# **Supplementary Information for**

## Deactivation Mechanisms of Cu-Zn-Al<sub>2</sub>O<sub>3</sub> in CO<sub>2</sub> Hydrogenation

### Induced by SO<sub>2</sub> Exposure

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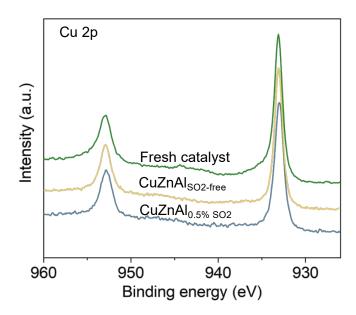


Fig. S1. XPS spectra of Cu 2p of fresh and used Cu-ZnO-Al\_2O\_3 catalysts.

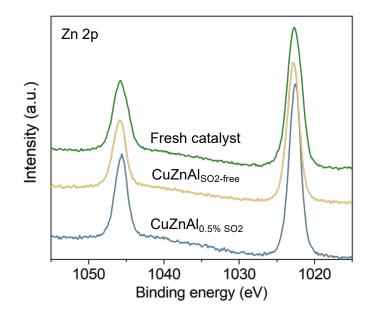


Fig. S2. XPS spectra of Zn 2p of fresh and used Cu-ZnO-Al\_2O\_3 catalysts.

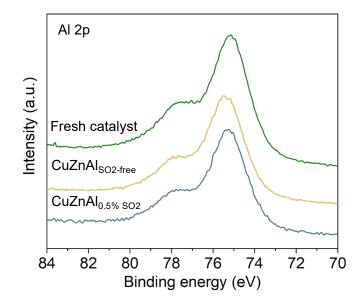
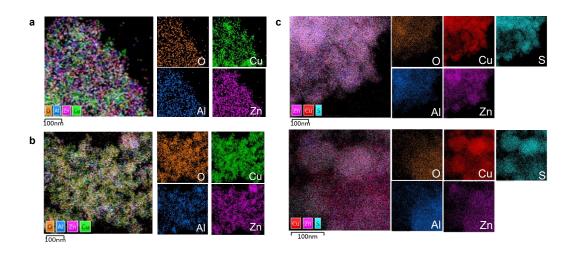


Fig. S3. XPS spectra of Al 2p of fresh and used Cu-ZnO-Al\_2O\_3 catalysts.



### Fig. S4. STEM analysis and EDX mapping of Cu-ZnO-Al\_2O\_3.

(a) Fresh catalyst. (b) The used catalyst exposed to  $H_2/CO_2/N_2$  (1:1:1) for 400 min at 500 °C. (c) The used catalyst exposed to  $H_2/CO_2/N_2$  (1:1:1) with 0.5% SO<sub>2</sub> for 400 min at 500 °C.

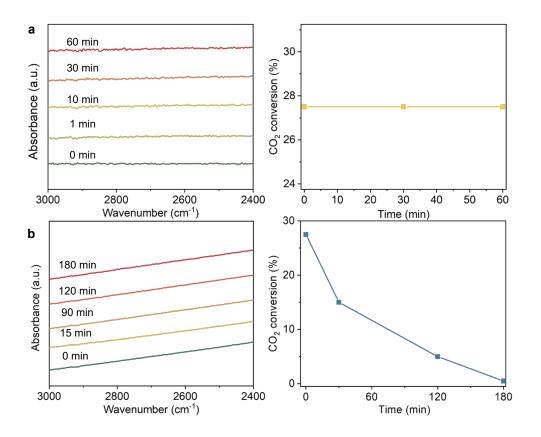
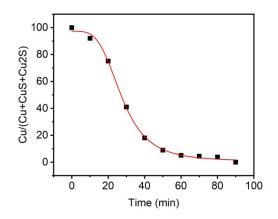


Fig. S5. Evolution of the surface functional groups over Cu-ZnO-Al $_2O_3$  with TOS.

The catalyst was first exposed to (a)  $CO_2/H_2/N_2$  (1:1:1) for 60 min, followed by (b) switching the gas flow to  $CO_2/H_2/N_2$  (1:1:1) with 0.5% SO<sub>2</sub>.  $CO_2$  conversion during the TOS of 180 min detected by gas analyzer. No  $CH_4$  formation was detected. Reaction conditions: 500 °C, 1 bar, gas flow rate of 30 mL min<sup>-1</sup>.



### Fig. S6 Experimental data and fit of metallic Cu phase disappearance kinetics

The normalized phase fraction evolution of Cu (derived from XRD peak area) was fitted using a power-law logistic function:

$$X(t) = 0.64 + 96.68 / (1 + (\frac{t}{27.3})^{3.8})$$

where:

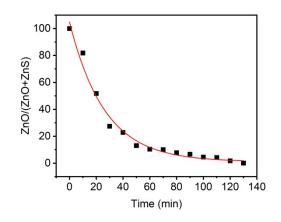
X<sub>0</sub>=0.64 represents the residual Cu fraction at equilibrium (unreacted Cu or background signal),

A=96.68 is the maximum amplitude of the reaction (total convertible Cu),

 $\tau$ =27.3 min is the characteristic time for 50% conversion,

n=3.8 is the growth exponent reflecting the reaction mechanism.

Model validation demonstrates excellent agreement with experimental XRD trends ( $R^2$ =0.978). The kinetic analysis of copper sulfidation reveals a diffusion-controlled nucleation-growth mechanism, characterized by a time constant  $\tau$ =27.3 min, indicating that 50% of Cu converts to CuS/Cu<sub>2</sub>S within ~27 min. The growth exponent n=3.8 aligns with 3D diffusion-limited Avrami-like kinetics (theoretical n=3-4), supporting a three-stage mechanism.



### Fig. S7 Experimental data and fit of ZnO phase disappearance kinetics

The normalized residual ZnO fraction X(t), derived from XRD peak area integration, was fitted using a singleexponential decay model with a baseline offset:

$$X(t) = 103.8e^{-\frac{t}{26.3}} + 1.08$$

where:

A=103.8 represents the initial ZnO content,

 $\tau$ =26.3 min is the characteristic time constant,

B=1.08 accounts for residual unreacted ZnO or instrumental background.

Model validation confirms the single-exponential decay model's superiority ( $R^2=0.983$ ). The sulfidation kinetics of ZnO follows a first-order process with a rate constant k=0.038 min<sup>-1</sup> and a half-life t<sub>1/2</sub>≈18.2 min, indicating rapid consumption of 50% ZnO within 18 min. A small residual fraction (~1%, B=1.08) persists due to kinetic limitations, likely from ZnS passivation layers blocking further sulfur diffusion. Mechanistically, the reaction proceeds via two distinct phases:

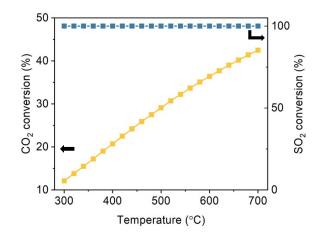


Fig. S8. Thermodynamic equilibrium calculation. (500°C, 0.5% SO<sub>2</sub>, H<sub>2</sub>/CO<sub>2</sub>=1:1), SO<sub>2</sub> is converted to H<sub>2</sub>S.

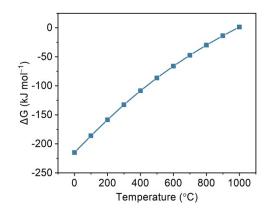


Fig. S9. Gibbs free energies of the reaction:  $SO_2(g) + 3H_2(g) \rightarrow H_2S(g) + 2H_2O(g)$ .

Table S1. XPS fitting parameters of	Cu LMM for fre	esh and use	d catalysts.
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Material	State	Cu LMM B.E. (eV)	FWHM (eV)	²L/G Mix (%)	Amount (%)
Fresh catalyst	Cu+	570.3		30	0
	Cu <sup>0</sup>	568.4	1.5	30	100
CuZnAl <sub>so2-free</sub>	Cu+	570.3	1.3	30	18
	Cu <sup>0</sup>	568.4	1.4	30	82
CuZnAl <sub>0.5% SO2</sub>	Cu+	570.3	1.8	30	58
	Cu <sup>0</sup>	568.4	1.7	30	42

<sup>a</sup> L/G: Lorentzian/Gaussian line shape.

Material	State	Zn LMM (eV)	FWHM (eV)	²L/G Mix (%)	Amount (%)
resh catalyst	Zn <sup>δ+</sup>	496.0	3.5	30	37
	Zn <sup>2+</sup>	499.5	3.5	30	63
CuZnAl <sub>SO2-free</sub>	Zn <sup>δ+</sup>	496.0	3.4	30	37
	Zn <sup>2+</sup>	499.5	3.5	30	63
CuZnAl <sub>0.5% SO2</sub>	Znδ+	496.0	3.5	30	33
	Zn <sup>2+</sup>	499.5	3.5	30	67

<sup>a</sup> L/G: Lorentzian/Gaussian line shape.

	Cu (mg g <sup>-1</sup> )	Zn (mg g <sup>-1</sup> )	Al (mg g <sup>-1</sup> )	Cu loading (wt.%)	ZnO loading (wt.%)	Al <sub>2</sub> O <sub>3</sub> loading (wt.%)	S (mg g <sup>-1</sup> )
Before reaction	461.9	182.4	49.1	59.1	29.0	11.9	-
CuZnAl <sub>s02-free</sub>	468.3	175.2	50.2	59.8	28.2	11.9	-
CuZnAI <sub>0.5% SO2</sub>	471.2	178.3	49.5	-	-	-	335.3

### Note S1:

Theoretical sulfur content for complete conversion of  $Cu \rightarrow Cu_2S$  and  $ZnO \rightarrow ZnS$  was calculated as follows:

- 1. Mass balance:
  - 1) Initial Cu: 591 mg/g<sup>-1</sup>  $\rightarrow$  Moles of Cu = 591 mg / 63.55 g mol<sup>-1</sup> = 9.30 mmol g<sup>-1</sup>
  - 2) Initial ZnO: 290 mg g<sup>-1</sup>  $\rightarrow$  Moles of Zn = (290 mg × 65.38/81.38) / 65.38 g mol<sup>-1</sup> = 3.56 mmol g<sup>-1</sup>

#### 2. Sulfur stoichiometry:

- 1)  $Cu_2S$  requires 4.65 mmol S g<sup>-1</sup> (9.30 mmol Cu × 1 mol S / 2 mol Cu).
- 2) ZnS requires 3.56 mmol S  $g^{-1}$ .
- 3) Total S = 4.65 + 3.56 = 8.21 mmol S  $g^{-1} \rightarrow 263$  mg S  $g^{-1}$  (26.3 wt%).

If Cu was fully converted to CuS, theoretical sulfur content for complete conversion of Cu  $\rightarrow$  CuS and ZnO  $\rightarrow$  ZnS was calculated as follows:

- 3. Sulfur stoichiometry:
  - 4) CuS requires 9.30 mmol S  $g^{-1}$  (9.30 mmol Cu × 1 mol S / 1 mol Cu).
  - 5) ZnS requires 3.56 mmol S  $g^{-1}$ .
  - 6) Total S = 9.30 + 3.56 = 12.86 mmol S  $g^{-1} \rightarrow$  412.3 mg S  $g^{-1}$  (41.2 wt%).