ -> e+CH ₃	
2	e+CH ₂ -> e+CH ₂	
3	e+C ₂ H ₆ -> e+C ₂ H ₆	
4	e+C ₂ H ₄ -> e+C ₂ H ₄	
5	e+C ₂ H ₂ -> e+C ₂ H ₂	
6	e+C ₃ H ₈ -> e+C ₃ H ₈	
7	e+C ₃ H ₆ -> e+C ₃ H ₆	Vibrational excitation
8	e+CH ₄ <->e+CH ₄ (v13)	
9	e+CH ₄ <->e+CH ₄ (v12)	
10	e+C ₂ H ₆ <->e+C ₂ H ₆ (v24)	
11	e+C ₂ H ₆ <->e+C ₂ H ₆ (v13)	
12	e+C ₂ H ₄ <->e+C ₂ H ₄ (v1)	
13	e+C ₂ H ₄ <->e+C ₂ H ₄ (v2)	
14	e+C ₂ H ₂ <->e+C ₂ H ₂ (v13)	
15	e+C ₂ H ₂ <->e+C ₂ H ₂ (v2)	

16	$e+C_2H_2 \rightarrow e+C_2H_2(v_5)$	
17	$e+C_3H_8 \rightarrow e+C_3H_8(v_1)$	
18	$e+C_3H_8 \rightarrow e+C_3H_8(v_2)$	
19	$e+C_3H_6 \rightarrow e+C_3H_6(v)$	
<hr/>		
20	$e+CH_4 \rightarrow e+CH_3+H$	
21	$e+CH_4 \rightarrow e+CH_2+H_2$	
22	$e+CH_4 \rightarrow e+C+2H_2$	
23	$e+C_2H_6 \rightarrow e+C_2H_4+H_2$	
24	$e+C_2H_4 \rightarrow e+C_2H_2+H_2$	Electron-impact dissociation
25	$e+C_2H_4 \rightarrow e+C_2H_3+H$	
26	$e+C_3H_8 \rightarrow e+C_3H_6+H_2$	
27	$e+C_3H_6 \rightarrow e+C_2H_2+CH_4$	
<hr/>		
28	$e+CH_4 \rightarrow 2e+CH_4^+$	
29	$e+CH_3 \rightarrow 2e+CH_3^+$	
30	$e+C_2H_6 \rightarrow 2e+C_2H_6^+$	
31	$e+C_2H_4 \rightarrow 2e+C_2H_4^+$	
32	$e+C_2H_2 \rightarrow 2e+C_2H_2^+$	
33	$e+C_3H_8 \rightarrow 2e+C_3H_8^+$	Electron-impact ionization
34	$e+C_3H_6 \rightarrow 2e+C_3H_6^+$	
35	$e+C_2H_5^+ \rightarrow C_2H_2+H+H_2$	
36	$e+C_2H_5^+ \rightarrow C_2H_3+2H$	
37	$e+C_2H_5^+ \rightarrow C_2H_2+3H$	

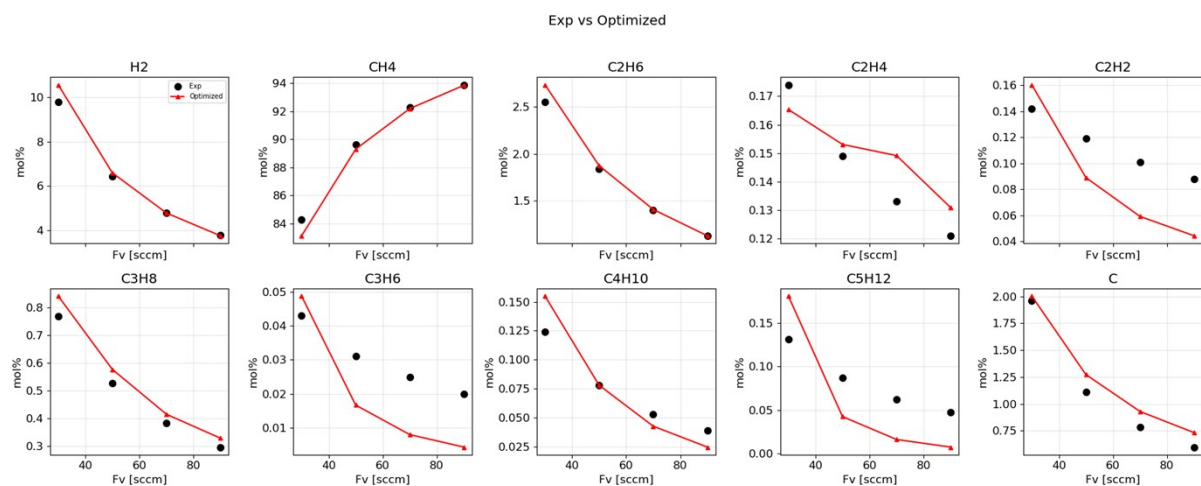


Fig S1. Comparison of experimental and predicted outlet compositions at different CH_4 inflow rates.

B. Feed gas composition

Table S4. Shale gas composition assumed in the present design.

Components	Composition (% by volume)
CH_4	92.61
C_2H_6	3.78
C_3H_8	1.42
C_4H_{10}	0.04
iso- C_4H_{10}	0.02
C_5H_{12}	0.02
iso- C_5H_{12}	0.01
C_6H_{14}	0.01
N_2	1.35
CO_2	0.67
CO	0.03
O_2	0.03
H_2S	0.01

C. Heat integration result

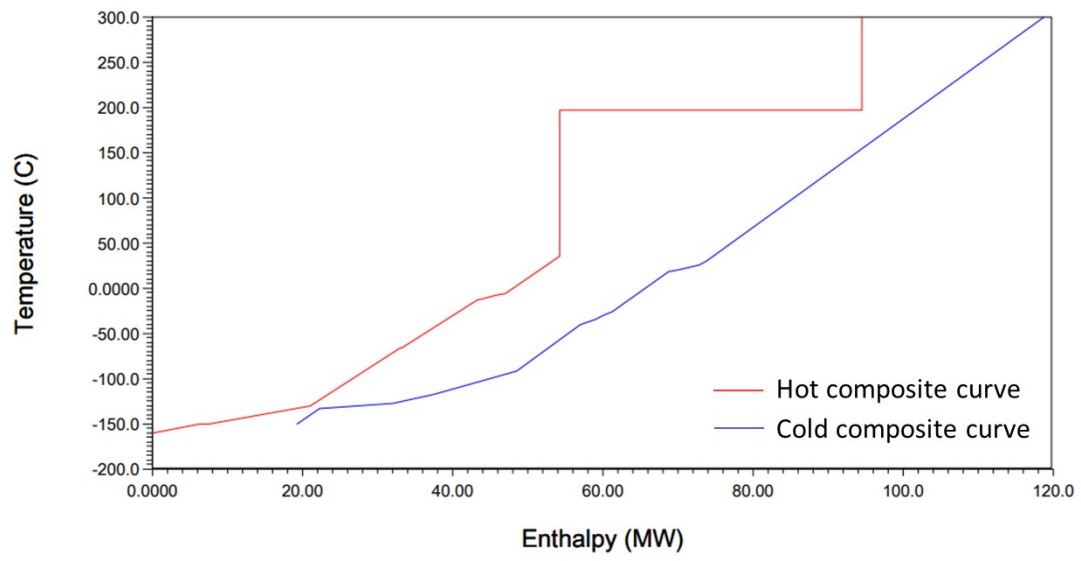


Fig S2. Composite curves for base case(On-site feed gas).

D. Process stream and equipment information

Table S5. Process major stream information.

Component	Unit	12	RXN	16	17	18	21	24	28	13-2	30	31
H ₂	kmol/hr	-	-	4914.8	4914.8	45.5	69.3	-	118.9	57.9	0.1	57.9
N ₂	kmol/hr	5856	5856	5856	5856	-	5856	2.6	3.4	3.4	0.2	3.4
CO ₂	kmol/hr	-	-	3.3	-	-	-	3.3	3.3	3.3	-	3.3
CO	kmol/hr	2.3	2.3	37.8	37.8	-	-	37.8	37.8	37.8	-	37.8
C (Cokes)	kmol/hr	-	-	1630.7	-	-	-	-	-	-	-	-
CH ₄	kmol/hr	5497.6	4247.6	3316.8	3316.8	-	-	136.8	6.8	3336.8	0.1	1.8
C ₂ H ₂	kmol/hr	-	-	173.2	173.2	-	-	173.2	173.2	-	-	-
C ₂ H ₄	kmol/hr	-	-	175	175	-	-	175	175	346.5	141.4	205.1
C ₂ H ₆	kmol/hr	224.9	224.9	63.6	63.6	-	-	63.6	63.6	65.3	1.2	65.3
C ₃ H ₈	kmol/hr	84.3	84.3	13.6	13.6	-	-	13.6	13.6	1.5	-	13.6
C ₄ H ₁₀	kmol/hr	2.3	2.3	1.8	1.8	-	-	1.8	1.8	0.5	-	1.8
C ₅ +	kmol/hr	1.2	1.2	2.5	2.5	-	-	2.5	2.5	1.2	-	2.5
Olefins	kmol/hr	1.2	1.2	24.9	24.9	-	-	24.9	24.9	24.9	-	24.9

E. Economic analysis

Table S6. List of major economic parameters and assumptions.

Shale gas prices (\$ per ton)	32.45
Methane (off-site pipeline gas) price (\$ per ton) ^a	200.0
Nitrogen (off-site pipeline gas) price (\$ per ton) ^a	150.8
Pd/WS ₂ catalyst price (\$ per ton) ^c	58.8
aMDEA price (\$ per ton) ^c	3006.8
Triethylene glycol price (\$ per ton) ^c	1200.9
Alumina price (\$ per ton) ^c	400.5
Waste disposal (\$ per ton) ^b	38.5
Wastewater treatment chemical price (\$ per ton) ^e	5778.4
Electricity price (\$ per kWh) ^e	0.07
Steam price (\$ per kWh) ^f	0.04
Discount rate (%)	10.0
Plant financing by equity (%) ^e	40.0
Plant life (years) ^e	30.0
Income tax rate (%) ^e	35.0
Interest rate for debt financing (%) ^e	8.0
Term for debt financing (years) ^e	10.0
General plant depreciation (years) ^e	7.0
Working capital (% of fixed capital investment) ^e	5.0
On-stream percentage after startup (%) ^e	90.0
Startup time (years) ^e	0.25
Revenue and costs during startup	
Revenue (% of normal) ^e	50.0
Variable costs (% of normal) ^e	75.0
Fixed costs (% of normal) ^e	100.0
Construction period (years) ^e	3.0
First 12 months' expenditures (%) ^e	8.0
Next 12 months' expenditures (%) ^e	60.0
Last 12 months' expenditures (%) ^e	32.0
^a Taken from Humbird et al. (2011)	
^b Taken from Davis et al. (2018)	
^c Taken from Liu et al. (2015)	
^d Taken from Kazi et al. (2010)	
^e Taken from Davis et al. (2015)	
^f Taken from Motagamwala et al. (2018)	

F. First-of-a-Kind (FOAK) plant analysis

Table S7. Parameters and equations used in pioneer plant analysis.

Parameter	Definition	Range	Value
Plant performance^a		0–89	25
	$= g(\text{process maturity, op}$ $\times \text{BALEQS} - 4.12 \times \text{WASTE}$		
NEWSTEPS	Number of new process steps based on block	≥ 0	3
BALEQS ^a	Percentage of heat and mass balance equations based on actual prior plant data	0–100	20
WASTE ^b	Factor for waste handling encountered during development	0–5	2
SOLIDS ^b	Factor for presence of solid feedstock or products	0 or 1	1
Cost growth		>0	0.52
	$= f(\text{technology complexit}$ $- 0.02125 \times \text{IMPURITIES}$ $- 0.06361 \times \text{PROJECT DEF}$		
PCTNEW	Estimate (%) of unproven technology incorporated in commercial use	0–100	40
IMPURITIES ^c	Factor for impurities present in process	0–5	2
COMPLEXITY ^d	Block count of all process steps in plant	≥ 1	6
INCLUSIVENESS ^c	Percentage of three factors: pre-startup personnel costs, pre-startup inventory cost, and land purchase	0–100	100
PROJECT DEFINITION ^d	Levels of site-specific information and engineering included in estimate	2–8	7
^a	Taken from Rubin et al. (2021)		
^b	Taken from Baccharini (2006)		
^c	Taken from Jia et al. (2010)		
^d	Taken from Loose et al. (2024)		

G. Project cost

Table S8. Result of project cost calculation.

Areas	Installed cost (\$)
Acid gas removal	35,393,754
TEG dehydration	2,108,810
Plasma reaction	14,337,491
PSA	16,873,696
LPG separation	4,556,420
Ethylene production	2,347,876
ISBL (inside battery limits)	75,618,046
Wastewater treatment	1,968,330
Storage	2,906,965
Heat and power generation	134,630,108
Utilities	38,060,602
OSBL (outside battery limits)	177,566,005
Total installed equipment	253,184,051
Warehouse	4% of ISBL 3,024,722
Site development	9% of ISBL 6,805,624
Additional piping	5% of ISBL 3,780,902
TDC (total direct costs)	266,795,299
Prorateable expenses	10% of TDC 26,679,530
Field expenses	10% of TDC 26,679,530
Home office & construction fee	20% of TDC 53,359,060
Project contingency	10% of TDC 26,679,530
Other costs (start-up, permits, etc)	10% of TDC 26,679,530
TIC (total indirect costs)	160,077,179
FCI (fixed capital investment)	456,660,152
Land	2% of FCI 9,133,203
Working capital	5% of FCI 22,833,008
TCI (total capital investment)	488,626,362

Table S9. Detailed equipment cost basis for major process units.

Section	Equipment / service	Design basis or sizing basis	Base capacity or flow (kg/h)	Actual capacity or flow (kg/h)	Scaling exponent	Purchased cost, base year (\$)	Base year	Purchased cost, project year (\$)	Installation factor	Installed cost, project year (\$)
Acid gas removal	AGRU	Feed gas throughput	223,000	407,349	0.6	13,127,000	2018	22,121,096	1.6	35,393,754
TEG dehydration	TEG unit	Dehydration gas throughput	1,055.7	276,385.8	0.7	21,400	2021	1,054,405	2.0	2,108,810
LPG separation	Demethanizer	Hydrocarbon separation train	416,544	41,440	0.6	1,450,000	2020	453,764	1.6	726,023
	Deethanizer	Hydrocarbon separation train	416,544	41,440	0.6	1,200,000	2020	375,529	1.6	600,847
	Debutanizer	Hydrocarbon separation train	416,544	41,440	0.6	1,000,000	2020	312,941	1.6	500,705
	Cryogenic compressor	Hydrocarbon separation train	416,544	41,440	0.6	2,750,000	2020	860,588	1.6	1,376,940
	Heat exchanger	Hydrocarbon separation train	416,544	41,440	0.6	800,000	2020	250,353	1.6	400,564
	Refrigeration system	Hydrocarbon separation train	416,544	41,440	0.6	1,900,000	2020	594,588	1.6	951,341
Ethylene production	Fixed-bed reactor	Hydrogenation section throughput	5,600	504.2	0.6	1,200,000	2025	283,032	2.2	622,669
	Pd-Ag/ α -Al ₂ O ₃ catalyst system	Hydrogenation section throughput	5,600	504.2	0.6	400,000	2025	94,344	1.5	141,516
	Feed preheater	Hydrogenation section throughput	5,600	504.2	0.6	150,000	2025	35,379	2.2	77,834
	Intercooler	Hydrogenation section throughput	5,600	504.2	0.6	120,000	2025	28,303	2.2	62,267
	Hydrogen compressor	Hydrogenation section throughput	5,600	504.2	0.6	300,000	2025	70,758	2.3	162,743
	Gas chromatograph	Hydrogenation section throughput	5,600	504.2	0.6	250,000	2025	58,965	1.8	106,137
	Control system (APC)	Hydrogenation section throughput	5,600	504.2	0.6	500,000	2025	117,930	1.5	176,895
	Pressure relief system	Hydrogenation section throughput	5,600	504.2	0.6	100,000	2025	23,586	2.0	47,172
	C ₂ H ₄ -PSA	Hydrogenation section throughput	5,600	504.2	1.0	1,200,000	2025	108,045	2.2	237,699
	Packaged auxiliaries and controls	Integrated ethylene finishing package	-	-	-	-	2021	396,080	1.8	712,944
Wastewater	Neutralization +	Wastewater flow	100,000	13,220	0.6	800,000	2011	302,820	1.6	484,512

treatment	settler									
	Organic removal (UF)	Wastewater flow	100,000	13,220	0.6	950,000	2011	359,599	1.6	575,358
	RO + polishing unit	Wastewater flow	100,000	13,220	0.6	1,500,000	2011	567,788	1.6	908,460
Storage	LPG storage tank	Product storage throughput	416,544	41,440	0.6	1,200,000	2020	375,529	2.0	751,058

I. Life-cycle assessment

Table S11. LCA data of shale gas-to-ethylene process

Input	Amount	Unit	Database
Methane, high pressure (pipeline grade) {GLO}, 2022/kg/RNA	3.002	kg	ecoinvent 3.6
Nitrogen, liquid {GLO} market for Cut-off, U	2.099	kg	ecoinvent 3.6
Pd/WS ₂ catalyst (1 wt% Pd) market group for Cut-off, U	0.102	kg	ecoinvent 3.6
Triethylene glycol (TEG), virgin {GLO} market for Cut-off, U	0.015	kg	ecoinvent 3.6
aMDEA (45 wt% aqueous solution), {GLO} Cut-off, U	0.008	kg	ecoinvent 3.6
Alumina, activated {GLO} /kg/RNA	0.019	kg	ecoinvent 3.6
Enzyme, Cellulase, Novozyme Celluclast/kg/RER	0.223	kg	ecoinvent 3.6
Heat, district or industrial, natural gas {GLO} market group for Cut-off, U	29.957	MJ	ecoinvent 3.6
Electricity, medium voltage {GLO} market group for Cut-off, U	5.405	MJ	ecoinvent 3.6
Output			
Ethylene, polymer grade	1.000	kg	ecoinvent 3.6
Carbon dioxide, biogenic	0.337	kg	ecoinvent 3.6
Carbon black	0.076	kg	ecoinvent 3.6
Vent gas (light ends)	1.041	kg	ecoinvent 3.6
Water	3.404	kg	ecoinvent 3.6
Dummy_Disposal, solid waste, unspecified, to unspecified landfill/kg/RNA	1.848	kg	USLCI

J. Sensitivity of pretreatment burden to shale gas composition variability

Table S12. Impact of shale gas compositions on the process economics.

	Raw shale gas CH ₄ (mol%)	Relative AGR + TEG cost	Estimated MSP change (%)	Estimated MSP (\$/ton C ₂ H ₄)
Low-CH ₄ case	87.61	1.08	1.44	916.41
Base case	92.61	1.00	0.00	903.40
High-CH ₄ case	97.61	0.96	-0.72	896.90

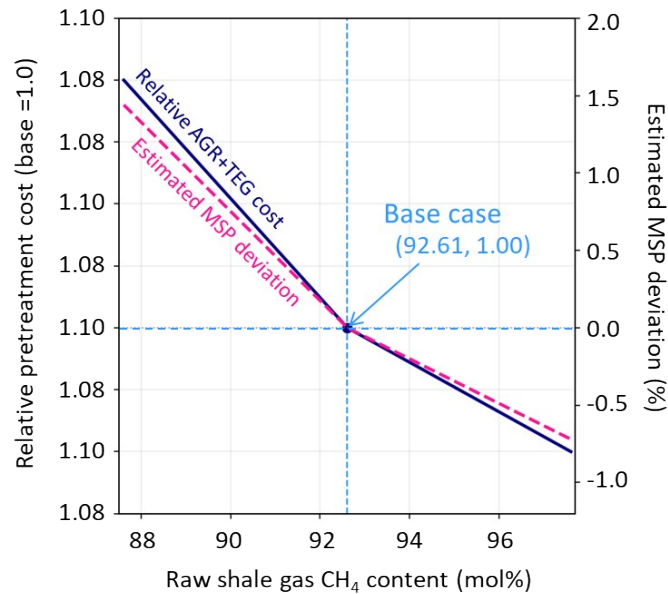


Fig S3. Sensitivity of pretreatment cost and propagated MSP to raw shale gas methane content.

To provide a quantitative indication of the potential economic effect of shale gas composition variability, a simple literature-informed sensitivity analysis was performed for the upstream pretreatment section. In the base design, the raw shale gas contains 92.61 mol% CH₄ and is conditioned through acid gas removal (AGR) and TEG dehydration prior to entering the plasma reactor. Because the reactor feed is defined after purification, variations in the raw shale gas composition are expected to affect primarily the pretreatment burden rather than the plasma reaction model or the downstream separation section itself. Previous shale gas processing studies have shown that raw gas composition variability can alter the burden of upstream treatment systems depending on methane content and impurity levels (He and You, 2014). In addition, dehydration studies have reported that higher acid gas content increases the water content of the treated gas and solvent losses, thereby increasing the burden of the TEG dehydration section (Perić et al., 2019), whereas the overall sensitivity of TEG systems is reflected mainly in operating burden rather than major changes in capital cost (Petropoulou et al., 2019).

Based on these observations, the methane content of the raw shale gas was varied by ± 5 mol% around the base composition, and the relative AGR + TEG pretreatment cost was conservatively varied from 0.96 to 1.08. The resulting propagated effect on the minimum selling price (MSP) was estimated using the pretreatment cost share in the overall process cost breakdown. As shown in Fig. S3, the relative pretreatment cost increases as the methane content of the raw shale gas decreases, while the corresponding MSP deviation remains limited. Across the examined range, the estimated MSP varies from -0.72% to $+1.44\%$ relative to the base-case MSP of $\$903.4/\text{ton C}_2\text{H}_4$. These results suggest that shale gas composition variability can influence the upstream conditioning burden, but its contribution to the overall process economics remains secondary relative to the dominant cost drivers considered in the main uncertainty analysis.

References

- Li H, Wu C, Zhang Q, Li X, Gao X. Synthesis of 1, 3-dioxolane from aqueous formaldehyde solution and ethylene glycol: kinetics and reactive distillation. *Industrial & Engineering Chemistry Research* 2019;58(17);7025-7036.
- Davis, R., Tao, L., Scarlata, C., Tan, E.C.D., Ross, J., Lukas, J., Sexton, D., 2015. Process Design and Economics for the Conversion of Lignocellulosic Biomass to Hydrocarbons: Dilute-Acid and Enzymatic Deconstruction of Biomass to Sugars and Catalytic Conversion of Sugars to Hydrocarbons. <https://doi.org/10.2172/1176746>
- Davis, R.E., Grundl, N.J., Tao, L., Bidy, M.J., Tan, E.C., Beckham, G.T., Humbird, D., Thompson, D.N., Roni, M.S., 2018. Process Design and Economics for the Conversion of Lignocellulosic Biomass to Hydrocarbon Fuels and Coproducts: 2018 Biochemical Design Case Update; Biochemical Deconstruction and Conversion of Biomass to Fuels and Products via Integrated Biorefinery Pathways. <https://doi.org/10.2172/1483234>
- Humbird, D., Davis, R., Tao, L., Kinchin, C., Hsu, D., Aden, A., Schoen, P., Lukas, J., Olthof, B., Worley, M., Sexton, D., Dudgeon, D., 2011. Process Design and Economics for Biochemical Conversion of Lignocellulosic Biomass to Ethanol: Dilute-Acid Pretreatment and Enzymatic Hydrolysis of Corn Stover.
- Rubin, E. S., et al. (2021). Cost guidelines for advanced energy systems: Learning curves and FOAK costs. Proceedings of the 15th Greenhouse Gas Control Technologies Conference.
- Baccarini, D. (2006). Merrow & Schroeder (1991) highlighted the important link between predicting cost growth... and project cost contingency by stating that cost growth can be viewed as inadequate contingency within cost estimates. In Proceedings of the AUBEA Conference. Curtin University.
- Jia, G., Ni, J., Chen, Z., Hong, B., & Lin, C. (2010). A project contingency framework based on uncertainty and its application to chemical plant projects. *Journal of Loss Prevention in the Process Industries*, 23(5), 635-642.
- Loose, V. W., & Roark, J. (2024). Progressing from first-of-a-kind to Nth-of-a-kind: Applying learning rates and contingency factors. *Journal of Process Safety and Environmental Protection*, 185, 883-894.