

Electronic Supplementary Information

**Vortex-Assisted Reverse-Phase Dispersive Liquid-Liquid
Microextraction for On-Site Determination of Ti, Cr, Mn, Ni, and
Cu in Lubricating Oil Using Total Reflection X-ray Fluorescence
Spectroscopy**

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Table S1. Factors and levels of the Plackett-Burman design

| Experimental factor | Low level (- 1) | High level (1) |
|--------------------------------------|--------------------|-------------------------|
| A: Sample volume (mL) | 1 | 5 |
| B: Extractant volume(μ L) | 50 μ L | 100 μ L |
| C: Acidity(mol L ⁻¹) | 0 | 0.1 mol L ⁻¹ |
| D: Vortex time(min) | 1 min | 3 min |
| E: Centrifugation conditions(min) | 0 | 3 min |

Table S2. Screening study matrix of the Plackett-Burman design

| Experiment | A | B | C | D | E |
|------------|---|-----|-----|---|---|
| 1 | 5 | 100 | 0.1 | 1 | 3 |
| 2 | 1 | 100 | 0.1 | 3 | 0 |
| 3 | 5 | 50 | 0.1 | 3 | 3 |
| 4 | 1 | 100 | 0 | 3 | 3 |
| 5 | 1 | 50 | 0.1 | 1 | 3 |
| 6 | 5 | 50 | 0 | 3 | 0 |
| 7 | 1 | 50 | 0 | 1 | 0 |
| 8 | 5 | 100 | 0 | 1 | 0 |
| 9 | 5 | 50 | 0.1 | 1 | 0 |
| 10 | 1 | 100 | 0 | 1 | 3 |
| 11 | 5 | 100 | 0.1 | 3 | 0 |
| 12 | 1 | 50 | 0 | 3 | 3 |

Table S3. Experimental results of the Plackett-Burman design

| Experiment | Ti | | Cr | | Mn | | Ni | | Cu | |
|------------|------|------|-------|-----|------|------|------|------|------|------|
| | AR | EF | AR | EF | AR | EF | AR | EF | AR | EF |
| 1 | 0.41 | 16.0 | 0.051 | 3.0 | 0.40 | 4.3 | 0.44 | 4.9 | 0.34 | 4.6 |
| 2 | 0.48 | 18.3 | 0.055 | 3.3 | 0.80 | 8.5 | 0.70 | 7.9 | 0.59 | 7.9 |
| 3 | 0.24 | 9.1 | 0.032 | 1.9 | 0.19 | 2.1 | 0.22 | 2.5 | 0.18 | 2.4 |
| 4 | 0.05 | 1.8 | 0.010 | 0.6 | 0.02 | 0.2 | 0.03 | 0.4 | 0.04 | 0.5 |
| 5 | 0.61 | 23.4 | 0.075 | 4.4 | 1.12 | 11.9 | 1.04 | 11.7 | 0.93 | 12.4 |
| 6 | 0.07 | 2.7 | 0.014 | 0.8 | 0.06 | 0.7 | 0.09 | 1.0 | 0.08 | 1.1 |
| 7 | 0.09 | 3.4 | 0.020 | 1.2 | 0.07 | 0.7 | 0.08 | 1.0 | 0.08 | 1.1 |
| 8 | 0.02 | 0.9 | 0.005 | 0.3 | 0.02 | 0.2 | 0.03 | 0.4 | 0.03 | 0.3 |
| 9 | 0.05 | 2.1 | 0.014 | 0.9 | 0.16 | 1.7 | 0.15 | 1.7 | 0.13 | 1.7 |
| 10 | 0.03 | 1.0 | 0.004 | 0.2 | 0.03 | 0.3 | 0.03 | 0.4 | 0.03 | 0.4 |
| 11 | 0.44 | 16.7 | 0.066 | 3.9 | 1.30 | 13.8 | 1.21 | 13.5 | 1.06 | 14.2 |
| 12 | 0.13 | 5.1 | 0.022 | 1.3 | 0.11 | 1.1 | 0.11 | 1.3 | 0.13 | 1.7 |

AR: Area ratio of the analyte element to the internal standard element

EF: Enrichment factor of the analyte element

Table S4. Factors and levels of the CCCD

| Factors | Level | | | Star points ($\alpha=1,414$) | |
|-------------------------------------|----------|-------------|-----------|-----------------------------------|-----------|
| | Low (-1) | Central (0) | High (+1) | $-\alpha$ | $+\alpha$ |
| Sample volume (mL) | 2 | 3 | 4 | 1.6 | 4.4 |
| Extractant volume (μL) | 58 | 75 | 93 | 50 | 100 |

Table S5. Optimization study matrix of the CCCD

| Experiment | Sample volume (mL) | Extractant volume (μL) |
|------------|--------------------|-------------------------------------|
| 1 | 2 | 58 |
| 2 | 4 | 58 |
| 3 | 2 | 93 |
| 4 | 4 | 93 |
| 5 | 1.6 | 75 |
| 6 | 4.4 | 75 |
| 7 | 3 | 50 |
| 8 | 3 | 100 |
| 9 | 3 | 75 |
| 10 | 3 | 75 |
| 11 | 3 | 75 |
| 12 | 3 | 75 |

Table S6. Experimental results of the CCCD

| Experiment | Ti | | Cr | | Mn | | Ni | | Cu | |
|------------|------|-----|-------|-----|------|------|------|------|------|------|
| | AR | EF | AR | EF | AR | EF | AR | EF | AR | EF |
| 1 | 0.08 | 3.1 | 0.015 | 0.9 | 0.30 | 7.9 | 0.27 | 7.5 | 0.24 | 7.9 |
| 2 | 0.05 | 1.9 | 0.013 | 0.8 | 0.20 | 5.4 | 0.20 | 5.5 | 0.17 | 5.7 |
| 3 | 0.11 | 4.1 | 0.012 | 0.7 | 0.46 | 12.2 | 0.36 | 10.0 | 0.36 | 12.1 |
| 4 | 0.06 | 2.1 | 0.008 | 0.5 | 0.22 | 5.9 | 0.20 | 5.7 | 0.19 | 6.3 |
| 5 | 0.07 | 2.5 | 0.014 | 0.8 | 0.34 | 9.1 | 0.29 | 8.1 | 0.30 | 9.9 |
| 6 | 0.03 | 1.2 | 0.010 | 0.6 | 0.12 | 3.3 | 0.10 | 2.9 | 0.15 | 5.1 |
| 7 | 0.11 | 4.2 | 0.022 | 1.3 | 0.47 | 12.5 | 0.43 | 12.0 | 0.36 | 11.9 |
| 8 | 0.17 | 6.5 | 0.037 | 2.2 | 0.61 | 16.1 | 0.54 | 15.2 | 0.47 | 15.8 |
| 9 | 0.20 | 7.8 | 0.038 | 2.2 | 0.79 | 21.1 | 0.68 | 19.1 | 0.64 | 21.4 |
| 10 | 0.20 | 7.5 | 0.034 | 2.0 | 0.80 | 21.2 | 0.69 | 19.4 | 0.63 | 21.1 |
| 11 | 0.16 | 6.3 | 0.029 | 1.7 | 0.67 | 17.8 | 0.58 | 16.3 | 0.54 | 17.9 |
| 12 | 0.17 | 6.4 | 0.031 | 1.8 | 0.64 | 17.1 | 0.55 | 15.3 | 0.51 | 17.1 |

AR: Area ratio of the analyte element to the internal standard element

EF: Enrichment factor of the analyte element

Table S7. Optimal values for Cu, Ni, Mo, Mn and Cr

| Analyte | Sample volume (mL) | Extractant volume(μ L) |
|---------|--------------------|-----------------------------|
| Ti | 2.9 | 80 |
| Cr | 2.9 | 78 |
| Mn | 2.8 | 79 |
| Ni | 2.9 | 78 |
| Cu | 2.8 | 79 |

Table S8. ANOVA tables of the CCD

| Analyte | Analysis of Variance | | | | | |
|-------------------|----------------------|--------|----------|----------|---------|---------|
| | Source | DF | Adj SS | Adj MS | F-Value | P-Value |
| Ti | Model | 5 | 0.037875 | 0.007575 | 17.29 | 0.002 |
| | Linear | 2 | 0.003812 | 0.001906 | 4.35 | 0.068 |
| | A | 1 | 0.002119 | 0.002119 | 4.83 | 0.070 |
| | B | 1 | 0.001694 | 0.001694 | 3.87 | 0.097 |
| | Square | 2 | 0.033964 | 0.016982 | 38.75 | 0.000 |
| | A*A | 1 | 0.033053 | 0.033053 | 75.42 | 0.000 |
| | B*B | 1 | 0.004349 | 0.004349 | 9.92 | 0.020 |
| | 2-Way Interaction | 1 | 0.000098 | 0.000098 | 0.22 | 0.653 |
| | A*B | 1 | 0.000098 | 0.000098 | 0.22 | 0.653 |
| | Error | 6 | 0.002629 | 0.000438 | | |
| | Lack-of-Fit | 3 | 0.001369 | 0.000456 | 1.09 | 0.474 |
| | Pure Error | 3 | 0.001260 | 0.000420 | | |
| | Total | 11 | 0.040504 | | | |
| | Cr | Source | DF | Adj SS | Adj MS | F-Value |
| Model | | 5 | 0.001083 | 0.000217 | 4.49 | 0.048 |
| Linear | | 2 | 0.000039 | 0.000020 | 0.41 | 0.682 |
| A | | 1 | 0.000021 | 0.000021 | 0.43 | 0.538 |
| B | | 1 | 0.000019 | 0.000019 | 0.39 | 0.555 |
| Square | | 2 | 0.001042 | 0.000521 | 10.80 | 0.010 |
| A*A | | 1 | 0.001029 | 0.001029 | 21.32 | 0.004 |
| B*B | | 1 | 0.000099 | 0.000099 | 2.06 | 0.202 |
| 2-Way Interaction | | 1 | 0.000001 | 0.000001 | 0.03 | 0.878 |
| A*B | | 1 | 0.000001 | 0.000001 | 0.03 | 0.878 |
| Error | | 6 | 0.000290 | 0.000048 | | |
| Lack-of-Fit | | 3 | 0.000250 | 0.000083 | 6.33 | 0.082 |
| Pure Error | | 3 | 0.000039 | 0.000013 | | |
| Total | | 11 | 0.001372 | | | |
| Mn | Source | DF | Adj SS | Adj MS | F-Value | P-Value |
| | Model | 5 | 0.563596 | 0.112719 | 18.71 | 0.001 |
| | Linear | 2 | 0.069749 | 0.034875 | 5.79 | 0.040 |
| | A | 1 | 0.052055 | 0.052055 | 8.64 | 0.026 |
| | B | 1 | 0.017694 | 0.017694 | 2.94 | 0.137 |
| | Square | 2 | 0.488804 | 0.244402 | 40.57 | 0.000 |
| | A*A | 1 | 0.462840 | 0.462840 | 76.84 | 0.000 |
| | B*B | 1 | 0.086402 | 0.086402 | 14.34 | 0.009 |
| | 2-Way Interaction | 1 | 0.005041 | 0.005041 | 0.84 | 0.396 |
| | A*B | 1 | 0.005041 | 0.005041 | 0.84 | 0.396 |
| | Error | 6 | 0.036142 | 0.006024 | | |
| | Lack-of-Fit | 3 | 0.016375 | 0.005458 | 0.83 | 0.560 |
| | Pure Error | 3 | 0.019767 | 0.006589 | | |
| | Total | 11 | 0.599737 | | | |

| | Source | DF | Adj SS | Adj MS | F-Value | P-Value |
|-------|-------------------|----------|----------|----------|---------|---------|
| Ni | Model | 5 | 0.408585 | 0.081717 | 15.97 | 0.002 |
| | Linear | 2 | 0.038590 | 0.019295 | 3.77 | 0.087 |
| | A | 1 | 0.030142 | 0.030142 | 5.89 | 0.051 |
| | B | 1 | 0.008448 | 0.008448 | 1.65 | 0.246 |
| | Square | 2 | 0.368250 | 0.184125 | 35.98 | 0.000 |
| | A*A | 1 | 0.355288 | 0.355288 | 69.43 | 0.000 |
| | B*B | 1 | 0.053250 | 0.053250 | 10.41 | 0.018 |
| | 2-Way Interaction | 1 | 0.001745 | 0.001745 | 0.34 | 0.581 |
| | A*B | 1 | 0.001745 | 0.001745 | 0.34 | 0.581 |
| | Error | 6 | 0.030703 | 0.005117 | | |
| | Lack-of-Fit | 3 | 0.014915 | 0.004972 | 0.94 | 0.518 |
| | Pure Error | 3 | 0.015788 | 0.005263 | | |
| | Total | 11 | 0.439288 | | | |
| Cu | Source | DF | Adj SS | Adj MS | F-Value | P-Value |
| | Model | 5 | 0.317721 | 0.063544 | 14.52 | 0.003 |
| | Linear | 2 | 0.036843 | 0.018422 | 4.21 | 0.072 |
| | A | 1 | 0.024682 | 0.024682 | 5.64 | 0.055 |
| | B | 1 | 0.012161 | 0.012161 | 2.78 | 0.147 |
| | Square | 2 | 0.278085 | 0.139043 | 31.78 | 0.001 |
| | A*A | 1 | 0.251004 | 0.251004 | 57.36 | 0.000 |
| | B*B | 1 | 0.068351 | 0.068351 | 15.62 | 0.008 |
| | 2-Way Interaction | 1 | 0.002792 | 0.002792 | 0.64 | 0.455 |
| | A*B | 1 | 0.002792 | 0.002792 | 0.64 | 0.455 |
| | Error | 6 | 0.026254 | 0.004376 | | |
| | Lack-of-Fit | 3 | 0.013251 | 0.004417 | 1.02 | 0.494 |
| | Pure Error | 3 | 0.013003 | 0.004334 | | |
| Total | 11 | 0.343974 | | | | |

Table S9. Quantitative accuracy before and after matrix effect correction using the standard addition method

| Analyte | True value | Before matrix correction | | After matrix correction | |
|---------|------------|---------------------------------|-----------------|---------------------------------|-----------------|
| | | Detection concentration /mg·L-1 | Recovery Rate/% | Detection concentration /mg·L-1 | Recovery Rate/% |
| Ti | 2.5 | 0.8 | 33 | 2.1 | 84 |
| Cr | 2.5 | 0.9 | 37 | 2.1 | 84 |
| Mn | 2.5 | 2.1 | 85 | 2.4 | 96 |
| Ni | 2.5 | 2.2 | 90 | 2.6 | 104 |
| Cu | 2.5 | 1.3 | 54 | 2.2 | 88 |

Table S10. Calculation of Penalty points (PP) for assessing the greenness of propose method and traditional method

| | This work | | Ref. 25 | |
|----------------------------------|------------------------------|---------------------|------------------------------|---------------------|
| | Penalty Item | Penalty Points (PP) | Penalty Item | Penalty Points (PP) |
| Reagents | Nitric Acid | 4 | Hydrochloric Acid | 4 |
| | Petroleum ether for dilution | 8 | Petroleum ether for dilution | 8 |
| | Reference materials | 1 | Reference materials | 1 |
| Instruments | TXRF analysis | 0 | MIP OES analysis | 1 |
| | Waste | 6 | Waste | 8 |
| Analytical Eco-Scale Total Score | 81 | | 78 | |

Table S11. Comparison of properties of petroleum ether, water and Deep Eutectic Solvents (DES)

| Solvent Type | Density (g/mL) | Polarity | Viscosity (cP) |
|----------------------|-----------------|---|---|
| Petroleum Ether | 0.64 - 0.66 | 0.01 (Extremely Low, Non-polar) | ~0.3 (Very Low) |
| Water | 0.997 (at 25°C) | 10.2 (High, Polar) | 0.89 (at 25°C) |
| DESs (General Range) | Typically > 1.0 | Tunable, Wide Range (Typically Moderate to Polar) | Very High (Typically ranges from 10 to > 50,000; significantly higher than water and petroleum ether) |

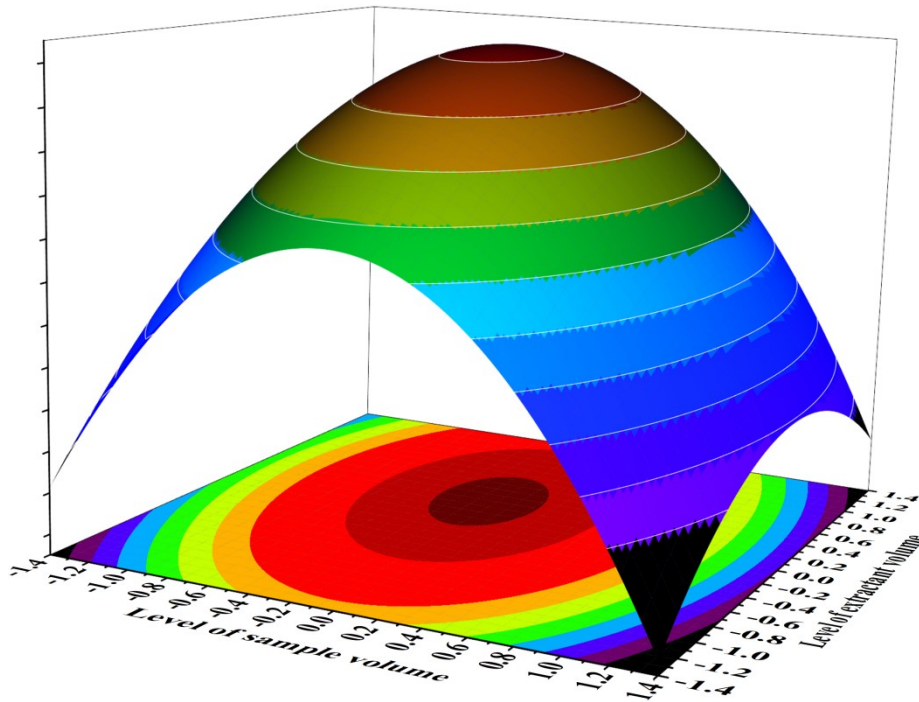


Figure S1. Response surface and contour plots from circumscribed central composite design for Ti

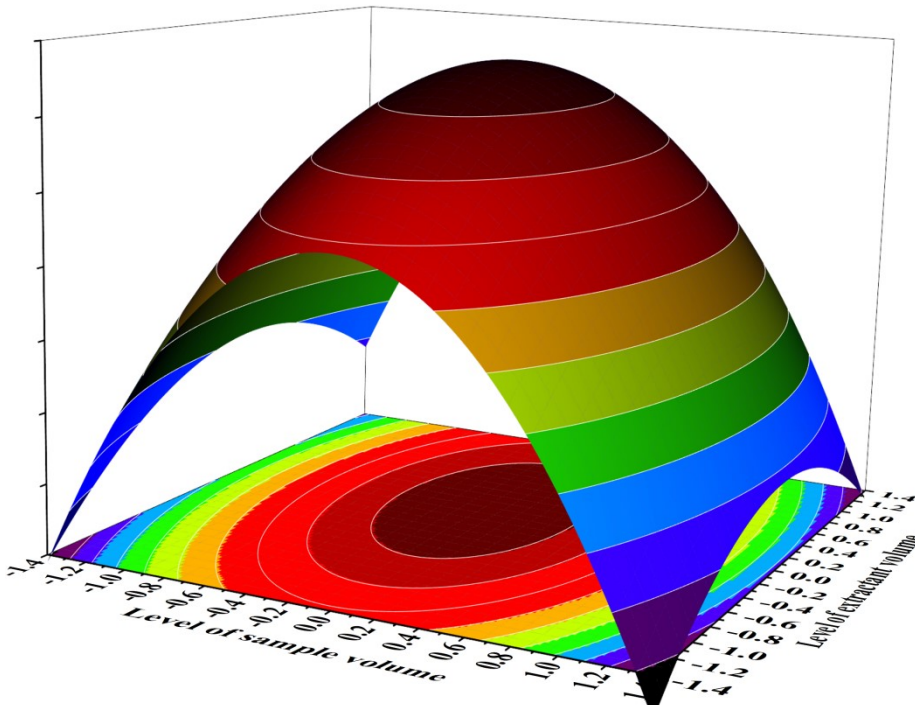


Figure S2. Response surface and contour plots from circumscribed central composite design for Cr

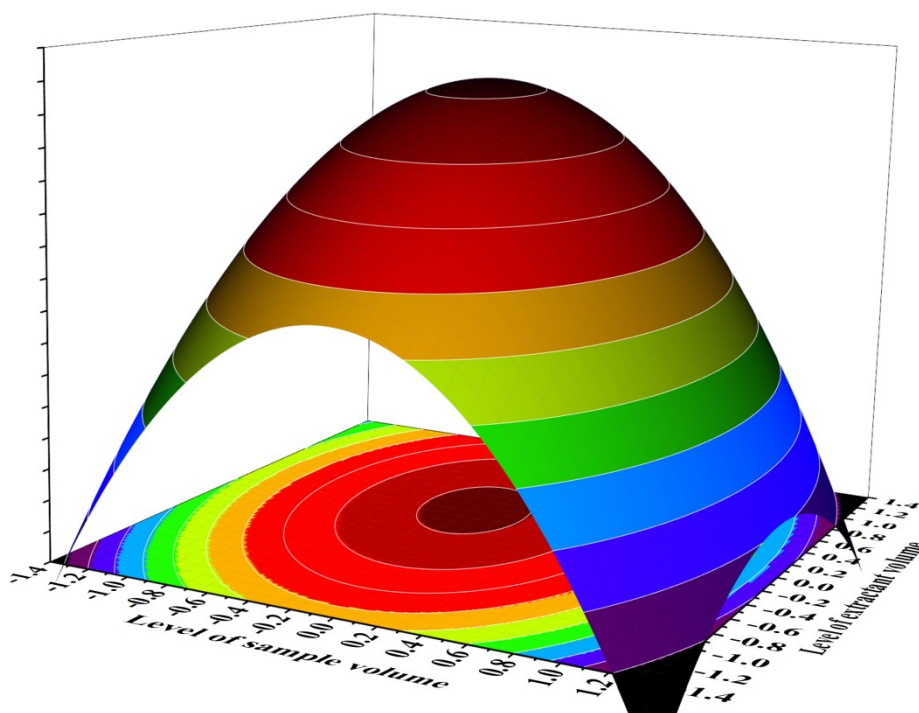


Figure S3. Response surface and contour plots from circumscribed central composite design for Mn

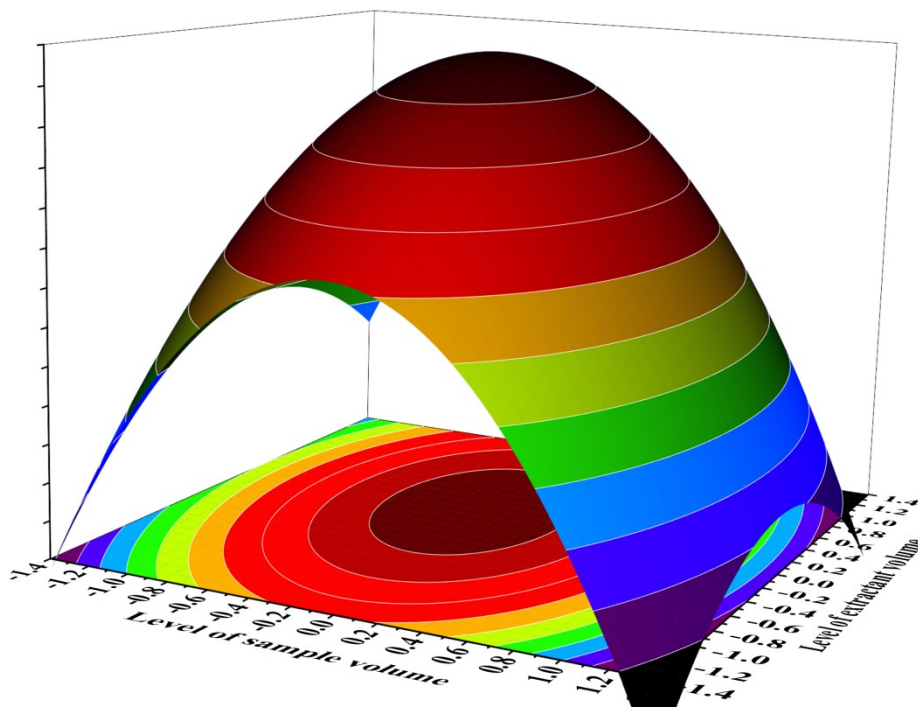


Figure S4. Response surface and contour plots from circumscribed central composite design for Ni

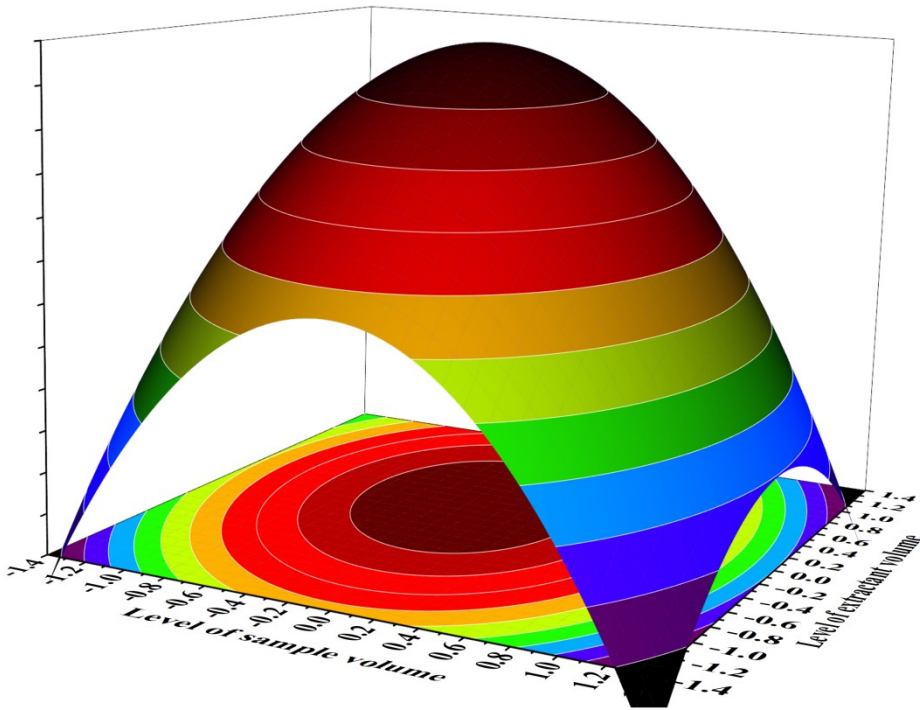


Figure S5. Response surface and contour plots from circumscribed central composite design for Cu