

Supplementary Information (SI) for Materials Horizons.

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Supplementary Information

Physically Programmed Vegan Leather Emulating the Mechanical and Sensory Characteristics of Animal Leather from Once-Discarded Gluten

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50 **Experimental Section**

51 **Materials**

52 Wheat vital gluten (protein 100%) was purchased from Sigma-Aldrich. Glycerol (99%, EP) and
53 iron(III) chloride hexahydrate (98%, EP) were obtained from Duksan Pure Chemical Co., Ltd. (Korea).
54 Tannic acid (ACS reagent) was purchased from Sigma-Aldrich. All chemical reagents were used as
55 received.

56

57 **Preparation of WG-vegan leather**

58 A brief fabrication procedure for WG-vegan leather is as follows. WG was employed to mimic the
59 protein structure of animal leather. Because films composed solely of WG were too brittle, glycerol was
60 added as a plasticizer. Glycerol, a byproduct derived from biodiesel production, is a biodegradable
61 natural plasticizer. Deionized (DI) water served as a processing solvent—subsequently removed during
62 later steps—and facilitated the formation of hydrogen bonds and disulfide linkages between glutenin
63 and gliadin of the gluten proteins.

64 WG-vegan leather was fabricated by compression & molding method according to following steps.
65 First, WG powder was sieved into uniform particles by a fine mesh sieve (pore size: 100 μm). Then WG
66 powder (30 g), glycerol (15 wt.% of WG), and DI water (15 mL) were mixed in a planetary mixer
67 (PLM-0.6K, DAEWHA Tech Co., Ltd, Korea) with two twist type blades at 150 rpm for 5 min. The
68 obtained dough was subjected to heat (60 °C) and pressure (5 MPa) for 90 s using a hot press machine
69 (QM900SA, QMESYS, Korea), and was molded into a film with a thickness of 1.5 mm. Then, the
70 surface of the WG film was exposed to 254 nm UV light (VL-6.LC, VILBER) for 1 h (6W powder)
71 and heated at 150°C for 5 minutes and subsequently. After that, the WG-leather was left in an oven at
72 30 °C overnight.

73

74 Characterization

75 Leather-like Physical Performance

76 Bovine leather (izleather, Korea), commercial PU leather (YBK, Korea), and commercial rubber
77 (Narabelt, Korea) were used for comparison. Mechanical properties of WG-vegan leathers were
78 measured by UTM (AGS-X Series, SHIMADZU). According to ISO 13934-2:2014 (Tensile properties
79 of fabrics - Determination of maximum force using the grab method), tensile strength and strain were
80 evaluated. The specimen was cut into a dog-bone shape (ISO 37-4) and subjected to mechanical
81 property testing at a pulling speed of 100 ms⁻¹. All measurements were performed five times for each
82 sample, and the average values were obtained. The water resistance properties were examined by water
83 contact angle (WCA) and swelling test. First, WCA was analyzed using a contact angle measurement
84 system by the sessile drop method, in which a 2 µL droplet of deionized water was placed on the surface
85 of each sample using a micropipette at a suitable distance to the testing platform. The angle formed by
86 the tangent of the droplet with the surface of each sample was recorded by digital camera (38MP FHD
87 Camera V6). The average WCA value was obtained by measuring five different spots on the surface of
88 each sample. Next, the swelling ratio was measured according to ASTM D471. The test specimen was
89 prepared by cutting it into a standard size (e.g., 25x25 mm² with a thickness of 2-3 mm) and measuring
90 its initial weight. The specimen was then immersed in water at room temperature for 24 h. After
91 immersion, the specimen was removed, gently blotted to remove surface water, and its weight was
92 measured again. The percentage change in mass was calculated to evaluate the water absorption
93 characteristics of the material. (W_t : Weight of the sample after swelling at time t , W_0 : Initial weight of
94 the sample before swelling).

95

$$96 \quad \text{Swelling Ratio (\%)} = (W_t - W_0) / W_0 \times 100$$

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99 Leather-like Texture Evaluation

100 The tactile properties were evaluated using a portable tribometer (Heidon, Portable Friction Meter,
101 94i-II, Japan). For skin friction measurements, ten participants were involved. Prior to testing, their
102 forearm skin was cleansed with a tissue soaked in 70% ethanol to remove sweat and dirt, followed by
103 a one-minute drying period. Friction values were recorded at ten different points on the forearm, and
104 the average value was calculated. To assess the friction between bovine leather or WG-vegan leather
105 and human skin, samples with a thickness of less than 1 mm were affixed to the metal surface of the
106 tribometer's sensor. Measurements were then taken at ten different positions on the randomly selected
107 participant's forearm.

108 Then, the vertical elasticity (Shore A hardness) test was conducted in accordance with ISO 868:2003.
109 The specimen was prepared by stacking three layers of 1.5 mm thick samples to achieve the required
110 thickness and was conditioned under standard testing conditions. The experiment was performed at a
111 temperature of 23°C and a relative humidity of 30%, using a Shore A durometer HBA 100-0 (SAUTER,
112 Germany). The indenter was positioned perpendicularly to the specimen, and the hardness value was
113 recorded 15 seconds after applying the load.

114 The lateral elasticity test was conducted following ASTM D1388-18 (Standard Test Method for
115 Stiffness of Fabrics: The Heart Loop Test) with slight modifications.^{S1} The sample dimensions were
116 adjusted to 5 × 9 × 10 cm. Each sample was formed into a loop, and after 1 minute, the distance from
117 the upper end to the lowest point of the loop was recorded. The change in distance was then calculated
118 using the following equation.

119

$$120 \quad \Delta d(\%) = (d_1 - d_0) / d_0 \times 100$$

121 (Δd : the change in the distance, d_0 : the distance of the loop before the measurement, d_1 : the distance
122 of the loop after 1 min). All measurements were repeated three times.

123

124 Protein Denaturation Analysis

125 The surface morphologies and detailed microstructures of the WG-vegan leathers were investigated
126 using scanning electron microscopy (SEM, Hitachi, S-4300SE). All samples were sputter-coated with
127 platinum using a magnetron sputter coater (108auto; Cressington Scientific Instruments, Watford, UK)
128 and then observed at an acceleration voltage of 3 kV. Fourier-transform infrared (FT-IR) spectroscopy
129 was performed using a Bruker VERTEX 80 V spectrometer. A Fourier transform-infrared (FT-IR)
130 spectrometer was used to examine the chemical structures of WG-vegan leathers. The FT-IR spectra of
131 the samples were recorded in the wavenumber range of 650–4000 cm^{-1} at a resolution of 0.4 cm^{-1} with
132 32 scans. Baseline normalization was carried out for each spectrum using OMNIC software (Thermo
133 Fisher Scientific, MA, USA). X-ray diffraction (XRD, Rigaku, D/MAX 2200V/PC) with Cu-K α
134 radiation ($\lambda = 0.154056 \text{ nm}$) was performed to evaluate the degree of intermolecular packing and
135 alignment of the WG-vegan leathers. The molecular structures of samples were examined in the 2 θ
136 range of 0–40 and carried out with a Cu-K α radiation source ($\lambda = 0.15406 \text{ nm}$) at 40 kV and 40 mA.

137 Free amino acids were analyzed using a Dionex Ultimate 3000 HPLC system (Thermo Scientific,
138 USA) with pre-column derivatization using borate buffer, OPA, and FMOc reagents. Separation was
139 performed on an Inno C18 column (4.6 \times 150 mm, 5 μm ; YoungJin Biochrom, Korea) at 40°C, using a
140 binary gradient of 40 mM sodium phosphate buffer (pH 7) and a mixture of water/acetonitrile/methanol
141 (10:45:45, v/v) at a flow rate of 1.5 mL/min. Detection was carried out by fluorescence (Ex/Em: 340/450
142 nm for OPA, 266/305 nm for FMOc) and UV at 338 nm. Samples were prepared by extracting 1 g of
143 sample with 50 mL of 0.1 M perchloric acid and 0.1% meta-phosphoric acid, followed by sonication,
144 shaking, filtration, and automated derivatization. Quantification was based on a 17-component amino
145 acid standard (Agilent).

146 LC-MS and LC-MS/MS analyses were performed using an Ultimate3000 system (Thermo Scientific,
147 USA) equipped with a Waters Cortecs T3 column (2.1 mm \times 150 mm, 1.6 μm , Waters). The column
148 temperature was maintained at 45°C. The mobile phases consisted of solvent A (0.2% formic acid in
149 water) and solvent B (0.2% formic acid in acetonitrile), with a flow rate of 0.25 mL/min. A gradient

150 elution was applied as follows: 0 min (99% A), 0.5 min (99% A), 25 min (75% A), 32 min (5% A), 35
151 min (5% A), 35.1 min (99% A), and 40 min (99% A). Mass spectrometric detection was carried out
152 using a Triple TOF 5600+ system (AB Sciex, USA) with electrospray ionization (ESI) in positive mode.
153 Data was acquired in full scan and information-dependent acquisition (IDA) mode. The MS scan range
154 was set to 100–2000 m/z, and the MS/MS scan range was 30–2000 m/z. Source conditions were as
155 follows: ion source gas 1 and 2 (nebulizer and heater gas) at 50 psi, curtain gas at 25 psi, and desolvation
156 temperature at 500°C. The ion spray voltage was set to +5.5 kV, declustering potential (DP) at 60 V,
157 collision energy (CE) at 10 V, and collision energy spread (CES) at 35 ± 15 V. Nitrogen (N₂) was used
158 as the collision gas.

159 Fluorescence microscope images were obtained using a Leica Thunder Imager equipped with a K8
160 CMOS camera (Leica Microsystems, Wetzlar, Germany) and controlled by LAS X software. To
161 compare the film before and after surface treatment, fluorescence was captured under the following
162 conditions: blue channel (excitation 390 nm/emission 420–460 nm), green channel (excitation 475
163 nm/emission 490–530 nm), yellow channel (excitation 560 nm/emission 565–615 nm), and red channel
164 (excitation 635 nm/emission 662–738 nm). All images were acquired using a 5× objective lens, with an
165 exposure time of 50 ms and LED power set to 20%.

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167 **Environmental Impacts**

168 Life cycle assessment (LCA) was conducted using the *openLCA* (version 2.4.1) with the ecoinvent
169 3.11 database (cut-off system model). The analysis was performed across five key processes: (1) gluten
170 extraction, (2) gluten dough processing, (3) hot pressing, (4) surface treatment, and (5) oven drying.
171 The electricity consumption of each process was measured using a power meter (Seojun Co., Ltd., South
172 Korea) and is presented in Table S4. The ecoinvent datasets used in this study include wheat flour,
173 deionized water, glycerin, and medium voltage electricity (cutoff). The climate change-global warming
174 potential (GWP100) was selected as the impact category, and the final product was assessed on a per 1
175 kg basis using the IPCC impact assessment method. The energy recovery values used in Scenario 3

176 were based on the data reported by *Yelin Deng, 2013*.

177 To investigate the biodegradability of WG-vegan leather, we conducted a bio-decomposition test
178 following the ISO 20200 standard method. Sample films with a thickness of 1.5 mm into $25 \times 25 \text{ mm}^2$
179 pieces and weighed them for four replicates. Prepared sample films were inserted at a depth of 4–6 cm
180 in perforated plastic boxes filled with compost consisting of sawdust (40%), rabbit feed (30%), ripe
181 compost (10%), corn starch (10%), saccharose (5%), corn seed oil (4%), and urea (1%), under
182 controlled conditions of 58°C and 55% humidity. At various time points (1,2,3,4,5,6, and 7 week), the
183 samples were retrieved to assess their disintegration. The degree of disintegration (D) was calculated
184 by using the following equation: $D = (m_i - m_f / m_i) \times 100$ where m_i is the initial dried sample mass, and
185 m_f is the dried sample mass after the test.

186 Superworms edibility test was adapted from the protocol reported by Jung et al. Superworms in their
187 larvae stage (*Z. atratus*) were acquired from a local supplier (Mealworm Nara, Yeosu, Korea), with a
188 length ranging from 5 to 6 cm. Prior to the feeding, the superworms were subjected to a 36h starvation
189 period. In a polypropylene container (D x H = 103 x 78.6 mm), a total of 30 superworms were fed WG-
190 heat film, WG-UV film, WG-leather as their exclusive diet respectively. For comparative purposes,
191 three control groups were set up: the first group was fed with bran, a feed widely used for superworms;
192 the second group was intentionally left unfed to induce a state of starvation; and the third group received
193 biodegradable plastics PLA & PBAT (Lotte Chemical, Korea). The superworms were incubated for 4
194 weeks at $26 \pm 1 \text{ }^\circ\text{C}$. To replace moisture, deionized water was provided, and dead superworms were
195 removed immediately. The superworm survival rate, body weight changes, and plastic consumption
196 were recorded every day. All treatments were carried out in triplicate.

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201 **Table S1. Sample name**

Sample	WG (g)	GL (g)	DI water (ml)	TA (g)	FeCl ₂ (g)	Surface treatment	6M HCl hydrolysis
WG-film (GL10)	30	3	15	-	-	-	-
WG-film, WG-film (GL15)	30	4.5	15	-	-	-	-
WG-film (GL20)	30	6	15	-	-	-	-
WG-film (GL25)	30	7.5	15	-	-	-	-
WG-film (brown)	30	4.5	15	0.9	-	-	-
WG-film (darkbrown)	30	4.5	15	0.9	0.3	-	-
WG-film (black)	30	4.5	15	0.3	0.9	-	-
WG-film (2h)	30	4.5	15	-	-	X	2h
WG-film (24h)	30	4.5	15	-	-	X	24h
WG-leather (2h)	30	4.5	15	-	-	O	2h
WG-leather (24h)	30	4.5	15	-	-	O	24h

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216 **Table S2. Tensile strength and elongation at break of different leathers (Ashby’s plot)**

Sample		Tensile strength (MPa)		Elongation at break (%)	
		Avg.	SD	Avg.	SD
WG- vegan leather	WG-film (GL10%)	14.8	4.43	23	2.45
	WG-film, WG-film (GL15%)	10.1	3.45	68	3.33
	WG-film (GL20%)	7.6	2.34	106	3.78
	WG-film (GL25%)	4.2	2.33	135	3.67
	WG-leather	12.1	1.65	64	5.75
	WG-leather (brown)	15.2	2.45	56	2.57
	WG-leather (dark brown)	16.7	3.31	51	3.67
	WG-leather (black)	17.2	2.55	44	4.32
Bovine leather		17.9	2.65	58	3.78
Commercial PU leather		8.4	3.34	62	4.65
Alternative leather	Pinatex ^{®21}	4.5	-	30	-
	Muskin ^{®21}	0.2	-	48	-
	Desserto ^{®23}	9.48	-	16	-
	Kombucha leather ²²	1.69	0.33	15	-
Solvent casted WG-film	WG film ²⁴	0.4	0.2	160	23
	WGP film ²⁵	1.75	-	90	-

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229 **Table S3. Amino-acid composition (HPLC) of WG-dough, WG-film and WG-leather**

Amino acid (%)	WG-dough	WG-film	WG-leather
Aspartic acid/Asparagine	2.7	2.82	2.78
Threonine	3.23	3.08	3.47
Serine	5.5	5.15	5.41
Glutamic acid/ Glutamine	34.62	27.53	34.06
Glycine	3.73	3.91	3.07
Alanine	3.73	6.75	2.53
Cystine	1.27	3.45	1.89
Valine	5.25	6.28	4.59
Methionine	1.31	0.47	1.61
Isoleucine	3.55	1.76	4.46
Leucine	6.69	7.04	7.65
Tyrosine	3.24	3.02	2.12
Phenylalanine	3.98	5.6	5.83
Histidine	2.97	3.28	2.7
Lysine	1.74	1.91	1.05
Arginine	2.67	2.92	4.23
Proline	13.82	15.03	12.55
Total	100	100	100

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236 **Table S4. LCA data**

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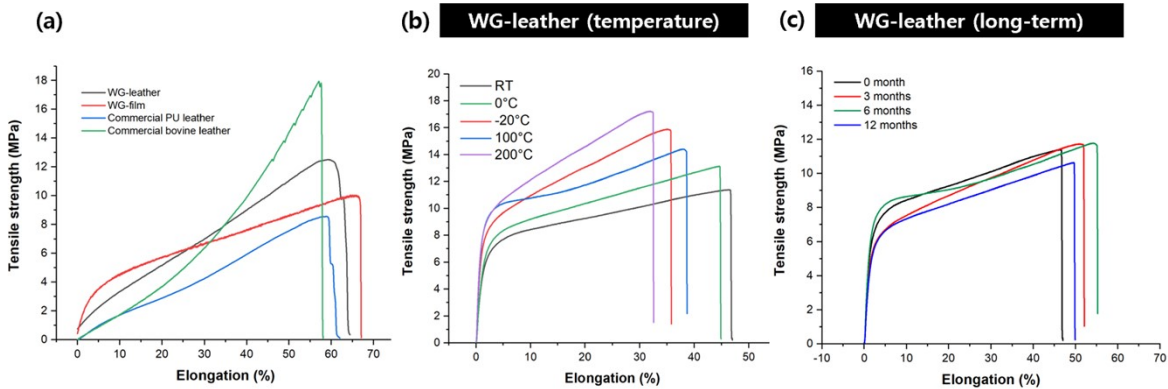
<Scenario 1>			
Process	Detail index	Energy consumption (kWh)	GWP 100 (kg CO ₂ eq)
1. Gluten extraction	cultivation, flour production, gluten separation, drying of 740g gluten powder (<i>Yelin Deng, 2013</i>)	-	1.16
2. Planetary mixing	planetary mixing with gluten, glycerol, and deionized water	0.08	0.32
3. Hot pressing	hot press gluten dough to gluten film	2.52	0.05
4. Surface treatment	heating, UV irradiation to gluten film	2.92	0.06
5. Oven drying	oven dry for 5 days	1.51	0.03
Total			1.63
<Scenario 2>			
Process	Detail index	Energy consumption (kWh)	GWP 100 (kg CO ₂ eq)
1. Planetary mixing	planetary mixing with gluten, glycerol, and deionized water	0.08	0.32
2. Hot pressing	hot press gluten dough to gluten film	2.52	0.05
3. Surface treatment	heating, UV irradiation to gluten film	2.92	0.06
4. Oven drying	oven dry for 5 days	1.51	0.03
Total			0.47
<Scenario 3>			
Process	Detail index	Energy consumption (kWh)	GWP 100 (kg CO ₂ eq)
1. Gluten extraction	cultivation, flour production, gluten separation, drying of 740g gluten powder (<i>Yelin Deng, 2013</i>)	-	1.16
2. Planetary mixing	planetary mixing with gluten, glycerol, and deionized water	0.08	0.32
3. Hot pressing	hot press gluten dough to gluten film	2.52	0.05
4. Surface treatment	heating, UV irradiation to gluten film	2.92	0.06
5. Oven drying	oven dry for 5 days	1.51	0.03
6. Energy recovery	incineration with energy recovery (<i>Yelin Deng, 2013</i>)		-0.078
Total			1.55

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239 The GWP100 values for each process in Scenario 1 were calculated using the openLCA software in
 240 conjunction with the Ecoinvent 3.11 dataset. In Scenario 2, the Gluten extraction stage was excluded,
 241 resulting in a calculated value of 0.47 kg CO₂-eq ($1.63 - 1.16 = 0.47$ kg CO₂-eq). For Scenario 3, the
 242 energy recovery value reported by Deng (2013) was applied, subtracting 0.078 kg CO₂-eq from 1.63 kg
 243 CO₂-eq, yielding a result of 1.55 kg CO₂-eq.

244 **Figure S1. S-S curve of WG-vegan and other leathers**

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247 S-S curves of (a) different types of leathers (b) WG-leathers at different temperatures (c) WG-leathers
248 after long-term storage

249 The stress–strain curves of commercial bovine leather, commercial PU leather, and WG-
250 based vegan leather (WG-film and WG-leather) were compared. Despite the decrease in
251 modulus, WG-leather retained a high toughness value ($4.65 \text{ MJ}\cdot\text{m}^{-3}$), slightly exceeding that
252 of WG-film ($4.58 \text{ MJ}\cdot\text{m}^{-3}$) and considerably higher than that of commercial PU leather (2.72
253 $\text{MJ}\cdot\text{m}^{-3}$). These results indicate that the physical surface treatment effectively tuned the
254 mechanical properties of WG-film to achieve leather-like flexibility, while maintaining
255 superior energy absorption performance compared to conventional PU leather.

256 Considering the practical conditions where WG-leather may be exposed to both elevated and
257 sub-zero temperatures, as well as prolonged storage under ambient environments, it was
258 necessary to evaluate its mechanical reliability under these realistic scenarios. The temperature
259 exposure tests were conducted by storing the samples in an oven at 100°C and 200°C , as well
260 as in a refrigerator (0°C) and a freezer (-20°C) for three days, followed by mechanical
261 property measurements. The results showed that, compared to room temperature, both high-
262 and low-temperature storage led to increased tensile strength and decreased elongation due to
263 additional curing. This indicates that the WG-leather exhibits a tensile strength of
264 approximately 17 MPa , comparable to that of natural leather, and maintains its mechanical
265 integrity without degradation even after storage under both high and low temperatures (Figure
266 S1. (b)).

267 Additionally, to examine the long-term stability of WG-leather, UTM measurements were

268 conducted after storage at room temperature for 0, 3, 6, and 12 months. For the long-term
269 storage test, WG-leather samples were kept in a low-density polyethylene (LDPE) bag without
270 desiccants at room temperature (RT) before measurement. The tensile strength slightly
271 increased up to 6 months and then showed a minor decrease after 12 months. Since these
272 variations remained within 10% of the initial tensile strength, the WG-leather is considered to
273 maintain stable mechanical properties during long-term storage (Figure S1. (c)).

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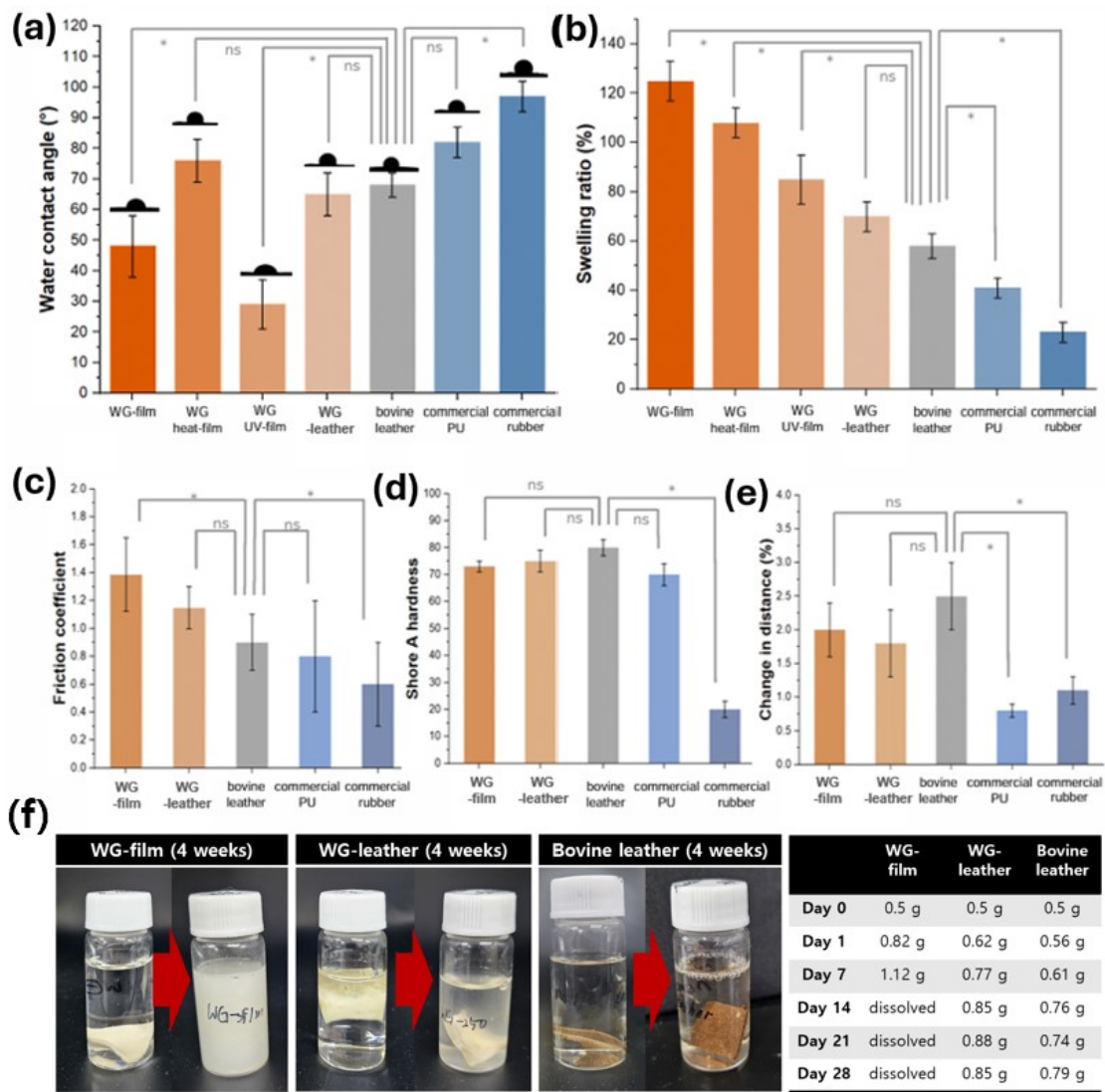
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293 **Figure S2. Physical & tactile properties of various leathers**



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295 (a) Water contact angle, (b) swelling ratio, (c) friction coefficient, (d) shore A hardness, (e) heart loop test (f)
296 long-term swelling test of various leathers (The error bars indicate the standard deviation (SD) of the mean (n =
297 3) and statistical significance was determined using unpaired two-tailed t-tests. $p \leq 0.05$ (*), $p \leq 0.01$ (**), and p
298 > 0.05 (ns, not significant))

299 We performed a long-term swelling test comparing WG-film, WG-leather, and bovine leather. Prior
300 to testing, the surface of bovine leather was gently abraded with sandpaper to eliminate the effects of
301 surface synthetic polymer coatings. After one month of water immersion, the WG-film completely
302 dissolved, whereas both WG-leather (denatured) and uncoated bovine leather remained structurally
303 intact without visible degradation. The uncoated bovine leather exhibited a swelling ratio of
304 approximately 60%, comparable to that of WG-leather, confirming that the surface treatment

305 substantially enhanced the water resistance of the WG-leather. This level of water resistance is
306 comparable to that of bovine leather, and it could be further improved by introducing sustainable
307 hydrophobic coatings.^{S6}

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335 **Figure S3. Different colors of WG-leather as a result of the pyrogallol-based natural**
336 **product coating.**



337 (a) WG-leather (b) WG-brown (C) WG-darkbrown (d) WG-black

338

339 The dyeing process was conducted to impart various colors to WG-leather. Utilizing nature-derived
340 tannic acid and iron(III) chloride, the beige WG-leather was dyed to achieve brown, gray, and black
341 colors. These solutions were incorporated into the WG-leather in place of deionized water before
342 planetary mixing, resulting in various colors. Tannic acid is a natural pyrogallol compound and is
343 derived from plants. tannic acid and iron(III) chloride have been traditionally utilized as dye and ink
344 ingredients, and the methodology is well established. Thanks to the hydrophilicity and miscibility of
345 the WG material, the samples were dyed homogeneously and well.

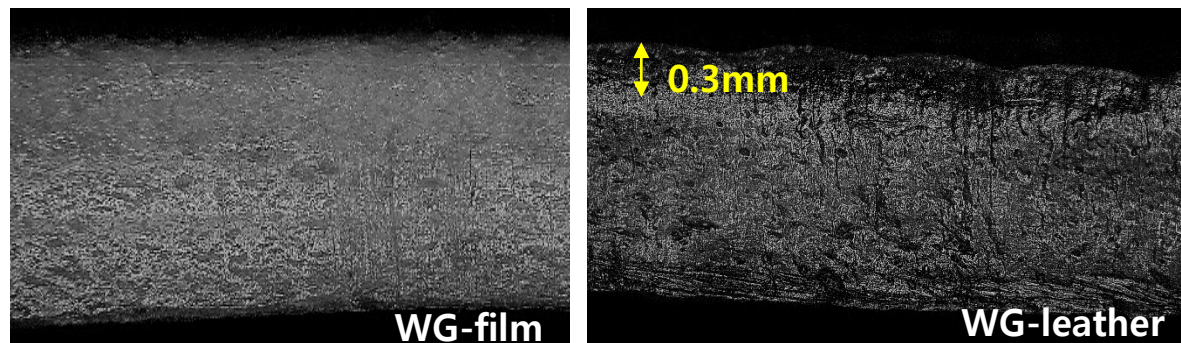
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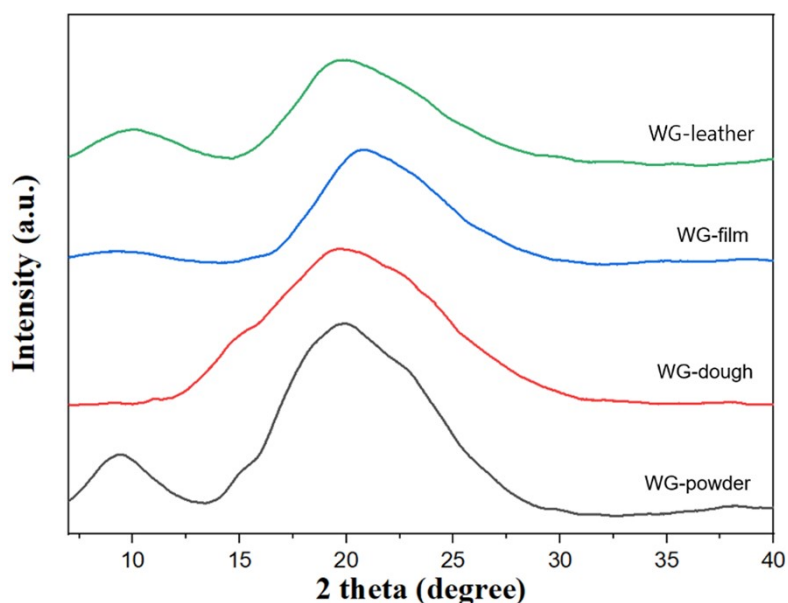
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Figure S4. Optical microscopy (OM) image of WG-film & WG-leather



Cross-sectional imaging was conducted using optical microscopy (OM) to compare the WG-film and WG-leather. In the WG-leather, which was subjected to additional high-temperature treatment and UV irradiation, a distinct coating layer approximately 0.3 mm thick was observed on the surface. In contrast, no such coating layer was present in the untreated WG-film. The formation of this coating layer is believed to have contributed to the enhanced hydrophobicity and water resistance of WG-leather.

371 **Figure S5. XRD**



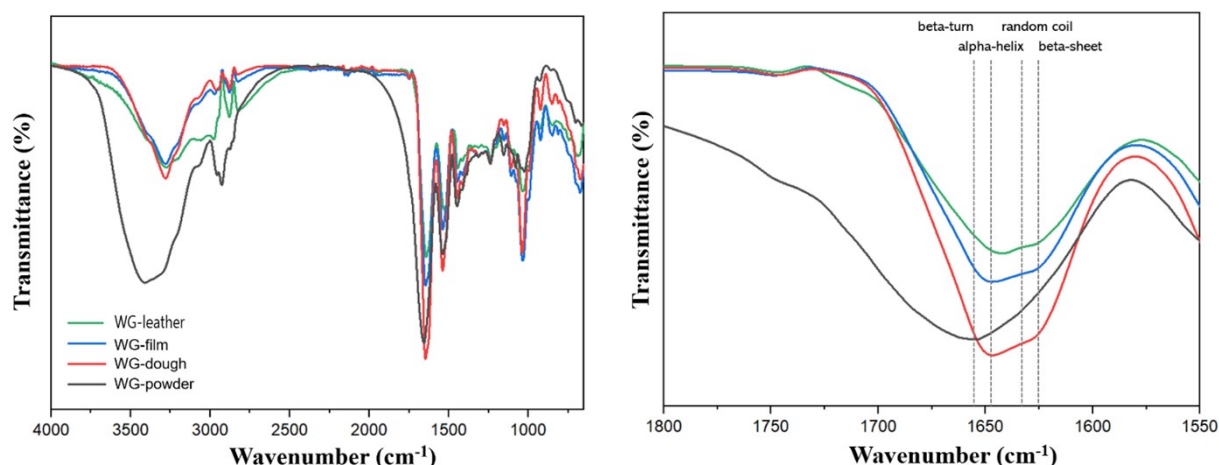
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374 XRD analysis was conducted to investigate the changes in the molecular structure of WG-powder,
 375 WG-dough, WG-film, and WG-leather under varying heat and pressure. In WG-powder, two broad
 376 peaks were observed around 10° and 20°, with full width at half maximum (FWHM) values of 3.07 and
 377 7.46, respectively.^{S2} When mixed with glycerol and water to form WG-dough, the peak around 10°
 378 has disappeared, with an increased FWHM of 9.53. This suggests that the original structure of gluten
 379 protein powder, with glutenin and gliadin arranged in an ordered manner, was reduced upon random
 380 mixing with plasticizers and water, resulting in an amorphous structure formed through disulfide and
 381 hydrogen bonds. In WG-film, two peaks emerged, both with an FWHM of 7.21, indicating the
 382 formation of a new structure. This recovery likely resulted from reduced molecular spacing and more
 383 ordered arrangements within the gluten complex under heat and pressure. Finally, WG-leather exhibited
 384 a general trend of reduced FWHM, with a value of 3.69 and 7.17, respectively. This suggests that
 385 additional surface heat treatment decreased hydrogen bonding between water and glycerol while
 386 increasing hydrogen bonding with proteins, leading to enhanced stability and the formation of a new
 387 structure.

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389 **Figure S6. FT-IR**

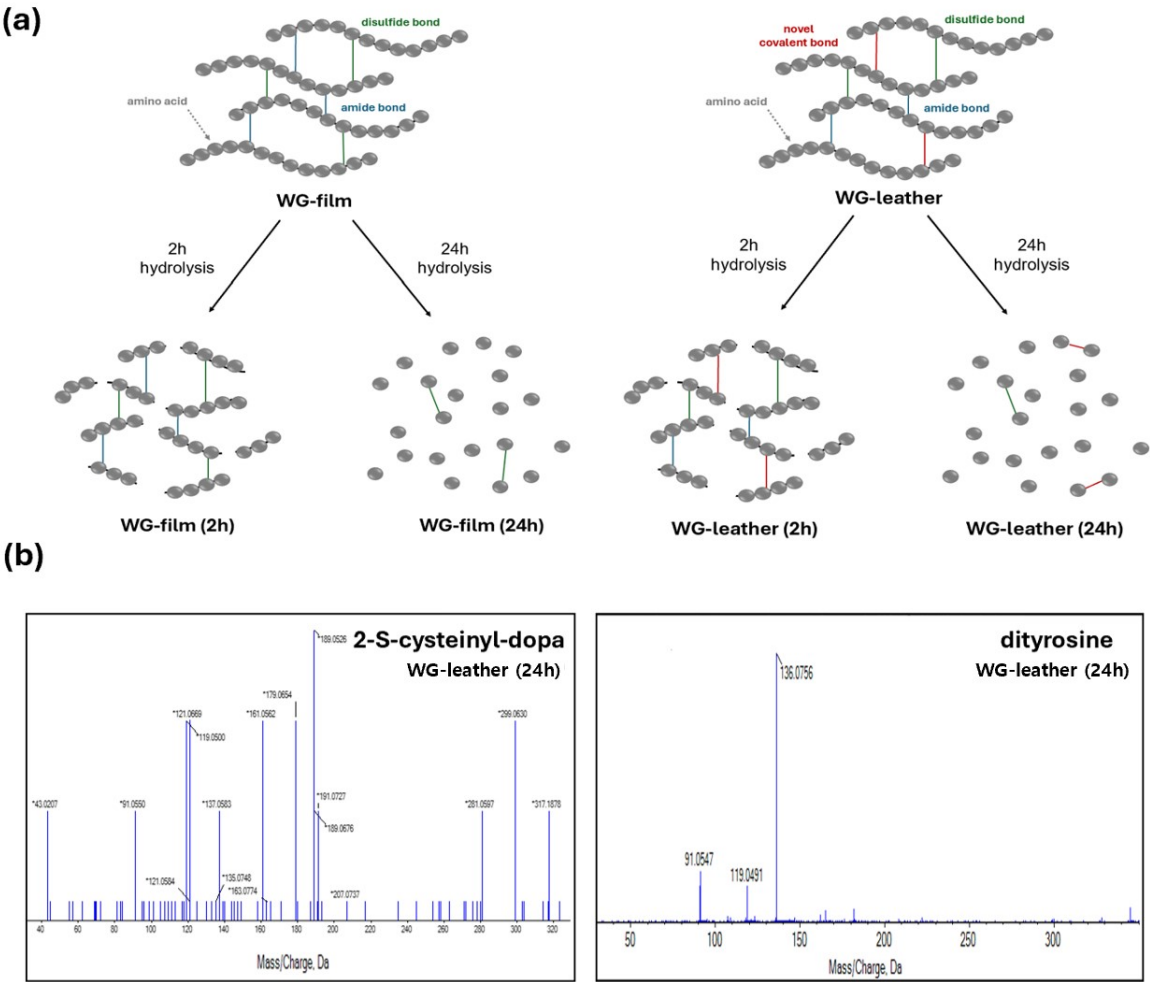


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392 FT-IR analysis was conducted to examine changes in the secondary structure of proteins in WG-vegan
393 leathers. The N-H stretching peak (3200–3500 cm⁻¹) was most prominently observed in WG powder,
394 which is attributed to the amine groups present at the terminal ends of amino acids. These peaks
395 decreased as the process progressed, likely due to the formation of hydrogen bonds and other types of
396 binding. Similarly, the O-H stretching peak (3200–3600 cm⁻¹) showed a decreasing trend upon heat
397 treatment, which can be attributed to the evaporation of water and glycerol caused by compression and
398 heat treatment. The C-H stretching peak was primarily observed in peaks abundant in sp³ carbons from
399 gluten proteins. If carbonization had occurred due to heat treatment, peaks corresponding to C=C (1620-
400 1680 cm⁻¹) and C≡C (1450-1600 cm⁻¹) would have formed. Therefore, it can be concluded that
401 carbonization did not take place.

402 In the amide I region (right side; 1550-1800 cm⁻¹), the beta-turn and alpha-helix peaks were dominant
403 in WG powder, while beta-sheet peak was scarcely observed. However, as WG transformed from
404 powder to dough, film, and leather, the beta-sheet peak increased, whereas the beta-turn and alpha-helix
405 peaks showed a decreasing trend^{S3}. It suggests the formation of a more stabilized and ordered layered
406 configuration through protein denaturation by thermal and UV treatments. Moreover, the overall peaks
407 in the amide I region exhibited a red shift, reflecting changes in the hydrogen bonding environment and
408 the reorganization of protein secondary structures during the transformation process.

Figure S7. 2h, 24h protein hydrolysis scheme and LC-MS/MS data



(a) WG-leather hydrolysis scheme
(b) LC-MS/MS spectrum of different compounds in WG-leather (24h)

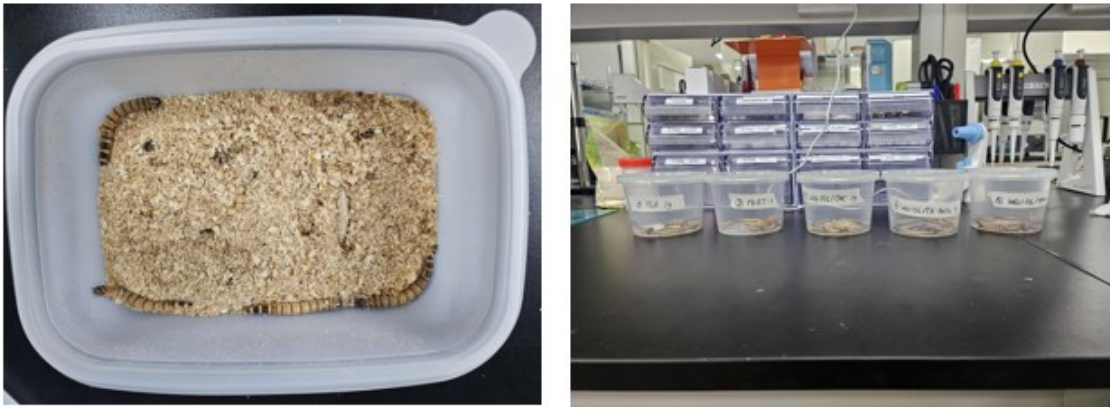
LC-MS/MS analysis was conducted on WG-film (untreated) and WG-leather (surface-treated) after 2-hour and 24-hour 6M HCl hydrolysis. Assuming that both the 24-hour hydrolyzed WG-film and WG-leather were completely broken into amino acid fragments, the remaining strong cross-linked structures were subsequently identified. 2-S-cysteinyl-DOPA and dityrosine—absent in WG-film—were identified in WG-leather and remained detectable even after prolonged hydrolysis.

422 **Figure S8. Soil degradation (ISO 20200)**



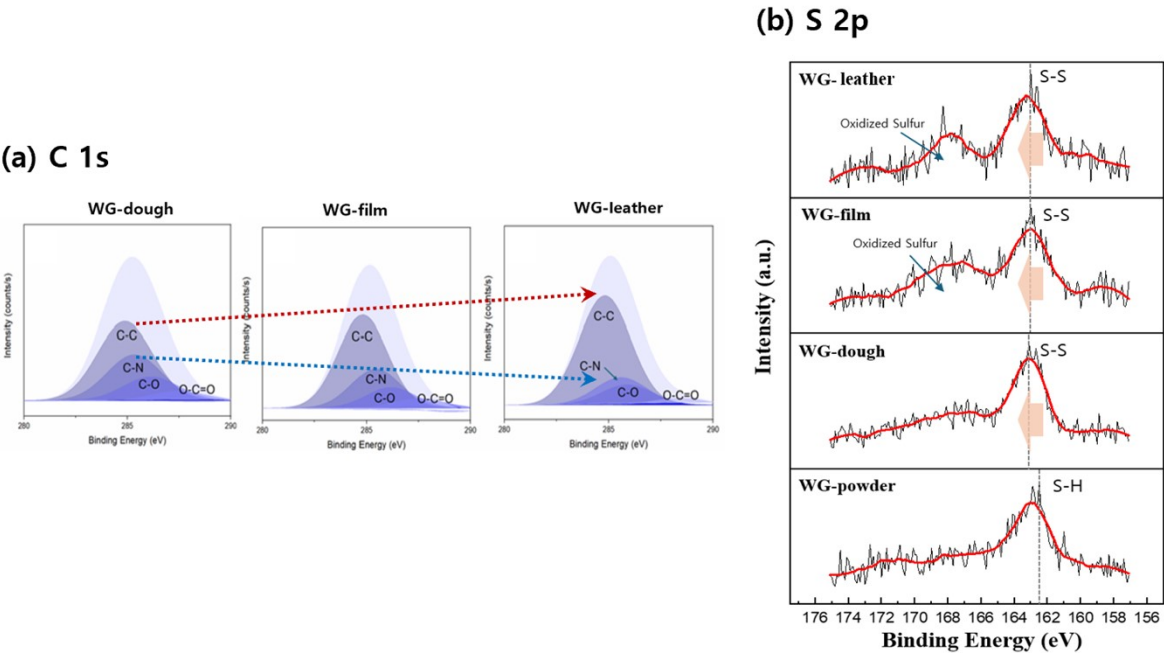
424 Soil biodegradation of PLA, PBAT, WG-heat film, WG-UV film, and WG-leather (7 weeks)

426 **Figure S9. Superworms edibility test**



428 Superworms edibility test of PLA, PBAT, WG-heat film, WG-UV film, and WG-leather (14 days)

438 **Figure S10. XPS analysis of WG-dough, WG-film and WG-leather**



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440 (a) C 1s (b) S 2p XPS analysis of WG-dough, WG-film and WG-leather

441 To examine the respective effects of heat and UV treatment, we performed XPS analyses on gluten-
442 dough, gluten-film, and gluten-leather samples. In the S 2p spectra, a relatively low sulfur intensity
443 was observed; however, progressive heat and UV treatments led to the formation of oxidized sulfur
444 species (166–170 eV) and a peak shift from the –SH signal (162 eV) to the disulfide (S–S) bond
445 region (163 eV).^{S7} In the C 1s spectra, the heat-treated WG-film exhibited a decrease in C–N bonding
446 and an increase in C–C bonding, and these trends became more pronounced in the UV-treated WG-
447 leather.^{S8} These results support that the surface treatment of WG-leather induced a reduction in C–N
448 (amide) bonds and an increase in C–C (covalent) bonds, accompanied by the formation and oxidation
449 of disulfide bonds in sulfur.

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455 **Movie S1. Elastic recovery test of bovine, PU and WG-leather**

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457 The video included the elastic recovery behavior of natural leather, synthetic PU leather, and gluten-
458 based leather. Natural leather exhibited quick elasticity with a recovery time of approximately 0.8
459 seconds, attributed to its fibrous collagen structure, which enables rapid elastic recovery. In contrast,
460 synthetic PU leather showed a slow recovery time of 2.3 seconds, likely due to its composite structure
461 incorporating nonwoven substrates and multiple laminated layers, which limit its ability to return
462 quickly to its original form. The gluten-based leather demonstrated an elastic recovery time of 2.0
463 seconds, showing a recovery profile closer to that of natural leather than PU leather, suggesting its
464 promise as a sustainable alternative with favorable tactile and functional properties.

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486

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